

Note the following equations:

$$\vec{i}_s = \frac{3}{2} \sqrt{2} I_s \angle \theta_{Is} = \sqrt{\frac{3}{2}} (i_{sd} + j i_{sq})$$

$$\vec{\lambda}_r(t) = -L_r \vec{i}_r(t) + L_m \vec{i}_s(t)$$

$$\lambda_{rq} = 0 \text{ and steady state } \Rightarrow T_{em} = \frac{P}{2} \lambda_{rd} i_{rq}, \omega_{slip} = \frac{2}{P} \frac{R_r i_{rq}}{\lambda_{rd}}, i_{sq} = \frac{L_r}{L_m} i_{rq}, i_{sd} = \frac{\lambda_{rd}}{L_m}$$

$$\begin{pmatrix} i_a(t) \\ i_b(t) \\ i_c(t) \end{pmatrix} = \sqrt{\frac{2}{3}} \begin{pmatrix} \cos \theta_{da} & -\sin \theta_{da} \\ \cos(\theta_{da} + 240^\circ) & -\sin(\theta_{da} + 240^\circ) \\ \cos(\theta_{da} + 120^\circ) & -\sin(\theta_{da} + 120^\circ) \end{pmatrix} \begin{pmatrix} i_{sd} \\ i_{sq} \end{pmatrix}$$

$$\theta_{da} = \omega t + \theta_{\lambda_r}$$

#### Problem 1

A four-pole star-connected induction motor used in a servo application has the following per-phase equivalent circuit parameters:

$$R_S = 20 \text{ m}\Omega, L_{LS} = 0.2 \text{ mH}, L_M = 7.2 \text{ mH}, L_{LR}' = 0.3 \text{ mH}, \text{ and } R_R' = 35 \text{ m}\Omega.$$

At the rated condition of 400 V line-line, 50 Hz, the machine pulls 225 A at a lagging power factor of 0.841. At time  $t = 0$ , the machine is in steady state.

- Taking the per-phase input voltage as the reference, calculate the per-phase rotor current phasor and the per-phase rotor flux-linkage phasor.
- Align the  $d$ -axis with the rotating rotor flux linkage state vector and calculate the rotor current and the rotor flux-linkage space vectors.
- Calculate  $\lambda_{rd}$  and  $i_{rq}$  and the resulting electromagnetic torque and slip and input currents  $i_{sd}$  and  $i_{sq}$ .
- Calculate the three phase currents at time  $t = 0$ .
- Calculate the three phase currents at  $t = 5 \text{ ms}$ .

$$\vec{V}_s = 230.9 \angle 0^\circ \text{ V}, \vec{I}_r = 195 \angle -7.3^\circ \text{ A}; \vec{\lambda}_r = 0.697 \angle -97.3^\circ \text{ Wb-turns}$$

$$\vec{i}_r^d = 413.6 \angle 90^\circ \text{ A}; \vec{\lambda}_r^d = 1.478 \angle 0^\circ \text{ Wb-turns}$$

$$\lambda_{rd} = 1.207 \text{ Wb-turns}; i_{rq} = 337.7 \text{ A}; T_{em} = 815.3 \text{ Nm}; s = 3.1\%; i_{sd} = 167.7 \text{ A}; i_{sq} = 351.8 \text{ A}$$

$$i_a(0) = 267.6 \text{ A}; i_b(0) = -282.9 \text{ A}; i_c(0) = +15.3 \text{ A}$$

$$i_a(5 \text{ ms}) = 172.2 \text{ A}; i_b(5 \text{ ms}) = 145.7 \text{ A}; i_c(5 \text{ ms}) = -317.8 \text{ A}$$

#### Problem 2

A four-pole star-connected induction motor used in a servo application has the following per-phase equivalent circuit parameters:

$$R_S = 1.77 \text{ }\Omega, L_{LS} = 14 \text{ mH}, L_M = 369 \text{ mH}, L_{LR}' = 12 \text{ mH}, \text{ and } R_R' = 1.34 \text{ }\Omega.$$

At the rated condition of 460 V line-line, 60 Hz, the machine pulls 3.753 A at a lagging power factor of 0.822. At time  $t = 0$ , the machine is in steady state.

- Taking the per-phase input voltage as the reference, calculate the per-phase rotor current phasor and the per-phase rotor flux-linkage phasor.
- Align the  $d$ -axis with the rotating rotor flux linkage state vector and calculate the rotor current and the rotor flux-linkage space vectors.
- Calculate  $\lambda_{rd}$  and  $i_{rq}$  and the resulting electromagnetic torque and slip.
- Calculate the three phase currents at time  $t = 0$ .

Note the following equations:

$$\vec{V}_s = 265.6 \angle 0^\circ \text{ V}, \vec{I}_r = 3.19 \angle -6.2^\circ \text{ A}; \vec{\lambda}_r = 0.66 \angle -96.2^\circ \text{ A Wb-turns}$$

$$\vec{i}_r^d = 6.77 \angle 90^\circ \text{ A}; \vec{\lambda}_r^d = 1.4 \angle -0^\circ \text{ Wb-turns}$$

$$\lambda_{rd} = 1.144 \text{ Wb-turns}; i_{rq} = 5.53 \text{ A}; 12.65 \text{ Nm}; 1.72\%$$

$$i_a(0) = 4.362A; i_b(0) = -4.79A; i_c(0) = 0.44A$$

### Problem 3

Consider the Westinghouse 22 kW, 8-pole machine at the rated condition of 400 V line-line, 50 Hz with the following parameters.

$R_S = 0.432 \Omega$ ,  $L_{LS} = 2.8 \text{ mH}$ ,  $L_M = 73 \text{ mH}$ ,  $L_{LR} = 2.8 \text{ mH}$ , and  $R_R = 0.49 \Omega$ . Also include the core loss equivalent resistance  $R_c = 417 \Omega$ .

- Taking the per-phase input voltage as the reference, calculate the per-phase rotor current phasor and the per-phase rotor flux-linkage phasor.
- Align the  $d$ -axis with the rotating rotor flux linkage state vector and calculate the rotor current and the rotor flux-linkage space vectors.
- Calculate  $\lambda_{rd}$  and  $i_{rq}$  and the resulting electromagnetic torque and slip.
- Calculate the three phase currents at time  $t = 0$ .

Note the following equations:

$$\bar{V}_s = 400 \angle 0^\circ \text{ V}, \bar{I}_r = 19.8 \angle -1.1^\circ \text{ A}; \bar{\lambda}_r = 1.2 \angle -91.1^\circ \text{ A Wb-turns}$$

$$\bar{i}_r^d = 42 \angle 90^\circ \text{ A}; \bar{\lambda}_r^d = 2.54 \angle 0^\circ \text{ Wb-turns}$$

$$\lambda_{rd} = 2.07 \text{ Wb-turns}; i_{rq} = 34.3 \text{ A}; 284 \text{ Nm}; 2.6\%$$

$$i_a(0) = 28.6A; i_b(0) = -34.8A; i_c(0) = 6.2A$$

### Problem 4

Consider the Westinghouse 22 kW, 8-pole machine with 400 V (line-line), 50 Hz.

At the rated condition determine the following. For simplicity, approximate the machine model as having parallel magnetizing and rotor resistance branches only, and neglect losses.

- Taking the per-phase input voltage as the reference, calculate the per-phase rotor current phasor and the per-phase rotor flux-linkage phasor.
- Align the  $d$ -axis with the rotating rotor flux linkage state vector and calculate the rotor current and the rotor flux-linkage space vectors.
- Calculate  $\lambda_{rd}$  and  $i_{rq}$  and the resulting electromagnetic torque and slip.
- Calculate the three phase currents at time  $t = 0$ .

Note the following equations:

$$\bar{V}_s = 400 \angle 0^\circ \text{ V}, \bar{I}_r = 20.23 \angle 0^\circ \text{ A}; \bar{\lambda}_r = 1.273 \angle -90^\circ \text{ A Wb-turns}$$

$$\bar{i}_r^d = 42.9 \angle 90^\circ \text{ A}; \bar{\lambda}_r^d = 2.70 \angle 0^\circ \text{ Wb-turns}$$

$$\lambda_{rd} = 2.21 \text{ Wb-turns}; i_{rq} = 35.04 \text{ A}; 309.1 \text{ Nm}; 2.5\%$$

$$i_a(0) = 28.6A; i_b(0) = -34.8A; i_c(0) = 6.2A$$

### Problem 5

Consider the Westinghouse 22 kW, 8-pole machine with 400 V (line-line), 50 Hz.

At the rated condition, operating in generator mode, determine the following. For simplicity, approximate the machine model as having parallel magnetizing and rotor resistance branches only, and neglect losses.

- Taking the per-phase input voltage as the reference, calculate the per-phase rotor current phasor and the per-phase rotor flux-linkage phasor.
- Align the  $d$ -axis with the rotating rotor flux linkage state vector and calculate the rotor current and the rotor flux-linkage space vectors.
- Calculate  $\lambda_{rd}$  and  $i_{rq}$  and the resulting electromagnetic torque and slip.
- Calculate the three phase currents at time  $t = 0$ .

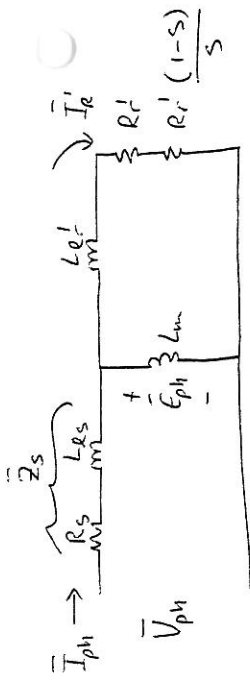
Note the following equations:

$$\bar{V}_s = 400 \angle 0^\circ \text{ V}, \bar{I}_r = 20.23 \angle 180^\circ \text{ A}; \bar{\lambda}_r = 1.273 \angle -90^\circ \text{ A Wb-turns}$$

$$\bar{i}_r^d = 42.91 \angle -90^\circ \text{ A}; \bar{\lambda}_r^d = 2.701 \angle 0^\circ \text{ Wb-turns}$$

$$\lambda_{rd} = 2.21 \text{ Wb-turns}; i_{rq} = -35.04 \text{ A}; -309.1 \text{ Nm}; -2.5\% \quad i_a(0) = -28.6A; i_b(0) = -6.2A; i_c(0) = 34.8A$$

Q1



$$R_s = 20 \text{ m}\Omega$$

$$R_r' = 35 \text{ m}\Omega$$

$$L_{es} = 0.2 \text{ mH}$$

$$L_{er}' = 0.3 \text{ mH} \quad L_m = 7.2 \text{ mH}$$

$$\Rightarrow L_s = 7.4 \text{ mH} \text{ and } L_r = L_m + L_{er}' = 7.5 \text{ mH}$$

$$@ 400 \text{ V, } f_e = 50 \text{ Hz}$$

$$I_{ph} = 225 \text{ A @ PF} = 0.841$$

$$V_{ph} = \frac{V_{LL}}{\sqrt{3}} = 230.9 \text{ V}$$

$$\text{PF} = 0.841 \Rightarrow \Theta = \cos^{-1} \text{PF} = -32.75^\circ$$

$$\Rightarrow \bar{I}_{ph} = 225 \angle -32.75^\circ \text{ A}$$

$$= (189.2 - j121.7) \text{ A}$$

$$\bar{Z}_s = \text{Stator Impedance}$$

$$= R_s + j\omega_e L_{es}$$

$$= (0.02 + j0.0628) \Omega$$

$$= 0.0659 \angle 72.3^\circ \Omega$$

$$\text{Let } \bar{V}_{zs} = \bar{Z}_s \cdot \bar{I}_{ph}$$

$$= (11.4 + j9.4) \text{ V}$$

$$\begin{aligned} \text{Back emf } \bar{E}_{ph} &= \bar{V} - \bar{V}_{zs} \\ &= (214.5 - j9.4) \text{ V} \\ &= 214.7 \angle -2.5^\circ \text{ V} \end{aligned}$$

$$\begin{aligned} \text{Let } \bar{I}_m &= \text{magnetizing current} \\ &= \frac{\bar{E}_{ph}}{j\omega_e L_m} = \frac{(214.5 - j9.4)}{j2\pi \cdot 50 \cdot 7.2 \times 10^{-3}} \text{ A} \end{aligned}$$

$$= -4.18 - j97.0 \text{ A}$$

$$= +97.0 \angle -92.5^\circ \text{ A}$$

Reflected rotor current

$$\bar{I}_R' = \bar{I}_{ph} - \bar{I}_m$$

$$= (193.4 - j24.7) \text{ A}$$

$$= 195 \angle -7.3^\circ \text{ A}$$

Rotor flux linkage

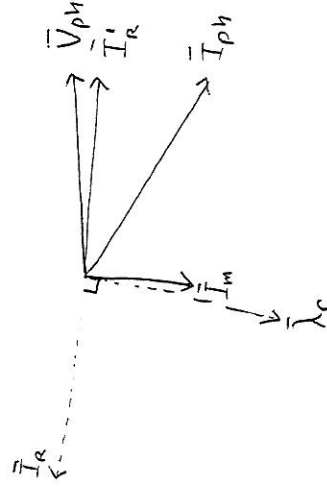
$$\bar{\lambda}_e = -L_r \bar{I}_R' + L_m \bar{I}_{ph}$$

$$= -7.5 \times 10^{-3} (193.4 - j24.7)$$

$$+ 7.2 \times 10^{-3} (189.2 - j121.7)$$

$$= (-0.088 - j0.69) \text{ Wb-turns}$$

$$= 0.697 \angle -97.3^\circ \text{ Wb-turns}$$



Space vectors @  $t=0$

$$\vec{\lambda}_r = \frac{3}{2} \sqrt{2} \hat{\lambda}_r \angle \theta_{\lambda_r}$$

$$= 1.478 \angle -97.3^\circ \text{ wb-turns}$$

Align d-axis with  $\vec{\lambda}_r$

$$\Rightarrow \vec{\lambda}_r^d = 1.478 \angle 0^\circ \text{ wb-turns}$$

$$\vec{I}_r' = \frac{3}{2} \sqrt{2} \hat{I}_r' \angle \theta_{I_r'}$$

$$= 413.6 \angle -7.3^\circ \text{ A}$$

$$\Rightarrow \vec{I}_r^{i,d} = 413.6 \angle +90^\circ \text{ A}$$

$$\vec{I}_{ph} = \frac{3}{2} \sqrt{2} \hat{I}_{ph} \angle \theta_r$$

$$= 477.3 \angle -32.75^\circ \text{ A}$$

$$\Rightarrow \vec{I}_{ph}^d = 477.3 \angle 64.5^\circ \text{ A}$$

Given  $\vec{\lambda}_r^d = \sqrt{\frac{3}{2}} (\lambda_{rd} + j\lambda_{rq}) \rightarrow 0$

$$\Rightarrow \lambda_{rd} = 1.207 \text{ wb-turns}$$

and  $\vec{I}_a^{i,d} = \sqrt{\frac{3}{2}} (\cancel{\lambda_{rd}} + j\lambda_{rq})$

$$\Rightarrow \lambda_{rq} = 337.7 \text{ A}$$

Given  $\vec{I}_{ph}^d = \sqrt{\frac{3}{2}} (\lambda_{rd} + j\lambda_{rq})$

$$= (205.4 + j430.8) \text{ A}$$

$$\Rightarrow \lambda_{rd} = 167.7 \text{ A}$$

$$\lambda_{rq} = 351.8 \text{ A}$$

$$T_{em} = \frac{P}{2} \lambda_{rd} \lambda_{rq}$$

$$= 815.3 \text{ Nm}$$

$$\omega_{slip} = \cancel{0.5} 0.779 \text{ rad/s}$$

$$\omega_{slip} = \frac{2}{P} R' \lambda_{rq}$$

$$= 4.896 \text{ rad/s}$$

$$f_{slip} = 0.779 \text{ Hz}$$

$$s = \frac{f_{slip}}{f_{syn}} = 0.031 \text{ or } 3.1\%$$

Phase currents

$$\text{@ } t=0, \quad \theta_{da} = \omega t + \theta_{lr} = \theta_{lr} \\ = -97.3^\circ$$

$$\begin{aligned} \Rightarrow i_a(0) &= \sqrt{\frac{2}{3}} (i_{sd} \cos \theta_{da} - i_{sq} \sin \theta_{da}) \\ &= \sqrt{\frac{2}{3}} (167.7 \cos(-97.3^\circ) - 351.8 \sin(-97.3^\circ)) \\ &= 267.6 \text{ A} \end{aligned}$$

$$\begin{aligned} i_b(0) &= \sqrt{\frac{2}{3}} (i_{sd} \cos(240^\circ - 97.3^\circ) - i_{sq} \sin(240^\circ - 97.3^\circ)) \\ &= -282.9 \text{ A} \end{aligned}$$

$$\begin{aligned} i_c(0) &= \sqrt{\frac{2}{3}} (i_{sd} \cos(120^\circ - 97.3^\circ) - i_{sq} \sin(120^\circ - 97.3^\circ)) \\ &= -15.3 \text{ A} \end{aligned}$$

$$\begin{aligned} \text{@ } t=5 \text{ ms} \quad \theta_{da} &= 2\pi f_e t + \theta_{lr} \\ &= 90^\circ + -97.3^\circ \\ &= -7.3^\circ \end{aligned}$$

$$\Rightarrow i_a(5) = 172.2 \text{ A}$$

$$i_b(5 \text{ ms}) = 145.7 \text{ A}$$

$$\text{and } i_c(5 \text{ ms}) = -317.8 \text{ A}$$