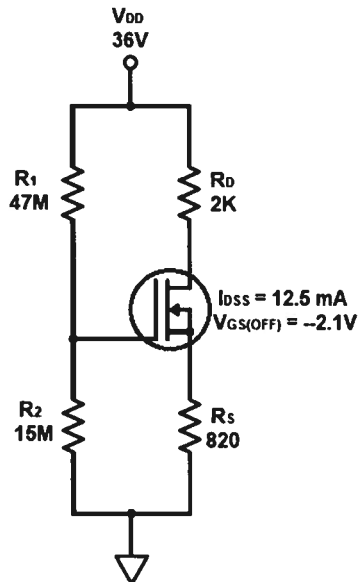


1) Refer to the following circuit:



Which specific type of field-effect transistor is this?

depletion-mode MOSFET

N-channel or p-channel?

Self-bias or voltage-divider bias?

$$V_{DS} > |V_{GS} - V_{GS(OFF)}|$$

$$5.542 > |-0.1478 - (-2.1)$$

yes, active region

Determine  $V_G$ ,  $V_{GS}$ ,  $V_S$ ,  $I_S$ ,  $I_D$ ,  $V_D$ , and  $V_{DS}$ . Check  $P_{diss}$  and verify that the transistor is operating in the active region.

$$V_G = V_{DD} \left( \frac{R_2}{R_1 + R_2} \right) = 36 \left( \frac{15}{15 + 47} \right) = 8.710 \text{ V}$$

$$a = \frac{I_{DSS} R_S}{V_{GS(OFF)}^2} = \frac{12.5 \cdot 820}{(-2.1)^2} = 2.324$$

$$b = \frac{2 I_{DSS} R_S}{|V_{GS(OFF)}|} + 1 = \frac{2 \cdot 12.5 \cdot 820}{2.1} + 1 = 10.76$$

$$c = I_{DSS} R_S - |V_G| = 12.5 \cdot 820 - 8.710 = 1.54$$

$$V_{GS}|_n = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

$$= \frac{-10.76 \pm \sqrt{10.76^2 - 4 \cdot 2.324 \cdot 1.5}}{2 \cdot 2.324}$$

$$V_{GS} = -0.1478 \text{ V}$$

$$V_S = V_G - V_{GS} = 8.710 - (-0.1478) = 8.858 \text{ V}$$

$$I_S = I_D = \frac{V_S - 0}{R_S} = \frac{8.858 - 0}{820} = 10.80 \text{ mA}$$

$$\text{check: } I_D = I_{DSS} \left( 1 - \frac{V_{GS}}{V_{GS(OFF)}} \right)^2 = 12.5 \left( 1 - \frac{-0.1478}{-2.1} \right)^2 = 10.80 \text{ mA}$$

$$V_D = V_{DD} - I_D R_D = 36 - 10.80 \cdot 2 = 14.4 \text{ V}$$

$$V_{DS} = V_D - V_S = 14.4 - 8.858 = 5.542 \text{ V}$$

$$P_{diss} = V_{DS} I_D$$

$$= 5.542 \cdot 10.80$$

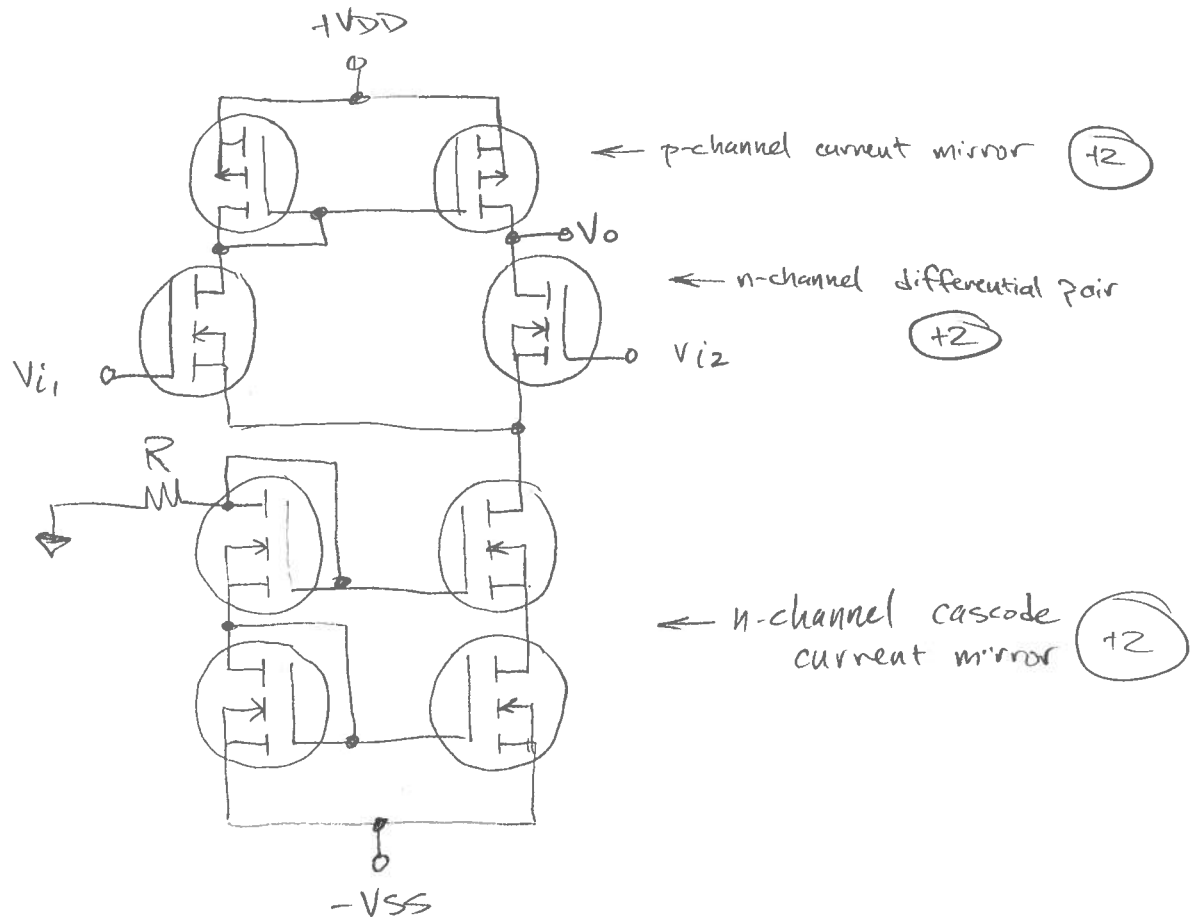
$$= 59.85 \text{ mW}$$

# SOLUTION

2) Design a CMOS differential amplifier that has a small-signal differential gain  $A_{dm} > 30 \text{ dB}$  and  $CMRR > 60 \text{ dB}$ . Draw the circuit carefully and explain your choice of active vs. passive drain load, resistive vs. current-mirror current sink, etc. Compute  $A_{dm}$  and  $CMRR$  for your circuit if  $K = 12 \text{ mA/V}^2$ ,  $|V_t| = 1.5 \text{ V}$ , and  $|V_A| = 180 \text{ V}$ . Set the total sink current to  $5.6 \text{ mA}$  and use E96 resistors. w/  $V_{DD} = \pm 12 \text{ V}$

$A_{dm} > 30 \text{ dB} \rightarrow$  better use active drain load

$CMRR > 60 \text{ dB} \rightarrow$  need cascode current mirror sink



Current sink:  $V_{GS} = \sqrt{\frac{I_D}{K}} + V_t = \sqrt{\frac{5.6}{12}} + 1.5 = 2.183 \text{ V}$  (12)

$R = \frac{|V_{SS}| - 2V_{GS}}{I_{REF}} = \frac{12 - 2 \cdot 2.183}{5.6} = 1.363 \text{ k}$  (12)

Use 1.37 k 1% (11)

to compute  $A_{dm}$ , need  $r_{op}$  of current mirror and  $r_{on}$  of diff pair; assumed equal.

$$\therefore r_o = \frac{|V_A|}{I_D} = \frac{180}{5.6/2} = 64.29 \text{ k}\Omega \quad (+2)$$

↑ per transistor in diff pair

$$g_m = 2\sqrt{K I_D} = 2\sqrt{12 \cdot \frac{5.6}{2}} = 11.59 \frac{\text{mA}}{\text{V}} \quad (+2)$$

$$\therefore A_{dm} \approx \frac{g_m r_o}{4} = \frac{11.59 \cdot 64.29}{4} = 186.3 \quad (+2)$$

$$\text{or } 45.4 \text{ dB} \quad (+1) > 30 \text{ dB} \quad (+1) \quad \checkmark$$

to compute CMRR, need  $r_{out}$  of current sink  
 - for cascode current mirror,  $r_{out} = g_m r_o^2$

$$g_m = 2\sqrt{K I_D} = 2\sqrt{12 \cdot 5.6} = 16.40 \text{ mA/V} \quad (+2)$$

$$r_o = \frac{|V_A|}{I_D} = \frac{180}{5.6} = 32.14 \text{ k}\Omega \quad (+2)$$

$$\text{then } r_{out} = 16.40 \cdot 32.14^2 = 16941 \text{ k}\Omega \quad (+2)$$

$$\text{or } 16.94 \text{ M}\Omega$$

$$\rightarrow \text{CMRR} = g_m^{\text{of diff pair!}} r_{out} = 11.59 \text{ m} \cdot 16.94 \text{ M} = 196345 \quad (+2)$$

$$\text{or } 106 \text{ dB} \quad (+1) > 60 \text{ dB} \quad (+1) \quad \checkmark$$