

MECH4450 Aerospace Propulsion

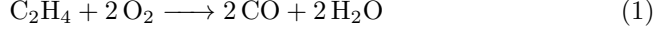
Major Assignment - Part 1

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The following finite rate chemistry mechanisms provide an accurate model of ethene combustion within a scramjet engine.



Information regarding the compositions of each reaction are stored as arrays (see Listing. 1), with the form of rows representing compounds and columns representing reaction. This method of information storage relies on each species being represented once within a single reaction which, while sufficient for this problem, requires improvement. Species are listed in the order of appearance; C2H4, O2, CO, H2O, CO2.

```

46   $\nu$  = np.array([
47      [-1., 0. ],
48      [-2., -0.5],
49      [ 2., -1. ],
50      [ 2., 0. ],
51      [ 0., 1. ]
52  ]).T
56   $\nu$ Exp = np.array([
57      [0.5, 0. ],
58      [0.65, 0.5],
59      [2., 1. ],
60      [2., 0. ],
61      [0., 1. ]
62  ]).T

```

Listing 1: Storage of reaction information

Stoichiometric coefficients are stored in ν , while experimentally derived rate coefficients are stored in ν Exp. The signs of stoichiometric coefficients are used to determine whether the respective species is a reactant or product of the reaction formulation. These signs are pre-computed, and stored in masks.

```

65  maskF = np.zeros_like( $\nu$ , dtype=bool)
66  maskR = np.zeros_like( $\nu$ , dtype=bool)
67  maskF[ $\nu$  < 0.] = True
68  maskR[ $\nu$  > 0.] = True

```

Listing 2: Reactant (**maskF**) and Product (**maskR**) species masks

The formation rates in $\text{kmol}/(\text{m}^3 \text{s})$ for the individual species are given as:

$$\frac{d[\text{C}_2\text{H}_4]}{dt} = -k_{1,f}[\text{C}_2\text{H}_4]^{0.5}[\text{O}_2]^{0.65} \quad (3a)$$

$$\frac{d[\text{O}_2]}{dt} = -2k_{1,f}[\text{C}_2\text{H}_4]^{0.5}[\text{O}_2]^{0.65} - \frac{1}{2}k_{2,f}[\text{CO}][\text{O}_2]^{0.5} + \frac{1}{2}k_{2,r}[\text{CO}_2] \quad (3b)$$

$$\frac{d[\text{CO}]}{dt} = 2k_{1,f}[\text{C}_2\text{H}_4]^{0.5}[\text{O}_2]^{0.65} - k_{2,f}[\text{CO}][\text{O}_2]^{0.5} + k_{2,r}[\text{CO}_2] \quad (3c)$$

$$\frac{d[\text{H}_2\text{O}]}{dt} = 2k_{1,f}[\text{C}_2\text{H}_4]^{0.5}[\text{O}_2]^{0.65} \quad (3d)$$

$$\frac{d[\text{CO}_2]}{dt} = k_{2,f}[\text{CO}][\text{O}_2]^{0.5} - k_{2,r}[\text{CO}_2] \quad (3e)$$

where $k_{1,f}$ is the forward rate of reaction for Eq. 1, and $k_{2,f}$ and $k_{2,r}$ are the forward and backward reaction rates for Eq. 2 respectively. As the first reaction

is uni-directional, the reverse reaction rate $k_{1,r}$ is set to 0. Forward reaction rates are calculated from the Arrhenius equation, using experimental values for the pre-exponential constant A and activation energy E_a .

$$k_{i,f} = A_i \exp\left(-\frac{E_{a,i}}{R_u T}\right) \quad (4)$$

Values for these constants are given in SI units of kmol, m and s in Table. 1.

	A	E_a
Eq. 1	1.739×10^9	1.485×10^5
Eq. 2	6.324×10^7	5.021×10^4

Table 1: Arrhenius equation constants

The reverse reaction rates are calculated using the equilibrium concentration coefficient K_c . This is related to the Gibbs free energy through the equilibrium pressure coefficient K_p .

$$K_p = \exp\left(-\frac{\Delta G^\circ(T)}{R_u T}\right) = K_c \left(\frac{p}{p^\circ}\right)^{\sum \nu} \quad (5)$$

The total change in Gibbs free energy is calculated as in Eq. 6, noting that the *signed* stoichiometric coefficients are used.

$$\Delta G^\circ(T) = \sum_i \nu_i \bar{g}_{f,i}^\circ(T) \quad (6)$$

$$K_p = \exp\left(-\frac{\sum_i \nu_i \bar{g}_{f,i}^\circ}{R_u T}\right) \quad (7)$$

This allows for a reduction in computation complexity, by calculating $K_{p,i}$ values for each individual species only once. Then the equilibrium concentration coefficient K_c can be calculated as

$$K_c = \exp\left(-\frac{\sum_i \nu_i \bar{g}_{f,i}^\circ}{R_u T}\right) \left(\frac{p^\circ}{p}\right)^{\sum_i \nu_i} = \prod_i \left[\exp(\ln K_{p,i}) \frac{p^\circ}{p}\right]^{\nu_i} \quad (8)$$

$$2.303 \log K_{p,i} = \ln K_{p,i} = -\frac{\bar{g}_{f,i}^\circ}{R_u T} \quad (9)$$

Values of $\log K_{p,i}$ are tabulated from The National Institute of Standards and Technology (1998), and interpolated for the current temperature. Storing the natural log of the value assists in quadratic interpolation, which is considered faster than attempting to use a spline interpolation method over the $k_{p,i}$ values themselves. This is implemented in a vectorised form shown in Listing 3, to improve efficiency.

```

84 def Kc(T, p):
85     Kf_i = np.array([pow(10, Kf(T)) for Kf in logKfuncs]) * (pRef/p)
86     forward = pow(Kf_i, maskF* $\nu$ Exp)
87     reverse = pow(Kf_i, maskR* $\nu$ Exp)
88     return np.prod(reverse, axis=1) / np.prod(forward, axis=1)

```

Listing 3: Calculation of equilibrium concentration coefficients

Note that the code uses the *unsigned* experimental coefficients, such as to explicitly match the ratio of rate coefficients. However, the definition from Gibbs free energy is based off stoichiometric coefficients. As these two sets of values are equal for the case of the second reaction, this is no concern for the specific case. If $\nu \neq \nu_{\text{Exp}}$ for a reaction requiring calculation of reverse reaction rates, it is predicted that using the ν_{Exp} values will provide the correct response.

The reverse reaction rate can then be calculated from the expression

$$K_c = \frac{k_f}{k_r} \longrightarrow k_r = \frac{k_f}{K_c} \quad (10)$$

where K_c is guaranteed to be a non-zero positive number. The rates of each species formation can then be expressed more generally as

$$\frac{d[X_i]}{dt} = k_f \prod_{i \in \text{reac}} \nu_i [X_i]^{\nu_{\text{Exp}_i}} - k_r \prod_{i \in \text{prod}} \nu_i [X_i]^{\nu_{\text{Exp}_i}} \quad (11)$$

The volumetric heat released per second from this reaction can be expressed as Eq. 12, with values of $\Delta h_{f,i}^\circ(T)$ tabulated from The National Institute of Standards and Technology (1998).

$$\dot{Q}''' = \sum_i \Delta h_{f,i}^\circ(T) \frac{d[X_i]}{dt} \quad (12)$$

Using the `maskF` and `maskR` arrays, both these calculations are implemented in a vectorised form as

```

115     ...
116     forward = kf * np.prod(pow( $\chi$ , maskF* $\nu$ Exp), axis=1)
117     reverse = kr * np.prod(pow( $\chi$ , maskR* $\nu$ Exp), axis=1)
118      $\chi$ Grad =  $\nu$ .T @ forward -  $\nu$ .T @ reverse
119     ...
120     hGrad = -sum([d $\chi$ _i*h_i(T) for d $\chi$ _i, h_i in zip( $\chi$ Grad, deltaHfuncs)])

```

Listing 4: Calculation of species rates of formation

where the array of concentrations is represented by χ . The full code is presented in the Appendix.

With an stoichiometric air-fuel ration, the molar fractions for C_2H_4 and O_2 can be calculated using Eq. 13. With an initial pressure and temperature of $p_0 = 70 \text{ kPa}$ and $T_0 = 1400 \text{ K}$, these equate to

$$\begin{aligned} n_{\text{init}} &= n_F + n_{\text{O}_2} + n_{\text{N}_2} = 1 + 3 \times (1 + 3.76) \\ [\text{C}_2\text{H}_4] &= \frac{n_F}{n_T} \frac{p_0}{R_u T_0} = 6.5445 \times 10^{-5} \text{ kmol/m}^3 \\ [\text{O}_2] &= \frac{n_{\text{O}_2}}{n_T} \frac{p_0}{R_u T_0} = 1.9633 \times 10^{-4} \text{ kmol/m}^3 \end{aligned} \quad (13)$$

Starting with these concentrations, and a reference enthalpy of $0 \text{ kJ}/(\text{kg K})$, the rates of species formation and heat release were integrated over 0.1 ms using the Python `scipy.integrate.solve_ivp` integrator with the `LSODA` method. The resulting graphs of concentration, rate of heat release, and net heat released are given in Fig. 1, 2 and 3 respectively.

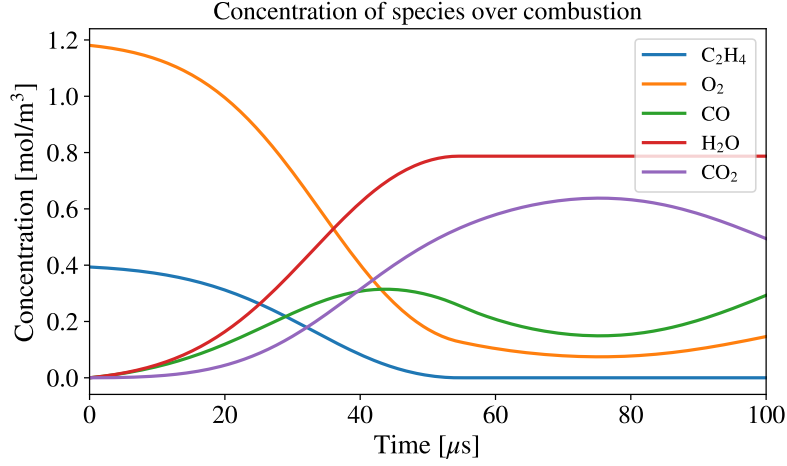


Figure 1: Concentration of species over combustion

It should be noted that as the solution progressed, it was necessary to clip values that tended below zero due to machine precision, to prevent complex valued non-physical solutions from being created. This leads to a discontinuity in the reaction rate when C_2H_4 is fully combusted, which is not noticeable in the species concentration solution, however can be seen in the rate of heat release (Fig. 2).

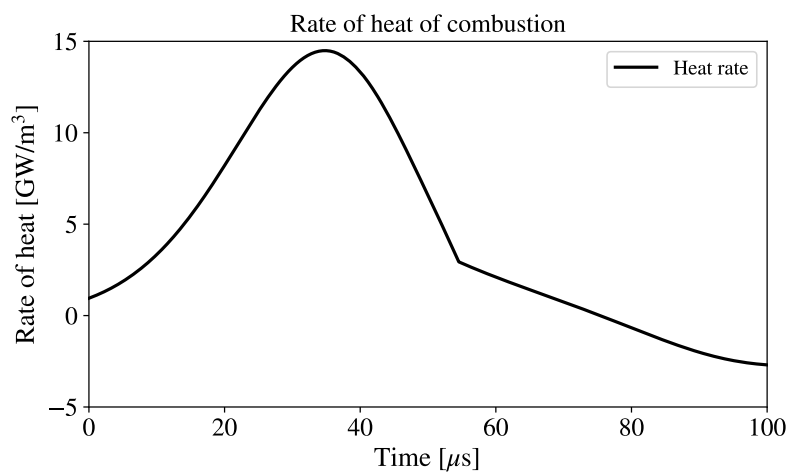


Figure 2: Rate of heat of combustion

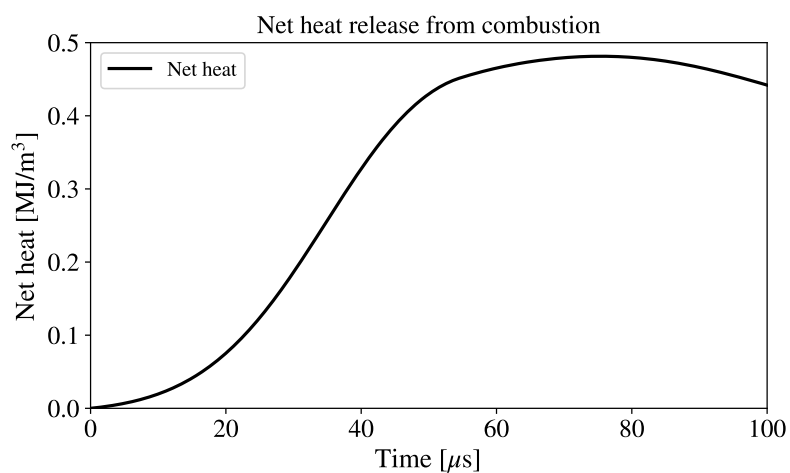


Figure 3: Net heat of combustion

References

The National Institute of Standards and Technology (1998). *NIST-JANAF Thermochemical Tables*. URL: <https://janaf.nist.gov/>.

Appendix

```
1 import math
2
3 import matplotlib.pyplot as plt
4 import numpy as np
5 import pandas as pd
6 from scipy import integrate
7 from scipy import interpolate
8
9 Ru = 8.314 # kJ/kmol.K
10 pRef = 100 # kPa
11
12 plt.style.use("PaperDoubleFig.mplstyle")
13
14
15 def lin(lower, upper, deltaX):
16     deltaY = upper - lower
17     grad = deltaY / deltaX
18
19     def inner(x):
20         return lower + grad*x
21
22     return inner
23
24
25 def vectorInterface(lengths):
26     L = [0, *np.cumsum(lengths)]
27
28     def wrapper(func):
29         def inner(t, args):
30             splitArgs = [args[l:r] for l, r in zip(L[:-1], L[1:])]
31             output = func(t, *splitArgs)
32             return np.hstack([*output])
33         return inner
34     return wrapper
35
36
37 # (row) species 0 :: C2H4
38 #               1 :: O2
39 #               2 :: CO
40 #               3 :: H2O
41 #               4 :: CO2
42
43 # (col) reaction 0 :: C2H4 + 2 O2 --> 2 CO + 2 H2O
44 #               1 :: CO + 1/2 O2 <-> CO2
45
46 # Stoichiometric coefficients
47 N = np.array([
48     [-1., 0. ],
49     [-2., -0.5],
50     [ 2., -1. ],
51     [ 2., 0. ],
52     [ 0., 1. ]
53 ]).T
54
55 # Experimental partial powers
56 NExp = np.array([
57     [0.5 , 0. ],
58     [0.65, 0.5],
59     [2. , 1. ],
```

```

60     [2. , 0. ],
61     [0. , 1. ]
62 ]).T
63
64 # Forward and reverse masks
65 maskF = np.zeros_like( $\nu$ , dtype=bool)
66 maskR = np.zeros_like( $\nu$ , dtype=bool)
67 maskF[ $\nu$  < 0.] = True
68 maskR[ $\nu$  > 0.] = True
69
70 chemData = []
71 for species in ("C2H4", "O2", "CO", "H2O", "CO2"):
72     data = pd.read_csv(f"chemData/{species}.txt", sep="\t", skiprows=1)
73     chemData.append(data[1:]) # Skip T=0K
74
75 logKfuncs, deltaHfuncs = [], []
76 for data in chemData:
77     T = data["T(K)"].values.astype(float)
78     logKf = data["log Kf"].values.astype(float)
79     deltaH = data["delta-f H"].values.astype(float) * 1e+03 # kJ/mol->kJ/kmol
80     logKfuncs.append(interpolate.interp1d(T, logKf, kind="quadratic"))
81     deltaHfuncs.append(interpolate.interp1d(T, deltaH, kind="quadratic"))
82
83
84 def Kc(T, p):
85     """Kc = Kp * pow(pRef/Ru*T,  $\nu$ Exp+...)"""
86     # NOTE: Account for partial pressures
87     Kf_i = np.array([pow(10, Kf(T)) for Kf in logKfuncs]) * (pRef/(Ru*T))
88     forward = pow(Kf_i, maskF* $\nu$ Exp)
89     reverse = pow(Kf_i, maskR* $\nu$ Exp)
90     return np.prod(reverse, axis=1) / np.prod(forward, axis=1)
91
92
93 def arrhenius(T):
94     return np.array([
95         1.739e+09 * math.exp(-1.485e+05 / (Ru*T)),
96         6.324e+07 * math.exp(-5.021e+04 / (Ru*T))
97     ])
98
99
100  $\Delta T$  = 0.1e-03
101 temp = lin(1400, 2800,  $\Delta T$ ) # K
102 pres = lin(70, 140,  $\Delta T$ ) # kPa
103
104
105 @vectorInterface((5, 1))
106 def gradient(t,  $\chi$ , h):
107     limit = ( $\chi$  < 0)
108      $\chi$ [limit] = 0
109
110     # Would normally calculate T from h = \int cp(T) dT
111     T, p = temp(t), pres(t)
112     kf = arrhenius(T)
113     kr = kf / Kc(T, p)
114     kr[0] = 0 # One way reaction
115
116     forward = kf * np.prod(pow( $\chi$ , maskF* $\nu$ Exp), axis=1)
117     reverse = kr * np.prod(pow( $\chi$ , maskR* $\nu$ Exp), axis=1)
118      $\chi$ Grad =  $\nu$ .T @ forward -  $\nu$ .T @ reverse
119      $\chi$ Grad[( $\chi$ Grad < 0)*limit] = 0

```



```

120
121     hGrad = -sum([dχi*hi(T) for dχi, hi in zip(χGrad, deltaHfuncs)])
122
123     return χGrad, hGrad
124
125
126     n = 1 + 3*(1 + 3.76)
127     χ0 = np.array(
128         [1/n, 3/n, 0.0, 0.0, 0.0]
129     ) * 70 / (Ru * 1400)
130     sol = integrate.solve_ivp(
131         gradient, (0, ΔT), np.append(χ0, 0.),
132         method="LSODA", events=None,
133         atol=1e-10, rtol=1e-10
134     )
135
136     t, y = sol.t, sol.y
137     print(f"The heat released is {y[-1][-1]*1e-03:.3f} MJ/m3")
138     print(np.array([1/n, 3/n, 0.0, 0.0, 0.0]))
139
140     fig, ax = plt.subplots()
141     formula = ("C$_2$H$_4$", "O$_2$", "CO", "H$_2$O", "CO$_2$")
142     [ax.plot(t*1e+06, y[i]*1e+03, label=formula[i]) for i in range(5)]
143     ax.legend()
144     ax.set_xlim([0, 100])
145     plt.xlabel(r"Time [ $\mu$ s]")
146     plt.ylabel("Concentration [mol/m3]")
147     plt.title("Concentration of species over combustion")
148     plt.savefig("../images/concentration.pdf")
149
150     fig, ax = plt.subplots()
151     ax.plot(sol.t*1e+06, sol.y[-1]*1e-03, "k-", label="Net heat")
152     ax.legend()
153     ax.set_xlim([0, 100])
154     ax.set_ylim([0, 0.5])
155     plt.xlabel(r"Time [ $\mu$ s]")
156     plt.ylabel("Net heat [MJ/m3]")
157     plt.title("Net heat release from combustion")
158     plt.savefig("../images/netHeat.pdf")
159
160     fig, ax = plt.subplots()
161     ax.plot(
162         sol.t*1e+06,
163         np.gradient(sol.y[-1], sol.t)*1e-06,
164         "k-", label="Heat rate"
165     )
166     ax.legend()
167     ax.set_xlim([0, 100])
168     ax.set_ylim([-5, 15])
169     plt.xlabel(r"Time [ $\mu$ s]")
170     plt.ylabel("Rate of heat [GW/m3]")
171     plt.title("Rate of heat of combustion")
172     plt.savefig("../images/heatRate.pdf")
173     plt.show()

```
