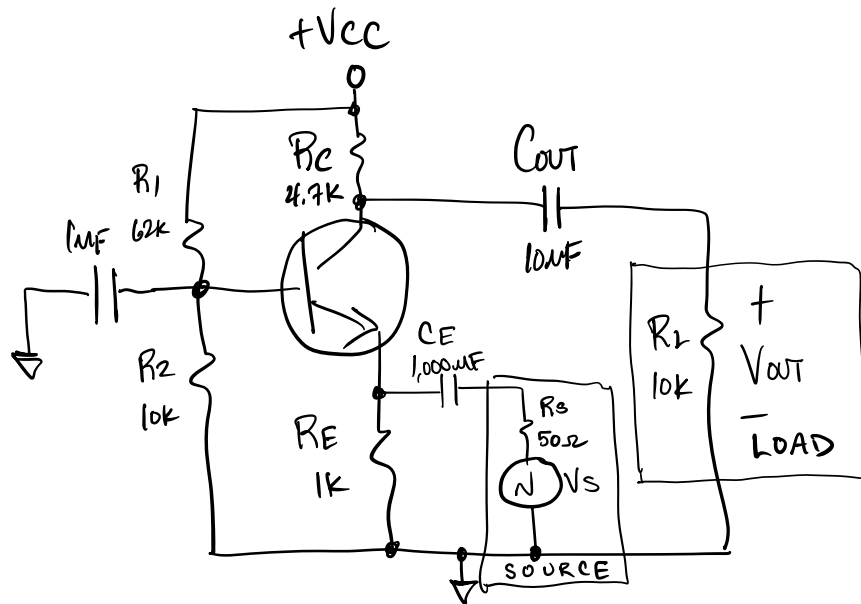
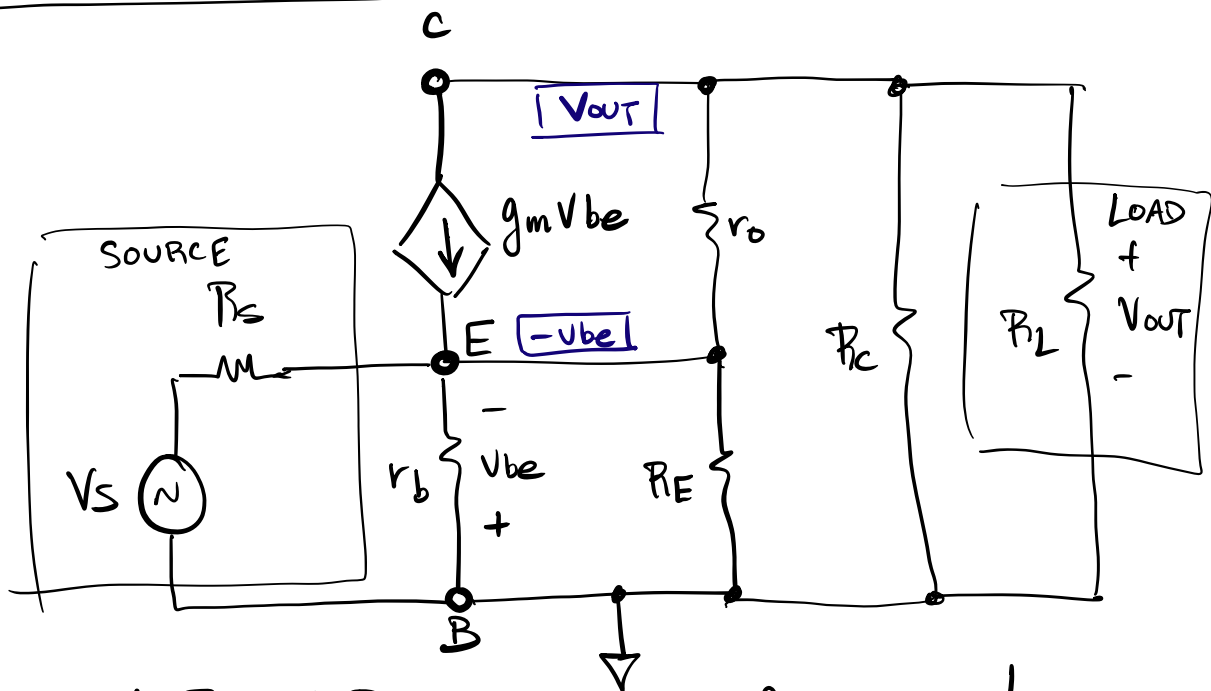


# Common-Base Amplifier



- alternate method of modulating  $V_{BE}$ !
- rather than couple  $V_S$  to the base and "ground" the emitter we couple  $V_S$  to the emitter and ground the base!
- this configuration suffers from very low  $R_{in}$ ;  
 $\sim r_e = \frac{1}{g_m}$ , thus it is not often used by itself, but as part of compound amplifier called the cascode.

# Mid-Frequency SSM of CB Amplifier



- note  $R_1$  and  $R_2$  are now gone from model!
- not quite so simple to determine input and output gains  
 $A_{v1}$  and  $A_{v2}$
- node voltage to the rescue!
- assume  $r_o$  is "large" and may be neglected

from the emitter terminal ( $-V_{be}$ ):

$$\frac{-V_{be} - V_S}{R_S} + \frac{-V_{be} - 0}{R_E} + \frac{-V_{be} - 0}{r_b} + g_m V_{be} = 0$$

$$-V_{be} \left( \frac{1}{R_S} + \frac{1}{R_E} + \frac{1}{r_b} + g_m \right) = \frac{V_S}{R_S}$$

$$A_{v1} = \frac{V_{be}}{V_S} = \frac{-1}{R_S \left( \frac{1}{R_S} + \frac{1}{R_E} + \frac{1}{r_b} + g_m \right)}$$

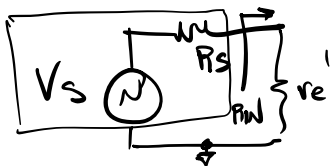
$$A_{v1} = - \frac{(R_S \parallel R_E \parallel r_b \parallel \frac{1}{g_m})}{R_S}$$

define  $re' = R_E \parallel r_b \parallel \frac{1}{g_m}$

then  $A_{v_1} = \frac{-R_S \parallel re'}{R_S} = \frac{-\cancel{R_S} re'}{(R_S + re') \cancel{R_S}}$

$A_{v_1} = \frac{-re'}{R_S + re'}$  ← voltage division between  $re'$  and  $R_S$ !

∴ clearly shows that  $R_{in} = re'$ !



∴ we already know  $g_m = 92.05 \text{ mA/V}$

$R_E = 1 \text{ k}\Omega$

$r_b = 2.173 \text{ k}\Omega$

$R_S = 50 \Omega$

$\frac{1}{g_m} = \frac{1}{92.05} = 0.01086 \text{ k}\Omega$

or  $10.86 \Omega$

∴  $re' = \frac{1}{g_m} \parallel R_E \parallel r_b \approx \frac{1}{g_m} = \underline{10.86 \Omega} \quad !!!$

$$A_{v1} = \frac{-r_e'}{R_s + r_e'}$$

$$= \frac{-10.86}{50 + 10.86} = \underline{-0.1784}$$

or -15 dB (inverting)

↑  
not much of an amplifier yet!

-- node voltage from the collector terminal, again neglecting  $r_o$ :

$$g_m v_{be} + \frac{V_{out} - 0}{R_c} + \frac{V_{out} - 0}{R_L} = 0$$

$$V_{out} \left( \frac{1}{R_c} + \frac{1}{R_L} \right) = -g_m v_{be}$$

$$A_{v2} = \frac{V_{out}}{v_{be}} = -g_m \left( \frac{1}{\frac{1}{R_c} + \frac{1}{R_L}} \right)$$

$$A_{v2} = -g_m (R_c \parallel R_L)$$

(just like common emitter!)

if  $g_m = 92.05$

$R_c = 4.7k$

$R_L = 10k$

$\left. \begin{matrix} R_c = 4.7k \\ R_L = 10k \end{matrix} \right\} R_c \parallel R_L = 3.197k$

about 0.7 dB  
higher than  
CE due to  $r_o$   
(big deal)

then  $A_{v2} = -92.05 \cdot 3.197 = \underline{-294}$  or 49 dB  
(inverting)

$$A_v = A_{v1} \times A_{v2} = -0.1784 \cdot -294$$

$$= \underline{+52.45} \text{ or } \underline{34 \text{ dB}}$$

Non-inverting!

.. so CB configuration has less gain and much lower  $R_{in}$  than CE.

## LF Response of CB Amplifier

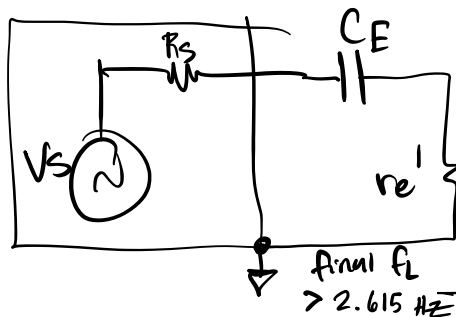
-- good news: capacitor to ground at base no longer creates high-pass filter

.. the capacitor at the collector ( $C_{out}$ ) does the same thing in CB as it does in CE; thus,

$$f_{Lout} = \frac{1}{2\pi C_{out} (r_o \parallel R_c + R_L)}$$

$$= \underline{1.12 \text{ Hz}} \text{ in previous example (with } r_o)$$

.. now  $C_E$  creates high-pass filter with  $R_s$  and  $r_{e'}$



$$\therefore f_{LIN} = \frac{1}{2\pi \cdot C_E \cdot (R_s + r_{e'})}$$

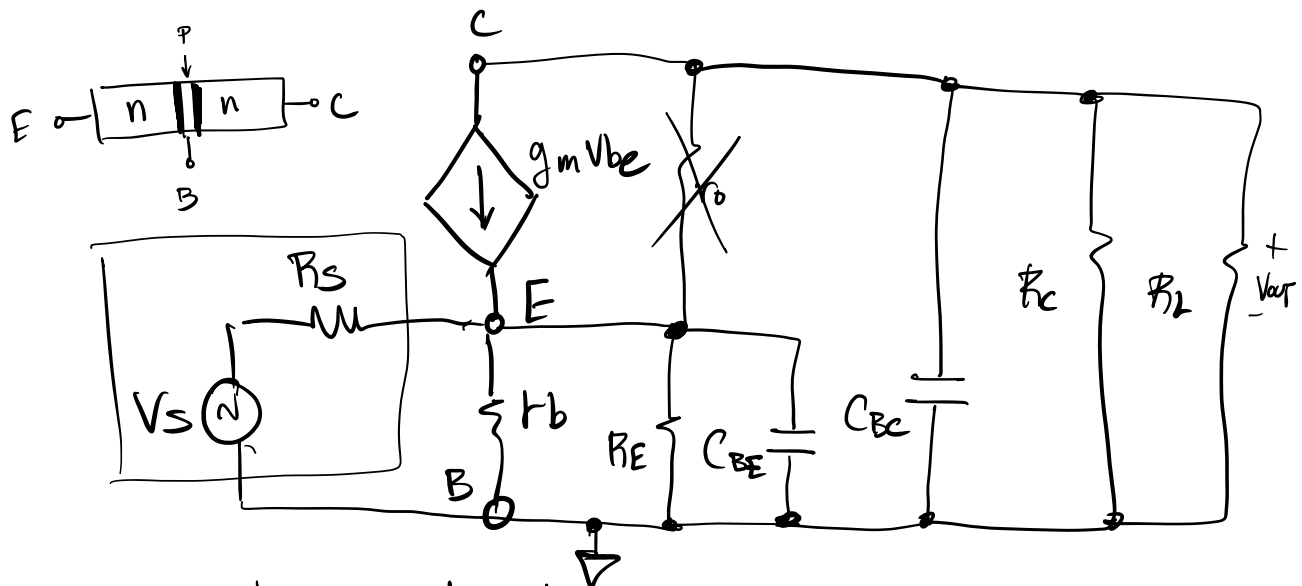
$$f_{LIN} = \frac{1}{2\pi \cdot 1000 \times 10^{-6} (50 + 10.86)}$$

$$= \underline{2.615 \text{ Hz}}$$

# HF Response of CB Amplifier

.. this is where things get interesting!

HF SSM:



.. note that we don't have any capacitance between input and output

→ No Miller Time !!!

.. just two simple low-pass filters!

$$f_{HIN} = \frac{1}{2\pi \cdot C_{BE} (R_s \parallel r_{e'})} \rightarrow \approx \frac{1}{g_m}$$

$$f_{HIN} = \frac{1}{2\pi \cdot 18 \times 10^{-12} (50 \parallel 10.86)} \rightarrow = 9.922 \text{ MHz}$$

↑  
from previous lecture!

$f_{HIN} = 991 \text{ MHz !!!}$

.. Compare this to 2.97 MHz of  $C_E$ , wow!

$$f_{H \text{ out}} \approx \frac{1}{2\pi \cdot C_{BC} (R_C \parallel R_L)}$$

$\hookrightarrow 4 \text{ pF} \quad \hookrightarrow 3.197 \text{ k}$

(Same as CE amplifier if you ignore  $r_o$ )

$$f_{H \text{ out}} = \underline{12.4 \text{ MHz}} \quad \left[ \text{was } 13.5 \text{ including } r_o \right]$$

$\rightarrow$  this is the dominant pole

$$\therefore \underline{f_H \approx 12.4 \text{ MHz}}$$

-- so despite lower gain and much lower  $R_{in}$ ,  
 CB has superior HF response to the CE configuration  
 -- we'll combine the two into the best of both worlds!