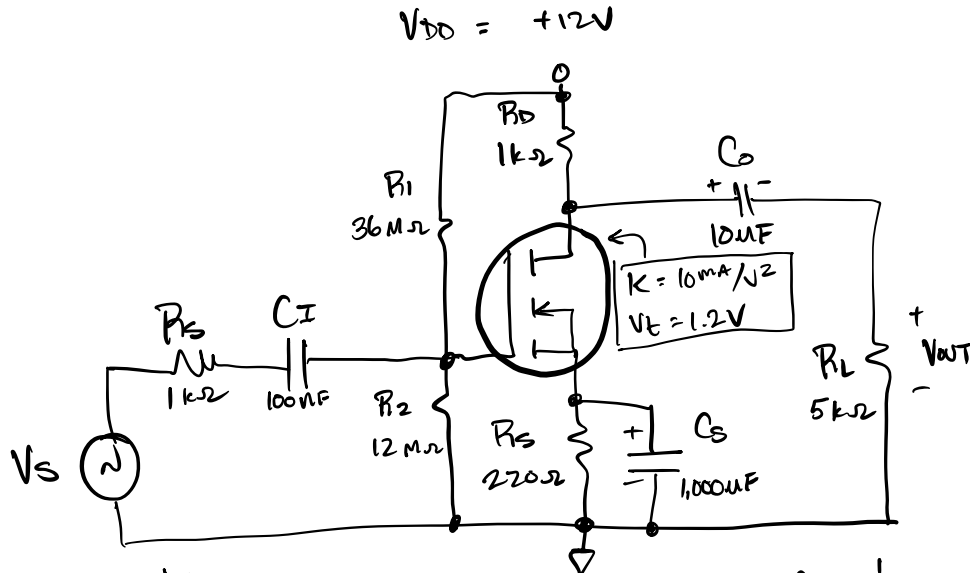


Common-Source Voltage Amplifier

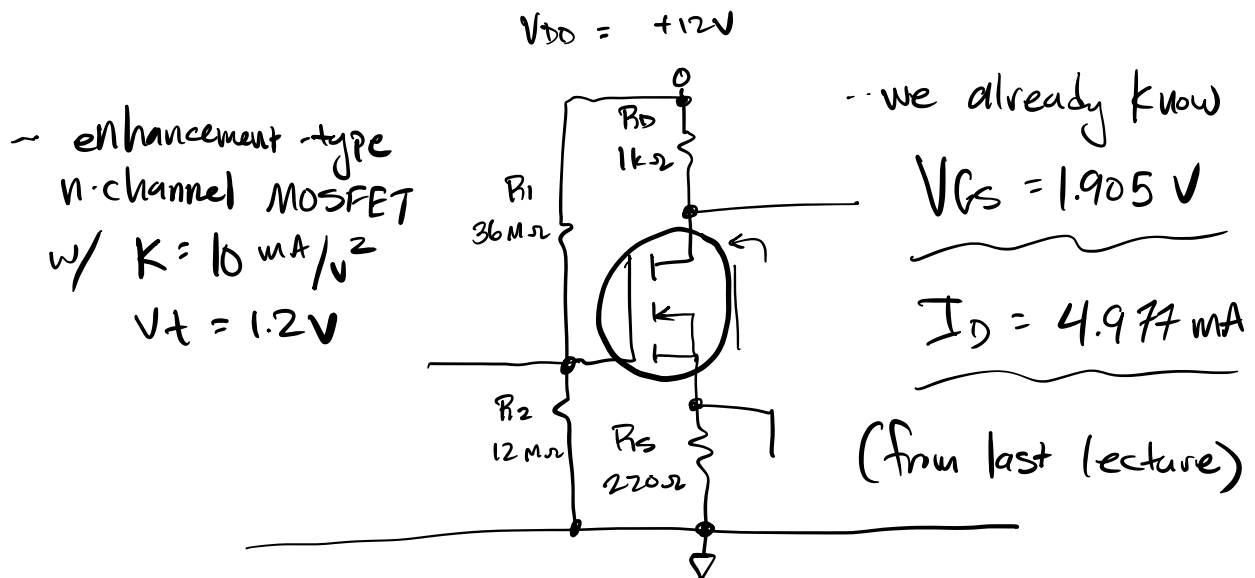


~ just like BJT common-emitter amplifier!

input: gate , output: drain , source is "grounded" by C_S .

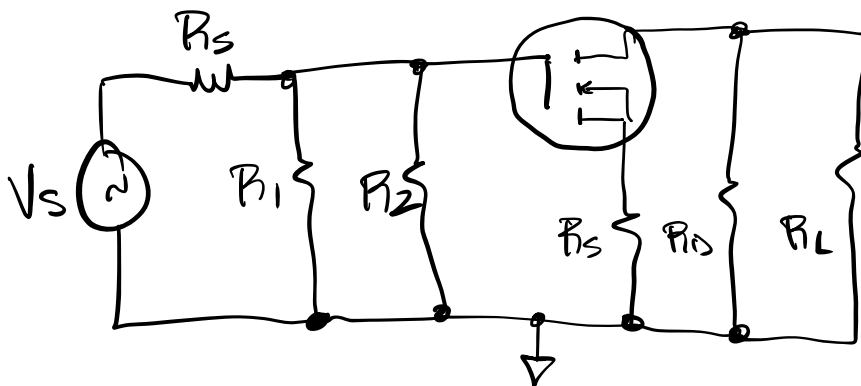
~ First, let's consider the DC circuit and perform DC analysis

~ capacitors are considered open circuits!

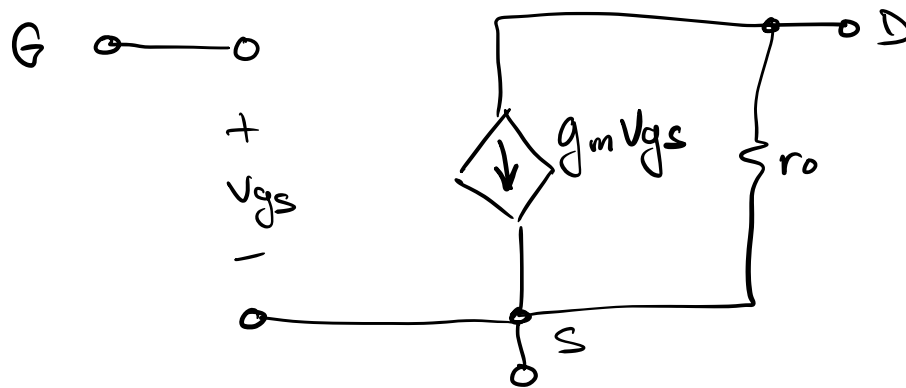


- .. next, we draw the mid-frequency AC circuit by considering capacitors as shorts, and V_{DD} becomes AC "ground."

MF AC Circuit :



- .. now we need a mid-frequency small-signal model for FET:



- .. doesn't this look familiar?

- .. there is one crucial difference .. no r_b (equivalent to small-signal base resistance r_b), because there is no gate current!

.. now we need equations for r_o and g_m :

$$r_o = \frac{|V_A|}{I_D} \leftarrow \text{yep, Early voltage!}$$

$$g_m = \frac{2\sqrt{I_D \cdot I_{DSS}}}{|V_{GS(off)}|} \quad \left[\text{JFET and depletion-MOSFET} \right]$$

$$g_m = 2\sqrt{K I_D} \quad \left[\text{enhancement MOSFET} \right]$$

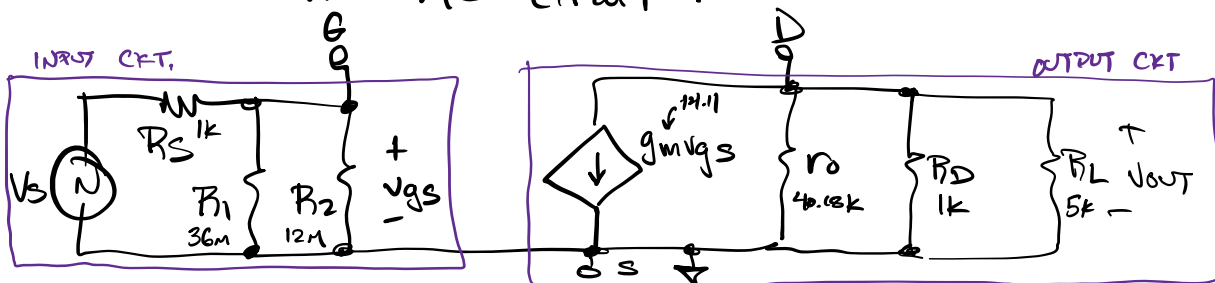
.. thus, for our example, assuming $V_A = 200V$ [typical]:

$$r_o = \frac{|V_A|}{I_D} = \frac{200}{4.977 \text{ mA}} = 40.18 \text{ k}\Omega$$

$$g_m = 2\sqrt{10 \cdot 4.977} = 14.11 \text{ mA/V} \leftarrow \text{low compared to BJTs!!! typical!!!}$$

$\sqrt{10 \text{ mA/V}^2 \cdot \text{mA}} = \text{mA/V}$

.. now let's combine the MF SSN with the MF AC circuit :



Input circuit:

-- just like BJT common-emitter configuration, define

$$R_G = R_1 \parallel R_2 = 36M \parallel 12M$$

$$\underline{R_G = 9 \text{ M}\Omega}$$

$$\text{thus, } V_{GS} = V_S \left(\frac{R_G}{R_G + R_S} \right)$$

$$\text{let } A_{v1} = \frac{V_{GS}}{V_S} = \frac{R_G}{R_G + R_S} = \frac{9M}{9M + 1k} = \underline{\underline{0.9999}}$$

... so basically 0dB!

-- Unlike the common-emitter amplifier, no significant voltage division at the input, thanks to no r_g , and high-resistance bias network!

Output circuit:

$$\text{define } \underline{R_D'} = R_D \parallel r_o = 1k \parallel 40.18k = \underline{\underline{0.9757k\Omega}}$$

$$\text{thus, } V_{out} = -g_m \cdot V_{GS} = -g_m (R_D' \parallel R_L)$$

$$\begin{aligned} \text{let } A_{v2} &= \frac{V_{out}}{V_{GS}} = -g_m (R_D' \parallel R_L) \rightarrow 0.8164k \\ &= -14.11 (0.9757 \parallel 5k) \end{aligned}$$

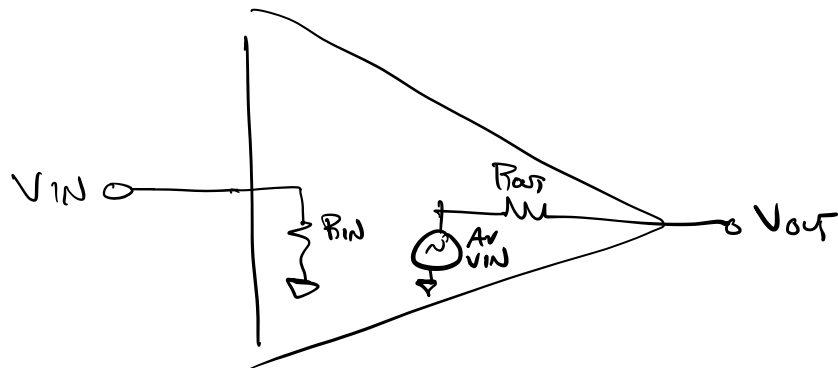
$$\underline{A_{v2} = -11.52} \quad \text{or} \quad \underline{21.23 \text{ dB}},$$

inverting

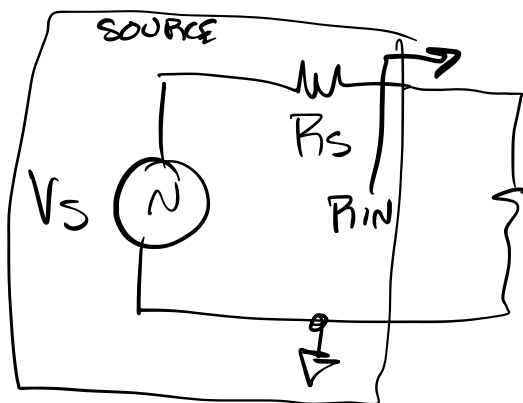
-- much lower gain than the BJT common-emitter examples!

Input and Output Resistances

remember :



-- looking into the input of the circuit from the perspective of V_S :



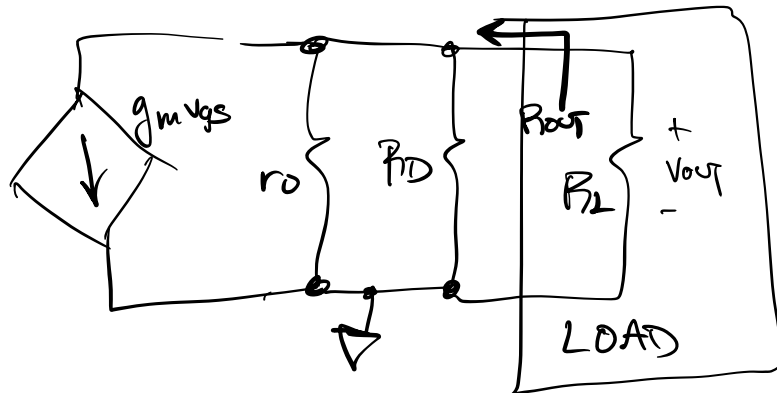
$$R_E = R_1 \parallel R_2$$

$$\underline{R_{IN} = R_E}$$

$$= 9 \text{ M}\Omega$$

-- much higher value than
common-emitter -- great!

-- looking into output from perspective of R_L :



$$\underline{R_{out} = R_D \parallel r_o = R_D' = 0.9757 \text{ k}\Omega}$$

-- this is about what we had with CE; not great.

-- So, in conclusion, common-source FET voltage amplifier is analogous in many ways to common-emitter BJT voltage amplifier, but offers much higher input resistance at the expense of lower gain.