

ME5005/ME4002 DESIGN FOR MANUFACTURE PRODUCTION ENGINEERING

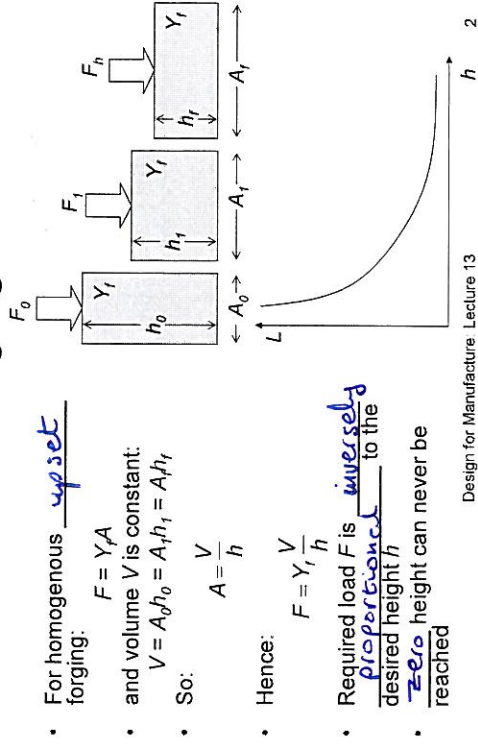
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Lecture 13: Design for Forging

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General forging loads



Web loading considerations

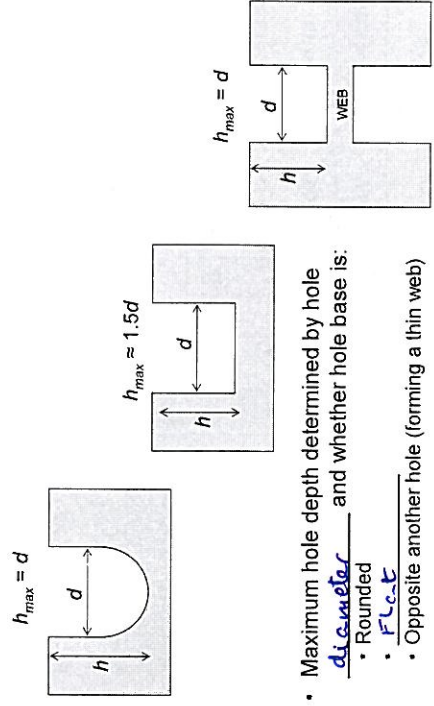
- Forging components with very thin webs requires:
 - Very high loads
 - increasing inversely proportional to web thickness
 - Special forging techniques (e.g. coining)
- Webs or thin areas parallel to the parting line are limited by:
 - Die geometry
 - Forging load and material flow
- Minimum and preferred thicknesses depending on plan area of web

Plan area (cm ²)	Minimum thickness (mm)	Preferred thickness (mm)
20	4	7
100	5	11
200	7	13
500	8	16
1000	10	18

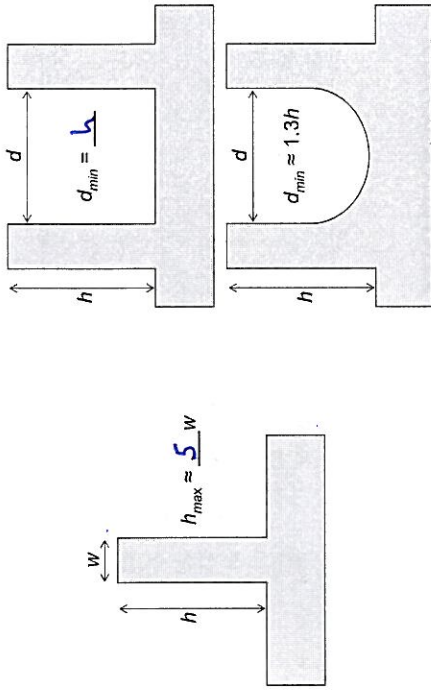
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Forging blind holes



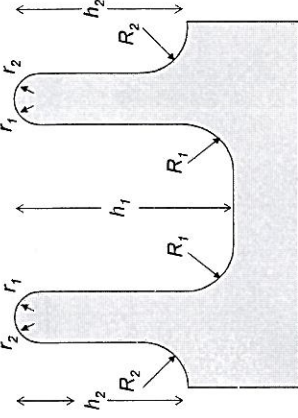
Forging ribs



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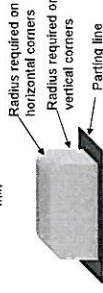
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Radiusing corners for forging



$r = 0.07h$	recommended
$r_{min} = 0.04h$	minimum
$R = 0.25h$	recommended
$R_{min} = 0.17h$	minimum

To compromise, use
 $R_{min} = 0.25h$ recommended

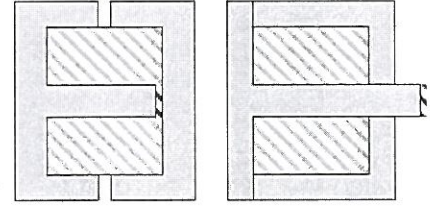


- All corners running parallel or perpendicular to the forming direction will require radiusing

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Forging through holes

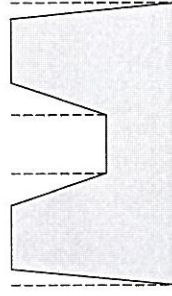


- Holes are not usually forged in a single operation
 - As hole is forged, a thin web is produced at the base of the hole
 - Thin webs require excessive loads, cannot forge to zero thickness
 - Large hole diameters will leave thicker webs as greater loads required
 - High stresses in the die cores
- Holes formed in two separate stages requiring different dies:
 - Create main shape
 - Punch through thin web in a second operation
- Forged holes mean extra dies
 - Increase in component cost
- Consider post-machining operation

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Draft angles



	INTERNAL	EXTERNAL
HAMMER	7° - 10°	5° - 7°
PRESS	3° - 5°	2° - 3°

- All surfaces perpendicular to parting lines will require draft angles
- Internal angles higher than external
 - Forged component recovers elastically when load is removed and grips any cores in the die
- Draft angles for presses are lower than for hammers
 - Hammer impacts are initially high energy and force the component onto the die
 - Presses have a continuous average load
- Forged component may be held in top part of die if top surface draft angles are reduced by $\frac{0.5^\circ}{1} - \frac{1}{1}$
 - Facilitates component removal

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Forging plant size

- Presses (hydraulic) preferred when large deformation of material is required
 - Apply a load without an impact
 - Load may be maintained continuously over the stroke length
 - Small: ~ 100 tonnes: €0.25M
 - Medium: ~ 500-1,000 tonnes: €1.0M
 - Large: ~ 5,000-10,000 tonnes: €5.0M - €10.0M
- Hammers preferred when large area thin sections are required
 - Apply a load utilizing an impact (kinetic energy)
 - Loads vary as the kinetic energy is used up
 - Load depends on the rate of deceleration
 - Small: ~ 500 m.kg
 - Medium: ~ 5,000 m.kg
 - Large: ~ 50,000 m.kg

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Estimate press loads

- Methods not accurate enough to guarantee a press working if near its maximum load
 - Gives an indication of plant size and cost
- For impression dies (most common):
 - Calculate the plan area A
 - Estimate flash loads
 - General rule of add 10% all the way around
 - Quick method - multiply plan area by $1.2 \times 1.2 = 1.44$
 - Estimate maximum true strain: $\epsilon = \ln(h_0/h_f)$
 - Estimate maximum flow stress: $Y_f = K\epsilon^n$
 - Estimate shape factor: $K_f = 6.0, 8.0$ or 10.0 (simple \rightarrow complex)
 - Use: $F = K_f Y A$
 - Include scaling factors for:
 - Aluminium: x 0.9 Stainless Steel: x 1.8 Titanium alloy: x 2.5
 - 20% increase in forging temperature: x 0.8

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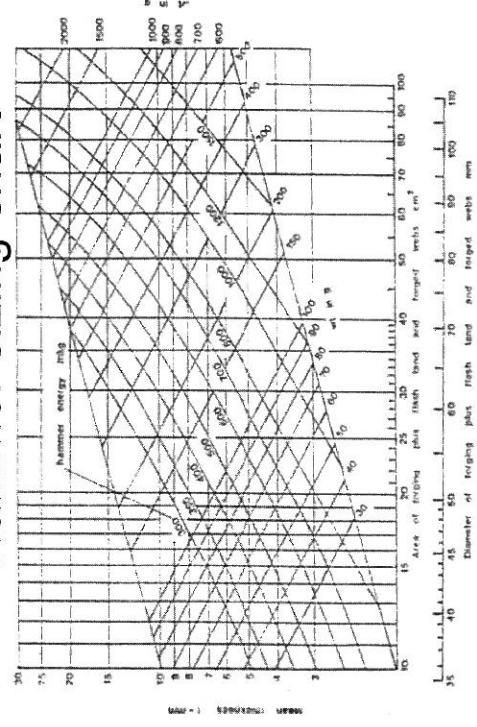
Estimate hammer energy

- Estimates more accurate but more complex
- Really requires die design and layout, but most parameters can be estimated
 - Calculate the component plan area A
 - Estimate flash load area
 - General rule of add 10% all the way around
 - Quick method - multiply plan area by 0.44
 - Calculate total plan area $A + A_{flash}$
 - Calculate the component volume V
 - Estimate flash volume using a flash thickness of 5 mm
 - Calculate total volume $V + V_{flash}$
 - Calculate mean thickness $t = \text{total volume/total area}$
 - Use a hammer sizing chart
 - Different charts exist for different materials and hammer sizes

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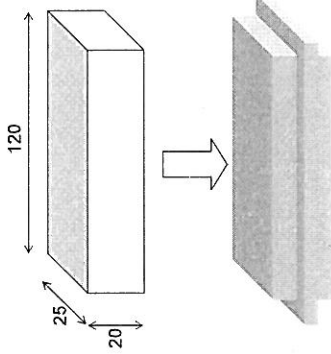
Hammer sizing chart



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Hammer sizing example #1

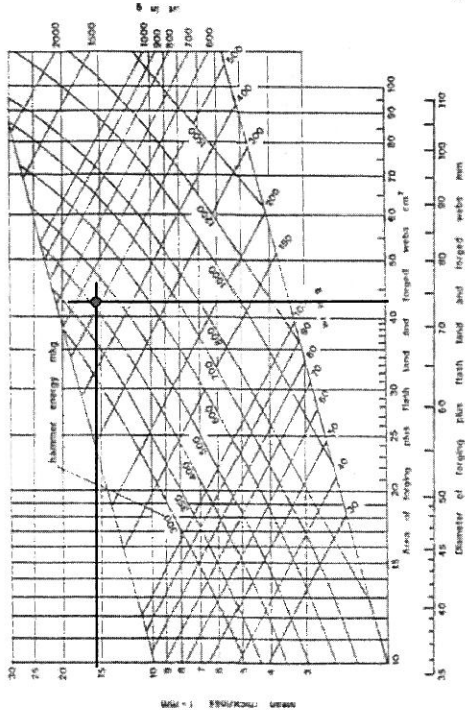
- Plan area: $120 \times 25 = 3,000 \text{ mm}^2$
- Flash area: $3,000 \times 0.44 = 1,320 \text{ mm}^2$
- Total plan area: $4,320 \text{ mm}^2 = 43.2 \text{ cm}^2$
- Component volume = $20 \times 3,000 = 60,000 \text{ mm}^3$
- Flash volume: $1,320 \times 5 = 6,600 \text{ mm}^3$
- Total volume: $60,000 + 6,600 = 66,600 \text{ mm}^3$
- Mean thickness = $66,600 / 4,320 = 15.42 \text{ mm}$
- Use chart
- Hammer energy = ??? m.kg



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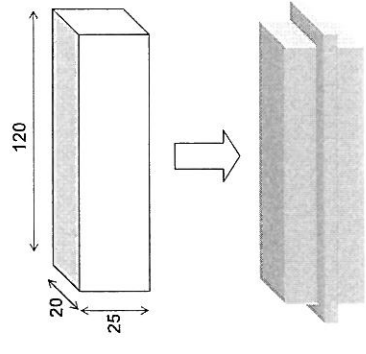
Hammer sizing chart



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Hammer sizing example #2

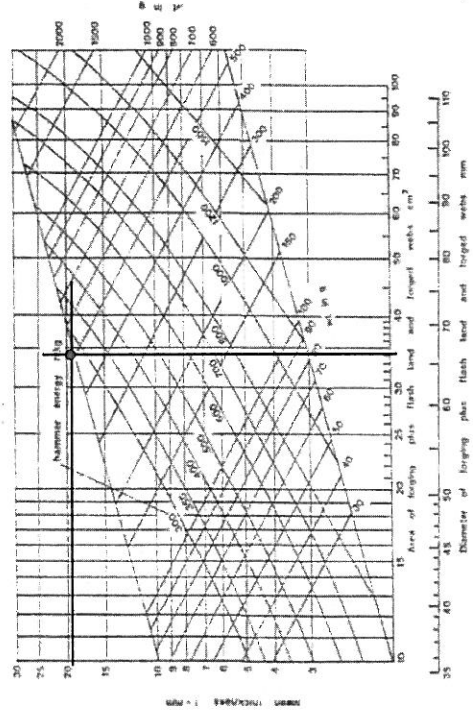
- Plan area: $120 \times 20 = 2,400 \text{ mm}^2$
- Flash area: $2,400 \times 0.44 = 1,056 \text{ mm}^2$
- Total plan area: $3,456 \text{ mm}^2 = 34.6 \text{ cm}^2$
- Component volume = $25 \times 2,400 = 60,000 \text{ mm}^3$
- Flash volume: $1,056 \times 5 = 5,280 \text{ mm}^3$
- Total volume: $60,000 + 5,280 = 65,280 \text{ mm}^3$
- Mean thickness = $65,280 / 3,456 = 18.89 \text{ mm}$
- Use chart
- Hammer energy = ??? m.kg



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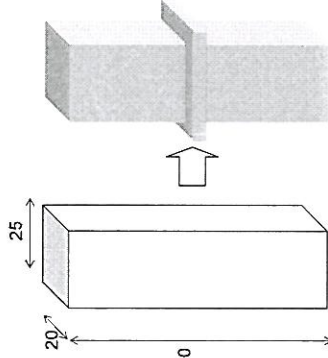
Hammer sizing chart



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Hammer sizing example #3

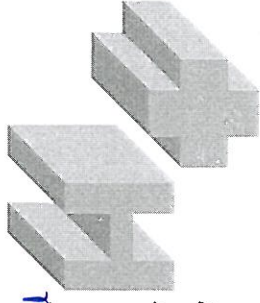
- Plan area: $25 \times 20 = 500\text{mm}^2$
- Flash area: $500 \times 0.44 = 220\text{mm}^2$
- Total plan area: $720\text{mm}^2 = 7.2\text{cm}^2$
- Component volume = $120 \times 500 = 60,000\text{mm}^3$
- Flash volume: $220 \times 5 = 1,100\text{mm}^3$
- Total volume: $60,000 + 1,100 = 61,100\text{mm}^3$
- Mean thickness = $61,100/720 = 84.9\text{mm}$
- Use chart
- Hammer energy = ???m.kg
- Plan area and mean thickness are not on the chart!!



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Component orientation



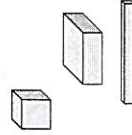
- Component orientation in the dies is vital when sizing forging plant
 - plan area is the surface area perpendicular to the forging load
- Example 3 is impossible to forge
 - Material must deform before perpendicular to the parting line
 - Flash lands will not be able to fill the cavity
- Example 2 is uncertain
 - Required hammer energy is on the boundary of the sizing chart
 - Insufficient accuracy to guarantee hammer size required
- Example 1 requires a 500m.kg hammer
- Shape and component complexity not considered, e.g.: holes
 - Same plan area A
 - Same volume V
 - Same flash area, volume and mean thickness t
 - 'H' section harder to forge than '+' section

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Estimate starting shape

- Choice of the correct pre-formed workpiece can simplify forging design
 - Try and minimise amount of deformation required
- Semi-finished pre-forms are standard:
 - Bars/rods (round, square, hexagonal), slab, plate, bloom
- Check overall dimensions of desired component:
 - If 3 axes are roughly equal:
 - Use bar, slab or plate
 - If 2 axes are larger than the other:
 - Use plate or slab
 - If 1 axis larger than the others:
 - Use rod or bar
- For significant deformation, starting shape not critical
 - e.g. round bar or square bar?



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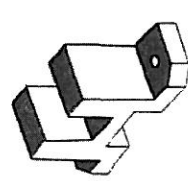
Component redesign

- Estimate starting shape of pre-formed workpiece
- Eliminate impossible geometry that cannot be forged
- Select suitable parting line(s) to avoid die kick
- Check suitability of individual features and redesign:
 - Ribs, webs, slots, holes
- Radius corners that require it (parallel to parting line)
- Check draft: internal, external, top/bottom die
- Check orientation of component in the dies
- Hammer or press?
 - May depend on orientation
- Estimate hammer/press size
- Re-check!

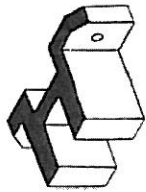
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Self-study exercise



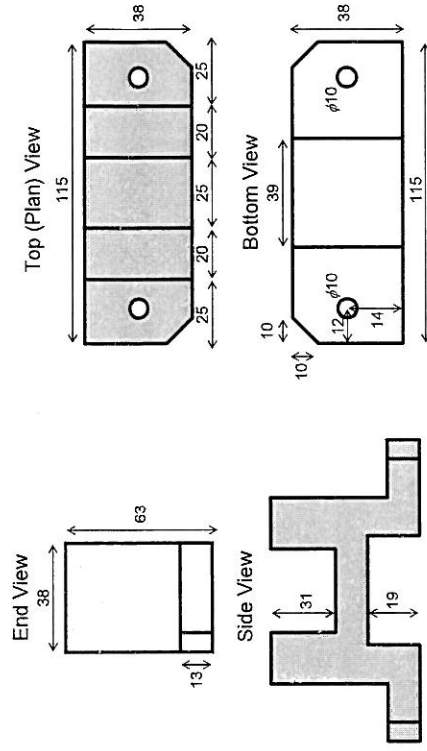
- Top slot of bracket holds edge of a large rectangular plate in a specific position
- Base slot fits over a guide rail
- No movement allowed between plate and clamp in *any* direction
- Bolt hole locations and chamfered corners locate with other geometry
- No cosmetic surfaces
- Increase in strength required
- Redesign for forging in aluminium alloy using:
 1. A hammer
 2. A hydraulic press
- Discuss the suitability for forging in *either* of the two orientations shown
 - Shaded surfaces give plan area



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Bracket dimensions (mm)



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