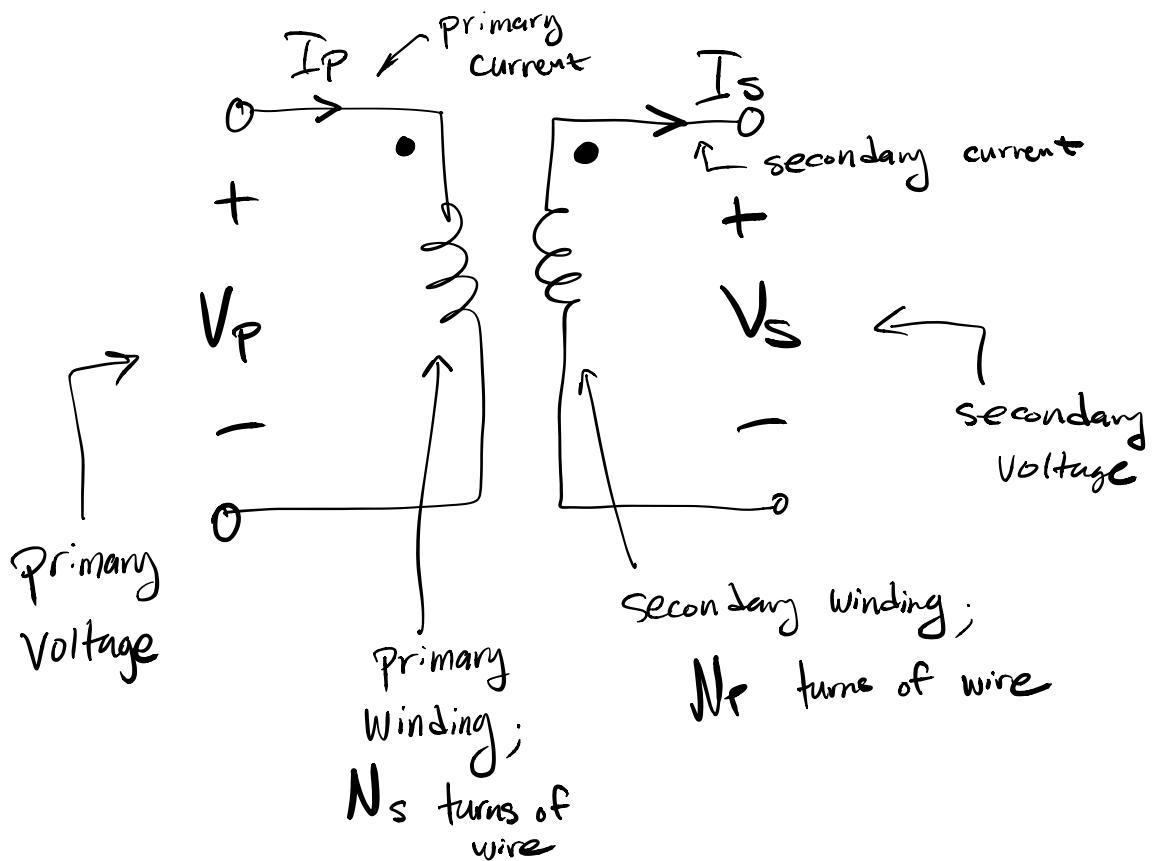


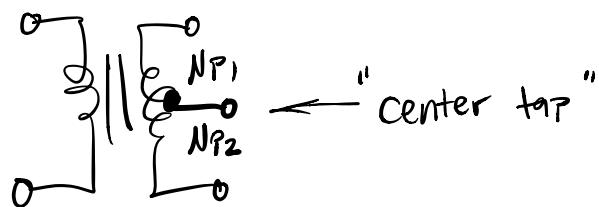
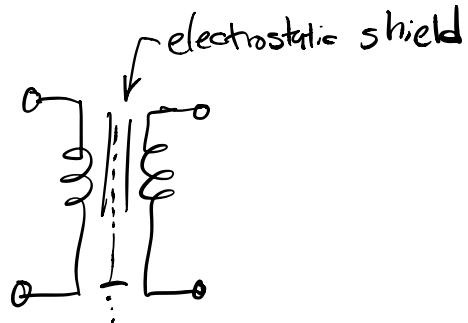
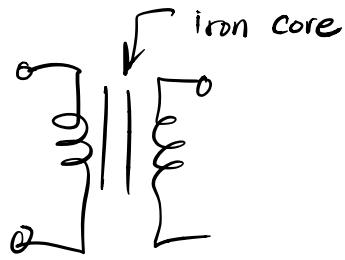
Ideal Transformers

principle: two magnetically-coupled inductors
may transform AC (only!) voltages or
currents by a ratio proportional to the
ratio of primary -to- secondary turns

Michael Faraday: August 1831



Symbolic Variations :



.. for an ideal (lossless) transformer :

$$\frac{V_S}{V_P} = \frac{N_S}{N_P}$$

$$V_S = V_P \left(\frac{N_S}{N_P} \right)$$

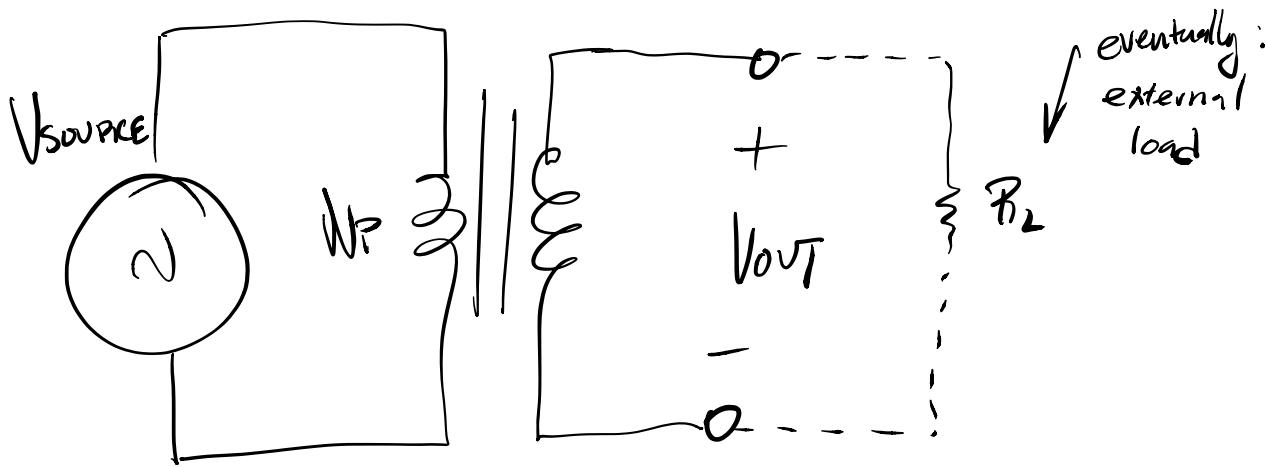
\uparrow turns ratio

ex: $N_P = 500$ turns

$N_S = 1,000$ turns

$V_{\text{SOURCE}} = 120 \sqrt{\text{RMS}} @ 60 \text{ Hz}$

Wall socket!



$$V_p = V_{\text{SOURCE}};$$

$$\therefore V_{\text{OUT}} = V_s = V_p \left(\frac{N_s}{N_p} \right)$$

$$= V_{\text{SOURCE}} \left(\frac{N_s}{N_p} \right)$$

$$= 120 \left(\frac{1000}{500} \right) = \underline{\underline{240 \text{ V}_{\text{RMS}}}}$$

When $N_s > N_p$, and therefore $V_s > V_p$,

We call this a step-up transformer.

ex: $N_P = 100$ turns, $N_S = 10$ turns, $V_{\text{source}} = 120V_{\text{rms}}$

$$V_{\text{out}} = V_S = V_P \left(\frac{N_S}{N_P} \right) = V_{\text{SOURCE}} \left(\frac{N_S}{N_P} \right)$$

$$= 120 \left(\frac{10}{100} \right) = \underline{\underline{12 \text{ V}_{\text{rms}}}}$$

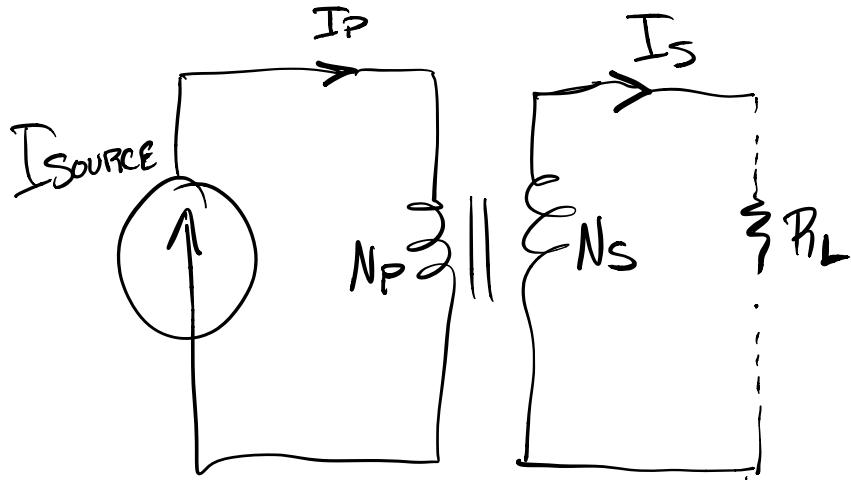
When $N_P > N_S$, we call this a
step down transformer

the current ratio is the inverse of
 the turns (and thus voltage) ratio

$$\frac{I_S}{I_P} = \frac{N_P}{N_S}$$

∴ $I_S = I_P \left(\frac{N_P}{N_S} \right)$

- you can use a transformer w/ a current source;



$$I_{SOURCE} = 280 \text{ mA RMS}$$

$$N_p = 300 \text{ turns}$$

$$N_s = 1200 \text{ turns}$$

$$\begin{aligned} I_s &= I_p \left(\frac{N_p}{N_s} \right) \\ &= 280 \left(\frac{300}{1200} \right) \\ &= \underline{70 \text{ mA RMS}} \end{aligned}$$

$N_s > N_p$, so it would be a voltage stepup transformer; but acts as a current stepdown transformer due to inverse relationship

Power

- ideal transformer is 100% efficient

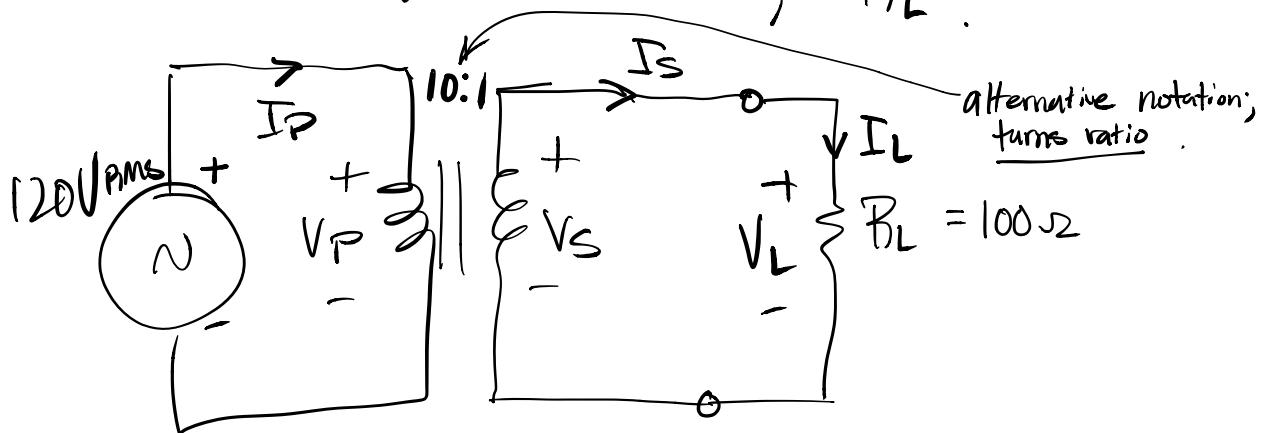
in reality: iron losses

- imperfect magnetic coupling due to core properties
- Eddy currents
- leakage inductance

Copper losses

- wire used to wind transformer has non-zero resistance
 - " I^2R losses"
- We assume ideal transformers in this course
- transformer manufacturers can estimate losses and somewhat compensate for them, if used as rated

- let's hook a stepdown transformer to an external load resistance, R_L .



- load voltage $V_L = V_S$

$$V_S = V_P \left(\frac{N_S}{N_P} \right) = 120 \left(\frac{1}{10} \right) = 12 \text{ V}_{\text{RMS}}$$

10-to-1 Stepdown

- load current $I_L = I_S = \frac{V_S}{R_L} = \frac{12}{100}$

$$I_L = 0.12 \text{ A}_{\text{RMS}}$$

- load power :

$$P_L = V_L I_L = V_S I_S = 12 \cdot 0.12 = 1.44 \text{ W}$$

dissipated
in R_L

• We know $I_S = I_P \left(\frac{N_p}{N_s} \right)$

∴ Primary current is $I_P = I_S \left(\frac{N_s}{N_p} \right)$

$$= 0.12 \left(\frac{1}{10} \right) = \underbrace{0.012 \text{ A}_{\text{RMS}}}_{\text{rise!}}$$

∴ power delivered by source :

$$P_{\text{SOURCE}} = -V_p \cdot I_p = -120 \cdot 0.012$$

$$= \underbrace{-1.44 \text{ W}}_{\text{rise!}} \quad \text{or } 1.44 \text{ W generated}$$

• transformer is (losslessly) trading voltage for current w/ perfect efficiency!

Reflected Impedance

- in the previous example: load connected to transformer secondary was $\underline{R_L} = 100 \Omega$
- we calculated a primary current of $0.012 A_{\text{RMS}}$ with a primary voltage of $120 V_{\text{RMS}}$
- what equivalent impedance does the source "think" it's driving?

$$\frac{V_P}{I_P} = \frac{120}{0.012} = 10,000 \Omega = \underline{100 R_L}$$

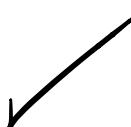
- the impedance relationship in a transformer is

$$\frac{Z_P}{Z_S} = \left(\frac{N_P}{N_S} \right)^2$$

$\downarrow \equiv \left(\frac{V_P}{V_S} \right)^2$

- that $10 \text{ k}\Omega$ is called the reflected impedance.

check: $Z_P = Z_S \left(\frac{N_P}{N_S} \right)^2$

$$= 100 \left(\frac{10}{1} \right)^2 = \underline{\underline{10 \text{ k}\Omega}}$$


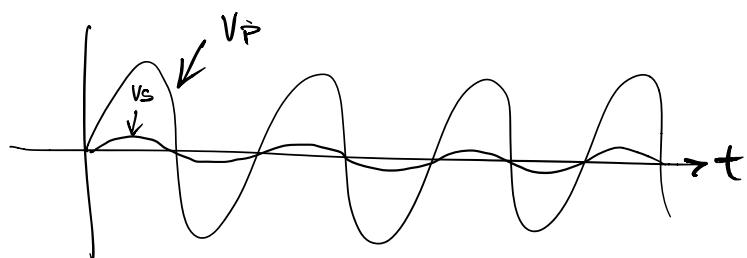
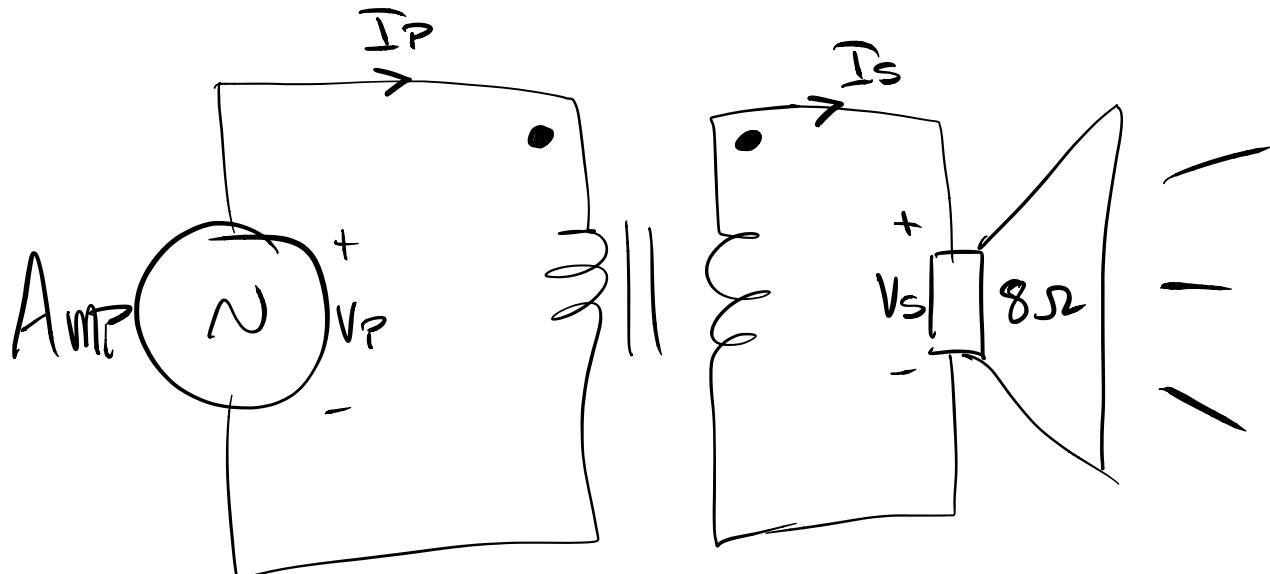
ex: a tube audio amplifier works best into
a $3.2 \text{ k}\Omega$ load.

- problem: you have an 8Ω speaker.

- solution: use a transformer to
match the impedances

- What turns ratio is needed?

- What are the primary and secondary
voltages and currents assuming
100W of audio power?



∴ NO polarity inversion if two "dots" are
on positive terminals of Vs and Vp

$$\frac{Z_p}{Z_s} = \left(\frac{N_p}{N_s} \right)^2$$

∴ turns ratio :

$$\frac{N_p}{N_s} = \sqrt{\frac{Z_p}{Z_s}} = \sqrt{\frac{3200}{8}}$$

= 20 : 1

- 100W into 8Ω :

$$P_s = \frac{V_s^2}{R_s} \rightarrow V_s^2 = P_s R_s$$

$$V_s = \sqrt{P_s R_s} = \sqrt{100 \cdot 8}$$

$$V_s = 28.28 \text{ V}_{\text{RMS}}$$

$$\therefore I_s = \frac{V_s}{R_s} = \frac{28.28}{8} = 3.535 \text{ A}_{\text{RMS}}$$

$$\frac{V_p}{V_s} = \frac{N_p}{N_s} \rightarrow V_p = V_s \left(\frac{N_p}{N_s} \right) \\ = 28.28 \left(\frac{20}{1} \right)$$

$$V_p = 565.6 \text{ V}_{\text{RMS}}$$

to get V_{peak}
from RMS

yikes!

$$565.6 \sqrt{2} \cdot 2 = \underbrace{1600 \text{ V}_{\text{PK-PK}}}_{\dots} \quad \text{yes, real figure!}$$

$$I_P = \frac{V_P}{R_P} = \frac{565.6}{3200} = 0.1768 \text{ A}_{\text{rms}}$$

↑
 reflected
 load Z

or 176.8 mA rms

- We're taking a tube amplifier, which is comfortable @ kV and mA, and interfacing with a speaker that wants V and A

→ the magic of the transformer /