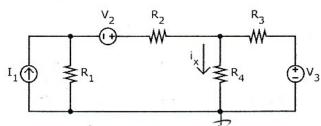
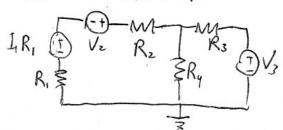
1. Calculate the value of current i_x . Parameter $I_1=4\,\mathrm{mA}$, $V_2=3\,\mathrm{V}$, $V_3=7\,\mathrm{V}$, $R_1=2\,\mathrm{k}\Omega$, $R_2=8\,\mathrm{k}\Omega$ and $R_4=4\,\mathrm{k}\Omega$.

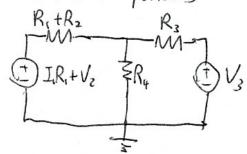
 $i_X = \begin{bmatrix} 20 \text{ pts.} \\ 0 \end{bmatrix}$



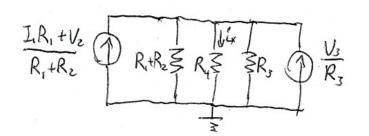
1) Source transform I:



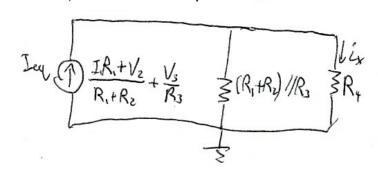
3 Sum series components



3 Source transform voltages:



4) Add currents and put Rz, R,+Rz in parallel;

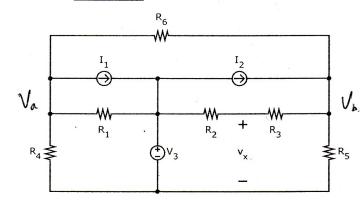


(5) Current divider:

Version	Answer
1	1,72mA
2	1.37 mA
3	1.04 mA

2. Find the value of the voltage v_x . Parameter $I_1=6\,\mathrm{mA}$, $I_2=9\,\mathrm{mA}$, $V_3=4\,\mathrm{V}$, $R_1=9\,\mathrm{k}\Omega$, $R_2=8\,\mathrm{k}\Omega$, $R_3=2\,\mathrm{k}\Omega$, $R_4=5\,\mathrm{k}\Omega$, $R_5=1\,\mathrm{k}\Omega$ and $R_6=7\,\mathrm{k}\Omega$.

$$v_x = \begin{bmatrix} 20 \text{ pts} \\ 1 \end{bmatrix}$$



Let
$$R_{23} = R_2 + R_3$$

 $R_{146} = R_1 / / R_4 / / R_6$

Write NV equations for Va, Vb;

$$\begin{cases} V_{a}: & V_{a}/R_{4} + \frac{V_{a}-V_{3}}{R_{1}} + I_{1} + \frac{V_{a}-V_{b}}{R_{6}} = 0 \\ V_{b}: & \frac{V_{b}-V_{3}}{R_{22}} + \frac{V_{b}}{R_{+}} - I_{2} + \frac{V_{b}-V_{a}}{R_{1}} = 0 \end{cases}$$

Isolate Va:

2
$$V_a = V_b - I_z R_6 + \frac{R_6}{R_T} V_b + \frac{R_6}{R_{25}} V_b - \frac{R_1}{R_{23}} V_3$$

Equate and solve for Vb:

$$V_{b} = \frac{R_{144}/R_{1}V_{3} - I_{1}R_{146} + I_{2}R_{4} + \frac{R_{6}}{R_{23}}V_{3}}{1 + \frac{R_{6}}{R_{5}} + \frac{R_{6}}{R_{23}} - \frac{R_{144}}{R_{6}}}$$

Once we know Vi

$$V_x = V_3 + \frac{R_2}{R_2 + R_3} (V_6 - V_3)$$

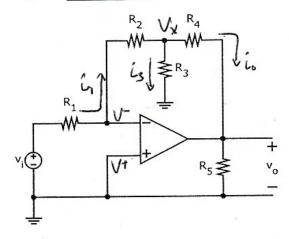
Thank of you

forgot this!

3. Opamp circuits with high closed-loop gain require large resistor ratios. On integrated circuits these take up significant area and are therefore costly. The circuit below uses a so-called T-network to reduce the required

Calculate the value of resistor R_3 such that $v_o/v_i = -91$. Use $R_1 = 4 \,\mathrm{k}\Omega$, $R_2 = R_4 = 9 \,\mathrm{k}\Omega$ and $R_5 = 3 \,\mathrm{k}\Omega$.

$$R_3 = {}^{20 \text{ pts.}}$$



$$L_1 = \frac{V_L}{R_1} \qquad V_x = -R_2 L_1 z - \frac{R_2}{R_1} V_1$$

$$V_0 = V_x - i_0 R_1 = -\frac{R_2}{R_1} V_i - R_4 \left(\frac{V_i}{R_1} + \frac{R_2}{R_1 R_2} V_i \right)$$

$$\frac{V_0}{V_1} = \frac{2R_2}{R_1} - \frac{R_2^2}{R_1 R_3}$$

solve for R3:

$$R_{s} = \frac{R_{2}^{2}}{R_{i}\left(-\frac{V_{0}}{V_{i}^{\prime}} - \frac{2R_{2}}{R_{i}}\right)}$$

4. The output voltage of a temperature sensor element is

$$v_t(T) = -2\frac{\mathsf{mV}}{{}^oC} \times T$$

where *T* is the temperature in degrees Celsius.

Design a thermometer circuit with output voltage

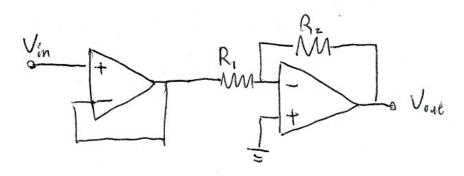
$$v_o(T) = 10 \frac{\text{mV}}{^oC} \times T$$

using the sensor, resistors, and ideal opamps. Your circuit should produce the correct output independent of the output resistance R_0 of the temperature sensor, which is in the range $50\,\mathrm{k}\Omega$... $100\,\mathrm{k}\Omega$. Draw the schematic diagram in the space provided below. Specify the values of all resistors (except R_0).

$$A_v = \frac{10}{-2} = -5$$

This suggests we need an inverting amplifier.

We also need a buffer for R. indopendence.



$$A = -\frac{Rz}{R_1} \implies \frac{Rz}{R_1} = S$$

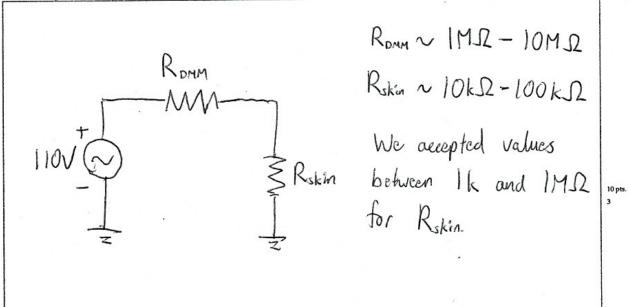
$$\Rightarrow Rz = SR_1$$

20 pts.

5. Suppose you stand barefoot on a wet floor with a hand-held digital voltmeter (DVM) in one hand. You insert one probe of the DVM into the hot output of a 110 V outlet and touch the other probe with your free hand.

Hypothetical experiment-don't try this!

a) Draw a circuit schematic of the situation. Use only circuit elements—sources and resistors—and their correct symbols. Do not draw pictures of elements. Assign reasonable values to all circuit components.



b) Would you get hurt? Explain!

No. Romm and Rokin form a voltage divider. So, Voltage aeross skin is relatively small.

Vskin ~ Rokin + Romm ~
$$\frac{10k}{10k+1M} \approx 1.1V$$
, which is safe.

Or, since Roma and Rokin are in series,

10 pts.