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**THE NATIONAL UNIVERSITY OF IRELAND, CORK**

**COLÁISTE NA hOLLSCOILE, CORCAIGH**  
**UNIVERSITY COLLEGE, CORK**

**SAMPLE PAPER – MARCH 2004**

**B. E. (ELECTRICAL & ELECTRONIC)**  
**B.E. (MICROELECTRONIC)**  
**M.ENG.SC. (MICROELECTRONIC)**  
**H.DIP. (MICROELECTRONIC)**

**RFIC DESIGN**  
**EE4011**

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Time allowed: 3 hours

Answer five questions

All questions carry equal marks.  
The use of a Casio fx570w or fx570ms calculator is permitted.  
Smith Charts are available on request.

1. (a) Show a small-signal model of a MOS transistor suitable for first-order analysis and from this derive an expression for the cut-off frequency of a MOS transistor. Assume the transistor is biased in saturation and that the current can be approximated by:

$$I_{DS} = \frac{1}{2} \frac{W}{L} \mu C_{OX} (V_{GS} - V_{TH})^2 (1 + \lambda V_{DS})$$

where the symbols have their usual meaning. Also assume that the only capacitance to be considered is the gate-source capacitance.

[10 marks]

- (b) A MOS transistor is biased in saturation and configured as a common-source two-port amplifier with the input applied to the gate (port 1) and the output taken from the drain (port 2). Determine the transistor cut-off frequency. Also determine the 4 two-port y-parameters at a frequency of 1GHz. The following bias conditions and device parameters should be used:

$W=10\mu\text{m}$ ,  $L=0.25\mu\text{m}$ ,  $T_{ox}=4\text{nm}$ ,  $\mu=400\text{cm}^2/\text{Vs}$ ,  $V_{GS}=2.5\text{V}$ ,  $V_{TH}=0.5\text{V}$ ,  
 $\lambda=0.1\text{ V}^{-1}$ .

[10 marks]

2. (a) Derive an expression for the noise figure of a two-port network driven by a source with impedance  $R_S$ . Assume that the two-port can be represented by a noiseless two-port with equivalent input-referred noise voltage and current sources.

[10 marks]

- (b) The equivalent input referred noise voltage and current sources of a bipolar transistor at moderate frequencies are given by:

$$\overline{v^2} = 4kT \left( r_b + \frac{1}{2g_m} \right) \Delta f \quad \overline{i^2} = 2q \frac{I_C}{\beta_f} \Delta f$$

where the symbols have their usual meaning and  $r_b$  is the parasitic base resistance.

A BJT is biased in the forward active region with a collector current,  $I_C = 1\text{mA}$  at 300K. It has a forward active current gain of 100 and a parasitic base resistance of  $50\Omega$ . Determine the noise figure for a bandwidth of 1Hz if it is driven by a source with the following impedances: (i)  $10\Omega$ , (ii)  $100\Omega$ , (iii)  $1000\Omega$ .

Make a rough estimate of the optimum source impedance to give the lowest noise figure.

[10 marks]

3. (a) Determine an expression for the 1dB compression point (P1dB) of an amplifier which can be described by the following equation:

$$y(t) = \alpha_1 x(t) + \alpha_3 x^3(t)$$

where  $x(t)$  and  $y(t)$  are the amplifier input and output waveforms respectively.

[10 marks]

- (b) For the amplifier described in part (a), determine the input amplitude corresponding to the 1dB compression point if  $\alpha_1 = 10$  and  $\alpha_3 = 0.1$ .

[5 marks]

- (c) An RF amplifier is supplied with <sup>two</sup> ~~an~~ input signal <sup>with</sup> power of 0dBm. The output power at the fundamental frequency is 20dBm and the output power ~~at the third harmonic~~ <sup>of the 3rd</sup> is -10dBm. Determine by graphical means or otherwise the input third-order intercept point (input IP3).

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[5 marks]

4. Outline the design procedure used when designing a microwave amplifier for maximum gain.

[8 marks]

A microwave junction transistor has the following characteristics (at 5 GHz with 50 ohm reference);

$$S_{11} = 0.5 \angle -145^\circ$$

$$S_{12} = 0.05 \angle 25^\circ$$

$$S_{21} = 2.75 \angle 190^\circ$$

$$S_{22} = 0.5 \angle -40^\circ$$

Check the stability of the device and design input and output matching networks for maximum power gain.

[12 marks]

5. (a) What do you understand by the “unilateral figure of merit” of a high-frequency amplifier?  
[8 marks]
- (b) Discuss the issue of “image frequencies” in RFIC transceiver design and the resulting effects on choice of topology.  
[12 marks]
6. (a) Illustrate a suitable topology for VCO based on the “negative- $g_m$ ” concept using MOSFETs.  
[5 marks]
- (b) An LC-based negative- $g_m$  oscillator uses an on-chip inductor of 3nH and has a parasitic capacitance of 1pF at the output nodes. If a diode with a  $M_j=0.5$  and  $V_j=0.8V$  is available, determine which value of the zero-biased capacitance is needed to ensure a minimum oscillation frequency of 1.8GHz from the VCO. Also determine what reverse bias is needed on the diodes if an operation frequency of 2GHz is desired.  
[10 marks]
- (c) Illustrate by means of suitable equations, the characteristic which primarily determines the linearity of the output frequency-control voltage relationship in varactor-diode based VCOs and suggest a diode structure which would give an ideal linear frequency-voltage relationship.  
[5 marks]
7. (a) Show a block diagram for a Type I Phase Locked Loop (PLL) consisting of a phase detector, a low-pass filter, a voltage controlled oscillator and a feedback divider (M) and from this determine the closed-loop transfer function of the Type I PLL.  
[10 marks]
- (b) Determine the damping-factor and the natural frequency of a Type I PLL with the following characteristics:  
 $K_{VCO}=100\text{MHz/V}$ ,  $K_{PD}=1\text{ V/rad}$ ,  $f_{LPF}=1\text{MHz}$ ,  $M=1000$ .  
[10 marks]