SCycle

June 12, 2018

SCycle was written primarily by Kali L. Allison (kallison@stanford.edu), based on an initial prototype by Brittany A. Erickson. Contributions to the code were made by Maxime Rivet and Weiqiang Zhu. The numerical method was additionally developed by Kenneth Duru and Brittany A. Erickson. Details are given in papers by the authors, particularly

Allison, Kali L., E. M. Dunham (2017), Earthquake cycle simulations with rate-and-state friction nd power-law viscoelasticity, Tectonophysics, doi:10.1016/j.tecto.2017.10.021.

Erickson, Brittany A., E. M. Dunham (2014), An efficient numerical method for earthquake cycles in heterogeneous media: Alternating subbasin and surface-rupturing events on faults crossing a sedimentary basin, Journal of Geophysical Research: Solid Earth, doi:110.1002/2013JB010614.

1 Introduction

SCycle (pronounced like cycle) is a code for simulating single earthquakes and sequences of earthquakes, aka earthquake cycles. It only supports the antiplane geometry in 2D, as shown in Figure 1.

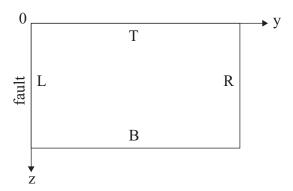


Figure 1: Diagram showing the geometry of the computational domain. Note that only the block to the right of the fault is included. The coordinate system's origin is at the upper left corner.

SCycle requires an input text file, provided as the first command line argument after the name of the executable. For example, if the code has been compiled into an executable named "main", and the input file is "in/ex1.in" then use this command to run the code from the command line on a single processor:

./main in/ex1.in

Or, to run using (for example) 4 processors, use:

mpirun -np 4 main in/ex1.in

Several example input files are provided:

- ex1.in Input file for a 1D earthquake cycle simulation with linear elastic off-fault material, using the quasidynamic approximation. The material properties are constant. This is 1D, meaning that the fault is a single point and the domain extends in the y-direction but not the z-direction.
- **ex2.in** Input file for a 2D earthquake cycle simulation with linear elastic off-fault material, using the quasi-dynamic approximation. The material properties are constant.
- ex3.in Input file for a 2D ice stream simulation with linear elastic ice, using the quasi-dynamic approximation. The material properties are constant, and it is assumed that the material to the left of the fault is perfectly rigid.
- **ex4.in** Input file for a 2D thermomechanical earthquake cycle simulation with power-law viscoelastic off-fault material, using a fixed-point iteration method to estimate steady state conditions.

2 Input parameters

A summary of parameters accepted by the input file is provided in the tables below. The bold red parameters are required. Those which are not red and bold have default values indicated in bold face in the rightmost column.

Input parameters are formatted as:

parameterName = value # optional comment

where the use of white space is important. Each parameter must be placed on its own line, and may not have any white space or characters before its name. The separation between a parameter and its value must be <space><equals sign><space>, with no extra spaces or characters. In the examples, # is used as the default comment symbol, but in actuality any input which does not perfectly match the format will be interpreted as a comment (i.e. misspelled parameters will be ignored, any text that follows the value will be ignored), so any symbol may effectively be used as a comment symbol.

Some depth-variable fields can be inputted via a pair of vectors, one listing values and the other listing the depths for those values. The code will linearly interpolate between these points, and will extrapolate if the model domain extends beyond the last point. An example is shown in Figure 2.

A word of caution: the input parameters are NOT in base SI units.

| Table 1: Input parameters to select what problem type to run: | | | |
|---|--|---------------------------|--|
| Input Parameter | Meaning | Allowed Values | |
| problemType | which problem type to run | strikeSlip, iceStream | |
| ${\bf momentum Balance Type}$ | how to treat inertial term in momen- | quasidynamic, | |
| | tum balance equation, also whether to | quasidynamic_and_dynamic, | |
| | use fixed point iteration or not | dynamic, steadyStateIts | |
| ${\it guessSteadyStateICs}$ | whether or not to try to converge to | 0 = no, 1 = yes | |
| | steady state initial conditions, based | | |
| | on a guess for steady state shear stress | | |
| | on the fault | | |

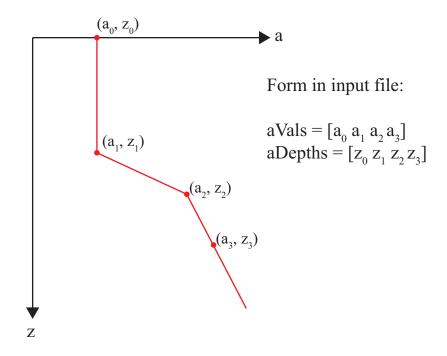


Figure 2: Example of a depth-dependent variable a, and the equivalent form for the input file.

Table 2: Basic input parameters for every simulation

| Input Parameter | Meaning | Allowed Values |
|------------------------|---|---|
| order | order of accuracy for spatial derivatives | 2, 4 |
| $\mathbf{N}\mathbf{y}$ | # of points in y-direction | must be large enough to resolve physics |
| $\mathbf{N}\mathbf{z}$ | # of points in z-direction | must be large enough to resolve physics |
| $\mathbf{L}\mathbf{y}$ | (km) domain size in y -direction | >0 |
| $\mathbf{L}\mathbf{z}$ | (km) domain size in z -direction | >0 |
| sbpType | type of SBP operators used | mc = matrix-based, compatible |
| | | mfc = matrix-based, fully compatible |
| | | $mfc_coordTrans = matrix-based, fully$ |
| | | compatible, allows curvilinear coordinate |
| | | transformation |
| bCoordTrans | if sbpType is mfc_coordTrans, then this | >0 |
| | argument tunes how extreme the grid | default: 5 |
| | space change in y is | |
| outputDir | full path to output | string |
| | | default: data/ |
| | | example: $/$ scratch/kallison/test_ |
| | | |

2.1 Time integration algorithms

Three explicit and two IMEX time integration algorithms are implemented. The simplest explicit method is forward Euler, called FEuler, which is provided for debugging purposes. The other two are adaptive Runge-Kutta methods, RK32 and RK43, where the first number in the name indicates the order of accuracy in time. Both methods select the size of the time step based on a user-specified subset of the explicitly integrated variables. The IMEX methods, RK32_WBE and RK43_WBE, use the same explicit integration scheme as the explicit methods, and additionally make an implicit integration call once per time step, in which the backward Euler method is used to integrate the implicit variables. Implicit variables may not be used to determine the magnitude of the time step. It is possible to vary the minimum and maximum permitted time step during run time by modifying the timeMoniter function.

Table 3: Time integration algorithms

| Innut Donometer | Magning | 9 |
|---|---|---------------------------------------|
| Input Parameter | Meaning | Allowed Values |
| timeIntegrator | time integration algorithm | FEuler, RK43 , RK32, RK32_WBE, |
| | | $RK43_WBE$ |
| timeControlType | control type for time step selection | options: P, PI, PID |
| stride1D | how frequently to write output for 1D | any integer |
| | files, in number of time steps | 0 to suppress output |
| | · • | default: 1 |
| stride2D | how frequently to write output for 2D | any integer |
| | files, in number of time steps | 0 to suppress output |
| | mos, in named of time steps | default: 1 |
| \max StepCount | maximum number of time steps to take | |
| maxstepCount | | any integer |
| • | before terminating the simulation | default: 10 ⁸ |
| initTime | (s) initial time | default: 0 |
| $\max Time$ | (s) final time | default: 10^{15} |
| initDeltaT | (s) size of first time step | default: 10^{-3} |
| $\min DeltaT$ | (s) minimum allowed time step | default: 10^{-3} |
| $\max DeltaT$ | (s) maximum allowed time step (can be | default: 10^{10} |
| | overridden if the user provides functions | |
| | to compute this as the simulation runs) | |
| atol | tolerance for selection of time step | default: 10^{-9} |
| timeIntInds | names of explicitly integrated variables to | no default values |
| umcmumas | be used to control time step size | example: [psi slip] |
| TT. | - | |
| normType | type of norm used to compute error and | L2_relative, L2_absolute |
| | determine magnitude of next time step | |

2.2 Rate-and-state friction

Rate-and-state friction is implemented as an algebraic equation relating fault strength to shear stress on the fault, which is solved for slip velocity. The regularized form is used, meaning that fault strength takes the form

$$F(\psi, V) = \sigma_N a \sinh^{-1} \left(\frac{V}{2v_0} e^{\psi/a} \right), \tag{1}$$

where ψ is the state variable and V is slip velocity. Several state evolution laws are implemented in the form

$$\dot{\psi} = G(V, \psi). \tag{2}$$

For the aging law

$$G(\psi, V) = \frac{bv_0}{d_c} \left(e^{(f_0 - \psi)/b} - \frac{V}{v_0} \right).$$
 (3)

For the slip law

$$\dot{\psi} = -V/d_c * (f - f_{ss}), \tag{4}$$

$$f_{\rm ss} = f_0 + (a - b) * \ln(V/v_0),$$
 (5)

$$f = a \sinh^{-1} \left(\frac{V}{2v_0} e^{\psi/a} \right). \tag{6}$$

(7)

For the slip law with flash heating

$$\dot{\psi} = -V/d_c * (f - f_{ss}), \tag{8}$$

$$f_{\rm ss} = \begin{cases} f_w + (f_{\rm LV} - f_w)(V_w/V), & \text{if } V \ge V_w \\ f_{\rm LV}, & \text{otherwise} \end{cases}$$
 (9)

$$f_{\rm LV} = f_0 + (a - b) * \ln(V/v_0)$$
(10)

$$f = a \sinh^{-1} \left(\frac{V}{2v_0} e^{\psi/a} \right). \tag{11}$$

$$V_w = \frac{\pi \alpha_{\rm th}}{D} \left(\frac{\rho c (T_w - T)}{\tau_c} \right)^2. \tag{12}$$

| Table 4: Basic rate-and-state friction input parameters | | | |
|---|--|---------------------------------|--|
| Input Parameter | Meaning | Allowed Values | |
| stateLaw | evolution law for state variable | agingLaw, slipLaw, flashHeating | |
| $\operatorname{rootTol}$ | relative tolerance for root-finding | default: 10^{-9} | |
| | algorithm | | |
| f0 | steady state friction coefficient at | default: 0.6 | |
| | v0 | | |
| v0 | (m/s) reference slip velocity | default: 10^{-6} | |
| cohesionVals, cohesionDepths | (MPa) cohesion | optional, defaults to 0 | |
| DcVals, DcDepths | (m) state evolution distance, also | required, no default | |
| | called L in the literature | | |
| ${ m aVals,\ aDepths}$ | direct effect parameter | required, no default | |
| bVals, bDepths | state evolution effect parameter | required, no default | |
| sigmaNVals, sigmaNDepths | (MPa) effective normal stress | required, no default | |
| $\operatorname{sigmaN_floor}$ | (MPa) floor for effective normal | optional, no default | |
| | stress (overrides sigmaNVals, sig- | example: 5 | |
| | maNDepths) | | |
| $sigmaN_{cap}$ | (MPa) ceiling for effective normal | optional, no default | |
| | stress (overrides sigmaNVals, sig- | example: 50 | |
| | maNDepths) | | |
| lockedVals, lockedDepths | depth range of fault over which to | default: 0 everywhere | |
| | force the fault to: creep at the | | |
| | loading rate (if value is ≤ -0.5), | | |
| | hold the slip velocity at zero (if | | |
| | value is ≥ 0.5), or allow friction | | |
| | to determine the slip velocity of | | |
| | the fault (if value is ≥ -0.5 and | | |
| | ≤ 0.5) | | |

Table 5: Additional input parameters used only if flash heating is used.

| Input Parameter | Meaning | Allowed Values |
|------------------|-------------------------------------|----------------|
| fw | fully weakened friction coefficient | no default |
| TwVals, TwDepths | (K) weakening temperature | no default |
| tau_c | (MPa) unweakened contact strength | no default |
| D | (μm) asperity diameter | no default |

2.3 Constituitive laws for off-fault material properties

SCycle supports two types of off-fault material: linear elastic, and power-law viscoelastic.

| Т | able 6: Input parameters for linear elastic | off-fault material |
|-------------------------|--|--|
| Input Parameter | Meaning | Allowed Values |
| vL | (m/s) loading velocity | default: 10^{-9} |
| $momBal_computeSxz$ | determines whether or not to compute | $0 = \mathbf{no}, 1 = \mathbf{yes}$ |
| | stress component σ_{xz} | |
| $momBal_computeSdev$ | determines whether or not to compute the deviatoric stress | $0 = \mathbf{no}, 1 = \mathbf{yes}$ |
| ${\rm momBal_bcR_qd}$ | type of right boundary condition for the momentum balance equation | symm_fault, rigid_fault, remoteLoading, freeSurface, tau, outGoingCharacteristics |
| momBal_bcT_qd | type of top boundary condition for the momentum balance equation | symm_fault, rigid_fault, remoteLoading, freeSurface, tau, outGoingCharacteristics no default |
| momBal_bcL_qd | type of left boundary condition for the momentum balance equation | <pre>symm_fault, rigid_fault, remoteLoad- ing, freeSurface, tau, outGoingCharac- teristics no default</pre> |
| ${\rm momBal_bcB_qd}$ | type of bottom boundary condition for the momentum balance equation | symm_fault, rigid_fault, remoteLoading, freeSurface , tau, outGoingCharacteristics no default |
| muVals, muDepths | (GPa) shear modulus | required, no default |
| rhoVals, rhoDepths | (g/cm^3) density | required, no default |
| linSolver | algorithm used to solve the momentum balance equation | MUMPSCHOLESKY (direct solver using the Cholesky factorization implemented by MUMPS), MUMPSLU (direct solver using the LU factorization implemented by MUMPS), AMG (algebraic multigrid method implemented by HYPRE), CG (conjugate gradient method preconditioned with HYPRE's AMG method) |
| kspTol | tolerance for linear solver method, if an | default: 10^{-9} |

Table 7: Additional input parameters for power-law viscoelastic off-fault material

iterative method is selected

| Input Parameter | Meaning | Allowed Values |
|-----------------|---|----------------------|
| AVals, ADepths | power-law parameter | required, no default |
| BVals, BDepths | power-law parameter equal to Q/R | required, no default |
| nVals, nDepths | power-law stress exponent | required, no default |
| $\max EffVisc$ | imposed ceiling for effective viscosity | |

2.4 Fixed point iteration for power-law viscoelastic simulations

SCycle includes a fixed point iteration method to find the steady-state behavior of the system.

| Input Parameter | Meaning | Allowed Values |
|-------------------------|--|--|
| $momBal_computeSxz$ | determines whether or not to compute stress component σ_{xz} | $0 = \mathbf{no}, 1 = \mathbf{yes}$ |
| $momBal_computeSdev$ | determines whether or not to compute the deviatoric stress | $0 = \mathbf{no}, 1 = \mathbf{yes}$ |
| $momBal_computeSdev$ | determines whether or not to compute the deviatoric stress | $0 = \mathbf{no}, 1 = \mathbf{yes}$ |
| $momBal_bcR_qd$ | type of right boundary condition for the momentum balance equation | symm_fault, rigid_fault, remoteLoading, freeSurface, tau, outGoingCharacteristics no default |
| ${\rm momBal_bcT_qd}$ | type of top boundary condition for the momentum balance equation | symm_fault, rigid_fault, remoteLoading, freeSurface, tau, outGoingCharacteristics no default |
| ${\rm momBal_bcL_qd}$ | type of left boundary condition for the momentum balance equation | symm_fault, rigid_fault, remoteLoading, freeSurface, tau, outGoingCharacteristics no default |
| $momBal_bcB_qd$ | type of bottom boundary condition for the momentum balance equation | symm_fault, rigid_fault, remoteLoading, freeSurface, tau, outGoingCharacteristics no default |
| fss_T | damping parameter for steady state temperature | 0 - 1 default: 0.1 |
| fss_EffVisc | damping parameter for effective viscos- | 0 - 1 |
| $\max EffVisc$ | ity (GPa s) ceiling value for effective vis- cosity | default: 0.1 default: 10 ³⁰ |
| gss_t | (millistrains) initial guess for viscous strain rate | default: 10^{-8} |
| $maxSSIts_effVisc$ | maximum allowed number of iterations to converge to steady state effective viscosity | default: 50 |
| $maxSSIts_timesteps$ | maximum allowed number of time steps for portion of steady state itera- | default: 2×10^4 |
| $atolSS_effVisc$ | tion involving explicit time integration absolute error for determining if effec- tive viscosity has converged | default: 10^{-3} |

2.5 Heat Equation

It is possible to additionally solve the heat equation with the any combination of the following source terms: frictional shear heating, viscous shear heating, and radioactive heat generation.

| Input Parameter | Meaning | Allowed Values |
|----------------------------|---|--|
| thermalCoupling | whether or not to simulate the heat equation, and to allow temperature changes to feed back into the other governing equations | coupled, uncoupled, no |
| ${\bf heat Equation Type}$ | what form of the heat equation to solve, steady state or including time dependence | transient, steadyState |
| with Visc Shear Heating | whether or not to include viscous shear heating | yes, no |
| with Radio Heat Generation | whether or not to include radioactive heat generation | yes, no |
| linSolver_heateq | linear solver algorithm for the heat equation | MUMPSCHOLESKY (direct solver using the Cholesky factorization implemented by MUMPS), MUMPSLU (direct solver using the LU factorization implemented by MUMPS), AMG (algebraic multigrid method implemented by HYPRE), CG (conjugate gradient method preconditioned with HYPRE's AMG method) |
| kspTol_heateq | tolerance for linear solver method, if an iterative method is selected | default: 10^{-9} |
| ${\bf rhoVals, rhoDepths}$ | (g/cm^3) density | required, no default |
| kVals, kDepths | (GW/m/K) conductivity | required, no default |
| TVals, TDepths | (K) temperature at the top and bottom of the domain (note: only used to set boundary conditions) | required, no default |
| he_A0Vals, he_A0Depths | $(\mu \text{ W/m}^3)$ radioactive heat generation parameter | required, no default |
| he_LVals, he_LDepths | (km) radioactive heat generation length scale | required, no default |
| wVals, wDepths | (m) frictional shear zone width | default: 0 |