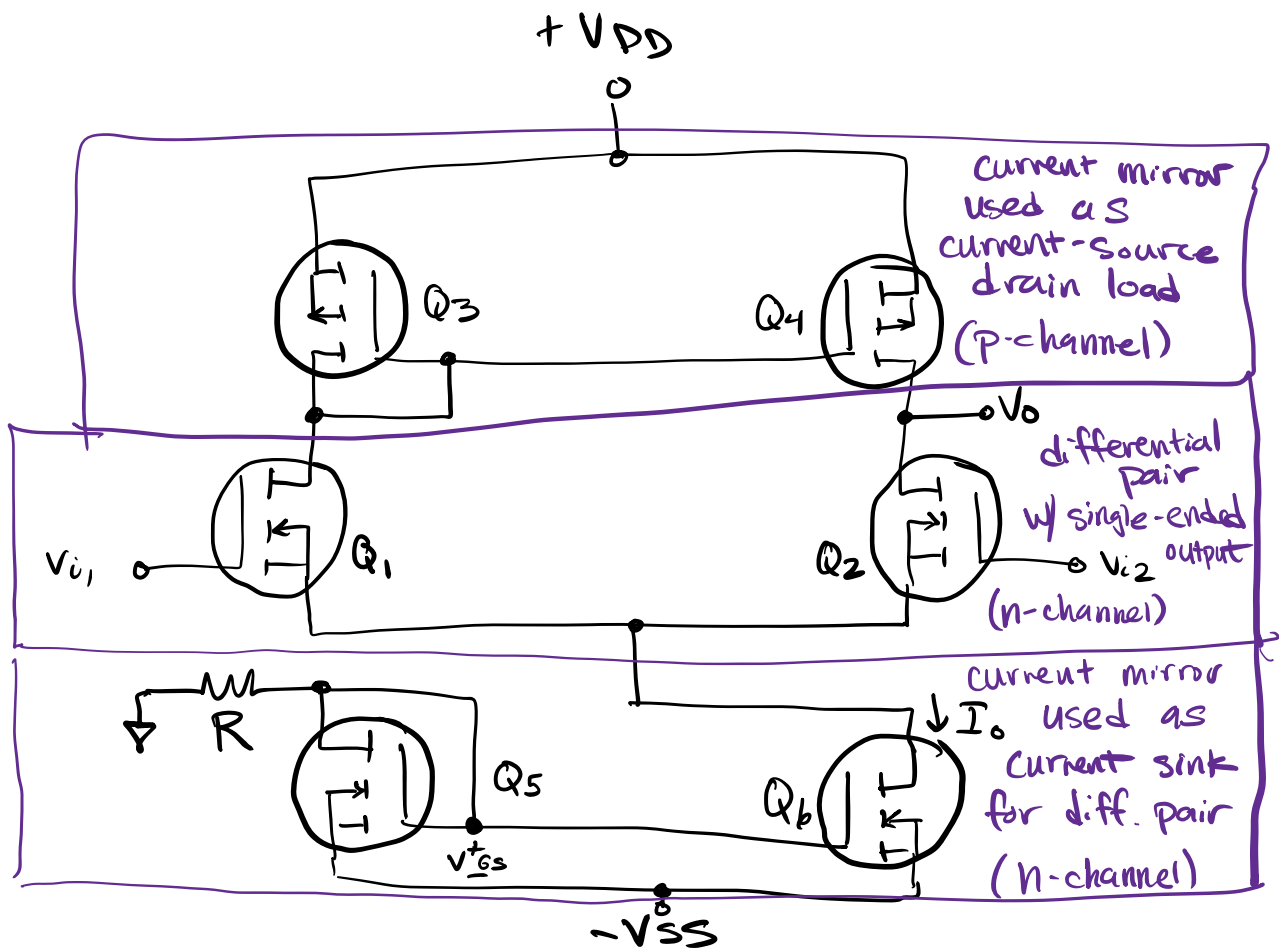


# MOSFET Differential Pair with Active Load

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- .. We have discussed the MOSFET differential pair and its performance in differential and common modes with different current sink dynamic resistances ( $r_{out}$ )
- .. in this circuit and drain-loaded amplifiers in general, overall gain is dominated by the  $g_m R_D$  term ( $R_D \ll r_o$ )
- ..  $R_D$  also plays a crucial role in the DC operating characteristics of the amplifiers
  - .. if we try to make  $R_D$  large to get more gain, it drops more DC voltage ( $I_D R_D$ ), necessitating either increased  $V_{DD}$  (expensive!), or reduced  $I_D$  (reduces gain!)
- .. Furthermore, often we really only need a differential input to accept balanced signals or a feedback loop; if we don't need the differential output, using a current-mirror as an active drain load greatly increases gain without increasing  $V_{DD}$  or  $I_D$



-- note: one resistor sets all DC operating conditions!

-- we can now set the drain current to a much wider choice of values to get the desired performance, without worrying about a drain resistor dropping too much voltage!

-- effective  $r_D = r_o$  ; much larger than any practical drain resistor  $R_D$ !

$$I_{REF} = \frac{0 - (-V_{SS} + V_{GS})}{R}$$

$$R = \frac{|V_{SS}| - V_{GS}}{I_{REF}}$$

if  $K = 10 \text{ mA/V}^2$ ,  $V_t = 1.2 \text{ V}$ ,  $V_{DD} = \pm 12 \text{ V}$

$$V_{GS} = \sqrt{\frac{I_D}{K}} + V_t$$

$$= \sqrt{\frac{2}{10}} + 1.2 = \underline{1.647 \text{ V}}$$

then  $R = \frac{12 - 1.647}{2} = 5.177 \text{ k}\Omega$ ;

Use  $5.23 \text{ k}\Omega$   
1%

- What about the diff pair itself?
- With no drain resistors, how do we know what  $V_D$  is and if it provides "wiggle room?"

Q3 is a p-channel MOSFET with its drain connected to its gate; thus,  $V_{DS3} = V_{GS3}$

-- Furthermore, its source is connected to  $V_{DD}$

$$\begin{aligned}\therefore V_{DS3} &= V_{D3} - V_{S3} \\ &= V_{D3} - V_{DD} = V_{GS3}\end{aligned}$$

$$\rightarrow \underline{V_{D3} = V_{DD} + V_{GS3}}$$

-- assuming  $K = 10 \text{ mA/V}^2$ ,  $V_t = -1.2 \text{ V}$  <sup>p-channel!</sup>,  $I_D = \underline{1 \text{ mA}}$  <sup>each half of diff pair!</sup>

$$\begin{aligned}V_{GS}|_P &= -\sqrt{\frac{I_D}{K}} + V_t \\ &= -\sqrt{\frac{1}{10}} + -1.2 \\ &= \underline{-1.516 \text{ V}}\end{aligned}$$

$$\text{then } V_{D3} = 12 + -1.516 = \underline{10.48 \text{ V}}$$

$\therefore$  this must also equal  $V_{D2} \leftarrow$  output of diff pair

-- if  $Q_3$  and  $Q_4$  are perfectly matched (same chip!!!)

$$\text{then } V_{D4} = V_{D3} = V_{D2} = V_{D1} = V_O = \underline{10.48 \text{ V}}$$

-- note: we are sitting pretty close to  $V_{DD}$  and won't have much upward wiggle room; but that's OK, these are usually low-level stages.

# Differential Gain of MOSFET Diff Pair w/ Active Load

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.. we have already established that the differential-mode gain to one output is

$$\frac{V_{o2}}{V_d} = \frac{+g_m R_D \parallel r_o}{2}$$

$\leftarrow = V_o$ ; we intentionally chose the non-inverting output! ☺

.. now  $R_D$  is replaced with  $r_D = r_o$  from active current-source load

.. let's call this  $r_{op}$  to distinguish it from the  $r_{on}$  of the diff pair itself

$$\text{then } A_d = \frac{g_m r_{op} \parallel r_{on}}{2}$$

.. and finally, if  $r_{op} \approx r_{on} = r_o$ , then  $r_{op} \parallel r_o = \frac{r_o}{2}$

$$A_d = \frac{g_m r_o}{4}$$

$$\begin{aligned} \therefore \text{if } g_m &= 2\sqrt{K I_D} \\ &= 2\sqrt{10 \cdot 1} = \underline{\underline{6.325 \text{ mA/V}}} \end{aligned}$$

$$r_o = \frac{|V_A|}{I_D} = \frac{100}{1} = \underline{\underline{100 \text{ k}\Omega}}$$

$$\text{then } A_d = \frac{6.325 \cdot 100}{4} = \underline{\underline{158.1}}$$

or 44 dB

.. pretty good for MOSFETs @ low current!

.. its because we replaced an  $R_D$  of  
1 or 2  $\text{k}\Omega$  with  $r_o \parallel r_o$  of  $\approx 50 \text{ k}\Omega$ !

.. an actual 100k drain resistor would  
have dropped 100V!

.. now the problem with increasing  $I_D$  to increase  $g_m$   
is that it decreases  $r_o$  faster!

$$g_m = 2\sqrt{K I_D} \quad (\text{'1/2 power})$$

$$r_o = \frac{|V_A|}{I_D} \quad (\text{linear!})$$

CMRR is still approximated the same way; thus,

$$CMRR = 20 \log_{10} (g_m r_{\text{sink}})$$

$$\begin{aligned} \text{for current mirror, } r_{\text{sink}} &= r_o = \frac{|V_A|}{I_D} \\ &= \frac{100}{2} \approx \underline{50 \text{ k}\Omega} \end{aligned}$$

$$CMRR = 20 \log_{10} (6.325 \cdot 50) = \underline{50 \text{ dB}}$$

-- use cascode current sink if you need higher performance

-- this is entering the realm of CMOS:

Complimentary Metal Oxide Semiconductor technology,

fabrication process for pairs of n-type and p-type MOSFETs on same chip

-- now 99% of integrated circuits are CMOS!

-- related to idea of replacing resistors with more transistors and avoiding capacitors)  $\rightarrow$  integrated circuits