

# CE394M: Critical State and Cam-Clay

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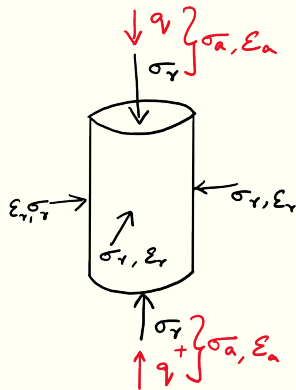
## 1 Critical State Soil Mechanics

Roscoe et al., (1958), Schofield & Worth (1968), Wood (1990):

- Provides a conceptual framework in which to interpret stress-strain-strength-volumetric strain response of soil.
- Started as a qualitative, rather than a mathematical model
- A unified framework of known or observed soil responses: drained / undrained / etc

# Critical state variables

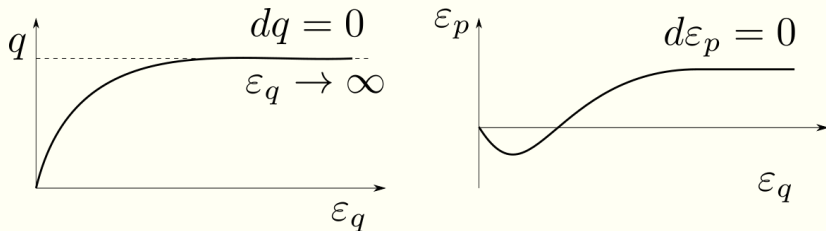
- Mean stress:  $p' = \frac{\sigma'_a + 2\sigma'_r}{3} = p - u$ .
- Deviatoric stress:  $q = \sigma'_a - \sigma'_r = \sigma_a - \sigma_r$
- Specific volume:  $v = \frac{V_T}{V_s} = \frac{V_s + V_v}{V_s} = 1 + e$ .



# Critical State Hypothesis: I

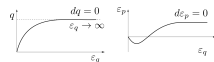
Roscoe, Schofield & Worth (1958): **At shear-failure, soil exists at a unique state**

- $d\varepsilon_q \gg 0$  unlimited shear strain potential.
- $dp' = dq = d\varepsilon_p = 0$  no change in  $p'$ ,  $q$ ,  $\varepsilon_p$ .
- Critical state stress ratio:  $\eta = q/p' = \text{const} = M$  at failure  $q = Mp'$ .



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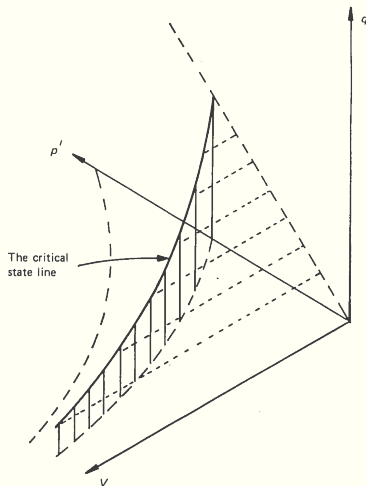


Soil is sheared to a point where stresses are stationary ( $dq = dp' = 0$ ) with no further change in volume ( $d\varepsilon_p = 0$ ), unlimited shear strains ( $d\varepsilon_q >> 0$ ) and  $q/p'$  has a fixed value: **critical state**.

$M$  can be related to  $\phi'$ :  $M = \frac{6 \sin \phi'}{3 - \sin \phi'}$ .

# Critical State Hypothesis: II

Critical state is a function of  $q, p', v$ .



The CSL ( $p', v, q$ ) space is given by the intersection of two planes:  $q = Mp'$  and a curved vertical plane  $v = \Gamma - \lambda \ln p'$



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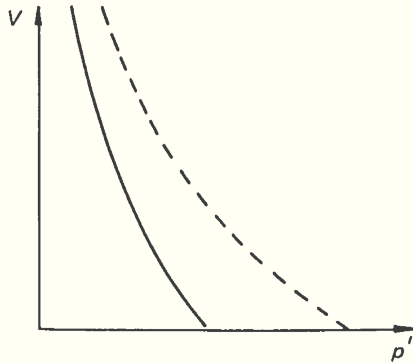
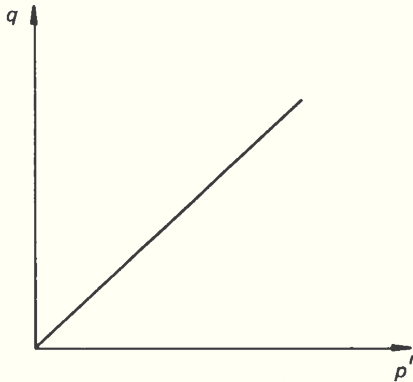
Critical state curve connecting critical state points:

- Critical state line
- Defined in 3D but we'll look at projections into  $q - p'$  and  $v - p'$  space



# Critical State Hypothesis: II

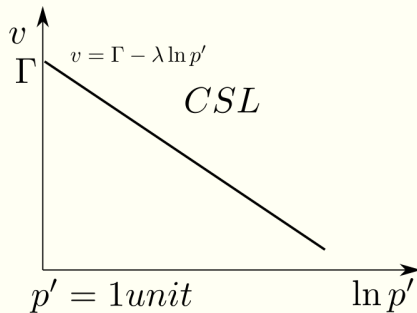
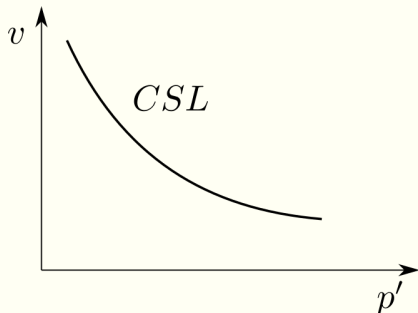
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The CSL in (a)  $(p', q)$  plot and (b)  $(p', v)$  plot (isotropic normal compression line is shown in dashed)

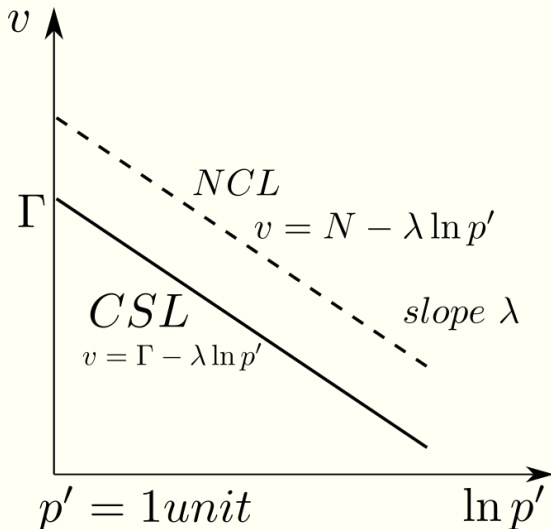
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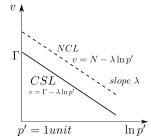
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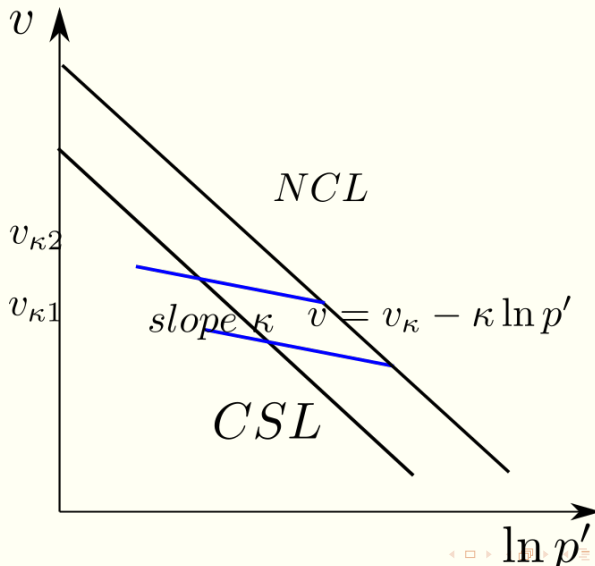




Isotropic virgin compression line (VCL)  $\eta = 0$ . NCL is parallel to CSL. VCL is  $\eta = 0$ , while CSL  $\eta = M$ . Oedometer falls between VCL and CSL at a constant  $\eta$ :  $0 < \eta < M$ .

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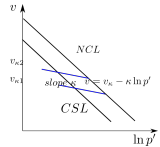
## CE394M: Cam-Clay

### └ Critical State Soil Mechanics

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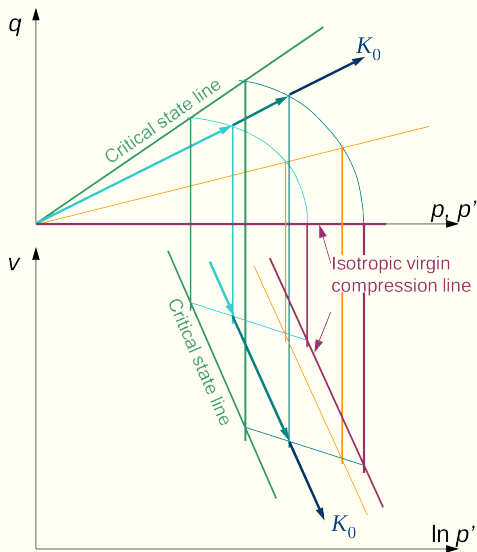
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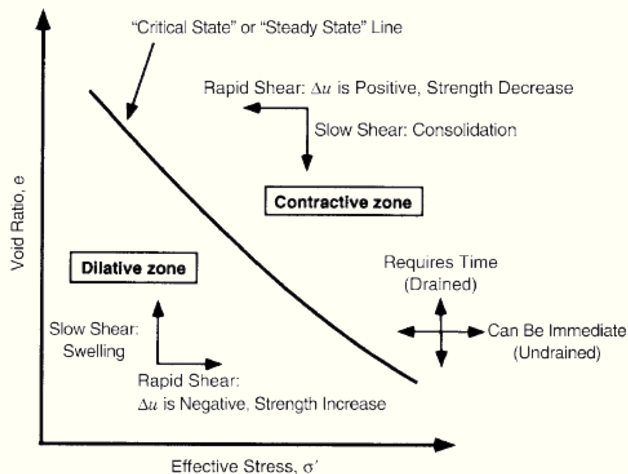


$v_\kappa$  depends on which  $\kappa$  line you are on.  $\kappa \neq c_r$  and  $\lambda \neq C_c$

# Stress paths $\sigma'_3/\sigma'_1 = K_c = \text{const}$

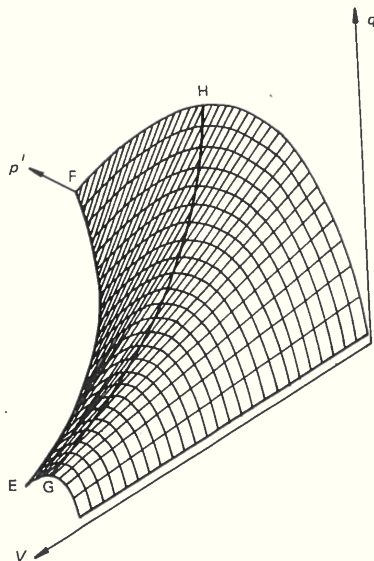


# Clay behavior





# Critical state boundary surface



# Summary of critical state behavior

- Can only traverse NCL in one direction
- Can traverse RCL ( $\kappa$ -line) in both directions
- To move from one  $\kappa$ -line to another must move along NCL. Hence, plastic volumetric strains must occur.
- Critical state line is **NOT** a yield surface. It's where it's going but a lot of plastic straining is needed to get there. (if  $CSL = F = 0$ ) then with associative flow rule  $d\varepsilon_p^p \neq 0$  at critical state. Real  $F$  is horizontal at critical state.