CE394M: FEM solvers and errors

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Overview

- Solving non-linear problems
 - Iterative solvers
 - Tangent stiffness
 - Newton Raphson

Linear and non-linear problems

Linear problems

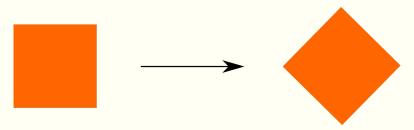
- The response can only be approximated as linear if its deformations/motions are small.
- In linear analyses, the response to individual load cases can be scaled and added to the results from other linear analyses, which is the principle of superposition.

Non-linear problems

- Superposition is invalid.
- The solution is an incremental/iterative process.
- An iteration is the solution of a system of equations linearised about the current state of the nonlinear physical problem.

Non-linearity in geotechnical engineering

- Material non-linearity
 - plasticity
- Contact
 - discontinuous source of non-linearity
- Large deformations and motions of a geotechnical structures
 - rotation, rigid body motion
 - often ignored, still in the research area.



No strains if linear strain-displacement relations are used.

Linear solvers

To solve a system of linear equations of the form Ka = b, there are two families of methods of solvers that can be used: direct and iterative.

- Direct solvers solve a system of linear equations in a predefined number of steps.
- Methods are based on Gauss elimination, with the most common method being LU decomposition.
- The time required to solve a linear system increases with the number of computer operations performed.
- For a direct linear solver applied to a dense system of size $n \times n$: CPU time = Cn^3 .
- If the number of degrees of freedom in a finite element simulation is doubled, the time required to solve the system will increase by a factor of 8!

Iterative solvers

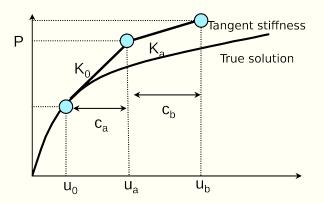
The system of equations that we derived from the finite element approximation of the BVP:

$$F_{\rm int}(u) - F_{\rm ext} = 0$$

At this point we remind ourselves that in the case of finite deformations, both $F_{\rm int}$ and $F_{\rm ext}$ are in general very nonlinear terms.

The integration has to be carried over the current volume and surface (of the finite element under consideration) that may in general depend on u in a highly non-linear fashion.

Tangent stiffness method



- Many small increments are need to obtain accurate solution
- Need to perform a parametric study to find the optimum incremental
- Defining increments is very important
- Program SAGE CRISP

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Solving non-linear problems
Tangent stiffness
Tangent stiffness method

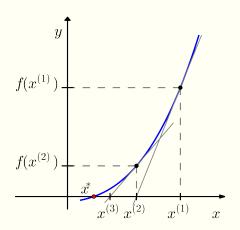


- Need to perform a parametric study to find the optimum incremental
- Defining increments is very important
 - agram SAGE CRISP

In the incremental solution we divide the load into increments $\Delta P = \lambda P$, where λ is also known as a load factor and apply a repeated solution of $\Delta u = K^{-1}\Delta P$.

Basically we divide the load into substeps, and treat each as linear - but that is usually not accurate enough and inefficient.

Newton Raphson method



$$x_{n+1} = x_n - \frac{f(x_n)}{f'(x_n)}$$





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Solving non-linear problems
Newton Raphson
Newton Raphson method



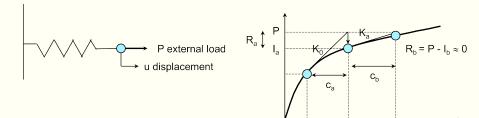
Newton's Method In Newton's method, the incremental loading is expressed as follows. The external load vector $F_{\rm ext}$ is gradually increased from 0 in order to reach a desired value ${\bf F}^*$. Assuming that ${\bf F}^*$ itself remains constant during the analysis in terms of its 'direction' and only its magnitude is changing, we can write $F_{\rm ext}=q$ known just to simplify our expression for the system of equations. Then we can control how the external

load vector increases or decreases by introducing a scalar quantity λ and express the system as follows:

$$R(u) = F_{\mathrm{int}} - F_{\mathrm{ext}} - > R(u) = F_{\mathrm{int}} - \lambda F_{\mathrm{ext}} == 0$$

Thus by increasing or decreasing λ we can control our load incrementation.

Newton Raphson method



• Using the initial stiffness K_0 , apply an increment of load δP , calculate an approximate solution c_a caused by this increment.

U∩

U_a

- The stiffness K_a is updated using the new position, and the internal force in the spring I_a is calculated.
- If the difference R_a between the total load applied to the spring, P, and I_a is smaller than the tolerance, $u_a = u_0 + c_a$ is the converged solution.

 u_b

Personnalisad udisplacement	$H_{i_{1}} = \bigcap_{l_{1} = l_{2} = l_{3} = l_{3}$
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- Using the initial stiffness K₀, apply an increment of load δP, calculate an approximate solution c₀ caused by this increment.
 The stiffness K₁ is updated using the new position, and the internal
- The stiffness K₃ is updated using the new position, and the interns force in the spring I₃ is calculated.
- If the difference R_a between the total load applied to the spring, P, and I_a is smaller than the tolerance, u_a = u₀ + c_a is the converged solution.
- If R_a is not small, a new displacement correction c_b is calculated by solving $c_b = R_a/K_a$
- The new displacement u_b is updated, and the internal force I_b in the updated configuration is calculated.
- The new force residual R_b is obtained. If $R_b < tolerance$, the solution is converged. If not, continue the iteration.

Newton Raphson method: Tolerance and Convergence

- Program ABAQUS
- Newton-Raphson is the most standard method to solve nonlinear problems in FE.
- A large error in the initial estimate can contribute to non-convergence of the algorithm.

Tolerance

- must be small enough to ensure that the approximate solution is close to the exact mathematical solution.
- must be large enough so that reasonable number of iterations are performed.

Quadratic convergence

• If the tangent stiffness is calculated correctly, *R* should reduce quadratically from one iteration to the next.