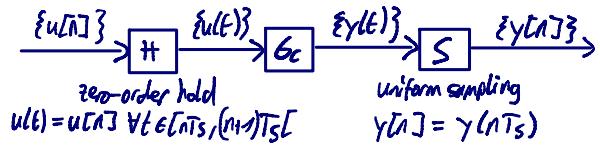


Continuous Time to Discrete Time



State-Space Representation

$$\begin{aligned} q(t) &= A_c q(t) + B_c u(t) & q[n+1] &= A_d q[n] + B_d u[n] \\ y(t) &= C_c q(t) + D_c u(t) & y[n] &= C_d q[n] + D_d u[n] \end{aligned}$$

Exact Discretization

Choose $C_d := C_c$ and $D_d := D_c$. Construct $M = \begin{bmatrix} A_c & B_c \\ 0 & 0 \end{bmatrix}$ and compute $e^{MT_s} = I + MT_s + \frac{(MT_s)^2}{2!} + \frac{(MT_s)^3}{3!} + \dots = \begin{bmatrix} A_d & B_d \\ 0 & I \end{bmatrix}$

Euler Forward Discretization

Choose $C_d := C_c$, $D_d := D_c$, $A_d := I + A_c T_s$, $B_d := B_c T_s$.

Linear Constant-Coefficient Difference Equations

LCDE

$$\sum_{k=0}^N a_k y[n-k] = \sum_{k=0}^M b_k u[n-k] \quad a_k, b_k \in \mathbb{R}, N, M \in \mathbb{N}$$

Convert to state-space by choosing $A_d = \begin{bmatrix} 0 & I \\ -a_0 & \dots -a_N \end{bmatrix}$, $B_d = \begin{bmatrix} 0 \\ b_0 \end{bmatrix}$, $C_d = [-a_N \dots -a_1]$, $D_d = [b_0]$ if $b_k = 0$ for all $k > 0$ and $a_0 = 1$. Otherwise, solve manually.

$$y[n] = \sum_{k=0}^N b_k u[n-k] \Rightarrow \text{the system has a FIR}$$

Convert to impulse response assuming $q[n] = 0$ for $n < 0$ by computing $h = \{0, CB, CAB, CA^2B, \dots, CA^{N-1}B\}$

System Properties

memoryless ($\Rightarrow y[n] = f_n(\{u[t]\})$)

causal ($\Rightarrow y[n] = f_n(\{u[n-k] \mid k \in \mathbb{N}\})$)

$\Leftrightarrow R[n] = 0$ for $n < 0$ if G is LTI
(or via transfer function)

linear (\Rightarrow All input signals u_1, u_2 , $\forall d_1, d_2 \in \mathbb{R}$,

$$G(d_1 u_1 + d_2 u_2) = d_1 G u_1 + d_2 G u_2$$

time-invariant ($\Rightarrow G\{u[n-k]\} = \{G(u)[n-k]\}$)

stable ($\Rightarrow \exists M \in \mathbb{R}$. Then. $|u[n]| < 1 \Rightarrow |G(u)[n]| < M$)

$$\Leftrightarrow \sum_{k=0}^{\infty} |G[k]| < \infty \quad \text{if } G \text{ is LTI}$$

(or via transfer function)

LTI-system response

Unit Impulse & Step Sequence

$$\{S[n]\} = \{..., 1, 0, 0, \dots\} \quad | \quad \{E[n]\} = \{..., 1, 1, 1, \dots\}$$

It holds that $s[n] = \sum_{k=-\infty}^n S[k]$ and $e[n] = \sum_{k=-\infty}^n E[k]$.

Impulse Response

An LTI-system G is fully characterized by $GS =: R$. Now,

$$Gu = G\left(\sum_{k=-\infty}^n u[k] \delta[n-k]\right) = \sum_{k=-\infty}^n u[k] G\{u[n-k]\} = u * R$$

If $R[n] = 0$ for $n > N$, then G has a FIR. If no such N exists, then G has an IIR.

Convolution Properties

commutative $u * h = R * u$, associative $(x * y) * z = x * (y * z)$,

$$\text{distributive } x * (h_1 + h_2) = x * h_1 + x * h_2$$

Exponential Series, Eigenfunctions & Z-Transform

Complex Exponential Series

For $\omega \in \mathbb{C}$ with the DT-frequency $\Omega \in [0, 2\pi]$ in $z = |z|e^{j\omega}$, define $x[n] := z^n = |z|^n (\cos(\Omega n) + j \sin(\Omega n))$.

Periodic Signals

x is M -periodic ($\Rightarrow \{x[n]\} = \{x[n+M]\}$)

N is the fundamental period ($\Rightarrow N = \min_{x \text{ is } M\text{-periodic}} M$)

Periodicity constraint

Sampling CT $t \mapsto \cos(wt)$ to $\{\cos(\Omega n)\}$ with $\Omega = wT_s$ and $w = 2\pi f$ where f is the frequency in Hz.

is N periodic ($\Rightarrow \exists M, N \in \mathbb{N}_0. \frac{\Omega}{2\pi} = \frac{m}{N}$)

N is the fundamental period ($\Rightarrow \frac{m}{N}$ is irreducible).

Eigenfunctions & Z-Transform

$$G\{z^n\} = \sum_{k=-\infty}^{\infty} R[k] z^{-k} = \left(\sum_{k=0}^{\infty} R[k] z^{-k} \right) z^n$$

Eigenvalue computed by z-transform $H(z)$ of h | Eigenfunction

Z-Transform Properties

linearity $d_1 X_1 + d_2 X_2 \Leftrightarrow d_1 X_1(z) + d_2 X_2(z)$

$$\text{Time-Shifting } \{x[n-k]\} \Leftrightarrow X(z) z^{-k}$$

$$\text{Convolution } x_1 * x_2 \Leftrightarrow X_1(z) \cdot X_2(z)$$

$$\text{Accumulation } \sum_{k=-\infty}^{\infty} x[k] \Leftrightarrow X(z) \frac{z}{z-1}$$

$$\text{Differentiation } \{nx[n]\} \Leftrightarrow -z \frac{d}{dz} X(z)$$

Transfer Function

An LTI system has the transfer function $H(z) = \frac{Y(z)}{U(z)}$ where $y = u * h \Leftrightarrow Y(z) = U(z) H(z)$.

Determine from LCDE using linearity and time-shifting.

Determine from state-space by computing $H(z) = C(zI - A)^{-1} B + D$.

$H(z)$ has stable and causal interpretation ($\Rightarrow |H(p)| = \infty \Rightarrow |p| < 1$)

$H(z)$ has stable interpretation ($\Rightarrow |H(p)| = \infty \Rightarrow |p| \neq 1$)

system causal ($\Rightarrow |H(p)| = \infty \Rightarrow |p| < 1$) \Leftrightarrow system stable

system anti-causal ($\Rightarrow |H(p)| = \infty \Rightarrow |p| \rightarrow |p| \geq 1$) \Leftrightarrow system stable

Fourier Transform

Frequencies & DT Fourier-Transform

$$6\{e^{j\omega n}\} = \sum_{k=-\infty}^{\infty} R[k] \{e^{j\omega n-k}\} = \sum_{k=0}^{\infty} R[k] e^{-jk\omega} \{e^{j\omega n}\}$$

Frequency response computed by DT-FT $H(\omega)$ of h | Frequency

DT-FT Properties

z-transform evaluated on unit circle $X(\omega) = X(z=e^{j\omega})$

$$\text{inverse } \{x[n]\} = \frac{1}{2\pi} \int_{-\pi}^{\pi} X(\omega) e^{jn\omega} d\omega$$

linearity $d_1 X_1 + d_2 X_2 \Leftrightarrow d_1 X_1(\omega) + d_2 X_2(\omega)$

$$\text{convolution } x_1 * x_2 \Leftrightarrow X_1(\omega) \cdot X_2(\omega)$$

$$\text{Parseval's Theorem } \sum_{n=-\infty}^{\infty} |x[n]|^2 \Leftrightarrow \frac{1}{2\pi} \int_{-\pi}^{\pi} |X(\omega)|^2 d\omega$$

Magnitude symmetry $x \in \mathbb{R}^\infty \Rightarrow X(\omega) = X(\omega - 2\pi)$ *

Brists if $\sum_{n=-\infty}^{\infty} |x[n]| < \infty$ or $x = \{e^{j\omega n}\} \Leftrightarrow X(\omega) = 2\pi \delta(\omega - \Omega_0)$

Fourier Series & Discrete Fourier Transform

DFS & DT-DFT

An N -periodic signal $x[n] = \frac{1}{N} \sum_{k=0}^{N-1} X[k] e^{j k \frac{2\pi}{N} n}$
for N -periodic DFS coefficients $X[k] = \sum_{n=0}^{N-1} x[n] e^{-j k \frac{2\pi}{N} n}$

Any finite signal can be extended to a periodic one and transformed via DFT. That is the DT-DFT.

DFS & DT-DFT Properties

Linearity $a_1 x_1 + a_2 x_2 \leftrightarrow a_1 \sum_{k=0}^{N-1} X_1[k] e^{j k \frac{2\pi}{N} n} + a_2 \sum_{k=0}^{N-1} X_2[k] e^{j k \frac{2\pi}{N} n}$

Parseval's Theorem $\sum_{n=0}^{N-1} |x[n]|^2 = \frac{1}{N} \sum_{k=0}^{N-1} |X[k]|^2$

Magnitude symmetry $x \in \mathbb{R}^\infty \Rightarrow X[N-k] = X^*[k] (\text{so } X[0] \in \mathbb{R})$

Response to Complex Exponential Series

$Y[k] = H(e^{j k \frac{2\pi}{N}}) U[k]$ holds for N -periodic $\sum_{n=0}^{N-1} c_n e^{j n \omega}$

$G\left\{\sum_{n=0}^{N-1} c_n e^{j n \omega}\right\} \xrightarrow{n \rightarrow \infty} H(e^{j \omega}) \{c_n\}$ for causal exp. series

Aliasing

The effect of multiple CT frequency mapping to the same DT frequency. Solution: Analog-filter st. $|w| < \frac{\pi}{T_S}$.

System Identification

White Noise

A sequence x of random variables with $E[x[n]] = 0$ and $E[x[n]x[n]] = \delta_{n,n}$, usually with $\text{Var}[x[n]] = 1$, has in expectation a flat frequency spectrum. Simulate via `rand(3) * (2 * np.random.uniform() - 1)` or `np.random.normal()`

Unit Impulse Method

① Measure $G\{x[n]\} = y$ in N samples.

② Estimate $H(k \frac{2\pi}{N}) := Y[k] = H(k \frac{2\pi}{N}) - \sum_{n=N}^{\infty} h[n] e^{-j k \frac{2\pi}{N} n}$.

Problem: MSE grows with N if measurement noise is involved.

Frequency Response Method

① Fix a target frequency $\omega_e = e^{\frac{j 2\pi}{N}}$, transient N_t , N , and AER.

② Measure $G\{A \cos(\omega_e n)\} = y$, and compute $Y[k] = \sum_{n=0}^{N-1} y[n] e^{-j \omega_e n}$

③ Estimate $H(\omega_e) := \frac{2|Y[k]|}{NA} = \frac{|Y[k]|}{N}$

④ Repeat for more k until satisfied.

Finding $H(z)$ from $H(e)$

$$H(z) = \frac{\sum_{k=0}^{M-1} b_k z^{-k}}{1 + \sum_{k=1}^K a_k z^{-k}} \stackrel{!}{=} H(e) \text{ when } z = e^{j \omega}, \quad H(e) = R e^{j \phi}$$

$$\Leftrightarrow \begin{bmatrix} R_1 \cos(\phi_1 - (A-1)\Omega_e) & \dots & -\cos((C-1)\Omega_e) \\ -R_1 \sin(\phi_1 - (A-1)\Omega_e) & \dots & \sin((C-1)\Omega_e) \end{bmatrix} \begin{bmatrix} a_1 \\ \vdots \\ a_K \end{bmatrix} = \begin{bmatrix} -R_1 \cos(\phi_1) \\ -R_1 \sin(\phi_1) \\ \vdots \\ 0 \end{bmatrix}$$

$$2L \times 1 \times B-1 \quad M \times 1 \quad 2L \times 1$$

Filtering



Non-causal Filtering

Chain a real, causal filter G with $H(z)$ and its anticausal counterpart \tilde{G} with $H(z^{-1})$ to create $y = \tilde{G} G u$ with $Y(e^{j \omega}) = |H(e^{j \omega})|^2 U(e^{j \omega})$. Note: No phase delay!

Anti-Aliasing CT-Filter

$$u(t) \xrightarrow{R \frac{d}{dt} + I} y(t) \quad \frac{Y(s)}{U(s)} = \frac{1}{RCs + 1} = \frac{w_c}{s + w_c} \text{ for cut-off } w_c = \frac{1}{RC}$$

FIR-Filters

An FIR filter is characterized by $R = [b_0, b_1, \dots, b_{M-1}]$

with $H(z) = \sum_{k=0}^{M-1} b_k z^{-k}$, where $M-1$ is the filter order.

Moving-Average Filter

$$y[n] = \frac{1}{M} \sum_{k=0}^{M-1} u[n-k] \Leftrightarrow H(z) = \frac{1}{M} \sum_{k=0}^{M-1} z^{-k} = \frac{1 - z^{-M}}{1 - z^{-1}}$$

Trick: Multiply both sides with $e^{-j \omega}$ and subtract modified from original.

Alternative: $y[n] = y[n-1] + \frac{u[n] - u[n-M]}{M}$ identical if no numerical errors happen. (x) Conversion yields non-causal WMA with $2M-1$ coefficients that has 0 phase and good mag.

Weighted MA-Filter

$$y[n] = \frac{1}{S} \sum_{k=0}^{M-1} w_k u[n-k] \text{ with } S = E w_k. \text{ Usually } S = \frac{M-K}{2}$$

IIR-Filters

An IIR filter is characterized by b_0, \dots, b_{M-1} and a_1, \dots, a_{N-1} with $y[n] = \sum_{k=0}^{M-1} b_k u[n-k] - \sum_{k=1}^{N-1} a_k y[n-k]$ and $H(z)$ above, where $\max(M-1, N-1)$ is the order.

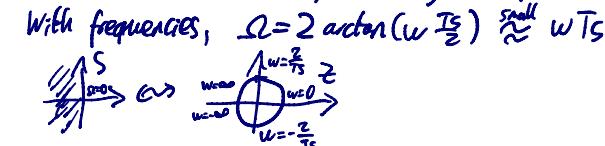
Butterworth Filter

In CT, $R(w) = \frac{1}{\sqrt{1-w^{2K}}}$ is a K -th order filter with corner frequency $\omega_c = \frac{\pi}{T_S}$. It has no ripples and is maximally flat.

The stable TF with that freq. resp. is $H(s) = (T_S \frac{1}{s} (s - s_c))^{-1}$ where $s_c = \exp(j \frac{(2k+K-1)\pi}{2K})$. Replacing $s \mapsto \frac{s}{w_c}$ changes the cut-off frequency to w_c .

Bilinear Transform

Convert from CT to DT by $s = \frac{z}{T_S} \left(\frac{z-1}{z+1} \right) \Leftrightarrow z = \frac{1 + s T_S}{1 - s T_S}$



Designing High-pass in CT / DT

Design low-pass for corner frequency $\frac{1}{w_c} / \pi = \omega_c$ with $H_{LP}(s/z)$. Then, $H_{HP}(s/z) = H_{LP}(s^{-1}/-z)$.

Designing Band-pass in CT

Design low-pass for corner frequency $w_h - w_l$ with $H_{LP}(s)$. Then $H_{BP}(s) = H_{LP}\left(\frac{s^2 + j w_l w_h}{s^2 + j w_h w_l}\right)$

Prewarping

We want $\frac{w_c}{T_S} = w_c$ but with large w_c , this doesn't hold. So, instead design for $\bar{w} = \frac{2}{T_S} \tan\left(\frac{w_c T_S}{2}\right)$

$$e^{j\theta} = \cos \theta + j \sin \theta \quad e^{-j\theta} = \cos \theta - j \sin \theta$$

$$\cos \theta = \frac{e^{j\theta} + e^{-j\theta}}{2} \quad \sin \theta = \frac{e^{j\theta} - e^{-j\theta}}{2j}$$

$$\sin^2 \theta = \frac{1 - \cos(2\theta)}{2} \quad \cos^2 \theta = \frac{1 + \cos(2\theta)}{2}$$

$$\sum_{k=0}^{\infty} \frac{1}{k!} = 1 + 1 + \frac{1}{2} + \frac{1}{6} + \dots = e$$

$$\sum_{k=1}^{\infty} \frac{1}{k^2} = 1 + \frac{1}{2} + \frac{1}{4} + \frac{1}{9} + \dots = \frac{\pi^2}{6}$$

$$\sum_{k=0}^{\infty} \left(\frac{1}{n}\right)^k = \frac{1}{n-1} \quad \sum_{k=0}^{\infty} \left(-\frac{1}{n}\right)^k = \frac{1}{n+1} \text{ for } n > 1$$