

2/5/09

Autumn 03

Q2(a) $M(z) = \sum_{k=1}^{\infty} m(k) z^{-k}$

$$M(z) = m_1 z^{-1} + m_2 z^{-2} + \dots + m_n z^{-n} + m_n z^{-n-1} + \dots$$

Since $R(z) = 1 - z^{-1}$

$$\begin{aligned} \frac{M(z)}{R(z)} &= (1 - z^{-1})(m_1 z^{-1} + m_2 z^{-2} + \dots + m_n z^{-n} + m_n z^{-n-1} + \dots) \\ &= m_1 z^{-1} + (m_2 - m_1) z^{-2} + (m_3 - m_2) z^{-3} + (m_4 - m_3) z^{-4} \end{aligned}$$

$$\begin{aligned} \Rightarrow Q(z) &= \frac{M(z)}{R(z)} = z^{-1} + (-0.5 - 1) z^{-2} + (0.3 + 0.5) z^{-3} + (0.1 - 0.3) z^{-4} \\ &= z^{-1} - 1.5 z^{-2} + 0.8 z^{-3} - 0.2 z^{-4} \end{aligned}$$

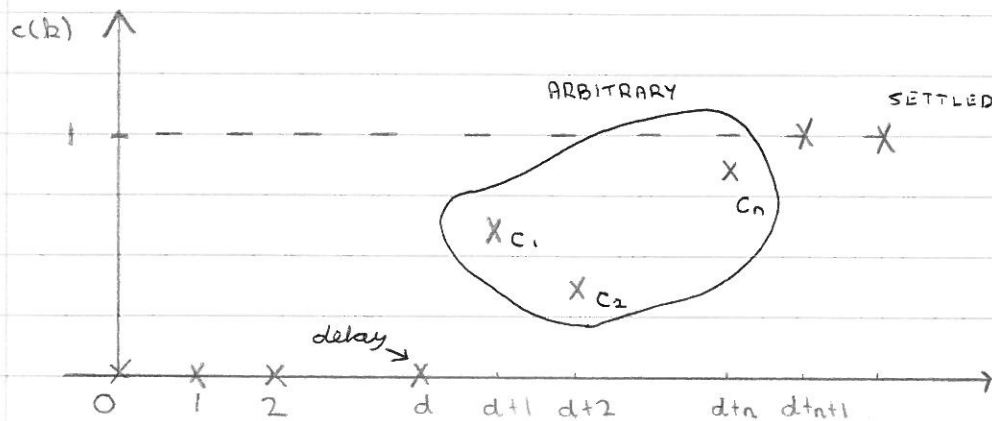
$$\begin{aligned} C(z) &= z^{-d} (c_1 z^{-1} + c_2 z^{-2} + \dots + c_n z^{-n} + z^{-n-1} + \dots) \\ \frac{C(z)}{R(z)} &= (1 - z^{-1}) z^{-d} (c_1 z^{-1} + c_2 z^{-2} + \dots + c_n z^{-n} + z^{-n-1} + \dots) \\ &= z^{-d} (c_1 z^{-1} + (c_2 - c_1) z^{-2} + (1 - c_n) z^{-n-1}) \end{aligned}$$

$$\Rightarrow P(z) = \frac{C(z)}{R(z)} = z^{-2} (0.4 z^{-1} + 0.4 z^{-2} - 0.3 z^{-3} + 0.1 z^{-4} + 0.1 z^{-5})$$

$$D(z) = \frac{Q(z)}{1 - P(z)} = \frac{z^{-1} - 1.5 z^{-2} + 0.8 z^{-3} - 0.2 z^{-4}}{1 - z^{-2} (0.4 z^{-1} + 0.4 z^{-2} - 0.3 z^{-3} + 0.1 z^{-4} + 0.1 z^{-5})}$$

Q2(a). Specify $D(z)$ to achieve the following for a unit step in $r(k)$

(i) Output $c(k)$ will settle to a steady-state of 1 within $(n+d+1)$ samples



Taking Z transform of the sequence $c(k)$

$$C(z) = \sum_{k=0}^{\infty} c(k) z^{-k}$$

$$\Rightarrow C(z) = z^{-d} (c_1 z^{-1} + c_2 z^{-2} + \dots + c_n z^{-n} + z^{-n-1} + z^{-n-2} \dots)$$

Since $R(z) = \frac{1}{1-z^{-1}}$ (unit step)

Then we can specify the desired step response $\frac{C(z)}{R(z)}$ as:

$$\begin{aligned} \frac{C(z)}{R(z)} &= (1-z^{-1}) z^{-d} (c_1 z^{-1} + c_2 z^{-2} + \dots + c_n z^{-n} + z^{-n-1} + z^{-n-2} \dots) \\ &= z^{-d} (c_1 z^{-1} + (c_2 - c_1) z^{-2} + \dots + (c_n - c_{n-1}) z^{-n} + (1 - c_n) z^{-n-1} + (1-1) z^{-n-2} \dots) \\ &= z^{-d} (c_1 z^{-1} + (c_2 - c_1) z^{-2} + \dots + (1 - c_n) z^{-n-1}) \end{aligned}$$

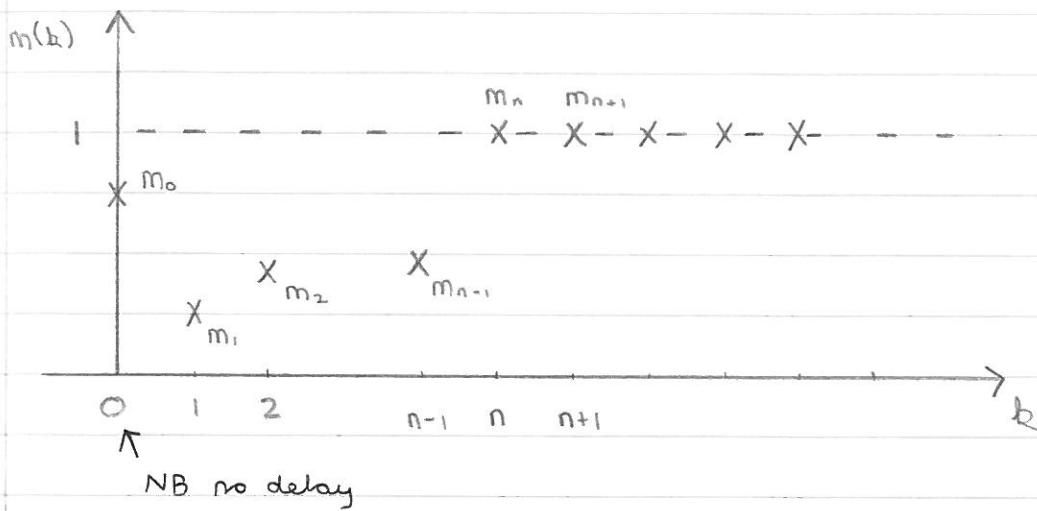
We then define

$$\frac{C(z)}{R(z)} = P(z) = z^{-d} (p_1 z^{-1} + p_2 z^{-2} + \dots + p_n z^{-n} + p_{n+1} z^{-(n+1)})$$

Note the constraint DC gain = 1

$$\Rightarrow \sum_{i=1}^{n+1} p_i = 1$$

(ii) The controller output $m(k)$ will settle to a steady state value within n samples



Taking Z transform of the sequence $m(k)$

$$M(z) = \sum_{k=0}^{\infty} m(k) z^{-k}$$

hence

$$M(z) = m_0 + m_1 z^{-1} + m_2 z^{-2} + \dots + m_{n-1} z^{-(n-1)} + m_n z^{-n} + m_{n+1} z^{-(n+1)} + \dots$$

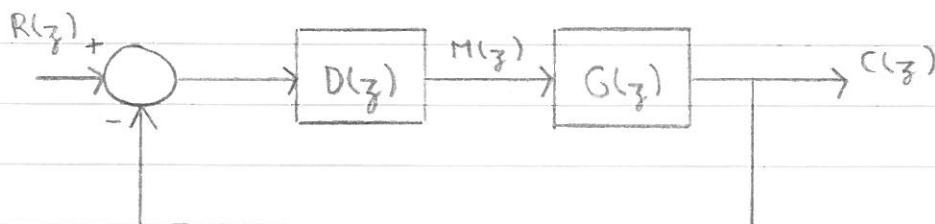
$$\text{Since } R(z) = \frac{1}{1-z^{-1}}$$

We can specify the desired controller

$$\begin{aligned} \frac{M(z)}{R(z)} &= (1-z^{-1}) (m_0 + m_1 z^{-1} + m_2 z^{-2} + \dots + m_{n-1} z^{-(n-1)} + m_n z^{-n} + m_{n+1} z^{-(n+1)} + \dots) \\ &= m_0 + (m_1 - m_0) z^{-1} + (m_2 - m_1) z^{-2} + \dots + (m_n - m_{n-1}) z^{-n} + (m_{n+1} - m_n) z^{-(n+1)} + \dots \\ &= m_0 + (m_1 - m_0) z^{-1} + \dots + (m_n - m_{n-1}) z^{-n} \end{aligned}$$

$$\frac{M(z)}{R(z)} = Q(z) = q_0 + q_1 z^{-1} + \dots + q_n z^{-n}$$

Consider the closed loop diagram



Then we can say

$$G(z) = \frac{z^{-d} (b_1 z^{-1} + b_2 z^{-2} + \dots + b_m z^{-m})}{1 - a_1 z^{-1} - a_2 z^{-2} - \dots - a_n z^{-n}} = \frac{C(z)}{M(z)} = \frac{\frac{C(z)}{R(z)}}{\frac{M(z)}{R(z)}} = \frac{P(z)}{Q(z)}$$

Since $P(z)$ is arbitrary, then why not specify it as

$$P(z) = \frac{z^{-d}(b_1 z^{-1} + b_2 z^{-2} + \dots + b_m z^{-m})}{b_1 + b_2 + \dots + b_m}$$

Then this choice of $P(z)$ forces the following choice of $Q(z)$

$$Q(z) = \frac{1 - a_1 z^{-1} - a_2 z^{-2} \dots - a_n z^{-n}}{b_1 + b_2 + \dots + b_m}$$

$$D(z) = \frac{1}{G(z)} \frac{\frac{C(z)}{R(z)}}{1 - \frac{C(z)}{R(z)}} = \frac{Q(z)}{1 - P(z)}$$

$$\Rightarrow D(z) = \frac{1 - a_1 z^{-1} - a_2 z^{-2} \dots - a_n z^{-n}}{1 - z^{-d}(b_1 z^{-1} + b_2 z^{-2} + \dots + b_m z^{-m})}$$

$$\sum P_i = 1$$

$$\Rightarrow D(z) = \frac{1 - a_1 z^{-1} - a_2 z^{-2} \dots - a_n z^{-n}}{(b_1 + b_2 + b_3 + \dots + b_m) - z^{-d}(b_1 z^{-1} + b_2 z^{-2} \dots + b_m z^{-m})}$$

$$= \frac{1 - a_1 z^{-1} - a_2 z^{-2} \dots - a_n z^{-n}}{\sum_{j=1}^m b_j - \sum_{j=1}^m b_j \sum_{i=1}^m z^{-d-j}}$$

$$= \frac{1 - \sum_{i=1}^n a_i z^{-i}}{\sum_{j=1}^m b_j (1 - z^{-d-j})}$$

Benefit

- eliminates ringing

Drawback

- if poles of $G(z)$ are outside unit circle, small errors in representing $G(z)$ poles will exponentially increase
- \Rightarrow closed loop process is unstable

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Q6a. $\frac{d}{dt} \underline{x}(t) = A \underline{x}(t) + B u(t) + E d(t)$
 $s \underline{X}(s) - \underline{x}(0) = A \underline{X}(s) + B U(s) + E D(s)$
 $(sI - A) \underline{X}(s) = B U(s) + E D(s) + \underline{x}(0)$
 $\underline{X}(s) = (sI - A)^{-1} (B U(s) + E D(s) + \underline{x}(0))$

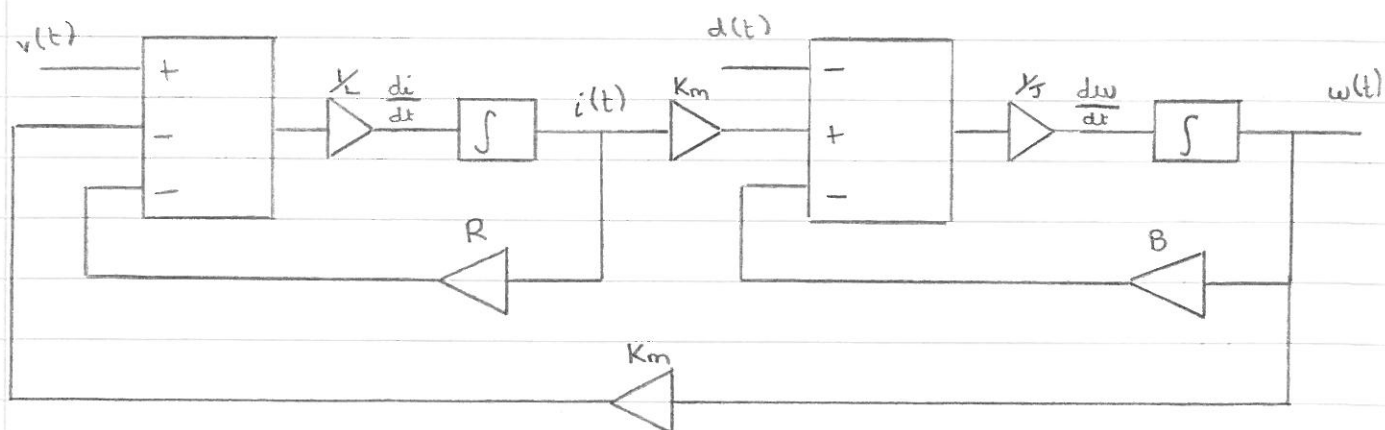
Let $(sI - A)^{-1} = \Phi(s)$
 $\underline{X}(s) = \Phi(s) \underline{x}(0) + \Phi(s) (B U(s) + E D(s))$
 $\underline{x}(t) = \Phi(t) \underline{x}(0) + \Phi(t) \otimes (B u(t) + E d(t))$
 $\underline{x}(t) = \Phi(t) \underline{x}(0) + \int_0^t \Phi(t-\tau) (B u(\tau) + E d(\tau)) d\tau$

(b) $I(s) = \frac{V(s) - K_m \Omega(s)}{Ls + R}$

$Ls I(s) + R I(s) = V(s) - K_m \Omega(s)$
 $L \frac{di}{dt} + R i(t) = v(t) - K_m \omega(t)$
 $\frac{di}{dt} = \frac{1}{L} (v(t) - K_m \omega(t) - R i(t))$

$\Omega(s) = \frac{K_m I(s) - D(s)}{Js + B}$

$Js \Omega(s) + B \Omega(s) = K_m I(s) - D(s)$
 $J \frac{d\omega}{dt} + B \omega(t) = K_m i(t) - d(t)$
 $\frac{d\omega}{dt} = \frac{1}{J} (K_m i(t) - B \omega(t) - d(t))$



$$\frac{d}{dt} \begin{bmatrix} \omega \\ i \end{bmatrix} = \begin{bmatrix} -\frac{B}{J} & \frac{K_m}{J} \\ -\frac{K_m}{L} & -\frac{R}{L} \end{bmatrix} \begin{bmatrix} \omega \\ i \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{L} \end{bmatrix} v + \begin{bmatrix} -\frac{1}{J} \\ 0 \end{bmatrix} d$$

(ii)