



ZJU-UIUC Institute

Zhejiang University / University of Illinois at Urbana-Champaign Institute



ECE 470: Introduction to Robotics

Lecture 10

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Dynamics

ECE 470 Introduction to Robotics

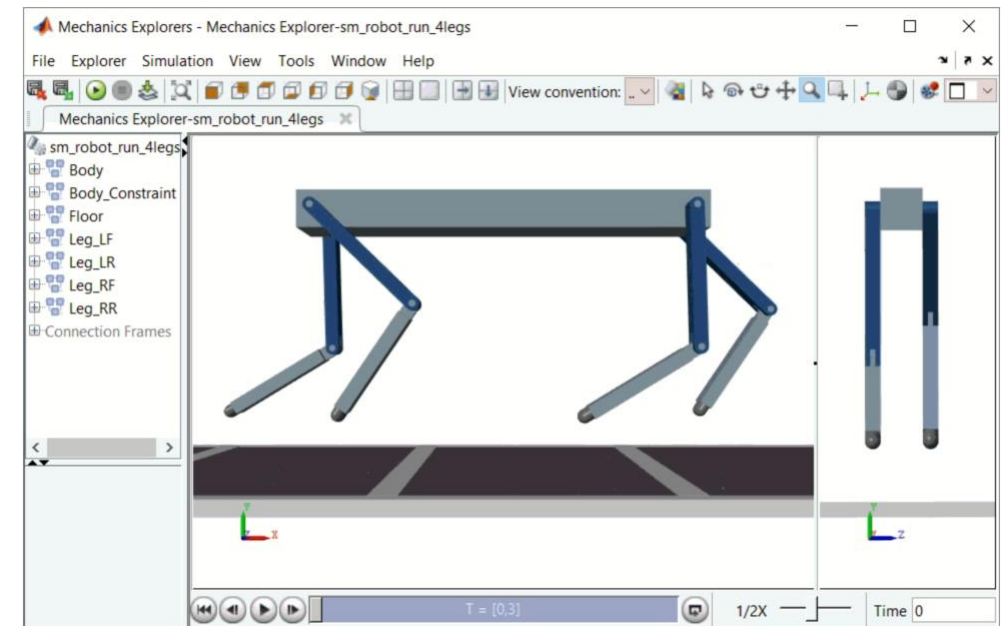
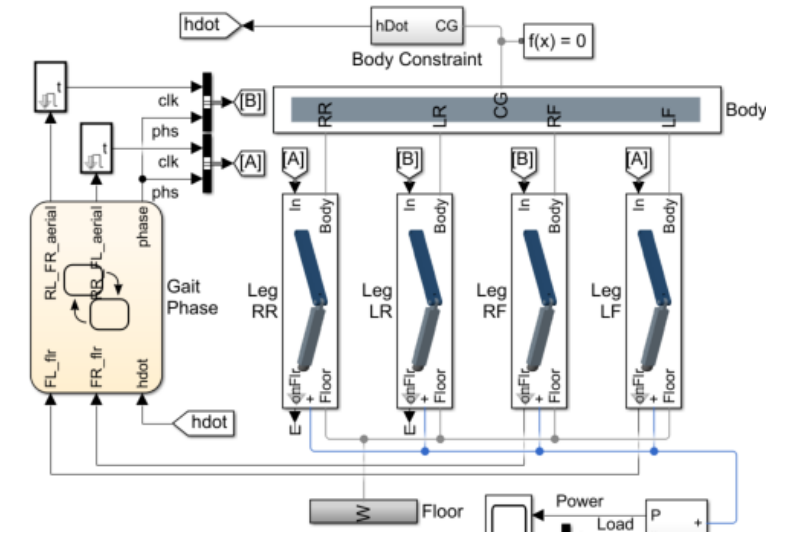
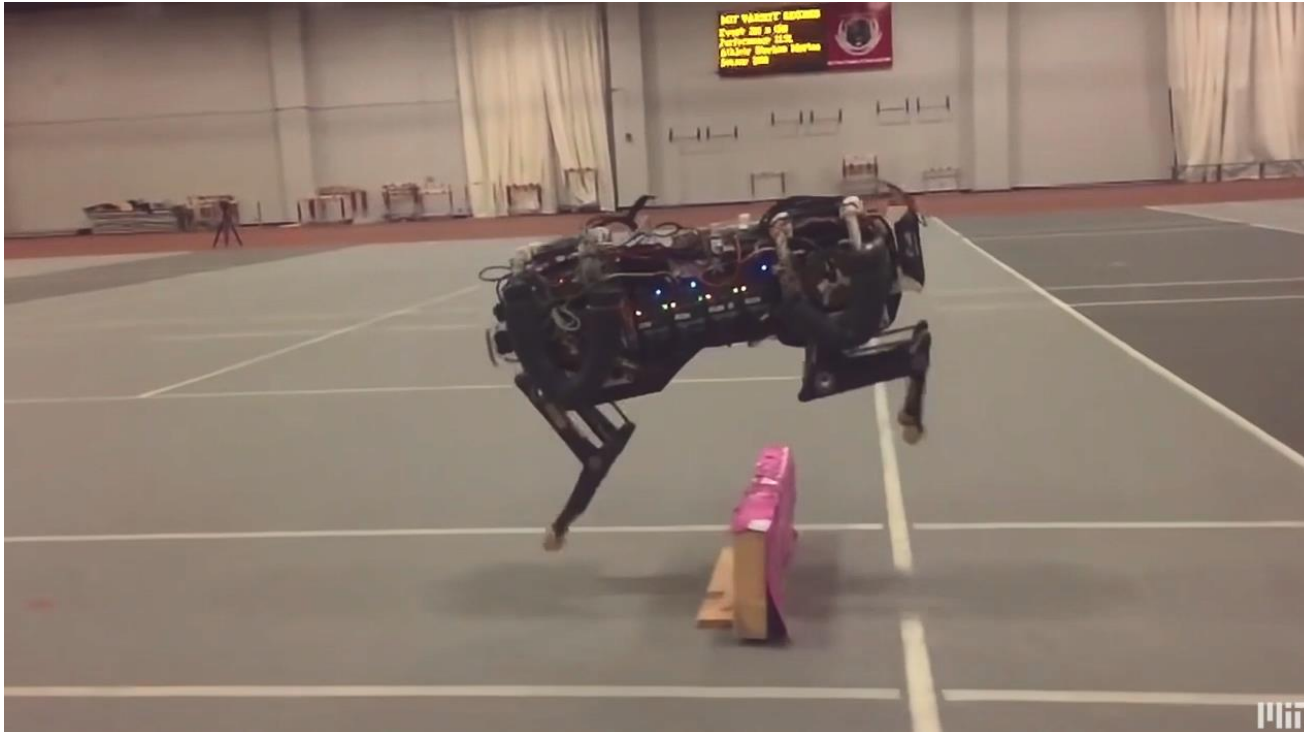
Syllabus and Schedule

• Lecture

O.	Overview	
	• Science & Engineering in Robotics	
I.	Spatial Representation & Transformation	Fundamentals
	• Coordinate Systems; Pose Representations; Homogeneous Transformations	Week 1-4
II.	Kinematics	
	• Multi-body frame assignment; D-H Convention; Joint-space; Work-space; Forward/Inverse Kinematics	Revision/ Quiz on Week 5
III.	Velocity Kinematics and Static Forces	
	• Translational/Rotational Velocity; Joint torque; Generalized Force Coordinates; Jacobian; Singularity	
IV.	Dynamics	Essentials
	• Lagrangian Formulation; Newton-Euler Equations of Motion	
V.	Control	Week 6-9
	• Independent Joint/Feedforward/Inverse Dynamics Controls; Controller Architectures	
VI.	Planning	Revision/ Quiz on Week 10
	• Joint-based Motion Planning; Cartesian-based Path Planning	
VII.	Robot Vision (and Perception)	Applied
	• Image Formation; Image Processing; Visual Tracking & Pose Estimation; Vision-based Control & Image-guided robotics	Week 11-13
		Revision/Reading Wk/ Exam on Week 14-16

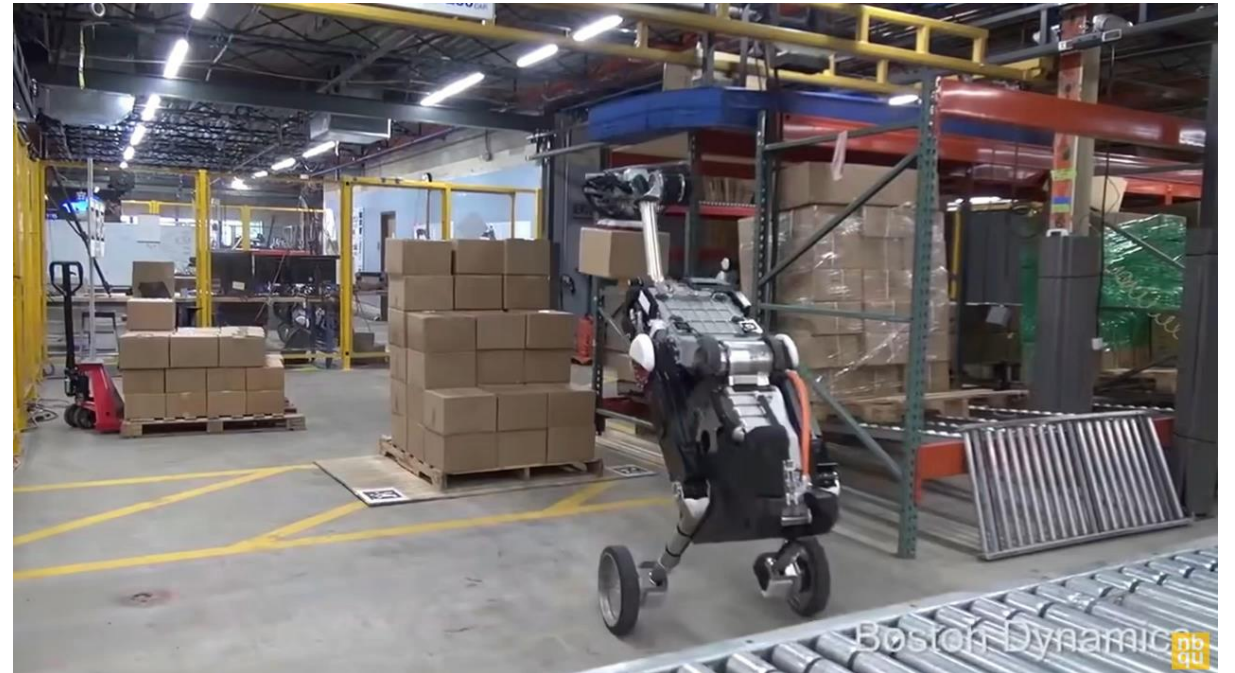
Robot Dynamics

- Example: Quadrupedal Robot



Importance of Simulation

- Why do we need more simulation before real test?

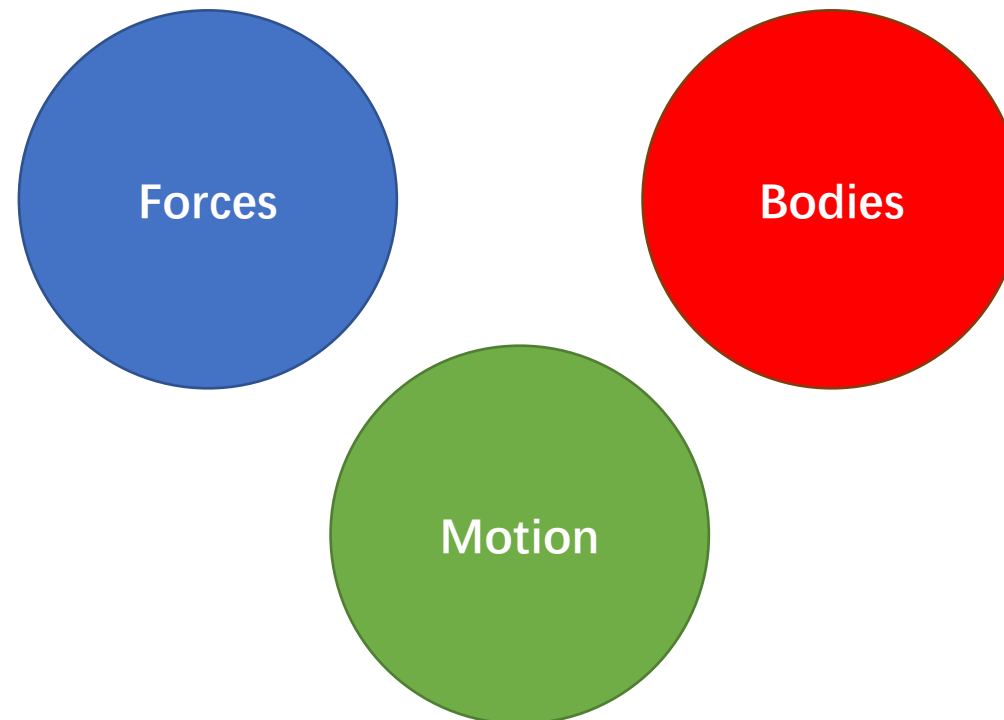


Robot Mechanics

- **Kinematics:** The science of motion without regards to the forces that cause it
 - Pose of the manipulator in static situations
 - Analyze (linear and angular) motion of bodies (/linkages)
- **Statics:** Bodies in equilibrium and force (/moment) relationship
- **Dynamics:** Concern with the forces (/torque) on bodies that cause motion
 - In ECE 470, we are interested in relating forces (/torque) and motion
 - i.e. Dynamic Equation

Robot Mechanics: Dynamics

- **Dynamics:** Concern with the forces (/torque) on bodies that cause motion



Robot Mechanics: Dynamics

- **Dynamics:** Concern with the forces (/torque) on bodies that cause motion

Dynamic equation:

- $\tau = M(\Theta)\ddot{\Theta} + V(\Theta, \dot{\Theta}) + G(\Theta)$
- $M(\Theta)$ is $n \times n$ mass matrix of the manipulator
- $V(\Theta, \dot{\Theta})$ is an $n \times 1$ vector of centrifugal and Coriolis terms
- $G(\Theta)$ is an $n \times 1$ vector of gravity terms

Cartesian Space: $\mathcal{F} = M_x(\Theta)\ddot{\chi} + V_x(\Theta, \dot{\Theta}) + G_x(\Theta),$

Formulating Dynamic Equations

Method (1) Newton-Euler: “Force balance”

Method (2) Lagrangian: Energy-based approach



Acceleration of Rigid Bodies

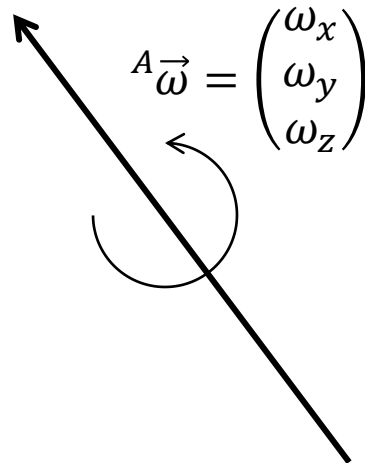
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In deriving velocity expression.....

$$\vec{P}_1 = \vec{P}_{B,ORG} + x \hat{i}_B + y \hat{j}_B + z \hat{k}_B$$

- Differentiating with respecting to time,

$$\vec{V}_1 = \vec{V}_{B,ORG} + \dot{x} \hat{i}_B + \dot{y} \hat{j}_B + \dot{z} \hat{k}_B + \underbrace{x \dot{\hat{i}}_B + y \dot{\hat{j}}_B + z \dot{\hat{k}}_B}_{\vec{\omega} \times (x \hat{i}_B + y \hat{j}_B + z \hat{k}_B)}$$



$$= \begin{pmatrix} 0 & -\omega_z & \omega_y \\ \omega_z & 0 & -\omega_x \\ -\omega_y & \omega_x & 0 \end{pmatrix} \begin{pmatrix} x \\ y \\ z \end{pmatrix}$$

Skew-symmetric matrices

Similarly for acceleration

$$\vec{V}_1 = \vec{V}_{B,ORG} + \dot{x} \hat{i}_B + \dot{y} \hat{j}_B + \dot{z} \hat{k}_B + \vec{\omega} \times \vec{P}_{1/B}$$

Differentiate w.r.t. time

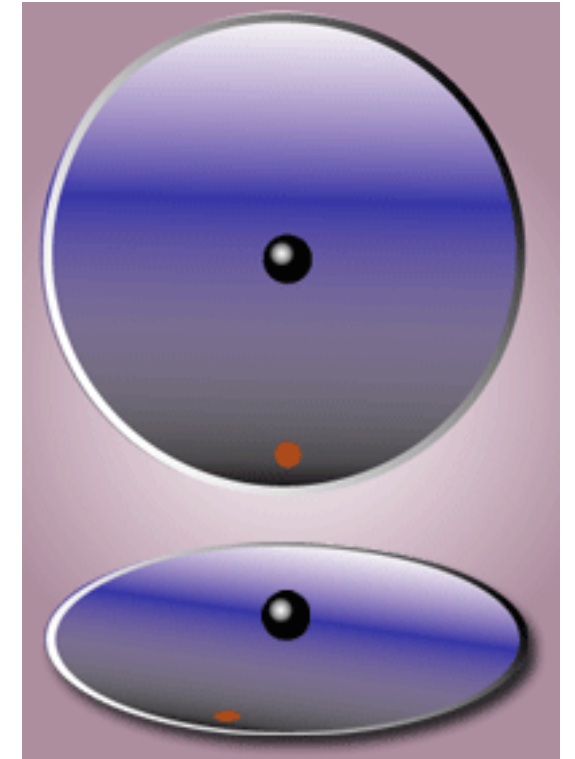
$$\begin{aligned} \dot{\vec{V}}_1 = \dot{\vec{V}}_{B,ORG} + \ddot{x} \hat{i}_B + \ddot{y} \hat{j}_B + \ddot{z} \hat{k}_B + \vec{\omega} \times \vec{V}_{1/B} \\ + \vec{\omega} \times (\vec{V}_{1/B} + \vec{\omega} \times \vec{P}_{1/B}) + \dot{\vec{\omega}} \times \vec{P}_{1/B} \end{aligned}$$

$$\begin{aligned} \dot{\vec{V}}_1 = \dot{\vec{V}}_{B,ORG} + \ddot{x} \hat{i}_B + \ddot{y} \hat{j}_B + \ddot{z} \hat{k}_B \\ + 2\vec{\omega} \times \vec{V}_{1/B} + \vec{\omega} \times \vec{\omega} \times \vec{P}_{1/B} + \dot{\vec{\omega}} \times \vec{P}_{1/B} \end{aligned}$$

coriolis acceleration

centrifugal acceleration

tangential acceleration



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In Velocity “Propagation” from link to link

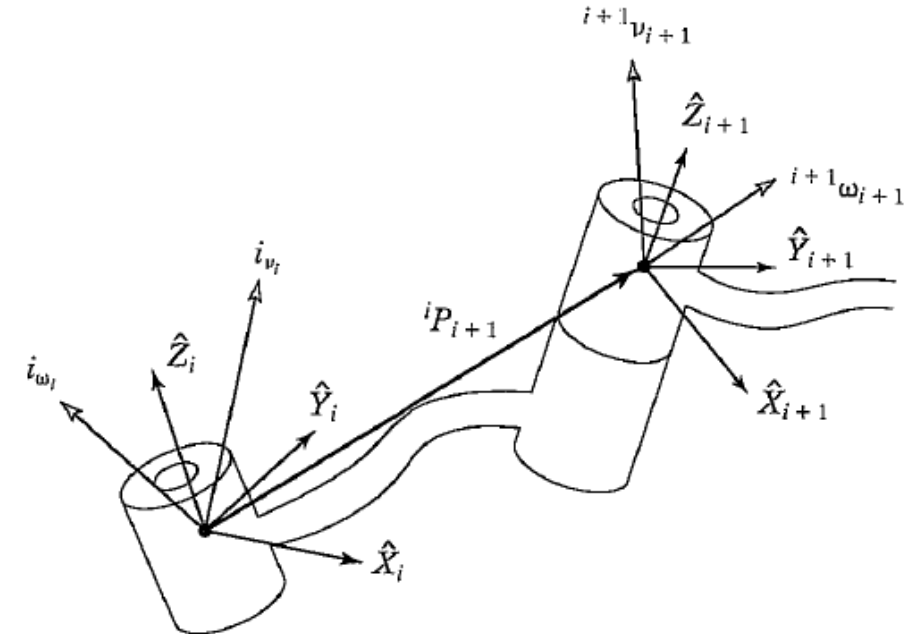
- Rotational velocities can be added when both ω vectors are written with respect to the same frame

$${}^i\omega_{i+1}^0 = {}^i\omega_i^0 + {}^{i+1}_iR \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

$${}^{i+1}\omega_{i+1}^0 = {}^{i+1}_iR {}^i\omega_i^0 + \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

* \hat{Z} in the direction of joint

Notation: In consideration of robot links, frame {0} is used as the reference frame. Meaning to say, ${}^{i+1}\omega_{i+1}$ is the absolute angular velocity of {i+1} expressed in frame {i+1}



In Velocity “Propagation” from link to link

- Linear velocities

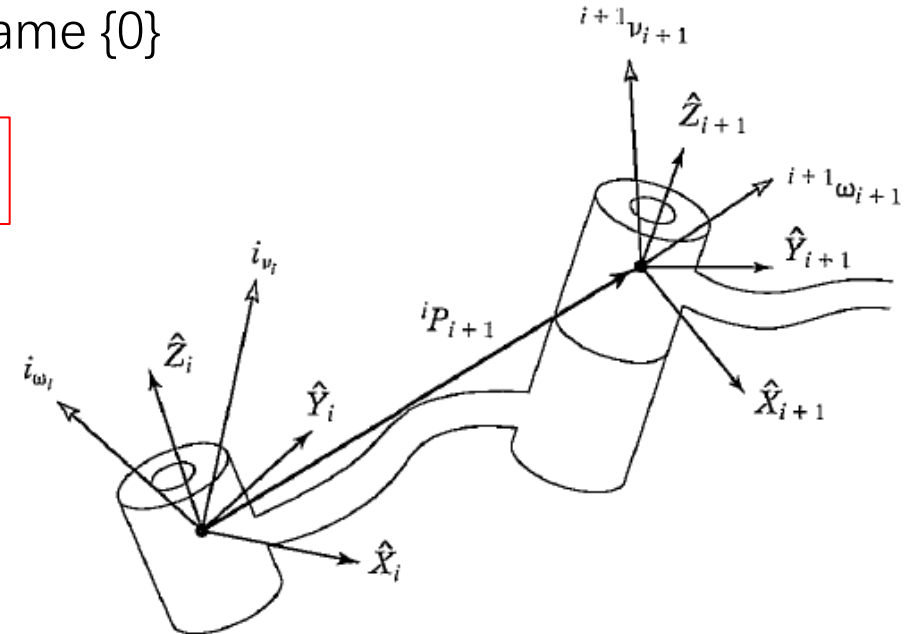
$${}^i v^0_{i+1} = {}^i v^0_i + {}^i \omega^0_i \times {}^i P_{i+1}$$

Differentiate w.r.t to frame {0}

$${}^{i+1} v^0_{i+1} = {}^{i+1}_i R \left({}^i v^0_i + {}^i \omega^0_i \times {}^i P_{i+1} \right)$$

* \hat{Z} in the direction of joint

Notation: In consideration of robot links, frame {0} is used as the reference frame. Meaning to say, ${}^{i+1} v_{i+1}$ is the absolute velocity of {i+1} origin expressed in frame {i+1}



Similarly in Acceleration for “Propagation” from link to link

$${}^0\omega_{i+1} = {}^0\omega_i + {}_{i+1}^0R \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

Differentiate wrt to time

$$\begin{aligned} {}^0\dot{\omega}_{i+1} &= {}^0\dot{\omega}_i + {}_{i+1}^0\dot{R} \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + {}_{i+1}^0R \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} \\ &= {}^0\dot{\omega}_i + {}_{i+1}^0\dot{R} {}_{i+1}^0R^T {}_{i+1}^0R \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + {}_{i+1}^0R \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} \\ &= {}^0\dot{\omega}_i + {}^0\Omega_i {}_{i+1}^0R \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + {}_{i+1}^0R \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} \\ &= {}^0\dot{\omega}_i + {}^0\omega_i \times {}_{i+1}^0R \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + {}_{i+1}^0R \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} \end{aligned}$$

$${}^{i+1}\dot{\omega}_{i+1}^0 = {}^{i+1}R {}^i\dot{\omega}_i + {}^{i+1}R {}^i\omega_i \times \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

- For prismatic joint, ${}^{i+1}\dot{\omega}_{i+1}^0 = {}^{i+1}R {}^i\dot{\omega}_i^0$

Since $\dot{\vec{V}}_1 = \dot{\vec{V}}_{B,ORG} + \ddot{x} \hat{i}_B + \ddot{y} \hat{j}_B + \ddot{z} \hat{k}_B + 2\vec{\omega} \times \vec{V}_{1/B} + \vec{\omega} \times \vec{\omega} \times \vec{P}_{1/B} + \vec{\omega} \times \vec{P}_{1/B}$

$${}^{i+1}\dot{v}_{i+1}^0 = {}^{i+1}R \left({}^i\dot{v}_i^0 + 0 + 0 + {}^i\omega_i^0 \times {}^i\omega_i^0 \times {}^iP_{i+1} + {}^i\dot{\omega}_i^0 \times {}^iP_{i+1} \right)$$

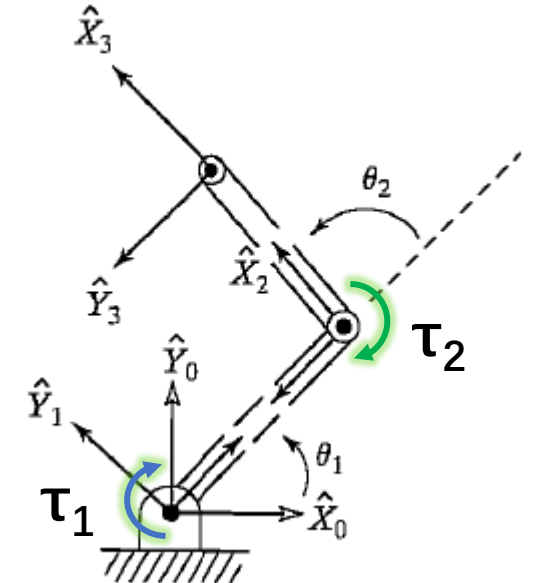
Q5.1 Example of acceleration

- Given the following 2-link planar manipulator in Q3.4, determine for each link the a) absolute angular acceleration, and b) joint absolute linear acceleration. Express the answer in their own frame.

$$\bullet \quad {}^0_1T = \begin{bmatrix} c\theta_1 & -s\theta_1 & 0 & 0 \\ s\theta_1 & c\theta_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad {}^1_2T = \begin{bmatrix} c\theta_2 & -s\theta_2 & 0 & l_1 \\ s\theta_2 & c\theta_2 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad {}^2_3T = \begin{bmatrix} 1 & 0 & 0 & l_2 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

- Assume acceleration due to gravity to be g
 - i.e.* ${}^0\dot{v}_0 = g\hat{Y}_0$

$${}^0\omega_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0v_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0\dot{\omega}_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0\dot{v}_0 = \begin{bmatrix} 0 \\ g \\ 0 \end{bmatrix}$$



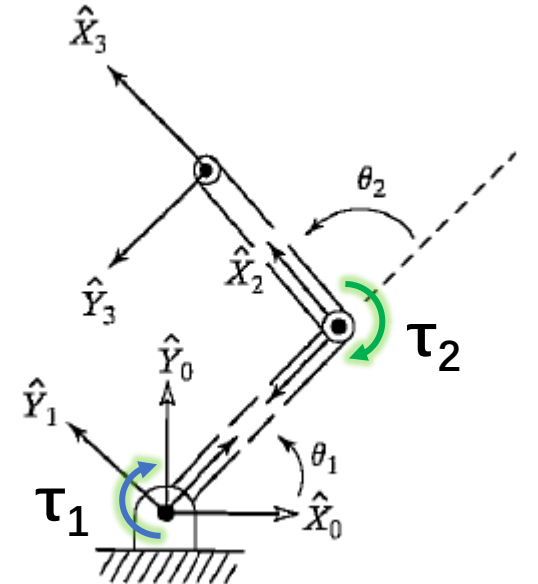
Q5.1 Example of acceleration

Assume ${}^0\dot{v}_0 = g \hat{Y}_0$

$${}^0_1R = \begin{bmatrix} c_1 & -s_1 & 0 \\ s_1 & c_1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$${}^1_2R = \begin{bmatrix} c_2 & -s_2 & 0 \\ s_2 & c_2 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$${}^0\omega_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0v_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0\dot{\omega}_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0\dot{v}_0 = \begin{bmatrix} 0 \\ g \\ 0 \end{bmatrix}$$



Q5.1 Example of acceleration

$${}^{i+1}\omega^0_{i+1} = {}^{i+1}_i R \ {}^i\omega^0_i + \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

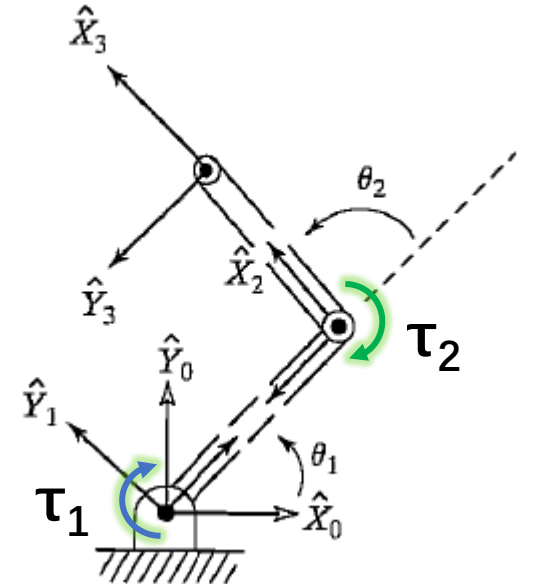
$${}^{i+1}\dot{\omega}^0_{i+1} = {}^{i+1}_i R \ {}^i\dot{\omega}_i + {}^{i+1}_i R \ {}^i\omega_i \times \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

$${}^{i+1}v^0_{i+1} = {}^{i+1}_i R \left({}^i v^0_i + {}^i\omega^0_i \times {}^i P_{i+1} \right)$$

$${}^{i+1}\dot{v}^0_{i+1} = {}^{i+1}_i R \left({}^i\dot{v}^0_i + {}^i\Omega_i \ {}^i\Omega_i \ {}^i P_{i+1} + {}^i\dot{\Omega}_i \ {}^i P_{i+1} \right)$$

• $i=0$

$${}^1\omega_1 = \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_1 \end{bmatrix}, \quad {}^1\dot{\omega}_1 = \begin{bmatrix} 0 \\ 0 \\ \ddot{\theta}_1 \end{bmatrix}, \quad {}^1\dot{v}_1 = \begin{bmatrix} c_1 & s_1 & 0 \\ -s_1 & c_1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ g \\ 0 \end{bmatrix} = \begin{bmatrix} g s_1 \\ g c_1 \\ 0 \end{bmatrix}$$



Q5.1 Example of acceleration

$${}^{i+1}\omega_i^0 = {}^{i+1}{}_iR \ {}^i\omega_i^0 + \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

$${}^{i+1}\dot{\omega}_i^0 = {}^{i+1}{}_iR \ {}^i\dot{\omega}_i^0 + {}^{i+1}{}_iR \ {}^i\omega_i^0 \times \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

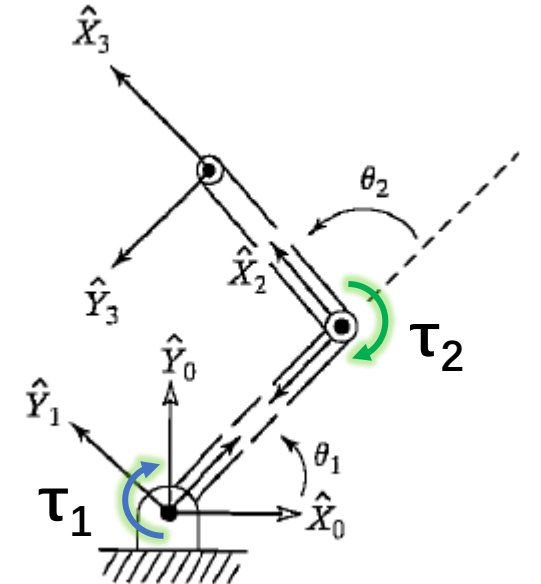
$${}^{i+1}v_i^0 = {}^{i+1}{}_iR \left({}^iv_i^0 + {}^i\omega_i^0 \times {}^iP_{i+1} \right)$$

$${}^{i+1}\dot{v}_i^0 = {}^{i+1}{}_iR \left({}^i\dot{v}_i^0 + {}^i\Omega_i \ {}^i\Omega_i \ {}^iP_{i+1} + {}^i\dot{\Omega}_i \ {}^iP_{i+1} \right)$$

• $i=1$

$${}^2\omega_2 = \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_1 + \dot{\theta}_2 \end{bmatrix}, \quad {}^2\dot{\omega}_2 = \begin{bmatrix} 0 \\ 0 \\ \ddot{\theta}_1 + \ddot{\theta}_2 \end{bmatrix},$$

$${}^2\dot{v}_2 = \begin{bmatrix} c_2 & s_2 & 0 \\ -s_2 & c_2 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} -l_1\dot{\theta}_1^2 + g s_1 \\ l_1\ddot{\theta}_1 + g c_1 \\ 0 \end{bmatrix} = \begin{bmatrix} l_1\ddot{\theta}_1^2 s_2 - l_1\dot{\theta}_1^2 c_2 + g s_{12} \\ l_1\ddot{\theta}_1^2 c_2 + l_1\dot{\theta}_1^2 s_2 + g c_{12} \\ 0 \end{bmatrix}$$



Newton-Euler Formulation

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