



ZJU-UIUC Institute

Zhejiang University / University of Illinois at Urbana-Champaign Institute



ECE 470: Introduction to Robotics

Lecture 15

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Schedule Check

• Lecture

O. Overview		
• Science & Engineering in Robotics		
I. Spatial Representation & Transformation		Fundamentals
• Coordinate Systems; Pose Representations; Homogeneous Transformations		Week 1-4
II. Kinematics		
• Multi-body frame assignment; D-H Convention; Joint-space; Work-space; Forward/Inverse Kinematics		Revision/ Quiz on Week 5
III. Velocity Kinematics and Static Forces		
• Translational/Rotational Velocity; Joint torque; Generalized Force Coordinates; Jacobian; Singularity		
IV. Dynamics		Essentials
• Acceleration of Body; Newton-Euler Approach; Lagrangian Formulation		
Week 8 → V. Control		Week 6-9
• Feedback Control, Independent Joint Control, Force Control		
VI. Planning		Revision/ Quiz on Week 10
• Joint-based Motion Planning; Cartesian-based Path Planning		
VII. Robot Vision (and Perception)		Applied
• Image Formation; Image Processing; Visual Tracking & Pose Estimation; Vision-based Control & Image-guided robotics		Week 11-13
		Revision/Reading Wk/ Exam on Week 14-16

Summary Recap of Robot Dynamics

- **Dynamics:** Concern with the forces (/torque) on bodies that cause motion
- **Representation:** Equation of Motion/ Dynamic Equation
- **Approaches:** (1) Newton-Euler & (2) Lagrangian Formulation

Recap N-E Method: Iteration through Links

Outwards Iteration

$${}^{i+1}\omega_{i+1}^0 = {}^{i+1}R {}^i\omega_i^0 + \dot{\theta}_{i+1} {}^{i+1}\hat{z}_{i+1}$$

$${}^{i+1}\dot{\omega}_{i+1}^0 = {}^{i+1}R \dot{\omega}_i^0 + {}^{i+1}R {}^i\omega_i^0 \times \dot{\theta}_{i+1} {}^{i+1}\hat{z}_{i+1} + \ddot{\theta}_{i+1} {}^{i+1}\hat{z}_{i+1}$$

$${}^{i+1}v_{i+1}^0 = {}^{i+1}R ({}^iv_i^0 + {}^i\omega_i^0 \times {}^ip_{i+1})$$

$${}^{i+1}\dot{v}_{i+1}^0 = {}^{i+1}R ({}^i\dot{\omega}_i^0 \times {}^ip_{i+1} + {}^i\omega_i^0 \times ({}^i\omega_i^0 \times {}^ip_{i+1}) + {}^i\dot{v}_i^0) + 2{}^{i+1}\omega_{i+1}^0 \times \dot{\theta}_{i+1} {}^{i+1}\hat{z}_{i+1} + \ddot{\theta}_{i+1} {}^{i+1}\hat{z}_{i+1}$$

$${}^{i+1}\dot{p}_{i+1}^0 = {}^{i+1}R ({}^i\omega_i^0 \times {}^ip_{i+1} + {}^i\omega_i^0 \times ({}^i\omega_i^0 \times {}^ip_{i+1}) + {}^i\dot{p}_i^0)$$

Newton Equation

$${}^{i+1}F_{i+1} = m_{i+1} {}^{i+1}\dot{v}_{i+1}^0$$

Euler Equation

$${}^{i+1}N_{i+1} = {}^{i+1}F_{i+1} + {}^{i+1}I_{i+1} {}^{i+1}\dot{\omega}_{i+1}^0 + {}^{i+1}\omega_{i+1}^0 \times {}^{i+1}I_{i+1} {}^{i+1}\dot{\omega}_{i+1}^0$$

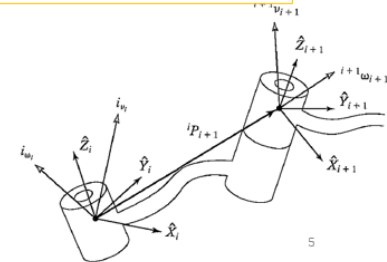
Inwards Iteration

$${}^if_i = {}^{i+1}R {}^{i+1}f_{i+1} + {}^iF_i$$

$${}^in_i = {}^in_i + {}^{i+1}R {}^{i+1}n_{i+1} + {}^iP_{C_i} \times {}^iF_i + {}^iP_{i+1} \times ({}^{i+1}R {}^{i+1}f_{i+1})$$

$$\tau_i = {}^in_i^T {}^i\hat{z}_i$$

$$\tau = M(\theta)\ddot{\theta} + V(\theta, \dot{\theta}) + G(\theta)$$



Recap: Velocity & Acceleration

$$\vec{V}_1 = \vec{V}_{B,ORG} + \dot{x} \hat{i}_B + \dot{y} \hat{j}_B + \dot{z} \hat{k}_B + \vec{\omega} \times \vec{P}_{1/B}$$

Differentiate w.r.t. time

$$\dot{\vec{V}}_1 = \dot{\vec{V}}_{B,ORG} + \ddot{x} \hat{i}_B + \ddot{y} \hat{j}_B + \ddot{z} \hat{k}_B + \vec{\omega} \times \vec{V}_{1/B} + \dot{\vec{\omega}} \times (\vec{V}_{1/B} + \vec{\omega} \times \vec{P}_{1/B}) + \vec{\omega} \times \dot{\vec{P}}_{1/B}$$

$$\dot{\vec{V}}_1 = \dot{\vec{V}}_{B,ORG} + \ddot{x} \hat{i}_B + \ddot{y} \hat{j}_B + \ddot{z} \hat{k}_B + 2\vec{\omega} \times \vec{V}_{1/B} + \vec{\omega} \times (\vec{\omega} \times \vec{P}_{1/B}) + \dot{\vec{\omega}} \times \vec{P}_{1/B}$$

Coriolis acceleration: $2\vec{\omega} \times \vec{V}_{1/B}$
Centrifugal acceleration: $\vec{\omega} \times (\vec{\omega} \times \vec{P}_{1/B})$
Tangential acceleration: $\dot{\vec{\omega}} \times \vec{P}_{1/B}$

Recap: Robot Dynamics

- **Dynamics:** Concern with the forces (/torque) on bodies that cause motion

Dynamic equation:

$$\tau = M(\theta)\ddot{\theta} + V(\theta, \dot{\theta}) + G(\theta)$$

$M(\theta)$ is $n \times n$ mass matrix of the manipulator

$V(\theta, \dot{\theta})$ is an $n \times 1$ vector of centrifugal and Coriolis terms

$G(\theta)$ is an $n \times 1$ vector of gravity terms

Cartesian Space: $\mathcal{F} = M_x(\theta)\ddot{x} + V_x(\theta, \dot{\theta}) + G_x(\theta)$

Recap: Lagrangian Approach

Method (2) Lagrangian: Energy-based approach

Potential energy of i th link:

$$u_i = -m_i {}^0g^T {}^0P_{C_i} + u_{ref}$$

0g is 3×1 gravity vector

${}^0P_{C_i}$ is the vector locating the center of mass of i th link

u_{ref} is the reference

Total potential energy is: $u = \sum_{i=1}^n u_i$

${}^0P_{C_i}$ is a function of $\theta, \sum_{i=1}^n u_i = u(\theta)$

Kinetic energy of the i th link is:

$$k_i = \frac{1}{2} m_i v_{C_i}^T v_{C_i} + \frac{1}{2} \omega_i^T I_i \omega_i$$

Must be positive

Kinetic energy of the manipulator is: $k = \sum_{i=1}^n k_i$

v_{C_i} and ω_i are functions of θ and $\dot{\theta}$

$$k(\theta, \dot{\theta}) = \frac{1}{2} \dot{\theta}^T M(\theta) \dot{\theta}$$

- Lagrangian dynamic formulation provides a means of deriving the equations of motion from a scalar function called the Lagrangian

- Lagrangian is defined as the difference between the kinetic and potential energy of a mechanical system

$$L(\theta, \dot{\theta}) \equiv k(\theta, \dot{\theta}) - u(\theta)$$

- Equations of motion are then given by:

$$\frac{d}{dt} \frac{\partial L}{\partial \dot{\theta}} - \frac{\partial L}{\partial \theta} = \tau$$

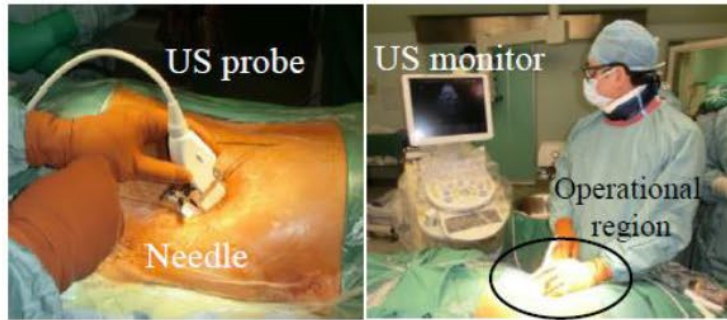
$$\tau = M(\theta)\ddot{\theta} + V(\theta, \dot{\theta}) + G(\theta)$$



Robot Control

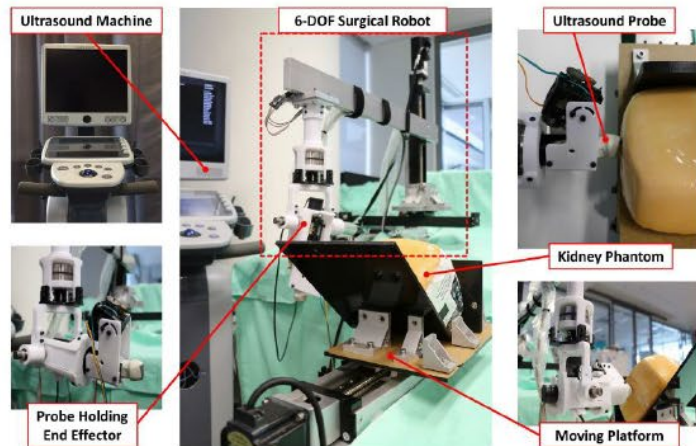
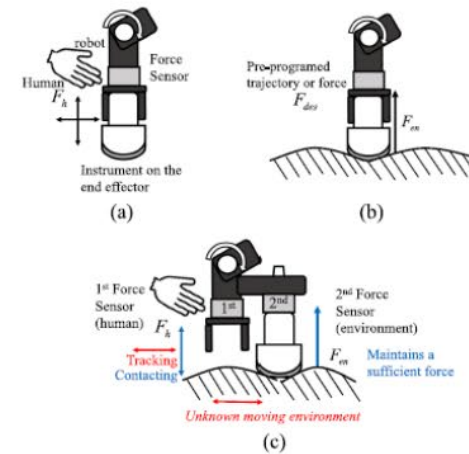
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Achieving Goals in Dynamic Systems

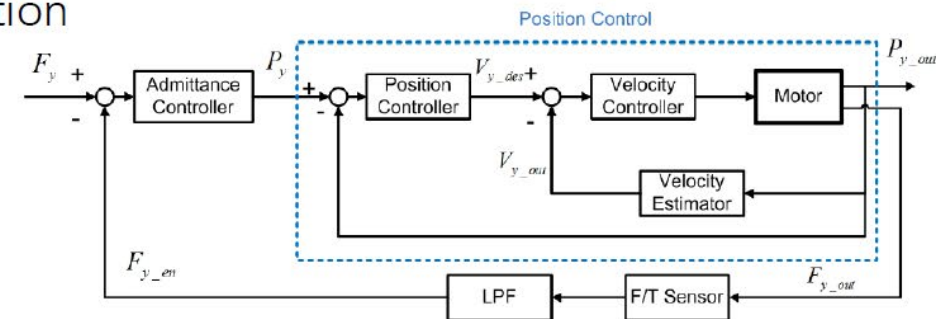


Understanding the physical problem

Modeling the systems



Design the solution



Control: Robotic Application

In robotics, we need control to perform motion

Drones



Legged Robots



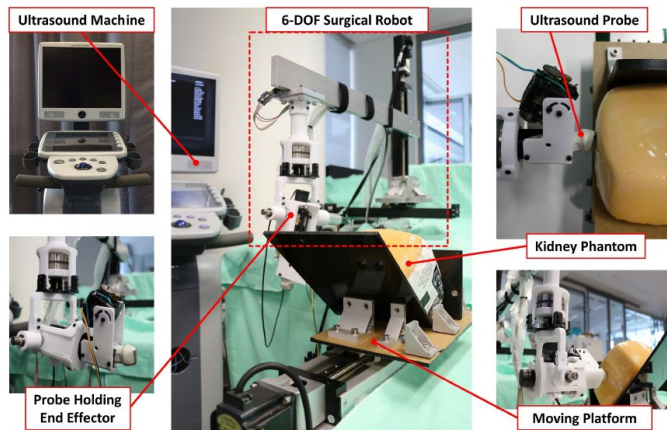
Manipulator



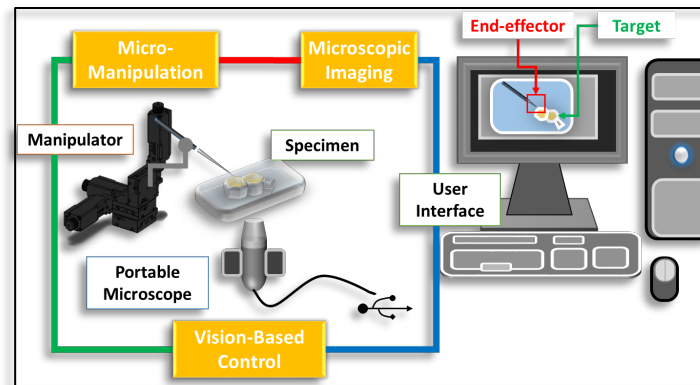
Mobile Robots



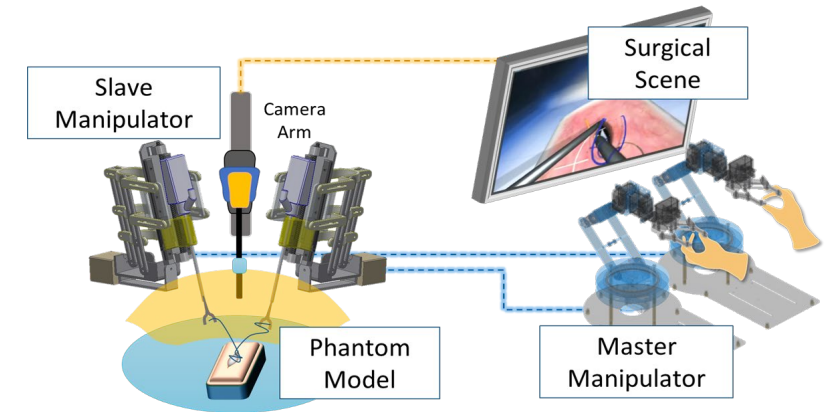
Control: Robotic Application



US-Guided Needle
Insertion Robot



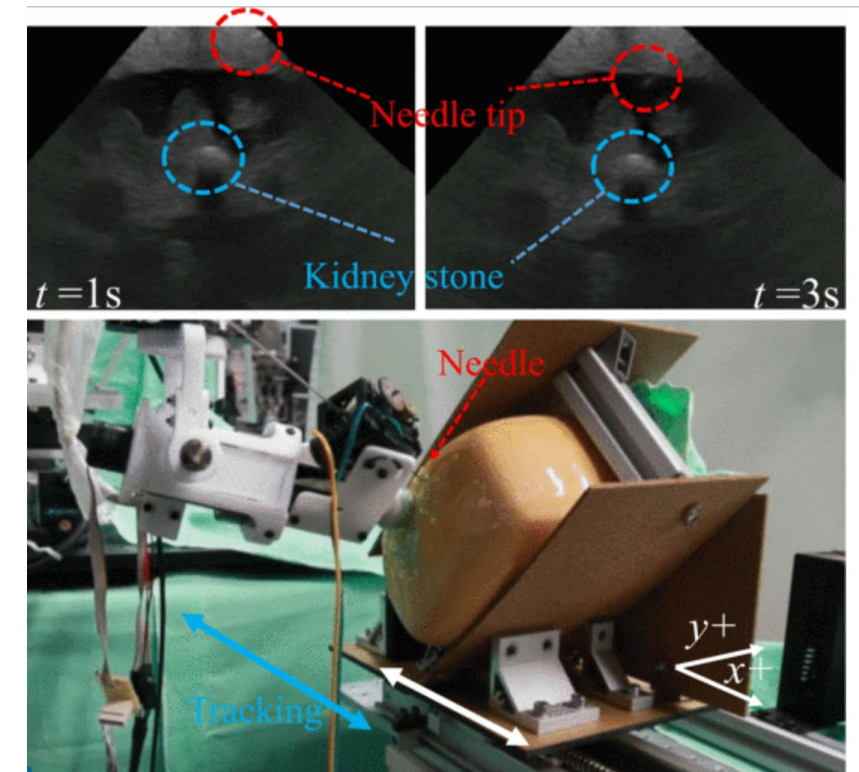
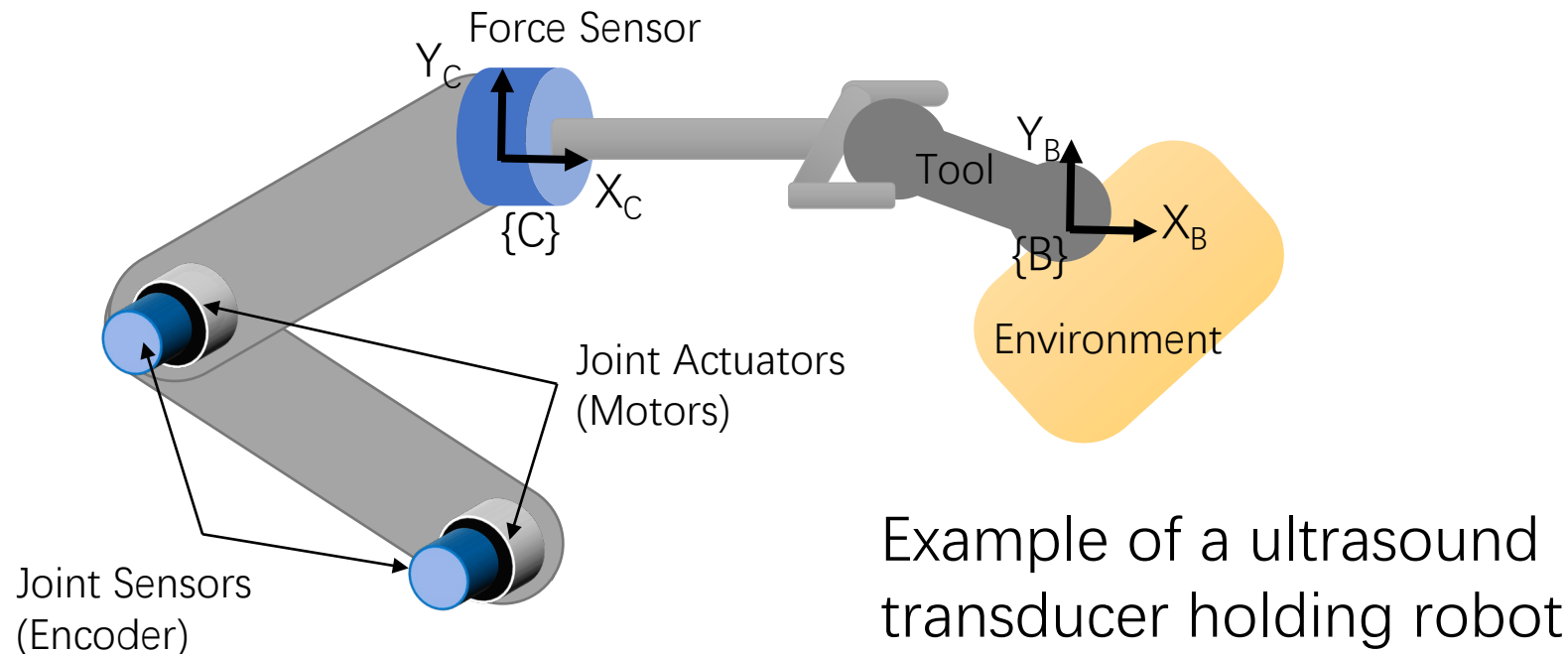
Vision-based Control Cell
Manipulation



Remote Control for
Tele-operation

Application Examples of Robotic Control

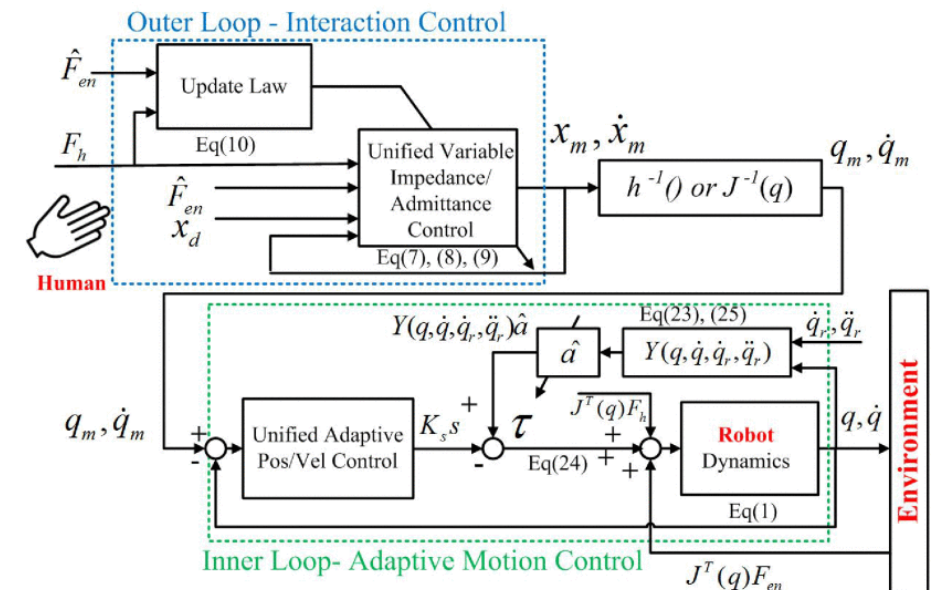
Case Example: Controlling a Robot to Track a Target on Ultrasound Image During Needle Insertion



Robot Control: Case Example

- A Control Scheme for Smooth Transition in Physical Human-Robot-Environment Between Two Modes: Augmentation and Autonomous

A Control Scheme for Smooth Transition in Physical Human-Robot-Environment between two Modes: Augmentation and Autonomous

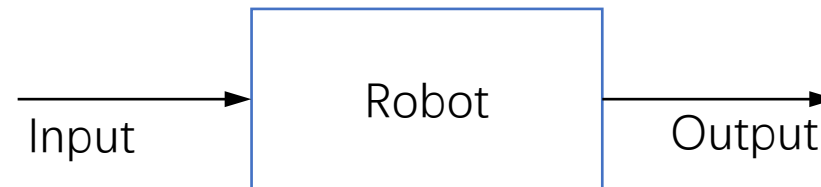


Robot Control

- Typically, we are interested in designing control systems that generate the **appropriate inputs** for the robotic system to achieve a **desired outcome** in a **dynamic environment** with a **specified performance**

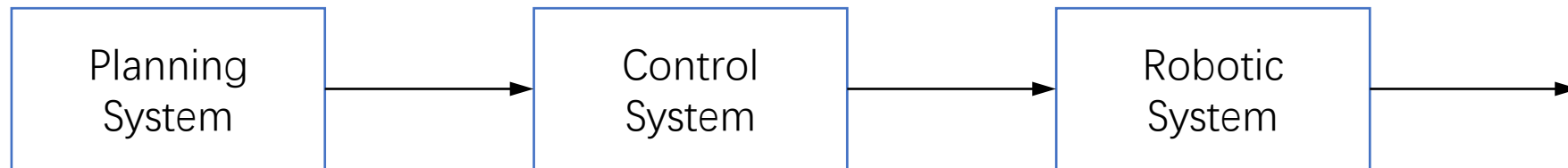
Robot Control

- **Robot Control:** Generate the input command to the robot to achieve a desired outcome



Deferred Topic: Planning

- The control system may take in command from a **planning system**

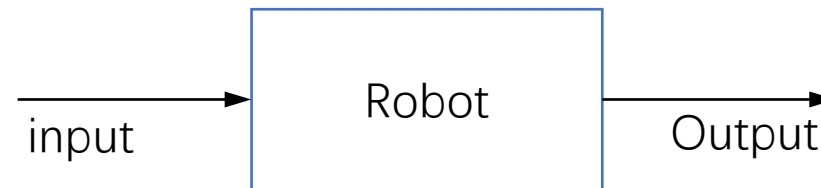


Feedback Control

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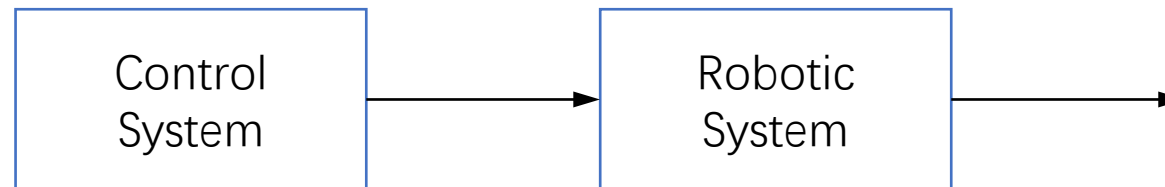
Robot Control

- The **control** problem is concerned with generating the appropriate inputs for the robotic system to achieve the desired outcome



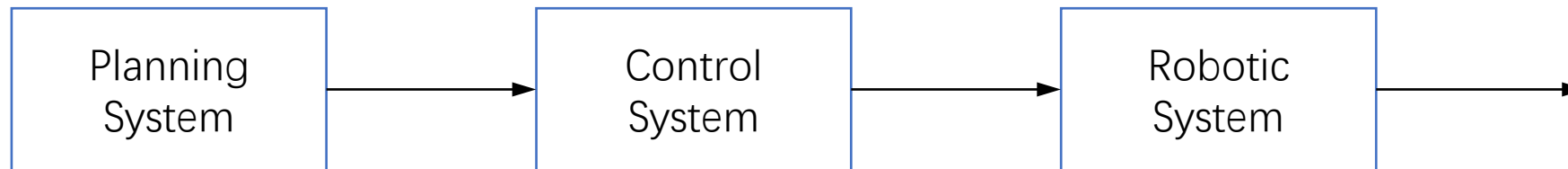
The big picture of robot control

- Design a control system that will generate the input to the robotic system so as to achieve a planned outcome



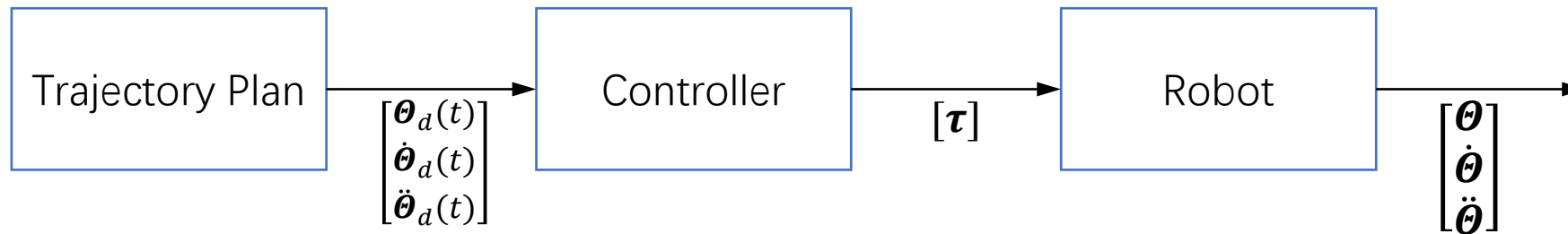
The big picture of robot control

- Design a control system that will generate the input to the robotic system so as to achieve a planned outcome
- The control system may take in command from a planning system



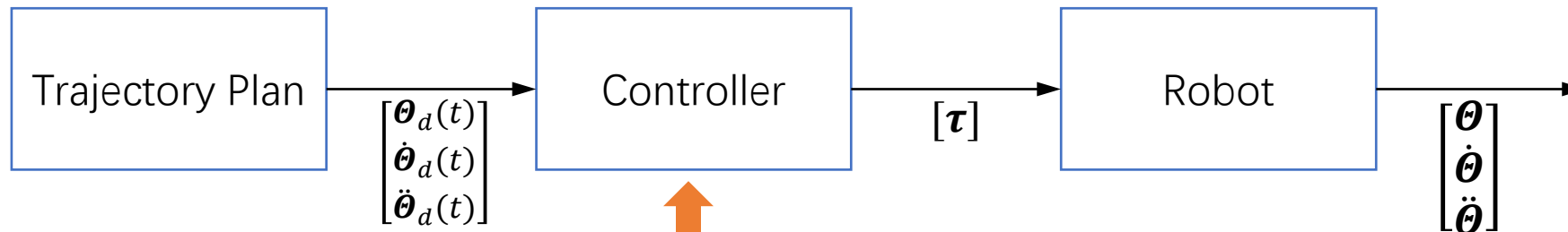
Robot Control: High-level Representation

Example: Control the robot to assume a desired motion profile by inputting the appropriate joint torque



Robot Control: High-level Representation

Example: Control the robot to assume a desired motion profile by inputting the appropriate joint torque



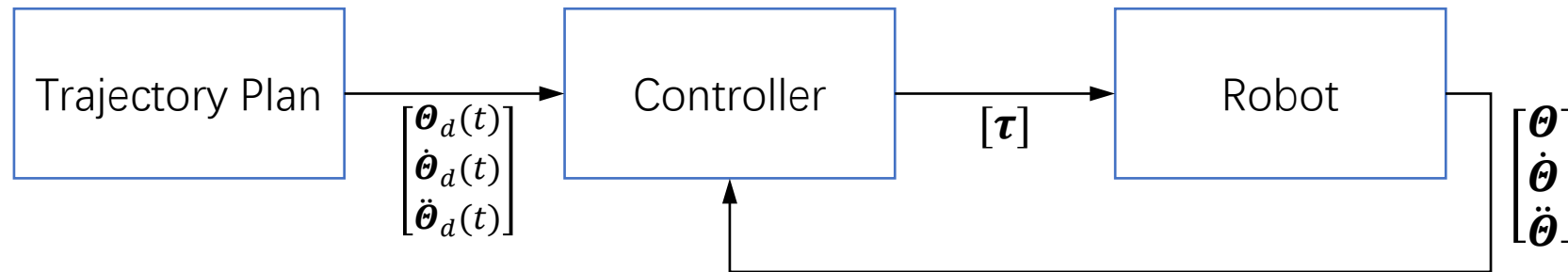
One way is to model the dynamics of the system such that the controller determines the τ to input with the dynamic equation

$$\tau = M(\theta_d)\ddot{\theta}_d + V(\theta_d, \dot{\theta}_d) + G(\theta_d)$$

This is referred to as **open-loop system** as the computed input to the robot is independent of the actual measurement of the robot motion

Robot Control: High-level Representation

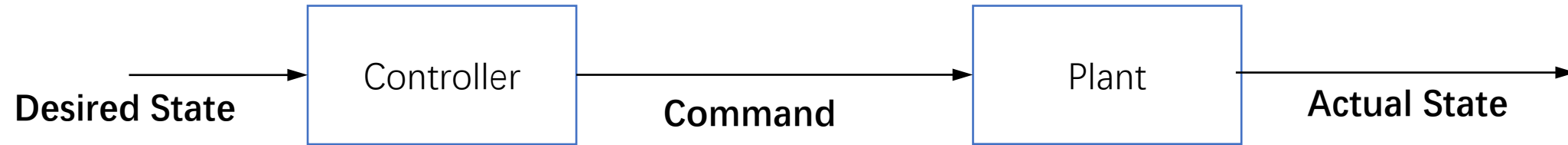
Example: Control the robot to assume a desired motion profile by inputting the appropriate joint torque



Through sensors we are able to feedback the measurement to produce the value of $[\tau]$ that will minimize the error between desired and actual targeted profile. This is known as a **closed-loop system**.

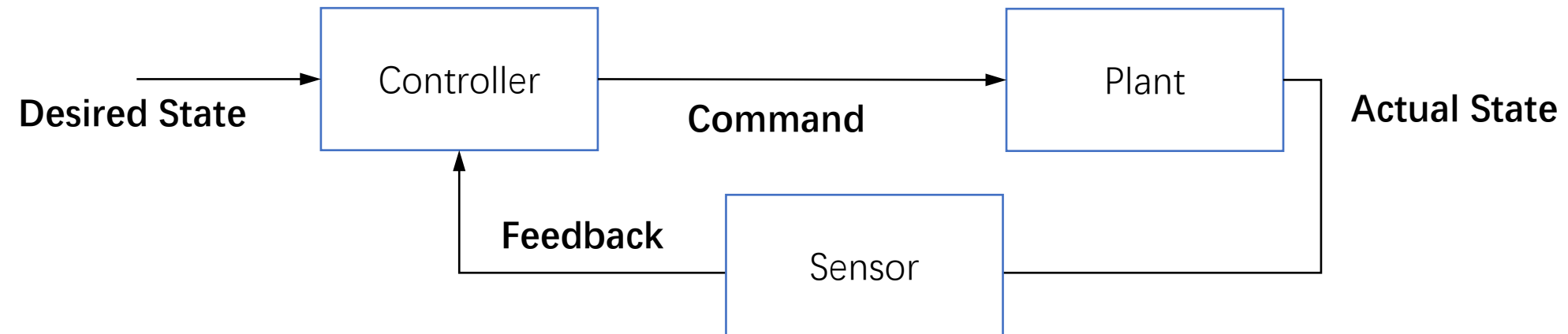
Feedback Control

Open-loop



Through preestablished model, generate the command that will achieve the desired state.

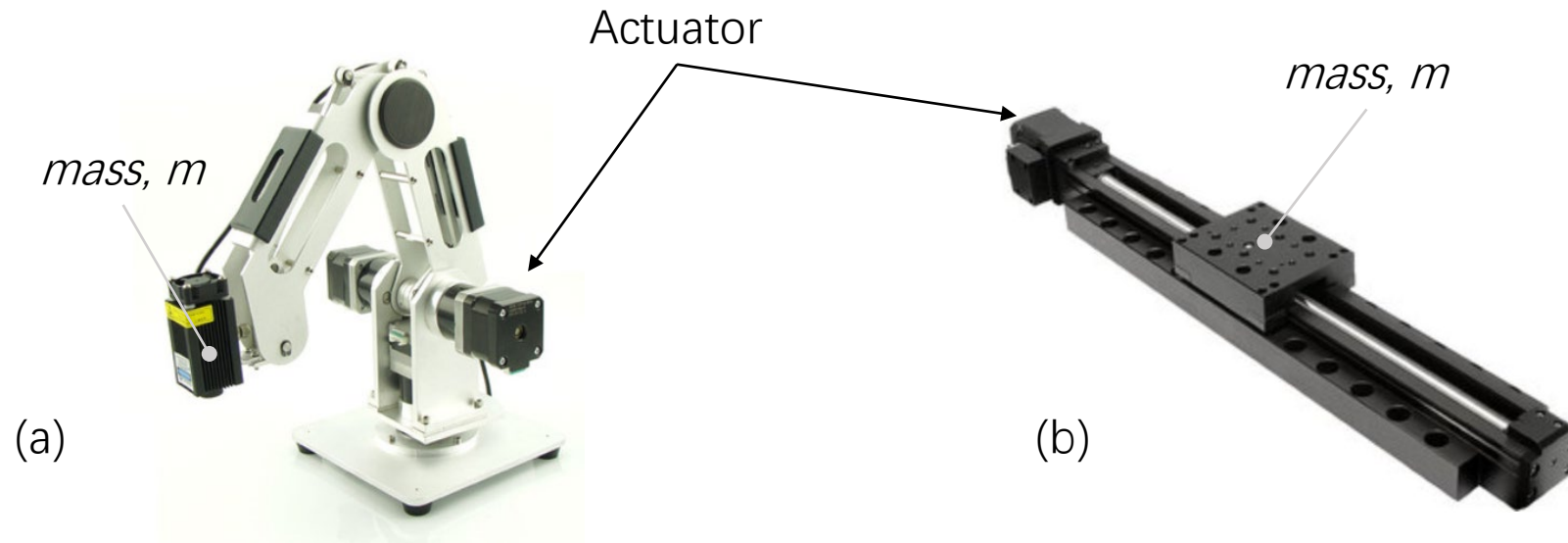
Closed-loop



Through sensors, we are able to **feedback** the measurement to produce the command that will minimize the error between desired and actual targeted profile.

Open vs. Closed loop

- Imagine you are controlling the position of the mass, m using a stepper motor by inputting the number of steps.
- Which mechanism (a) or (b) will open loop control be more suitable for? Discuss.



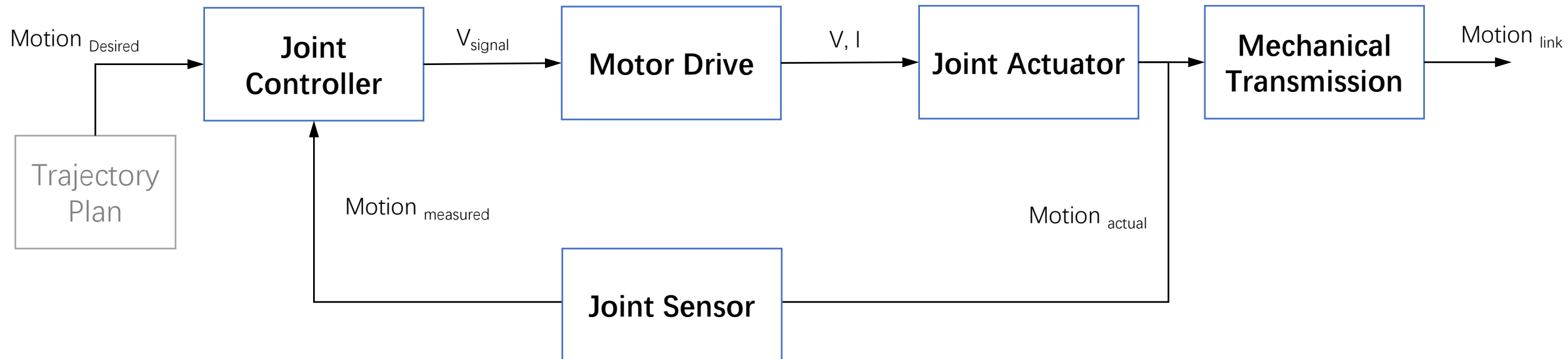


Joint Control

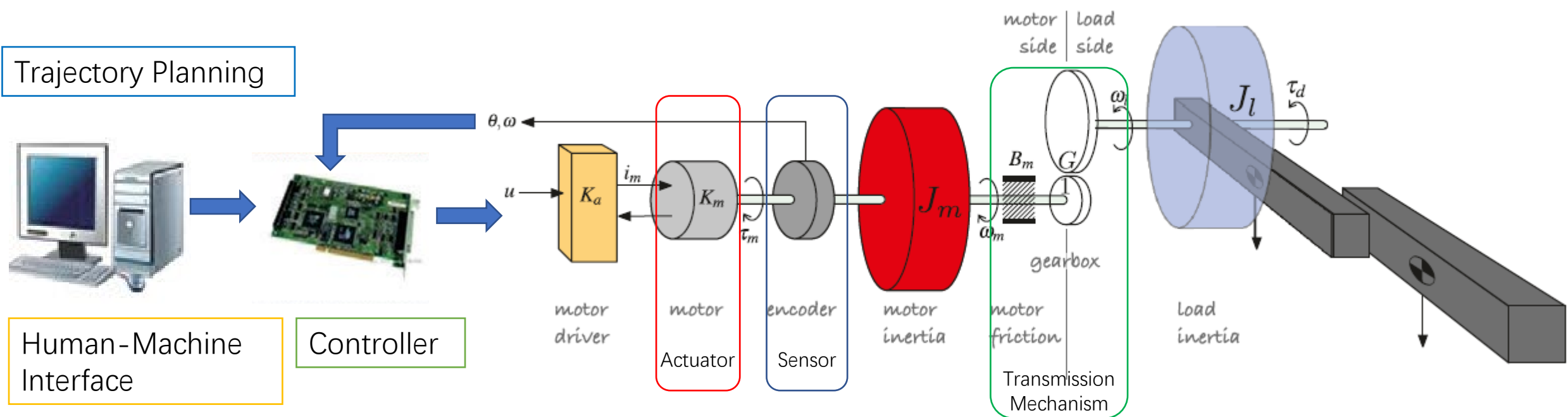
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Joint Control in Robotic System

Components of a robot joint control system

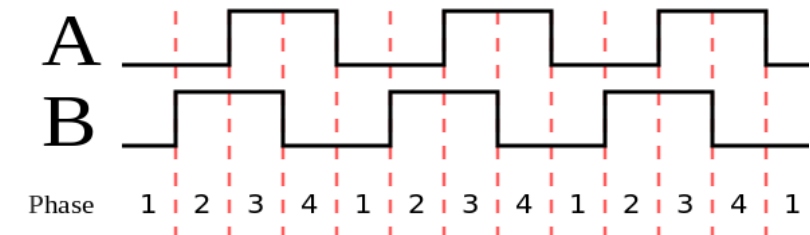
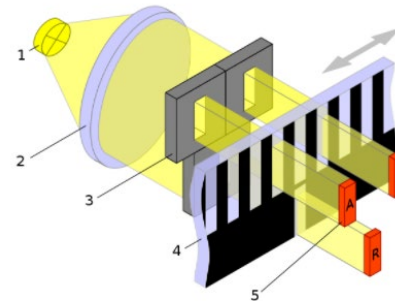
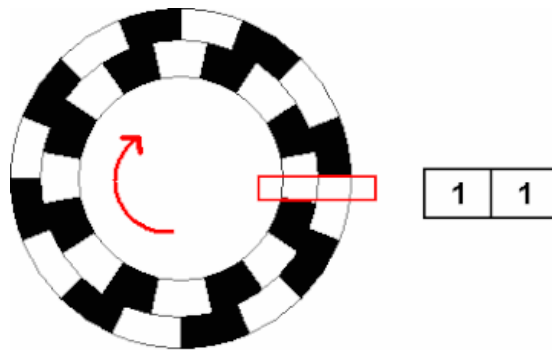


Joint Control in Robotic System



Robot Joint Sensor

- Position Sensing
 - Range Sensor (Linear)
 - Quadrature Encoder (Angular)



Robot Joint Sensor

- Force Sensing
 - Strain Gauge
 - Load Cell
 - Hall Sensor for Current Measure

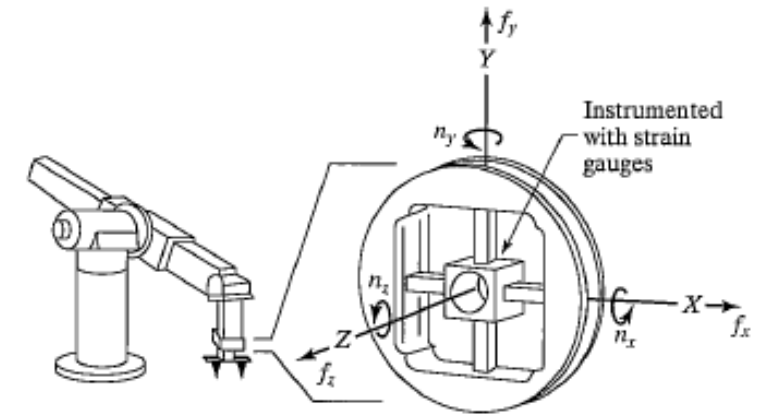
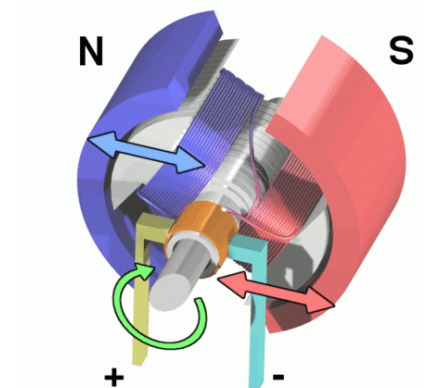
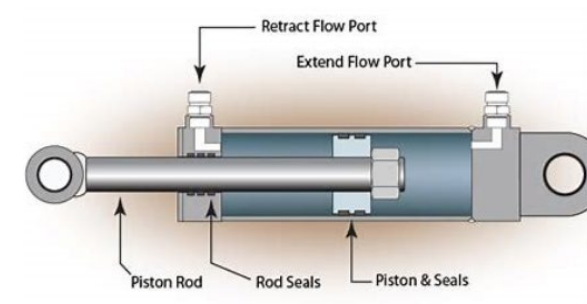


Figure 8.19 textbook (Craig, 3rd ed.)

Robot Joint Actuator

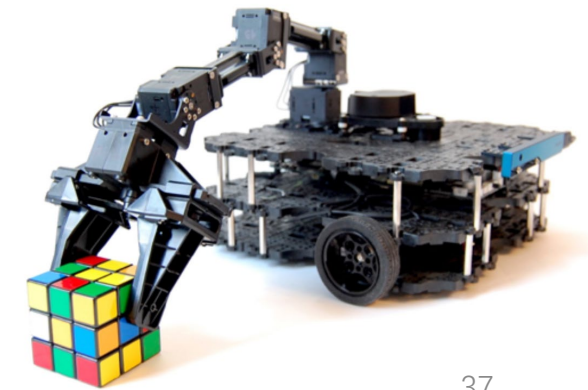
- Devices that power motion
- Principle of force/torque generation
 - Hydraulic
 - Pneumatic
 - Electric
 -
- Type of motion
 - Linear
 - Rotational
 - Vibration
 - Reciprocation
 - Free form
 -

By Rocketmagnet (hugo@shadowrobot.com) - Shadow Robot Company, CC BY-SA 3.0, <https://commons.wikimedia.org/w/index.php?curid=2107309>



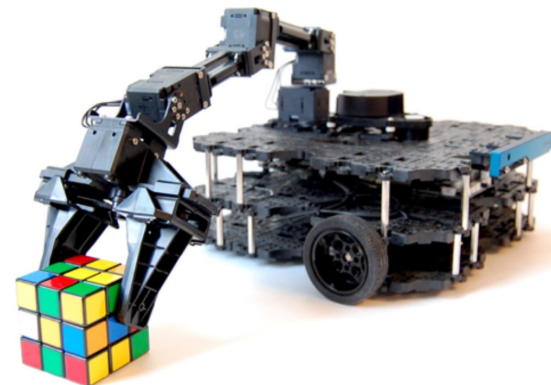
Robot Joint Actuator

- Different actuation principles for different robotics applications
- For examples:
 - Hydraulic for industrial robots → high torque on direct drive
 - Pneumatic for soft robotics → flexible configuration
 - Electric for relatively lightweight robotic platforms → requiring ease of interface



Robot Joint Actuator

- Different nature of motion for different applications
- For examples:
 - Linear for positioning in cartesian workspace
 - Rotational for continuous circular motion wheeled robot

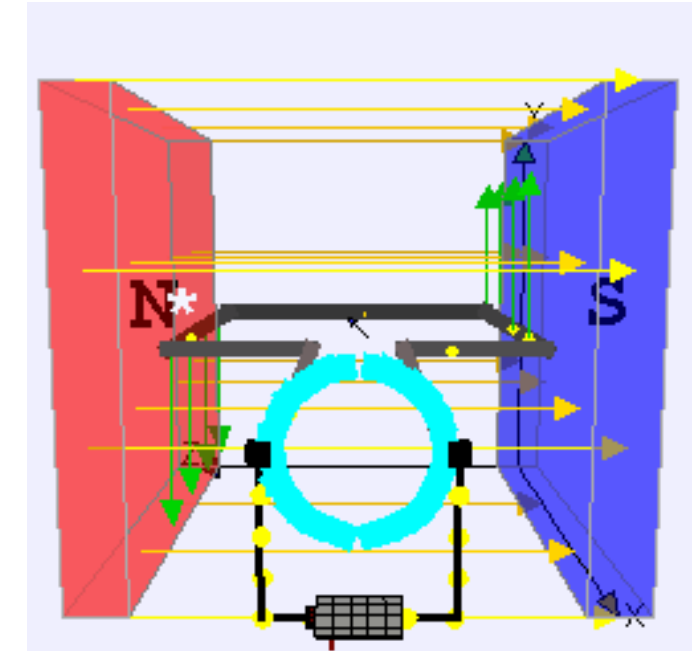
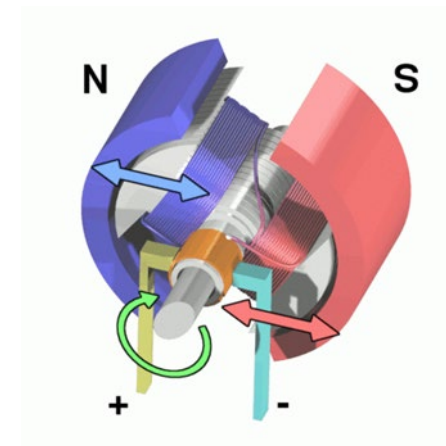
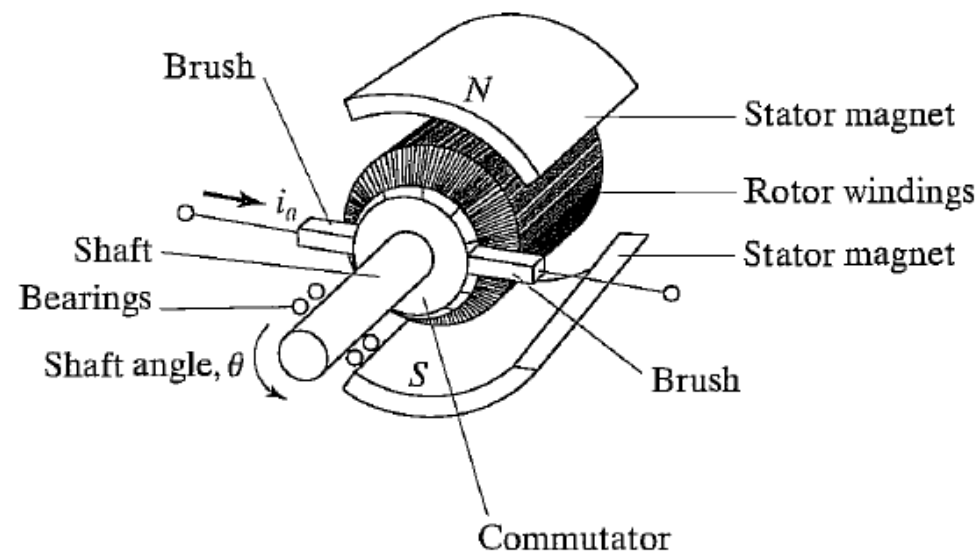


Robot Joint Actuator

- Electric motor
 - Direct-Current (DC) motor
 - Stepper motor
 - Alternating Current (AC) motor
 - Ultrasonic
 - Piezoelectric

Robot Joint Actuator

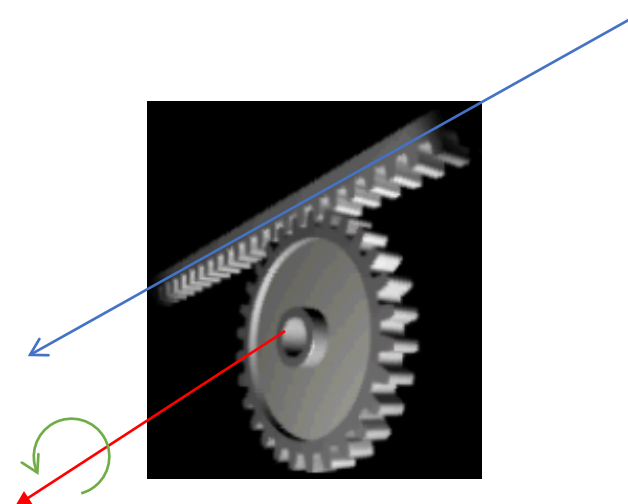
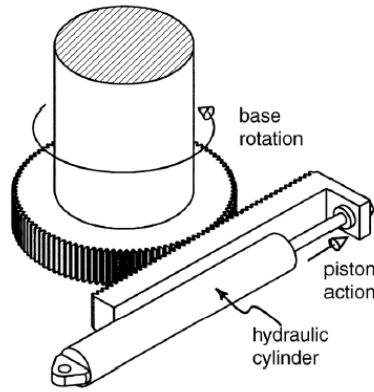
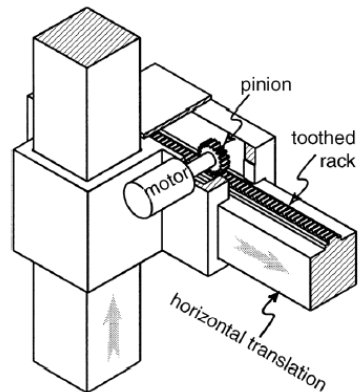
- In this course, we look at DC motor



By Lookang many thanks to Fu-Kwun Hwang and author of Easy Java Simulation = Francisco Esquembre - Own work <http://iwant2study.org/ospsg/index.php/interactive-resources/physics/05-electricity-and-magnetism/09-electromagnetic-induction/313-ejs-model-dcmotor10>, CC BY-SA 3.0, <https://commons.wikimedia.org/w/index.php?curid=15736309>

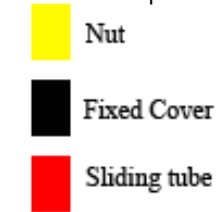
Robot Joint Actuator

- Transmission System

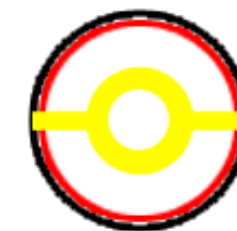


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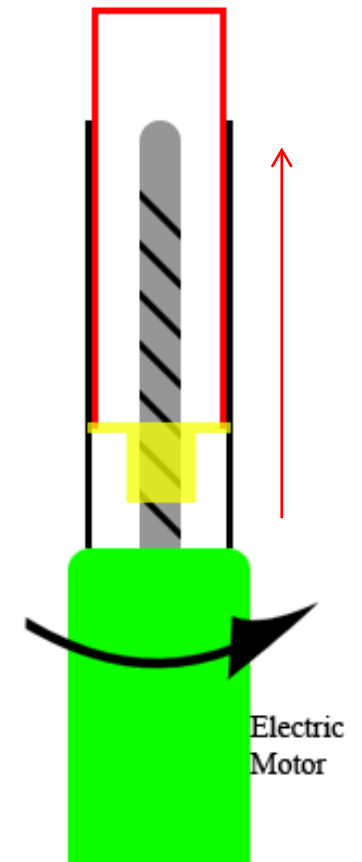
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Yellow nut interlocks with black tube to prevent the nut/red tube assembly from rotating with respect to the black tube.



Bottom View
(not including motor)



Robot Joint Actuator

- Transmission System for
 - Speed-Reducing & Torque-Increasing, or Vice-Versa
 - Remote Driving of Joint
 - Convert motion type

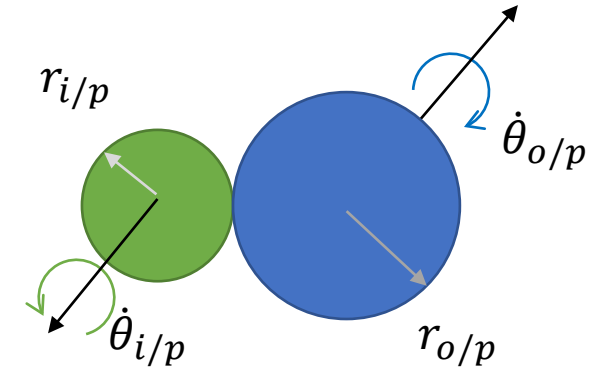
Robot Joint Actuator

- Transmission System
 - Speed-Reducing & Torque-Increasing, or Vice-Versa
 - Remote Driving of Joint
 - Convert motion type

Speed-Reduction $\dot{\theta}_{o/p} = \frac{1}{\eta} \dot{\theta}_{i/p}$

Torque-Increment $\tau_{o/p} = \eta \tau_{i/p}$

Gear Ratio $\eta = \frac{r_{o/p}}{r_{i/p}} = \frac{\tau_{o/p}}{\tau_{i/p}} = \frac{\dot{\theta}_{i/p}}{\dot{\theta}_{o/p}}$



Control of 2nd Order System

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Designing Robot Control System

- The central question in designing a control system is the performance specification
 - System response
 - Stability analysis

Second-Order System

Equation of Motion (EOM),

$$\sum F = -F_{drag} - F_{spring}$$
$$m\ddot{x}(t) = -b\dot{x}(t) - kx(t)$$
$$m\ddot{x}(t) + b\dot{x}(t) + kx(t) = 0$$

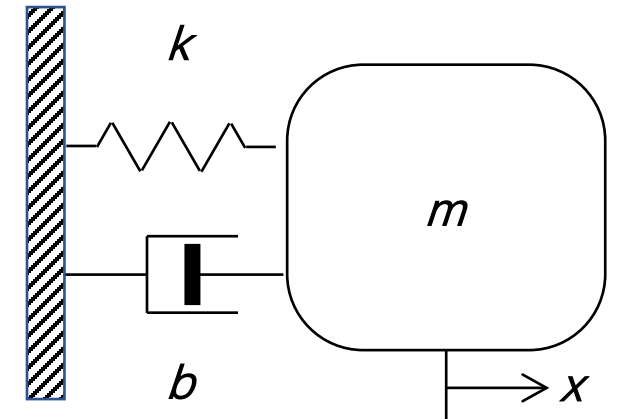
Taking Laplace Transform,

$$m[s^2X(s) - sx(0) - \dot{x}(0)] + b[sX(s) - x(0)] + kX(s) = 0$$

$$(ms^2 + bs + k)X(s) = m[sx(0) - \dot{x}(0)] + bx(0)$$

$$X(s) = \frac{(ms - b)x(0) - m\dot{x}(0)}{ms^2 + bs + k}$$

Characteristic Equation: $ms^2 + bs + k = 0$



Second-Order System

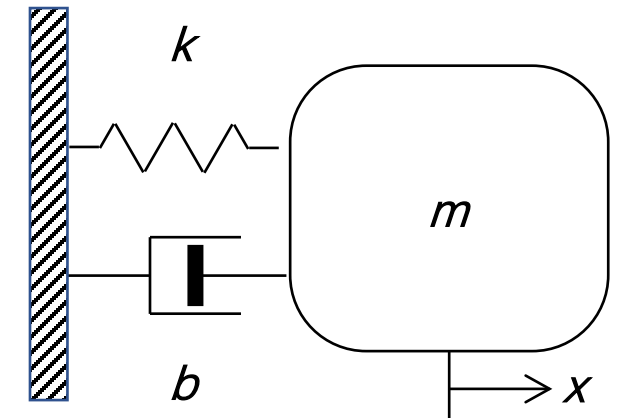
Solving the 2nd order ODE,

$$s_1 = -\frac{b}{2m} + \frac{\sqrt{b^2 - 4mk}}{2m}, \quad s_2 = -\frac{b}{2m} - \frac{\sqrt{b^2 - 4mk}}{2m}$$

System Response,

Overdamped	$b^2 - 4mk > 0$	Real and unequal roots
Underdamped	$b^2 - 4mk < 0$	Complex roots
Critically damped	$b^2 - 4mk = 0$	Real and Equal roots

The Natural response in time domain can be obtained



Second-Order System

General Solutions

Overdamped $b^2 - 4mk > 0$

Real and unequal roots: $s_1 \neq s_2$

$$x(t) = c_1 e^{s_1 t} + c_2 e^{s_2 t}$$

Underdamped $b^2 - 4mk < 0$

Complex roots: $s_{1,2} = \lambda \pm \mu i$

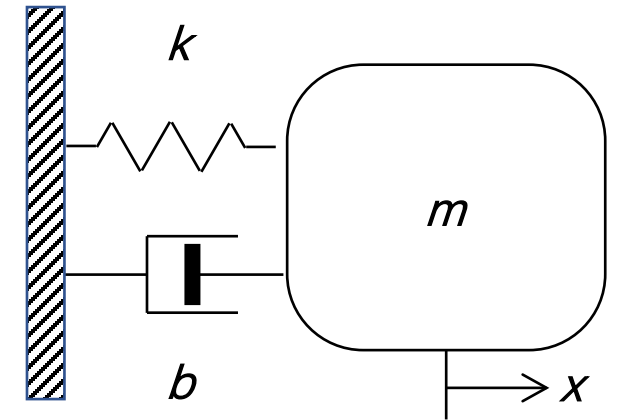
$$x(t) = c_1 e^{\lambda t} \cos(\mu t) + c_2 e^{\lambda t} \sin(\mu t)$$

Critically damped $b^2 - 4mk = 0$

Real and Equal roots $s_1 = s_2$

$$x(t) = (c_1 + c_2 t) e^{s_{1,2} t}$$

where c_1 and c_2 are constants determined by initial conditions
i.e. initial position and velocity



Example 6.2: Overdamped

Example 9.1 in textbook (Craig, 3rd ed.)

The block mass is released from $x = -1$ at rest, $m = 1$, $b = 5$ and $k = 6$

Characteristic Equation $s^2 + 5s + 6 = 0$

with real and unequal root $s_1 = -2$ and $s_2 = -3$

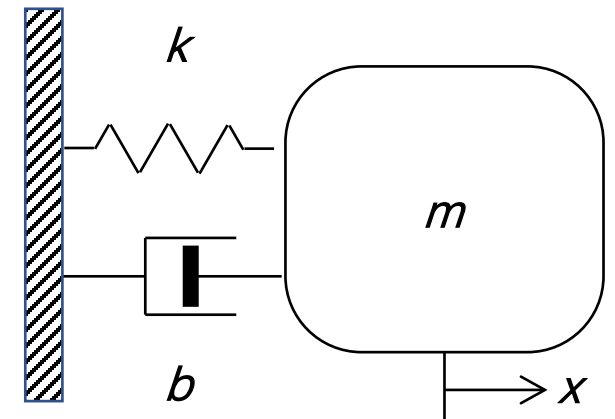
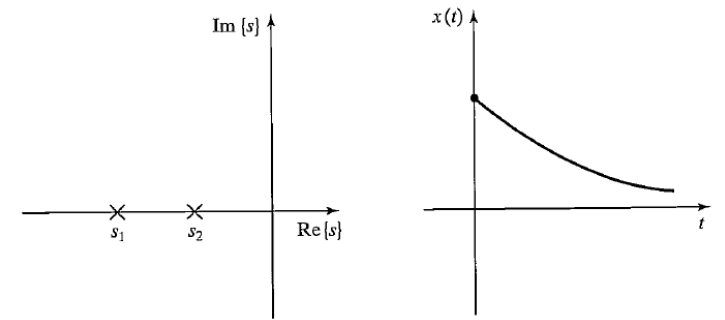
System response $x(t) = c_1 e^{-2t} + c_2 e^{-3t}$

using $x(0) = -1$ $c_1 + c_2 = -1$

using $\dot{x}(0) = 0$ $-2c_1 - 3c_2 = 0$

Satisfying the initial conditions: $c_1 = -3$ and $c_2 = 2$

Motion for $t \geq 0$ $x(t) = -3e^{-2t} + 2e^{-3t}$



Example 6.3 Underdamped

Example 9.2 in textbook (Craig, 3rd ed.)

The block mass is released from $x = -1$ at rest, $m = 1$, $b = 1$ and $k = 1$

Characteristic Equation $s^2 + s + 1 = 0$

with complex roots: $s_{1,2} = -\frac{1}{2} \pm \frac{\sqrt{3}}{2}i$

System response: $x(t) = e^{-\frac{t}{2}} \left(c_1 \cos\left(\frac{\sqrt{3}}{2}t\right) + c_2 \sin\left(\frac{\sqrt{3}}{2}t\right) \right)$

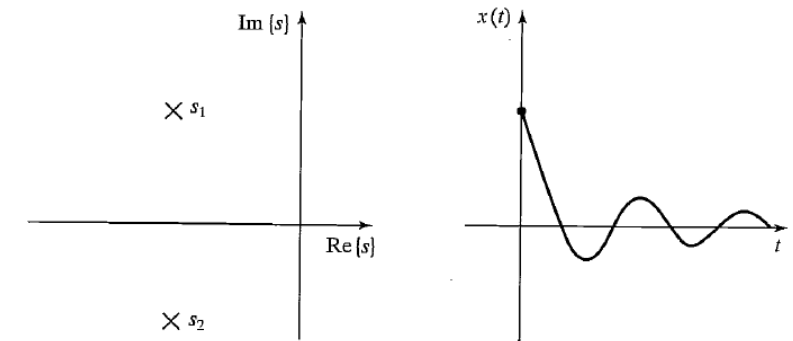
using $x(0) = -1$ $c_1 = -1$

using $\dot{x}(0) = 0$ $-\frac{1}{2}c_1 + \frac{\sqrt{3}}{2}c_2 = 0$

Satisfying the initial conditions: $c_1 = -1$ and $c_2 = -\frac{\sqrt{3}}{3}$

Motion for $t \geq 0$ $x(t) = e^{-\frac{t}{2}} \left(-\cos\left(\frac{\sqrt{3}}{2}t\right) - \frac{\sqrt{3}}{3} \sin\left(\frac{\sqrt{3}}{2}t\right) \right)$

$$x(t) = \frac{\sqrt{3}}{3} e^{-\frac{t}{2}} \cos\left(\frac{\sqrt{3}}{2}t + \frac{5\pi}{6}\right)$$

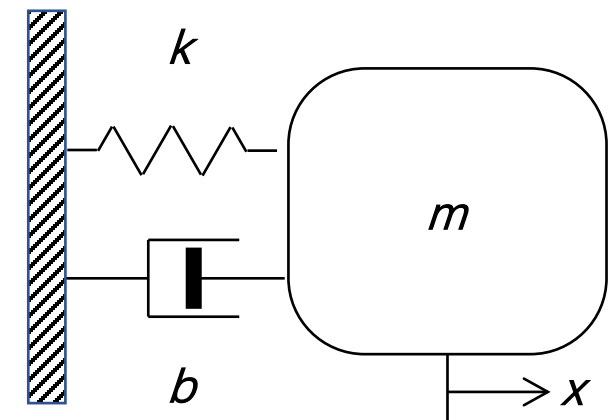


Recall R-formula

$$x(t) = r e^{\lambda t} \cos(\mu t - \delta),$$

$$r = \sqrt{c_1^2 + c_2^2},$$

$$\delta = \text{Atan2}(c_2, c_1).$$



Example 6.3 Underdamped

Example 9.2 in textbook (Craig, 3rd ed.)

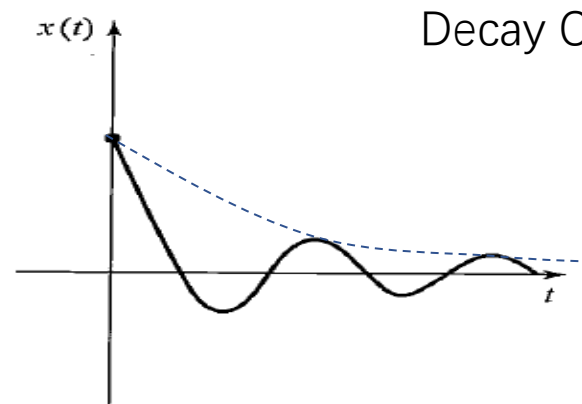
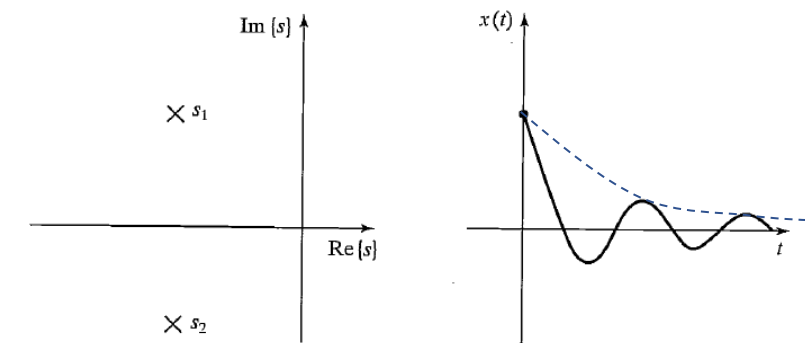
The block mass is released from $x = -1$ at rest, $m = 1$, $b = 1$ and $k = 1$

Characteristic Equation $s^2 + s + 1 = 0$

Motion for $t \geq 0$

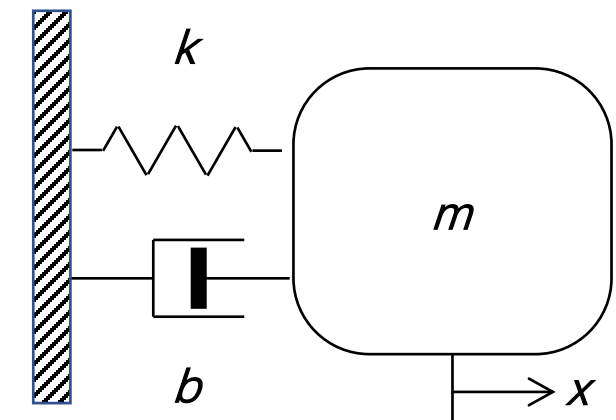
$$x(t) = e^{-\frac{t}{2}} \left(-\cos\left(\frac{\sqrt{3}}{2}t\right) - \frac{\sqrt{3}}{3} \sin\left(\frac{\sqrt{3}}{2}t\right) \right)$$

$$x(t) = \frac{\sqrt{3}}{3} e^{-\frac{t}{2}} \cos\left(\frac{\sqrt{3}}{2}t + \frac{5\pi}{6}\right)$$



Decay Constant

Damped Frequency



Example 6.4 Critically Damped

The block mass is released from $x = -1$ at rest, $m = 1$, $b = 4$ and $k = 4$

Characteristic Equation $s^2 + 4s + 4 = 0$

with real and equal root $s_1 = s_2 = -2$

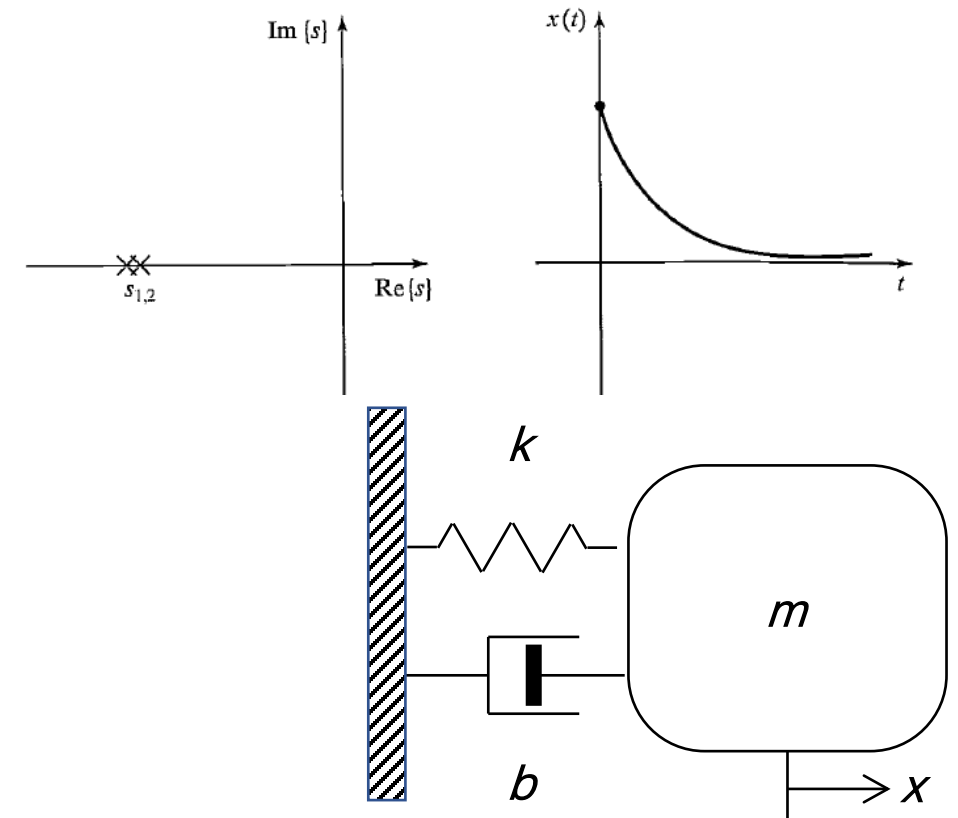
System response $x(t) = (c_1 + c_2 t)e^{-2t}$

using $x(0) = -1$ $c_1 = -1$

using $\dot{x}(0) = 0$ $-2c_1 + c_2 = 0$

Satisfying the initial conditions: $c_1 = -1$ and $c_2 = -2$

Motion for $t \geq 0$ $x(t) = (-1 - 2t)e^{-2t}$



Second-Order System

From Ex 6.2-4, the systems are all **stable** where m, b and $k > 0$

In free oscillation, the system has natural response

In control applications, the system has forced response

Second-Order System

The Dynamics of the Mass-Spring-Damper System

$$m\ddot{x}(t) + b\dot{x}(t) + kx(t) = 0$$

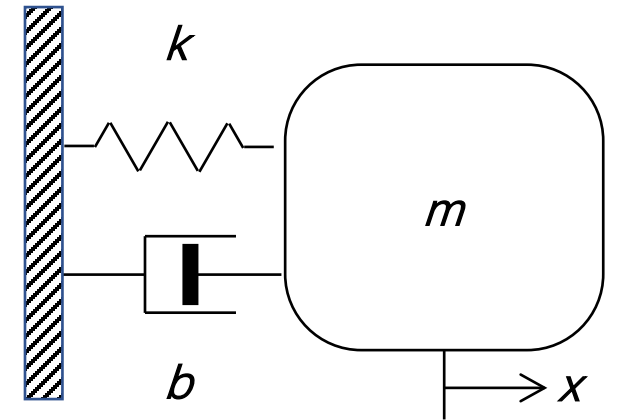
can be described as an oscillatory 2nd order system

$$\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = 0$$

characterized by

$$\text{Natural frequency: } \omega_n = \sqrt{\frac{K}{m}}$$

$$\text{Damping Ratio: } \zeta = \frac{1}{2} \sqrt{\frac{b^2}{mk}}$$



Second-Order System

Oscillatory 2nd order system with free response

Homogenous ODE $\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = 0$

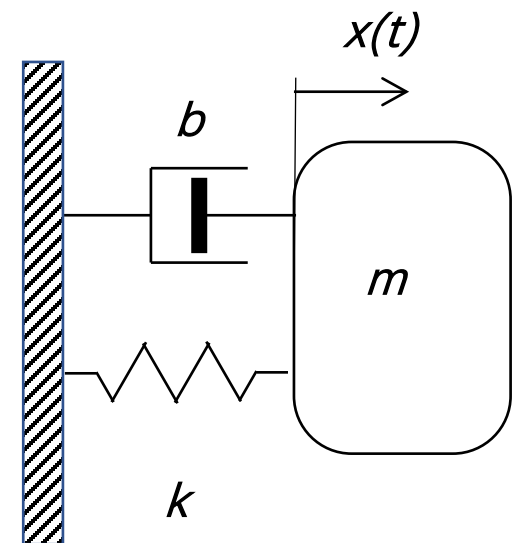
Free response

Overdamped $\zeta > 1$ Real and unequal roots: $s_1 = s_2$

Critically damped $\zeta = 1$ Real and Equal roots $s_1 \neq s_2$

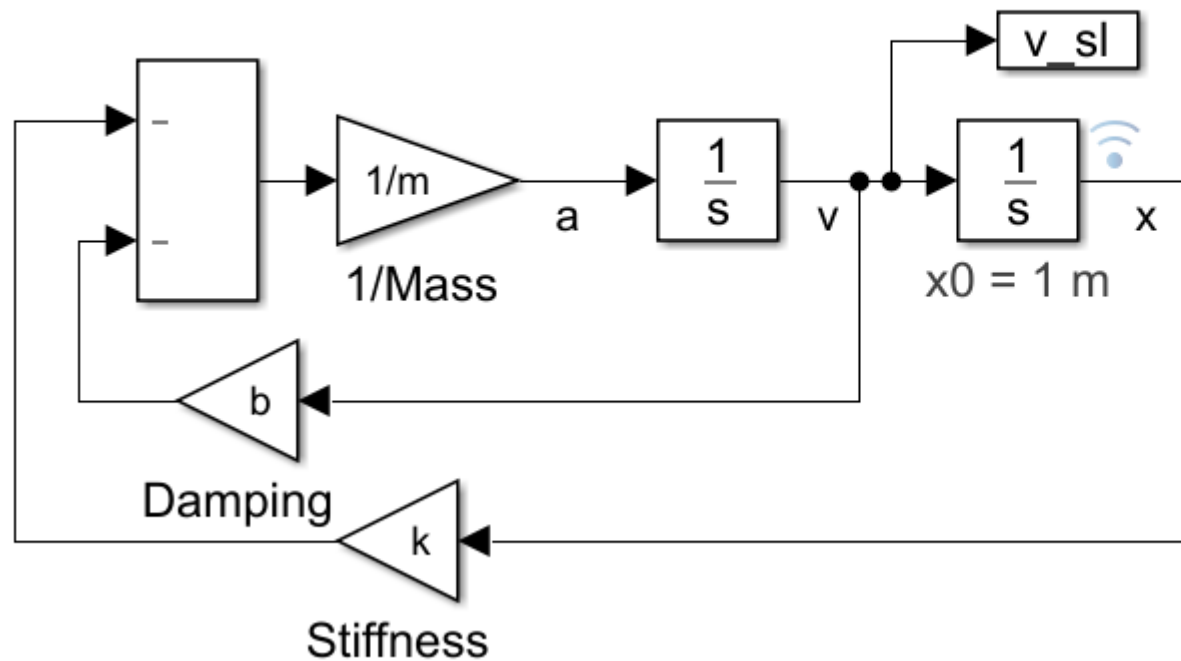
Underdamped $0 < \zeta < 1$ Complex roots: $s_{1,2} = \lambda \pm \mu i$

No damping $\zeta = 0$ Imaginary roots: $s_{1,2} = \pm \mu i$



Simulation Demo

Simulink Model



Simscape Model

