



## ECE 470: Introduction to Robotics

### Lecture 12

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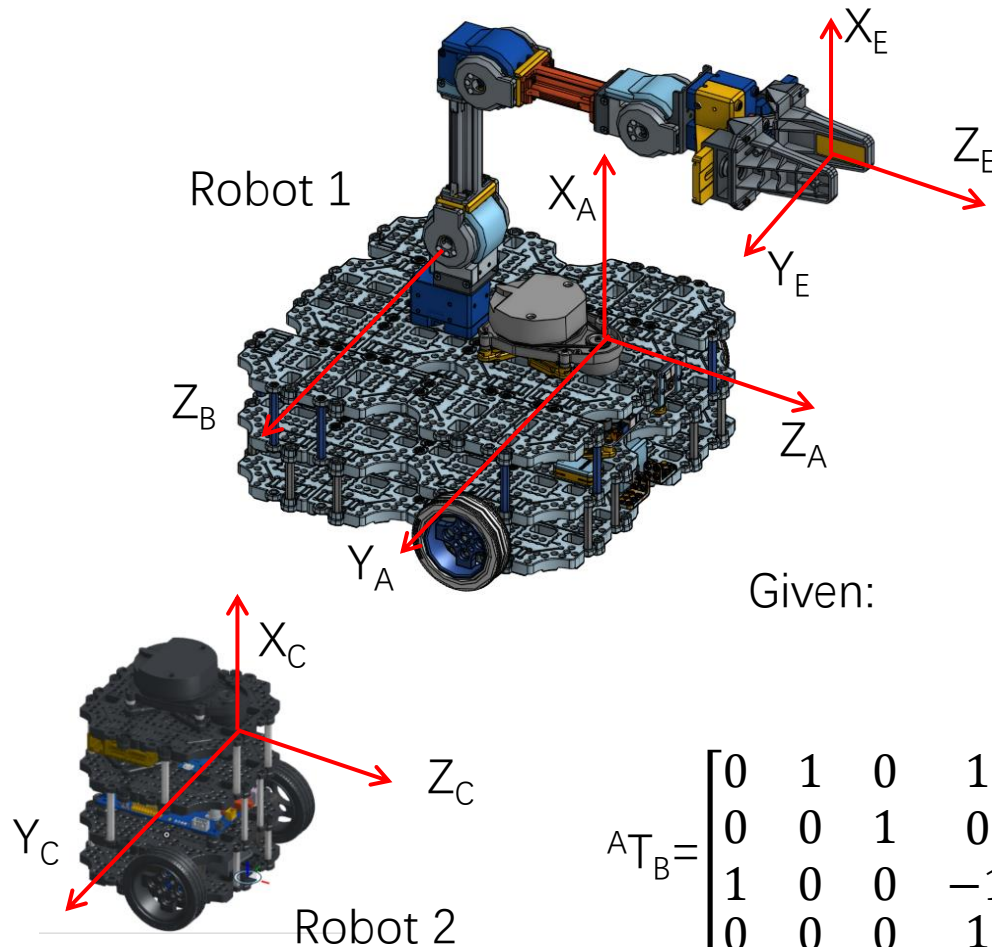
[liangjingyang@intl.zju.edu.cn](mailto:liangjingyang@intl.zju.edu.cn)

Wechat ID: Liangjing\_Yang

# Lecture Outline

- Review Quiz
- Recap Structure of Dynamic Equation/Equation of Motion (EOM); Acceleration of Rigid Body
- Newton-Euler Formulation

# Review Quiz I



Given:

$${}^A T_B = \begin{bmatrix} 0 & 1 & 0 & 1 \\ 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & -1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^B T_E = \begin{bmatrix} 0 & 0 & 1 & 2 \\ 1 & 0 & 0 & 1 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^A T_C = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

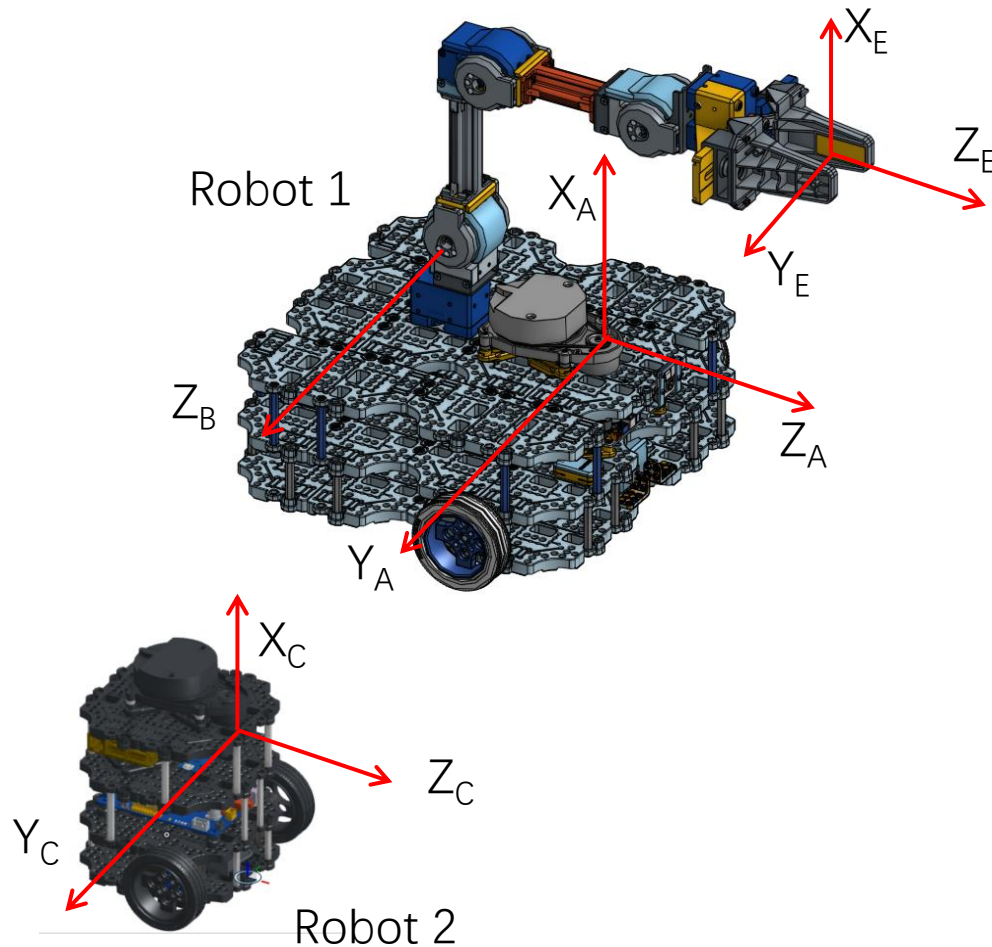
Robot 1 and Robot 2 went through some transformations in the following order

1. Robot 2 moves around Robot 1 such that  $\{C\}$  rotates  $90^\circ$  about axis  $X_A$  to become  $\{C1\}$ .
2. Robot 2 rotates about itself such that  $\{C1\}$  rotates  $90^\circ$  about axis  $X_{c1}$  to become  $\{C2\}$ .
3. Robot 1 moves forward such that  $\{A\}$ ,  $\{B\}$  and  $\{E\}$  translate along the vector  ${}^A(0, 0, 2)'$  to become  $\{A3\}$ ,  $\{B3\}$  and  $\{E3\}$
4. The arm on Robot 1 moves such that  $\{E3\}$  rotates  $90^\circ$  about axis  $Z_B$  to become  $\{E4\}$

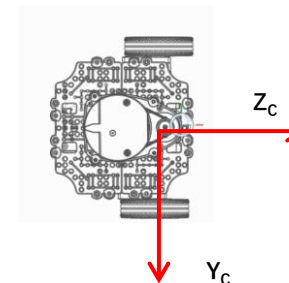
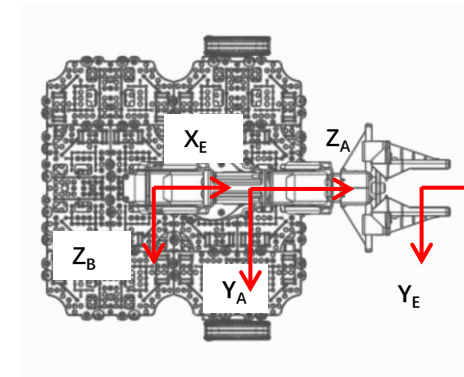
Obtain the expression for

- i.  ${}^A T_{C1}$  (3 Points)
- ii.  ${}^A T_{C2}$  (3 Points)
- iii.  ${}^{A3} T_{C2}$  (3 Points)
- iv.  ${}^{E3} T_{C2}$  (3 Points)
- v.  ${}^{C2} T_{E4}$  (4 Points)

# Review Quiz I



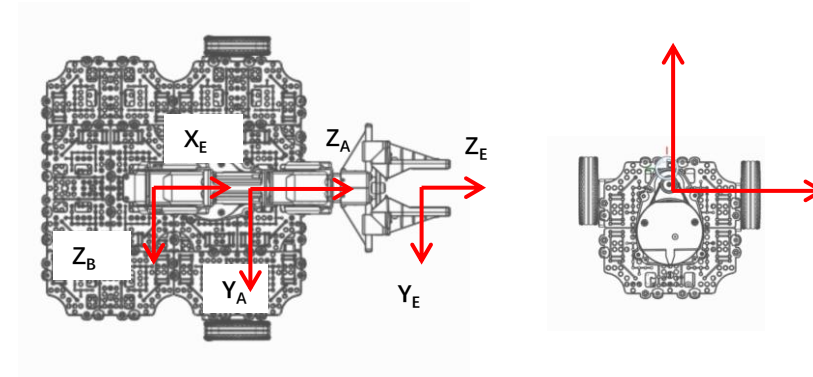
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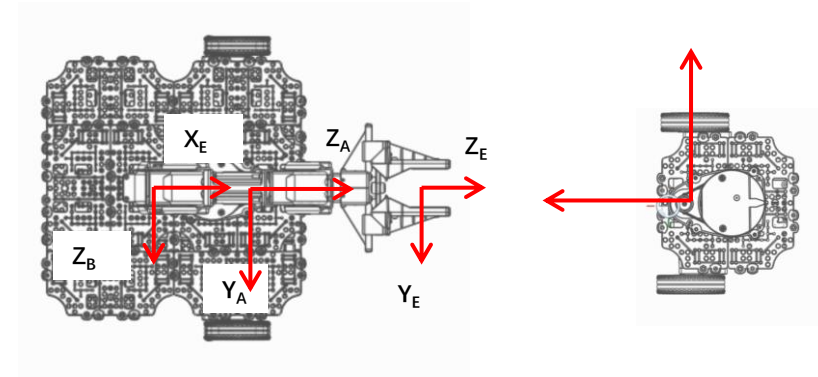
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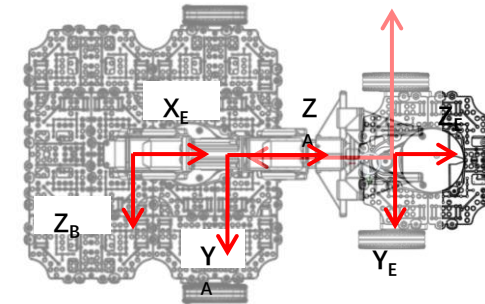
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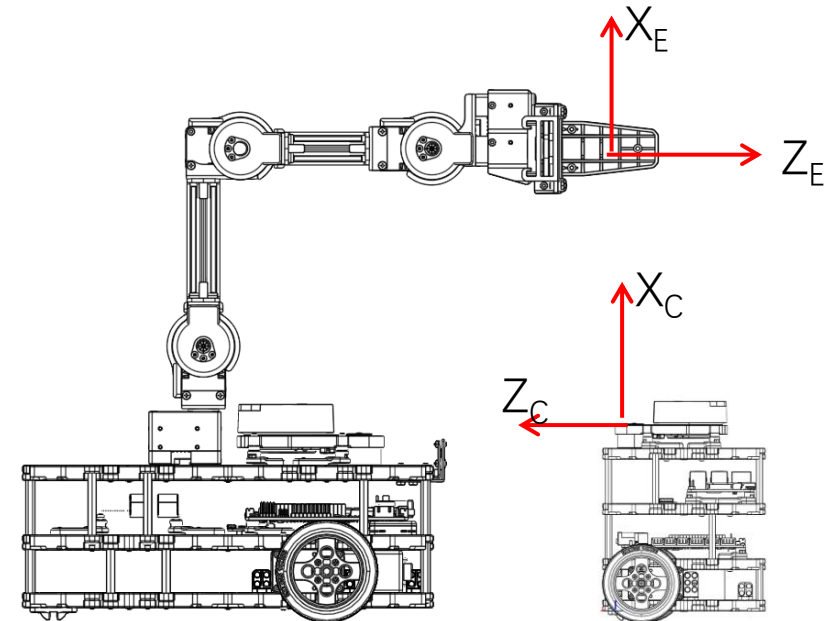
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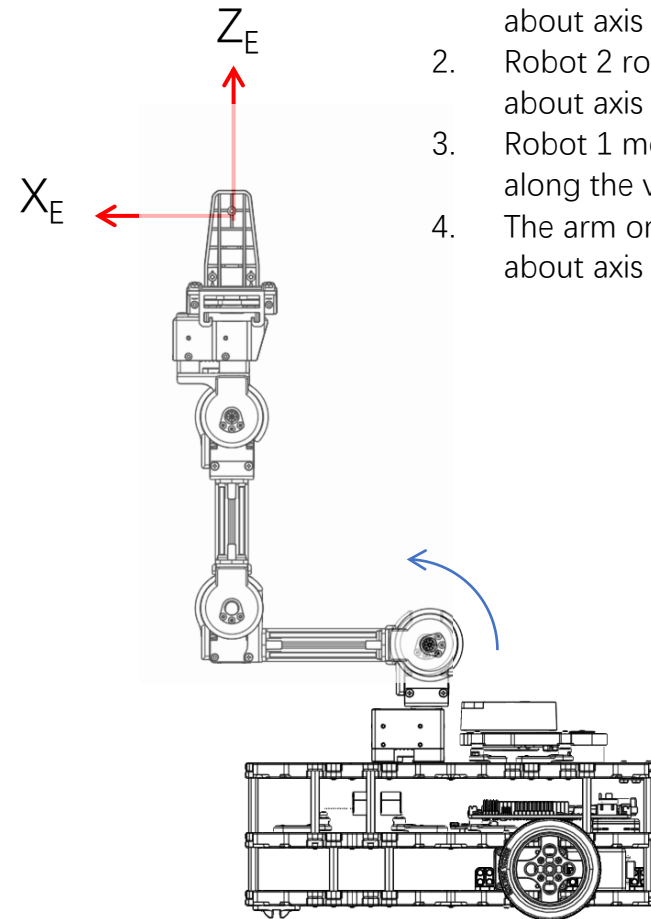
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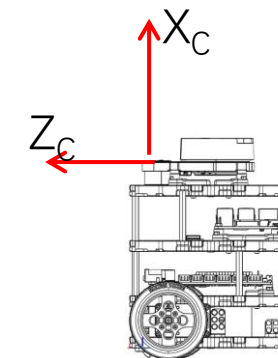


# Review Quiz I



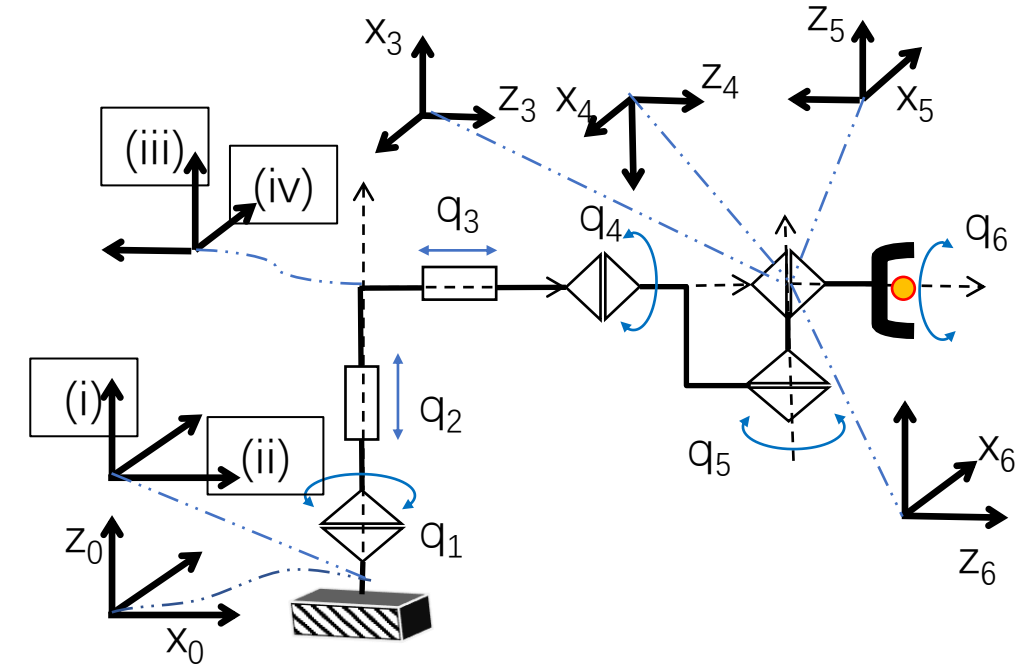
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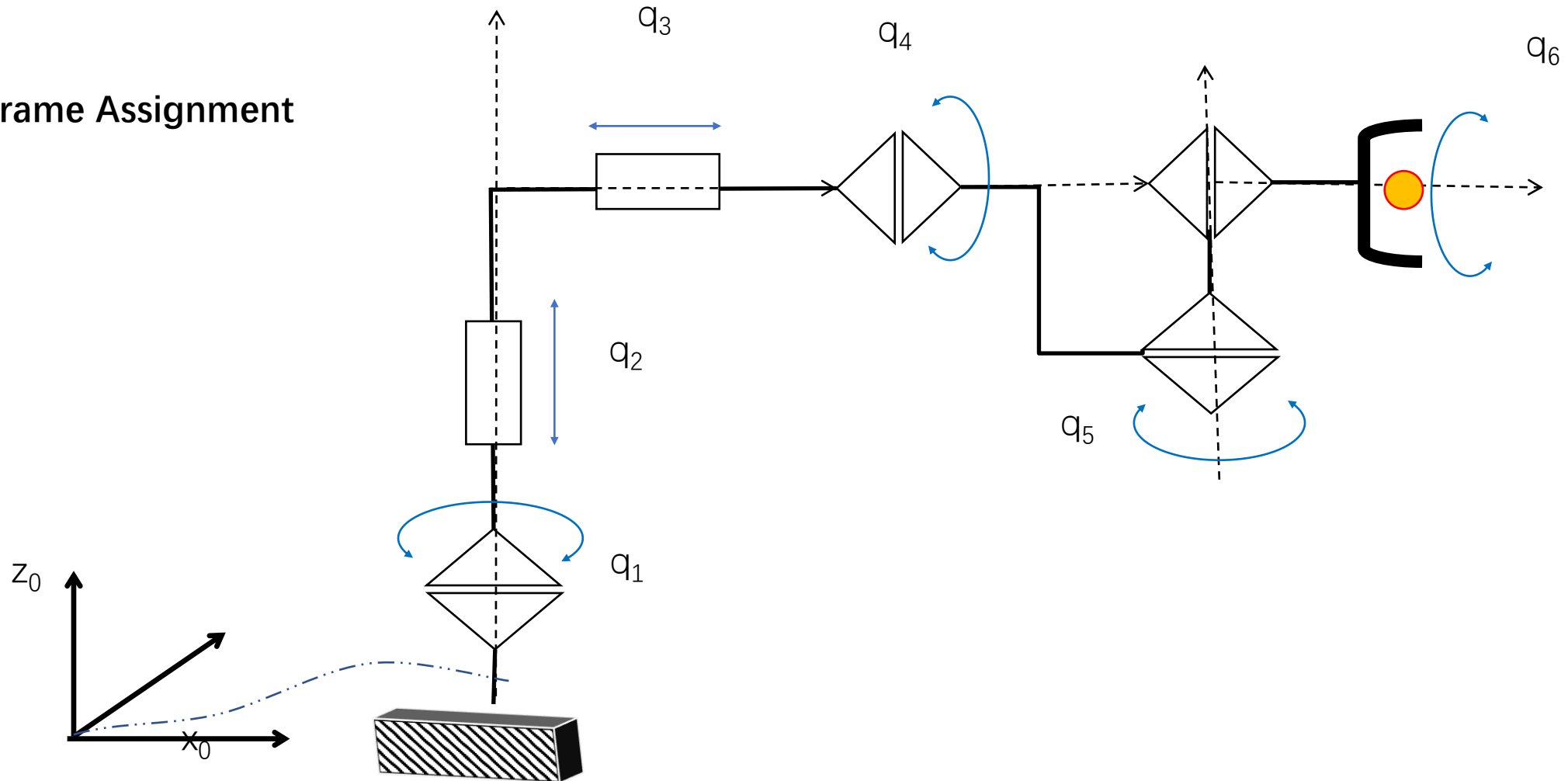
# Review Quiz I

	Link Twist $\alpha_{i-1}$	Link Length $a_{i-1}$	Joint Angle $\theta_i$	Link offset $d_i$
${}^0_1T$	0	0	$q_1=0$	0
${}^1_2T$	0	0	$90^\circ$	$q_2=d_2$
${}^2_3T$	$90^\circ$	0	(v) _____ ?	(vi) _____ ?
${}^3_4T$	(vii) _____ ?	(viii) _____ ?	(ix) _____ ?	0
${}^4_5T$	(x) _____ ?	(xi) _____ ?	$q_5=180^\circ$	(xii) _____ ?
${}^5_6T$	$90^\circ$	0	$q_6=0$	0



# Review Quiz I

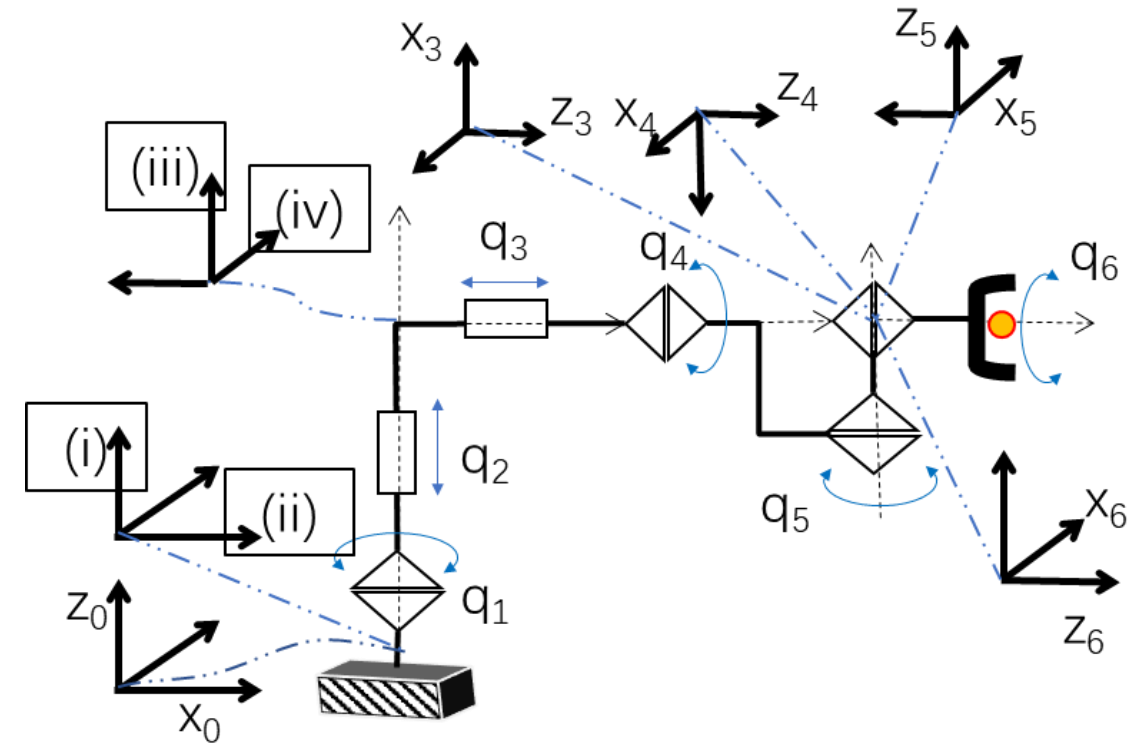
## 1. Frame Assignment



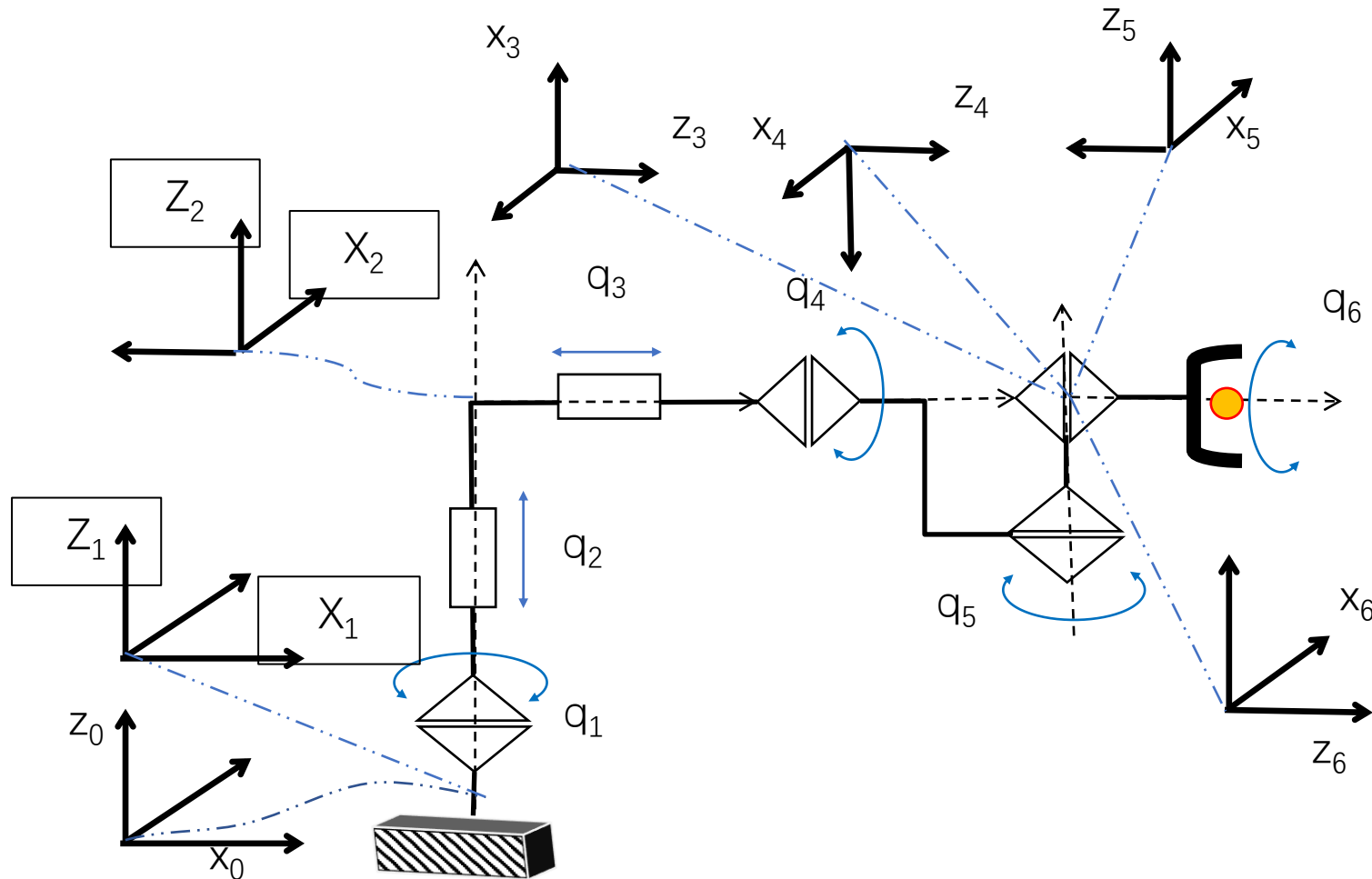
# Review Quiz I

## 2. D-H Table

	Link Twist $\alpha_{i-1}$	Link Length $a_{i-1}$	Joint Angle $\theta_i$	Link offset $d_i$
${}^0T_1$				
${}^1T_2$				
${}^2T_3$				
${}^3T_4$				
${}^4T_5$				
${}^5T_6$				



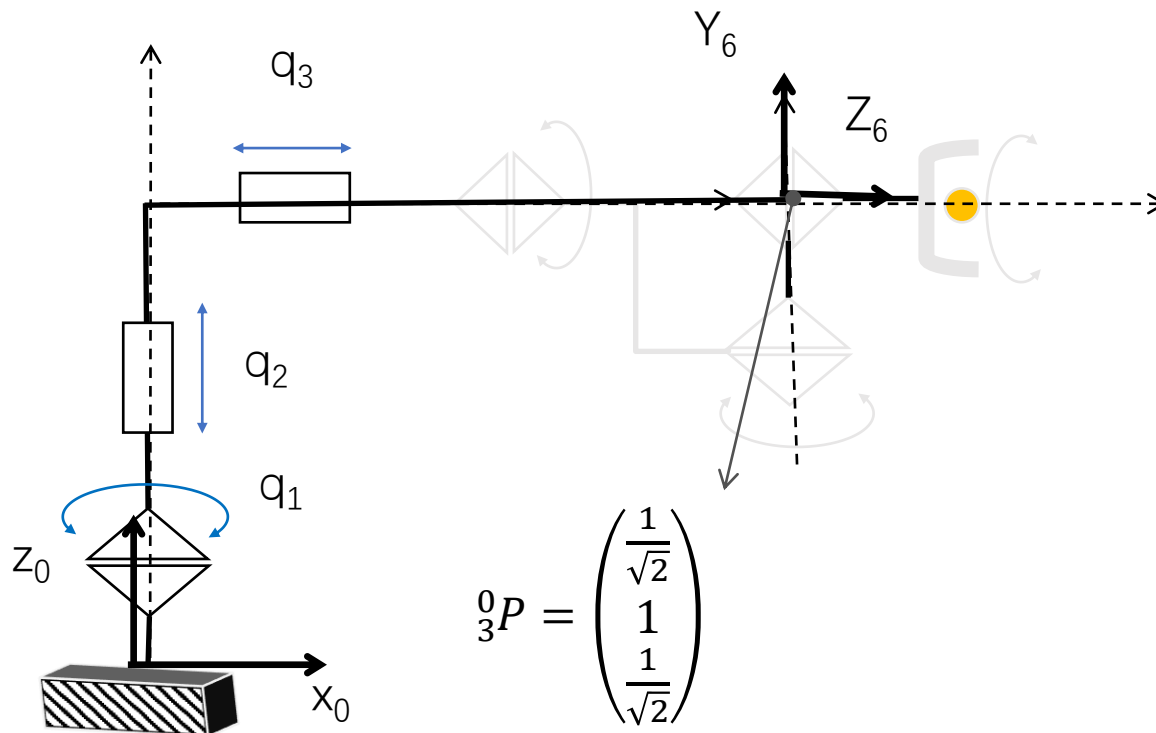
# Review Quiz I



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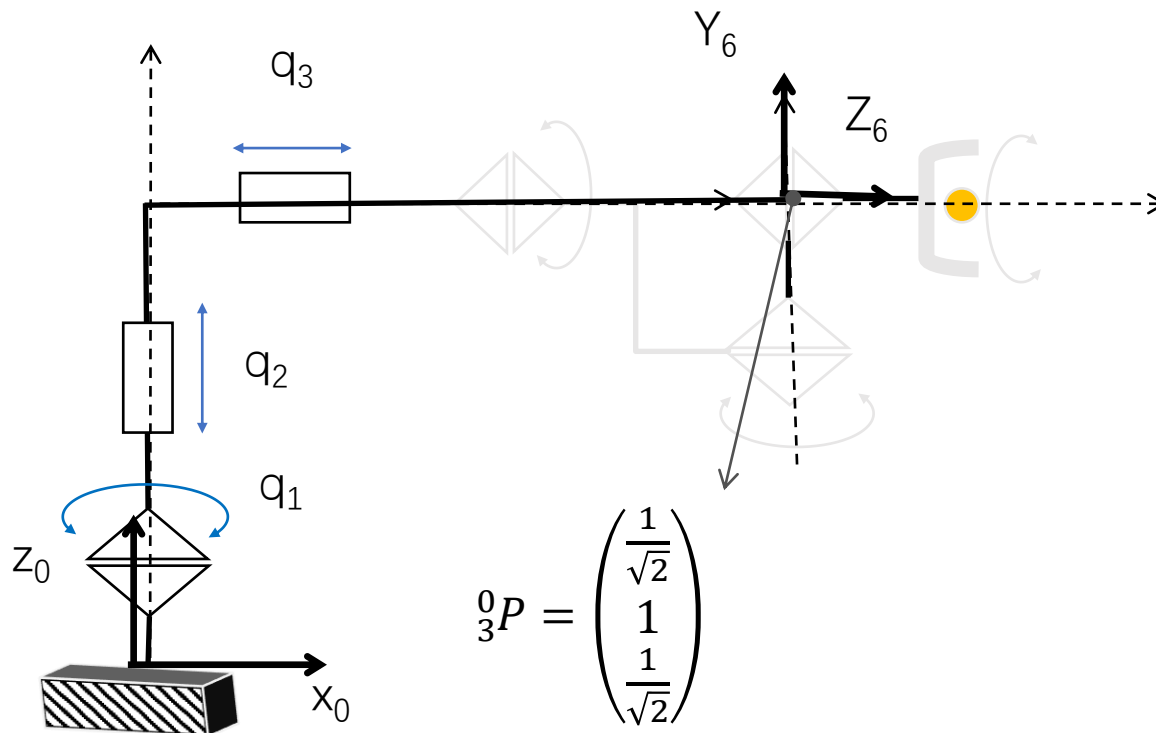
Forward kinematics:

Inverse kinematics:



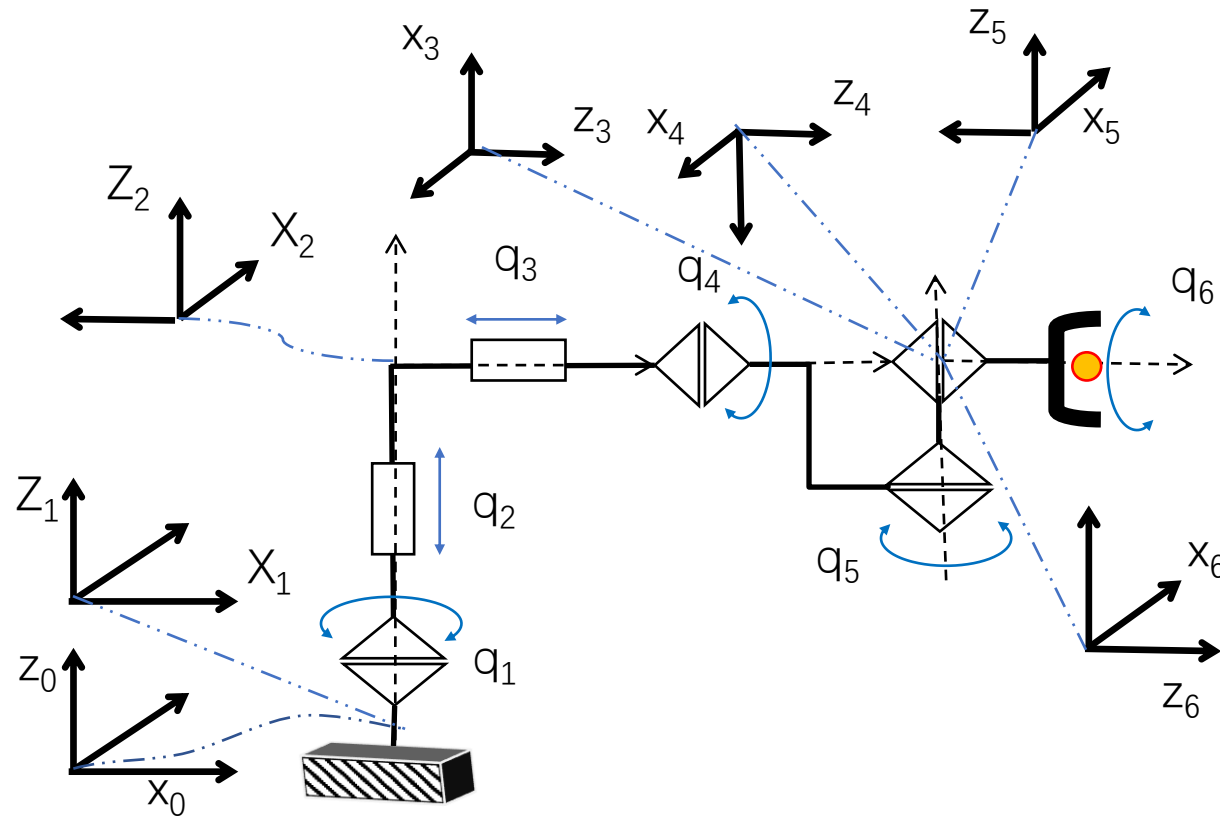
# Review Quiz I

## Workspace Analysis



# Review Quiz I

## Manipulability





# Recap: Acceleration

$$\vec{P}_1 = \vec{P}_{B,ORG} + x \hat{i}_B + y \hat{j}_B + z \hat{k}_B$$

Differentiating with respecting to time,

$$\vec{V}_1 = \vec{V}_{B,ORG} + \dot{x} \hat{i}_B + \dot{y} \hat{j}_B + \dot{z} \hat{k}_B + x \dot{\hat{i}}_B + y \dot{\hat{j}}_B + z \dot{\hat{k}}_B$$

$$\vec{V}_1 = \vec{V}_{B,ORG} + \dot{x} \hat{i}_B + \dot{y} \hat{j}_B + \dot{z} \hat{k}_B + \vec{\omega} \times \vec{P}_{1/B}$$

Differentiate w.r.t. time

$$\begin{aligned} \dot{\vec{V}}_1 = \dot{\vec{V}}_{B,ORG} + \ddot{x} \hat{i}_B + \ddot{y} \hat{j}_B + \ddot{z} \hat{k}_B + \vec{\omega} \times \vec{V}_{1/B} \\ + \vec{\omega} \times (\vec{V}_{1/B} + \vec{\omega} \times \vec{P}_{1/B}) + \dot{\vec{\omega}} \times \vec{P}_{1/B} \end{aligned}$$

$$\begin{aligned} \dot{\vec{V}}_1 = \dot{\vec{V}}_{B,ORG} + \ddot{x} \hat{i}_B + \ddot{y} \hat{j}_B + \ddot{z} \hat{k}_B \\ + 2\vec{\omega} \times \vec{V}_{1/B} + \vec{\omega} \times \vec{\omega} \times \vec{P}_{1/B} + \dot{\vec{\omega}} \times \vec{P}_{1/B} \end{aligned}$$

coriolis acceleration

centrifugal acceleration

tangential acceleration

# Recap: Acceleration for “Propagation” from link to link

$${}^0\omega_{i+1} = {}^0\omega_i + {}_{i+1}^0R \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

Differentiate wrt to time

$$\begin{aligned} {}^0\dot{\omega}_{i+1} &= {}^0\dot{\omega}_i + {}_{i+1}^0\dot{R} \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + {}_{i+1}^0R \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} \\ &= {}^0\dot{\omega}_i + {}_{i+1}^0\dot{R} {}_{i+1}^0R^T {}_{i+1}^0R \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + {}_{i+1}^0R \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} \\ &= {}^0\dot{\omega}_i + {}^0\Omega_i {}_{i+1}^0R \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + {}_{i+1}^0R \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} \\ &= {}^0\dot{\omega}_i + {}^0\omega_i \times {}_{i+1}^0R \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + {}_{i+1}^0R \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} \end{aligned}$$

$${}^{i+1}\dot{\omega}_{i+1}^0 = {}^{i+1}R {}^i\dot{\omega}_i + {}^{i+1}R {}^i\omega_i \times \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

- For prismatic joint,  ${}^{i+1}\dot{\omega}_{i+1}^0 = {}^{i+1}R {}^i\dot{\omega}_i$  0

Since  $\dot{\vec{V}}_1 = \dot{\vec{V}}_{B,ORG} + \ddot{x} \hat{i}_B + \ddot{y} \hat{j}_B + \ddot{z} \hat{k}_B + 2\vec{\omega} \times \vec{V}_{1/B} + \vec{\omega} \times \vec{\omega} \times \vec{P}_{1/B} + \vec{\omega} \times \vec{P}_{1/B}$

$${}^{i+1}\dot{v}_{i+1}^0 = {}^{i+1}R \left( {}^i\dot{v}_i^0 + 0 + 0 + {}^i\omega_i^0 \times {}^i\omega_i^0 \times {}^iP_{i+1} + {}^i\dot{\omega}_i^0 \times {}^iP_{i+1} \right)$$

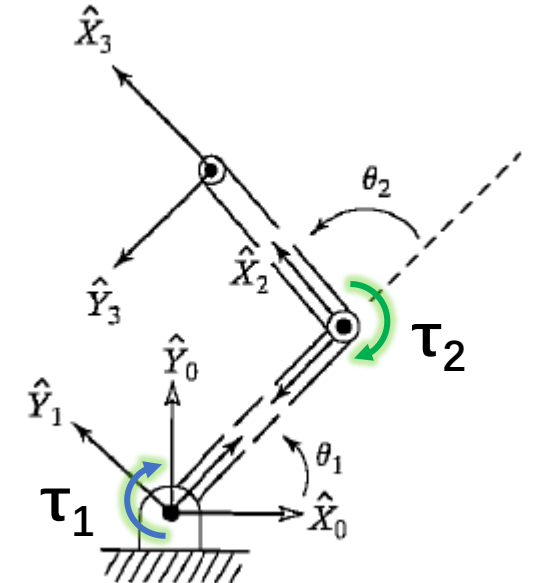
# Q5.1 Example of acceleration

- Given the following 2-link planar manipulator in Q3.4, determine for each link the a) absolute angular acceleration, and b) joint absolute linear acceleration. Express the answer in their own frame.

$$\bullet \quad {}^0_1T = \begin{bmatrix} c\theta_1 & -s\theta_1 & 0 & 0 \\ s\theta_1 & c\theta_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad {}^1_2T = \begin{bmatrix} c\theta_2 & -s\theta_2 & 0 & l_1 \\ s\theta_2 & c\theta_2 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad {}^2_3T = \begin{bmatrix} 1 & 0 & 0 & l_2 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

- Assume acceleration due to gravity to be  $g$ 
  - i.e.*  ${}^0\dot{v}_0 = g\hat{Y}_0$

$${}^0\omega_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0v_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0\dot{\omega}_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0\dot{v}_0 = \begin{bmatrix} 0 \\ g \\ 0 \end{bmatrix}$$



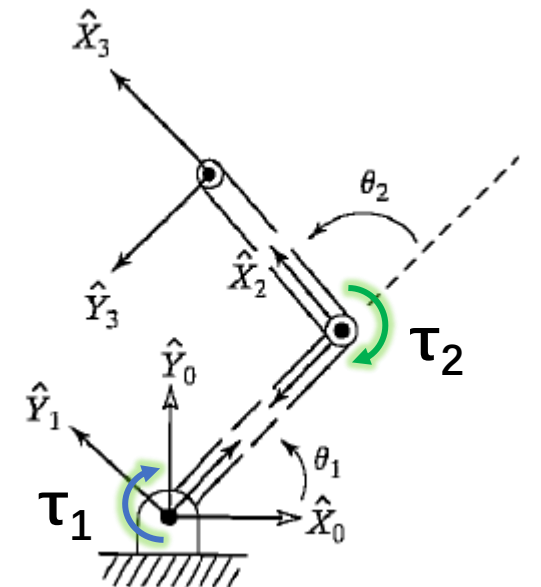
# Q5.1 Example of acceleration

Assume  ${}^0\dot{v}_0 = g \hat{Y}_0$

$${}^0_1R = \begin{bmatrix} c_1 & -s_1 & 0 \\ s_1 & c_1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$${}^1_2R = \begin{bmatrix} c_2 & -s_2 & 0 \\ s_2 & c_2 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$${}^0\omega_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0v_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0\dot{\omega}_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0\dot{v}_0 = \begin{bmatrix} 0 \\ g \\ 0 \end{bmatrix}$$



# Q5.1 Example of acceleration

$${}^{i+1}\omega^0_{i+1} = {}^{i+1}_i R \ {}^i\omega^0_i + \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

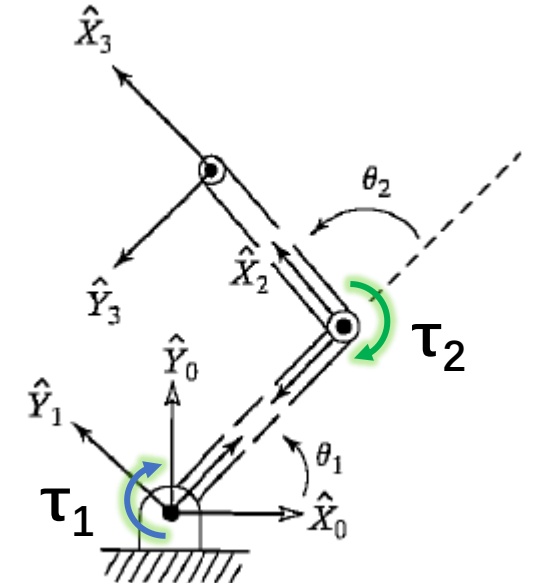
$${}^{i+1}\dot{\omega}^0_{i+1} = {}^{i+1}_i R \ {}^i\dot{\omega}_i + {}^{i+1}_i R \ {}^i\omega_i \times \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

$${}^{i+1}v^0_{i+1} = {}^{i+1}_i R \left( {}^i v^0_i + {}^i\omega^0_i \times {}^i P_{i+1} \right)$$

$${}^{i+1}\dot{v}^0_{i+1} = {}^{i+1}_i R \left( {}^i\dot{v}^0_i + {}^i\Omega_i \ {}^i\Omega_i \ {}^i P_{i+1} + {}^i\dot{\Omega}_i \ {}^i P_{i+1} \right)$$

•  $i=0$

$${}^1\omega_1 = \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_1 \end{bmatrix}, \quad {}^1\dot{\omega}_1 = \begin{bmatrix} 0 \\ 0 \\ \ddot{\theta}_1 \end{bmatrix}, \quad {}^1\dot{v}_1 = \begin{bmatrix} c_1 & s_1 & 0 \\ -s_1 & c_1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ g \\ 0 \end{bmatrix} = \begin{bmatrix} g s_1 \\ g c_1 \\ 0 \end{bmatrix}$$



# Q5.1 Example of acceleration

$${}^{i+1}\omega_i^0 = {}^{i+1}R_i {}^i\omega_i^0 + \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

$${}^{i+1}\dot{\omega}_i^0 = {}^{i+1}R_i {}^i\dot{\omega}_i^0 + {}^{i+1}R_i {}^i\omega_i^0 \times \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

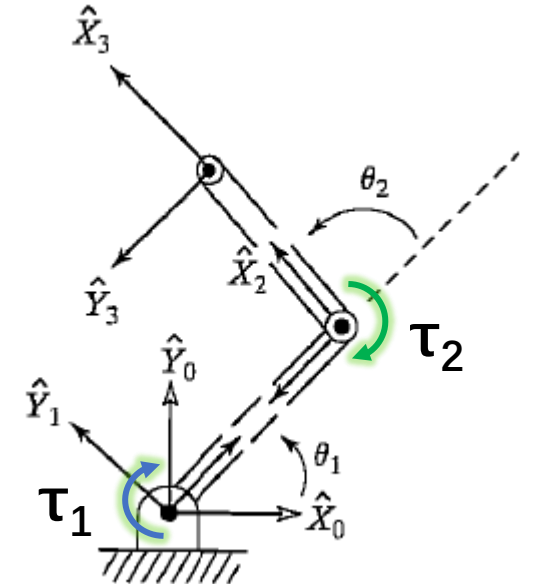
$${}^{i+1}v_i^0 = {}^{i+1}R_i ({}^i v_i^0 + {}^i\omega_i^0 \times {}^i P_{i+1})$$

$${}^{i+1}\dot{v}_i^0 = {}^{i+1}R_i ({}^i\dot{v}_i^0 + {}^i\Omega_i {}^i\Omega_i {}^i P_{i+1} + {}^i\dot{\Omega}_i {}^i P_{i+1})$$

•  $i=1$

$${}^2\omega_2 = \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_1 + \dot{\theta}_2 \end{bmatrix}, \quad {}^2\dot{\omega}_2 = \begin{bmatrix} 0 \\ 0 \\ \ddot{\theta}_1 + \ddot{\theta}_2 \end{bmatrix},$$

$${}^2\dot{v}_2 = \begin{bmatrix} c_2 & s_2 & 0 \\ -s_2 & c_2 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} -l_1 \dot{\theta}_1^2 + g s_1 \\ l_1 \ddot{\theta}_1 + g c_1 \\ 0 \end{bmatrix} = \begin{bmatrix} l_1 \ddot{\theta}_1^2 s_2 - l_1 \dot{\theta}_1^2 c_2 + g s_{12} \\ l_1 \ddot{\theta}_1^2 c_2 + l_1 \dot{\theta}_1^2 s_2 + g c_{12} \\ 0 \end{bmatrix}$$



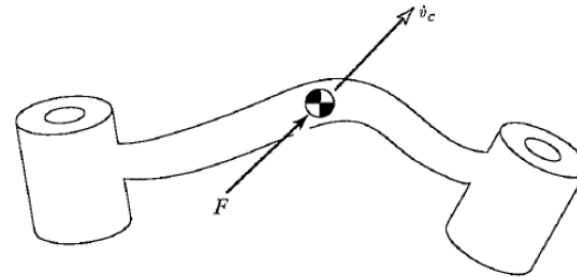
# Newton-Euler Formulation

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# Newton's Law of Motion

Newton's 2<sup>nd</sup> Law

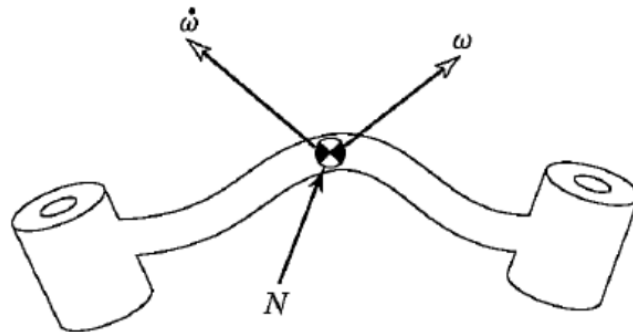
$$F_i = m\dot{v}_{C_i}$$



Euler's equation (Torque)

$$N_i = {}^{C_i}I \dot{\omega}_i + \omega_i \times {}^{C_i}I \omega_i$$

Frame {C} is located at the center of mass





# Force and Torque

## Notation:

- $f_i$  is the force exerted on link  $i$  by link  $i - 1$
- $n_i$  is the torque exerted on link  $i$  by link  $i - 1$
- $F_i$  is the net force exerted on the CG
- $N_i$  is the net torque exerted on the CG

- Summing forces acting on link  $i$ ,

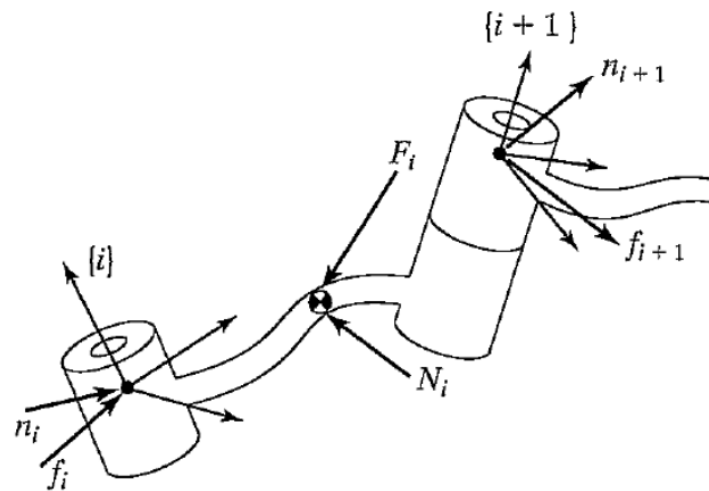
$${}^iF_i = {}^if_i - {}_{i+1}{}^iR {}^{i+1}f_{i+1}$$

$${}^if_i = {}_{i+1}{}^iR {}^{i+1}f_{i+1} + {}^iF_i$$

- Summing torques about CM of link  $i$ ,

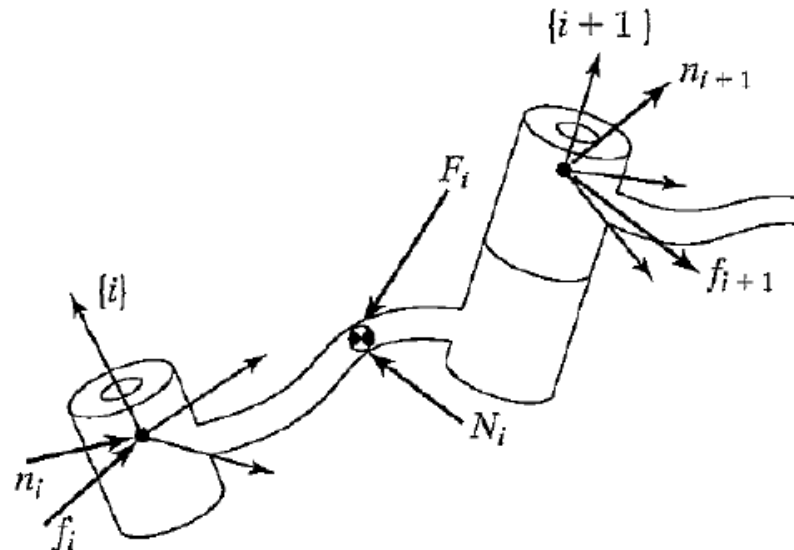
$$\begin{aligned} {}^iN_i &= {}^in_i - {}^in_{i+1} + (-{}^iP_{C_i}) \times {}^if_i - ({}^iP_{i+1} - {}^iP_{C_i}) \times {}^if_{i+1} \\ &= {}^in_i - {}_{i+1}{}^iR {}^{i+1}n_{i+1} - {}^iP_{C_i} \times ({}^if_i - {}_{i+1}{}^iR {}^{i+1}f_{i+1}) \\ &\quad - {}^iP_{i+1} \times {}^if_{i+1} \end{aligned}$$

$${}^in_i = {}^iN_i + {}_{i+1}{}^iR {}^{i+1}n_{i+1} + {}^iP_{C_i} \times {}^iF_i + {}^iP_{i+1} \times ({}_{i+1}{}^iR {}^{i+1}f_{i+1})$$



# Force and Torque

- Torque required by motor:
  - $\tau_i = {}^i n_i^T {}^i \hat{Z}_i$  (ie dot product of the two vectors)
    - Dot product because the rest are reaction forces
- In the case of prismatic joint, force required by actuator:
  - $F_i = {}^i f_i^T {}^i \hat{Z}_i$



Recall in Wk 04: **Jacobian**

For a rotational joint,

$$J_i = \begin{bmatrix} Z_{i-1} \times (P_N - P_{i-1}) \\ Z_{i-1} \end{bmatrix}$$

For a translational joint,

$$J_i = \begin{bmatrix} Z_{i-1} \\ 0 \end{bmatrix}$$

# Iterative Newton-Euler Formulation

## Outwards

$${}^{i+1}\omega^0_{i+1} = {}^{i+1}_i R \, {}^i\omega^0_i + \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

$${}^{i+1}\dot{\omega}^0_{i+1} = {}^{i+1}_i R \dot{\omega} + {}^{i+1}_i R \, {}^i\omega^0_i \times \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

$${}^{i+1}v^0_{i+1} = {}^{i+1}_i R \left( {}^iv^0_i + {}^i\omega^0_i \times {}^iP_{i+1} \right)$$

$$\begin{aligned} {}^{i+1}\dot{v}^0_{i+1} = {}^{i+1}_i R \left( {}^i\dot{\omega}^0_i \times {}^iP_{i+1} + {}^i\omega^0_i \times \left( {}^i\omega^0_i \times {}^iP_{i+1} \right) + {}^i\dot{v}^0_i \right) \\ + 2 {}^{i+1}\omega^0_{i+1} \times \dot{d}_{i+1} {}^{i+1}\hat{Z}_{i+1} + \ddot{d}_{i+1} {}^{i+1}\hat{Z}_{i+1} \end{aligned}$$

$${}^{i+1}\dot{v}^0_{i+1} = {}^{i+1}_i R \left( {}^i\dot{\omega}^0_i \times {}^iP_{i+1} + {}^i\omega^0_i \times \left( {}^i\omega^0_i \times {}^iP_{i+1} \right) + {}^i\dot{v}^0_i \right)$$

# Iterative Newton-Euler Formulation

- Newton and Euler

$${}^i\dot{v}_{Ci}^0 = {}^i\dot{\omega}_i^0 \times {}^iP_{Ci} + {}^i\omega_i^0 \times ({}^i\omega_i^0 \times {}^iP_{Ci}) + {}^i\dot{v}_i^0$$

$${}^{i+1}F_{i+1} = m_{i+1} {}^{i+1}\dot{v}_{Ci+1}$$

$${}^{i+1}N_{i+1} = {}^{Ci+1}I_{i+1} {}^{i+1}\dot{\omega}_{i+1} + {}^{i+1}\omega_{i+1} \times {}^{Ci+1}I_{i+1} {}^{i+1}\omega_{i+1}$$

# Iterative Newton-Euler Formulation

- Inwards

$${}^i f_i = {}_{i+1}^i R {}^{i+1} f_{i+1} + {}^i F_i$$

$${}^i n_i = {}^i N_i + {}_{i+1}^i R {}^{i+1} n_{i+1} + {}^i P_{C_i} \times {}^i F_i + {}^i P_{i+1} \times ({}_{i+1}^i R {}^{i+1} f_{i+1})$$

$$\tau_i = {}^i n_i^T {}^i \hat{Z}_i$$

## Q5.2 Example of Dynamics

- Given the following 2-link planar manipulator in Q3.4, Given the following two-link planar manipulator, and assuming all the mass exists as a point mass at the distal end of each link, determine the torque required by each motor.

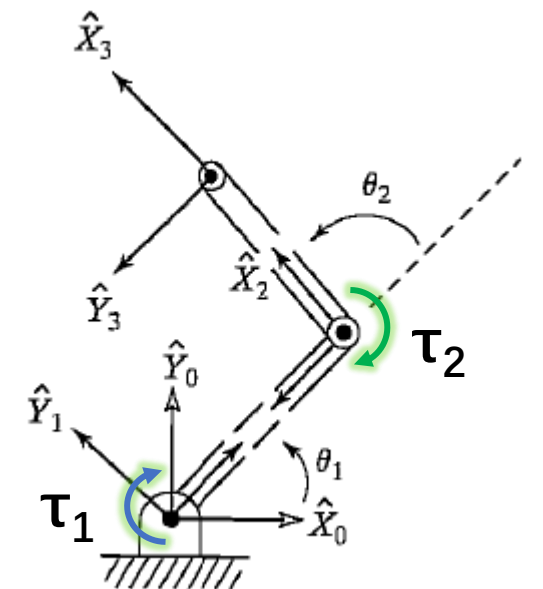
- Previously,

$$\cdot \quad {}^0_1T = \begin{bmatrix} c\theta_1 & -s\theta_1 & 0 & 0 \\ s\theta_1 & c\theta_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad {}^1_2T = \begin{bmatrix} c\theta_2 & -s\theta_2 & 0 & l_1 \\ s\theta_2 & c\theta_2 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad {}^2_3T = \begin{bmatrix} 1 & 0 & 0 & l_2 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

- Assume acceleration due to gravity to be  $g$

- i.e.*  ${}^0\dot{v}_0 = g\hat{Y}_0$

$${}^0\omega_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0v_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0\dot{\omega}_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad {}^0\dot{v}_0 = \begin{bmatrix} 0 \\ g \\ 0 \end{bmatrix}$$



# Q5.2 Example of Dynamics

$${}^0_1R = \begin{bmatrix} c_1 & -s_1 & 0 \\ s_1 & c_1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$${}^1_2R = \begin{bmatrix} c_2 & -s_2 & 0 \\ s_2 & c_2 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$${}^0\omega_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, {}^0v_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, {}^0\dot{\omega}_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix},$$

$${}^0\dot{v}_0 = \begin{bmatrix} 0 \\ g \\ 0 \end{bmatrix}$$

$i=0$

$${}^1\omega_1 = \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_1 \end{bmatrix}, {}^1\dot{\omega}_1 = \begin{bmatrix} 0 \\ 0 \\ \ddot{\theta}_1 \end{bmatrix}, {}^1v_1 = \begin{bmatrix} c_1 & -s_1 & 0 \\ s_1 & c_1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ g \end{bmatrix}$$

$i=1$

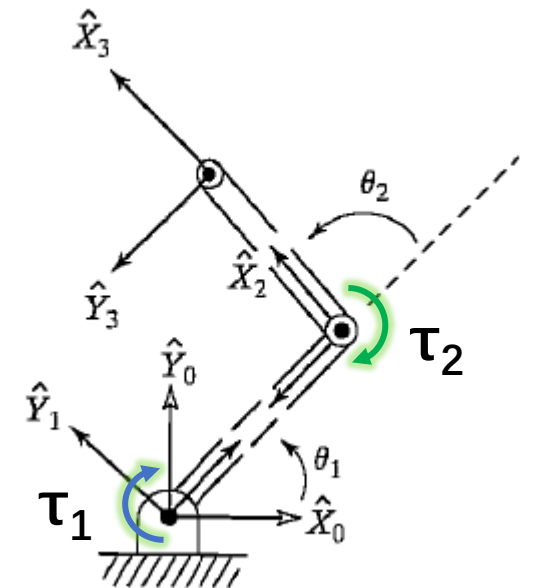
$${}^2\omega_2 = \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_1 + \dot{\theta}_2 \end{bmatrix}, {}^2\dot{\omega}_2 = \begin{bmatrix} 0 \\ 0 \\ \ddot{\theta}_1 + \ddot{\theta}_2 \end{bmatrix}, {}^2v_2 = \begin{bmatrix} c_2 & -s_2 & 0 \\ s_2 & c_2 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} -l_1\dot{\theta}_1^2 + gs_1 \\ -l_2\ddot{\theta}_1 + gc_1 \\ 0 \end{bmatrix} = \begin{bmatrix} l_1\ddot{\theta}_1^2 s_2 - l_1\dot{\theta}_1^2 c_2 + gs_{12} \\ l_1\ddot{\theta}_1^2 c_2 - l_1\dot{\theta}_1^2 s_2 + gc_{12} \\ 0 \end{bmatrix}$$

$${}^{i+1}\omega_{i+1}^0 = {}^{i+1}_iR {}^i\omega_i^0 + \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

$${}^{i+1}\dot{\omega}_{i+1}^0 = {}^{i+1}_iR \dot{\omega} + {}^{i+1}_iR {}^i\omega_i^0 \times \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

$${}^{i+1}v_{i+1}^0 = {}^{i+1}_iR ({}^iv_i^0 + {}^i\omega_i^0 \times {}^iP_{i+1})$$

$${}^{i+1}\dot{v}_{i+1}^0 = {}^{i+1}_iR ({}^i\dot{\omega}_i^0 \times {}^iP_{i+1} + {}^i\omega_i^0 \times ({}^i\omega_i^0 \times {}^iP_{i+1}) + {}^i\dot{v}_i^0)$$



# Q5.2 Example of Dynamics

For  $i=0$ ,

$${}^1\dot{v}_{C_1} = \begin{bmatrix} gs_1 \\ gc_1 \\ 0 \end{bmatrix} + \begin{bmatrix} -l_1\dot{\theta}_1^2 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ l_1\ddot{\theta}_1 \\ 0 \end{bmatrix} = \begin{bmatrix} -l_1\dot{\theta}_1^2 + gs_1 \\ l_1\ddot{\theta}_1 + gc_1 \\ 0 \end{bmatrix}$$

$${}^1F_1 = \begin{bmatrix} -m_1l_1\dot{\theta}_1^2 + m_1gs_1 \\ m_1l_1\ddot{\theta}_1 + m_1gc_1 \\ 0 \end{bmatrix}$$

$${}^1N_1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

For  $i=1$ ,

$${}^2\dot{v}_{C_2} = \begin{bmatrix} l_1\ddot{\theta}_1^2s_2 - l_1\dot{\theta}_1^2c_2 + gs_{12} \\ l_1\ddot{\theta}_1^2c_2 + l_1\dot{\theta}_1^2s_2 + gc_{12} \\ 0 \end{bmatrix} + \begin{bmatrix} -l_2(\dot{\theta}_1 + \dot{\theta}_2)^2 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ l_2(\ddot{\theta}_1 + \ddot{\theta}_2) \\ 0 \end{bmatrix}$$

$${}^2F_2 = \begin{bmatrix} m_2l_1\ddot{\theta}_1s_2 - m_2l_1\dot{\theta}_1^2c_2 + m_2gs_{12} - m_2l_2(\dot{\theta}_1 + \dot{\theta}_2)^2 \\ m_2l_1\ddot{\theta}_1c_2 + m_2l_1\dot{\theta}_1^2s_2 + m_2gc_{12} + m_2l_2(\ddot{\theta}_1 + \ddot{\theta}_2) \\ 0 \end{bmatrix}$$

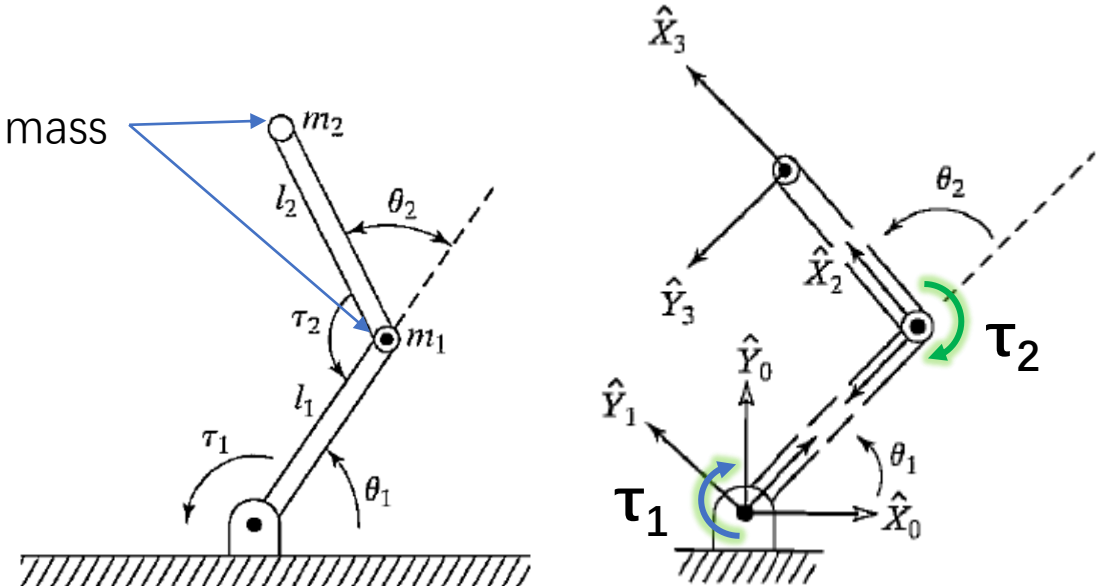
$${}^2N_2 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$${}^i\dot{v}_{C_i}^0 = {}^i\dot{\omega}_i^0 \times {}^iP_{C_i} + {}^i\omega_i^0 \times ({}^i\omega_i^0 \times {}^iP_{C_i}) + {}^i\dot{v}_i^0$$

$${}^{i+1}F_{i+1} = m_{i+1} {}^{i+1}\dot{v}_{C_{i+1}}$$

$${}^{i+1}N_{i+1} = {}^{Ci+1}I_{i+1} {}^{i+1}\dot{\omega}_{i+1} + {}^{i+1}\omega_{i+1} \times {}^{Ci+1}I_{i+1} {}^{i+1}\omega_{i+1}$$

Pointed mass





# Q5.2 Example of Dynamics

$${}^i f_i = {}_{i+1}^i R {}^{i+1} f_{i+1} + {}^i F_i$$

For  $i=2$ ,

$${}^2 n_2 = \begin{bmatrix} {}^2 f_2 = {}^2 F_2 \\ 0 \\ 0 \\ m_2 l_1 l_2 \ddot{\theta}_1 c_2 + m_2 l_1 l_2 \dot{\theta}_1^2 s_2 + m_2 l_2 g c_{12} + m_2 l_2^2 (\ddot{\theta}_1 + \ddot{\theta}_2) \end{bmatrix}$$

$${}^i n_i = {}^i N_i + {}_{i+1}^i R {}^{i+1} n_{i+1} + {}^i P_{C_i} \times {}^i F_i + {}^i P_{i+1} \times ({}_{i+1}^i R {}^{i+1} f_{i+1})$$

$$\tau_i = {}^i n_i^T {}^i \hat{Z}_i$$

Torque required by motor 2

Pointed mass

$$\text{For } i=1, \quad {}^1 f_1 = \begin{bmatrix} c_2 & -s_2 & 0 \\ s_2 & c_2 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} m_2 l_1 s_2 \ddot{\theta}_1 - m_2 l_1 c_2 \dot{\theta}_1^2 + m_2 g s_{12} - m_2 l_2 (\ddot{\theta}_1 + \dot{\theta}_2)^2 \\ m_2 l_1 c_2 \ddot{\theta}_1 + m_2 l_1 s_2 \dot{\theta}_1^2 + m_2 g c_{12} + m_2 l_2 (\ddot{\theta}_1 + \ddot{\theta}_2) \\ 0 \end{bmatrix}$$

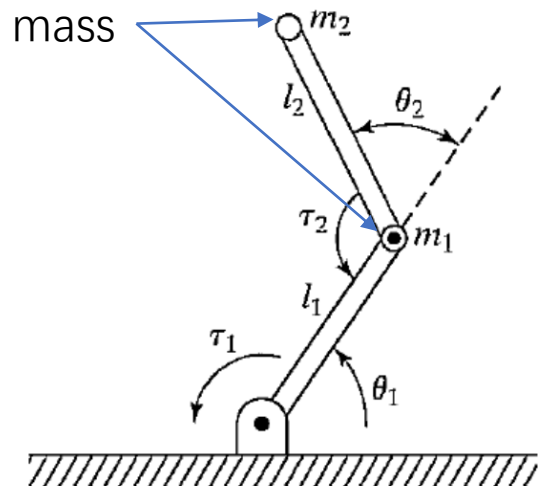
$$+ \begin{bmatrix} -m_1 l_1 \dot{\theta}_1^2 + m_1 g s_1 \\ m_1 l_1 \ddot{\theta}_1 + m_1 g c_1 \\ 0 \end{bmatrix},$$

$${}^1 n_1 = \begin{bmatrix} 0 \\ 0 \\ m_2 l_1 l_2 c_2 \ddot{\theta}_1 + m_2 l_1 l_2 s_2 \dot{\theta}_1^2 + m_2 l_2 g c_{12} + m_2 l_2^2 (\ddot{\theta}_1 + \ddot{\theta}_2) \end{bmatrix}$$

$$+ \begin{bmatrix} 0 \\ 0 \\ m_1 l_1^2 \ddot{\theta}_1 + m_1 l_1 g c_1 \end{bmatrix}$$

Torque required by motor 1

$$+ \begin{bmatrix} 0 \\ 0 \\ m_2 l_1^2 \ddot{\theta}_1 - m_2 l_1 l_2 s_2 (\dot{\theta}_1 + \dot{\theta}_2)^2 + m_2 l_1 g s_{12} \\ + m_2 l_1 l_2 c_2 (\ddot{\theta}_1 + \ddot{\theta}_2) + m_2 l_1 g c_{12} \end{bmatrix}$$



# Dynamic Equation

$$\tau = M(\Theta)\ddot{\Theta} + V(\Theta, \dot{\Theta}) + G(\Theta)$$

$M(\Theta)$  is  $n \times n$  mass matrix of the manipulator

$V(\Theta, \dot{\Theta})$  is an  $n \times 1$  vector of centrifugal and Coriolis terms

$G(\Theta)$  is an  $n \times 1$  vector of gravity terms

# Dynamic Equation

Using the previous case as the example,  $\tau_2 = m_2 l_1 l_2 \ddot{\theta}_1 c_2 + m_2 l_1 l_2 \dot{\theta}_1^2 s_2 + m_2 l_2 g c_{12} + m_2 l_2^2 (\ddot{\theta}_1 + \ddot{\theta}_2)$

$$M(\Theta) = \begin{bmatrix} l_2^2 m_2 + 2l_1 l_2 m_2 c_2 + l_1^2 (m_1 + m_2) & l_2^2 m_2 + l_1 l_2 m_2 c_2 \\ l_2^2 m_2 + l_1 l_2 m_2 c_2 & l_2^2 m_2 \end{bmatrix}$$

$$V(\Theta, \dot{\Theta}) = \begin{bmatrix} -m_2 l_1 l_2 s_2 \dot{\theta}_2^2 - 2m_2 l_1 l_2 s_2 \dot{\theta}_1 \dot{\theta}_2 \\ m_2 l_1 l_2 s_2 \dot{\theta}_1^2 \end{bmatrix}$$

$$G(\Theta) = \begin{bmatrix} m_2 l_2 g c_{12} + (m_1 + m_2) l_1 g c_1 \\ m_2 l_2 g c_{12} \end{bmatrix}$$



# Lagrangian Approach

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