

Processed Text

molecule article fluorine containing flow modifier bn pps composite enabled low surface energy bocaol
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matrix thermally conductive coefficient that filled with better dispersion in the epoxy matrix
the thermally conductive coefficient λ is $1.5 \times 10^{-2} \text{ W/m}\cdot\text{K}$ at 25°C and $1.5 \times 10^{-2} \text{ W/m}\cdot\text{K}$ at 25°C
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review 3 11 cf obtained dopo 8 64 g 0 04 mol added system molecules2022 27 8066 3of11 reacted 12
h room temperature complete conversion dopo tested via ftir ethanol removed using rotary evaporator
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appears 1650 cm⁻¹ indicates base appears at 1650 cm⁻¹ and the peak of CF appears at 1650 cm⁻¹ which indicates triggered aldol polymerization. Amino silicone oil 3 trifluoromethyl the triggered aldol polymerization between amino silicone oil and 3 trifluoromethyl benzaldehyde. Si-DF performed addition reaction. DPO-Si-DF benzaldehyde. The Si-DF performed through the addition reaction of DPO and Si-DF. Additionally, peak CH₃ is absent. Wavenumber Si-DF indicating additionally the peak of CH₃ is absent at the same wavenumber for Si-DF. Indicating DPO successfully carried addition reaction intermediate containing CH₃ group. 14 20 22 containing the CH₃ group. 14 20 22. Figure 3a the peaks at 0 12 0 16 ppm. 1H NMR spectrum Si-DF displayed figure 3a. Peak 0 12 0 16 0 32 0 46 ppm and 1 16 1 42 ppm are attributed to the protons in Si-CH₃. Si-CH₃ ppm 0 32 0 46 ppm. 1 16 1 42 ppm attributed proton Si-CH₃. Si-CH₃ respectively peak 5 29 5 32 ppm. 5 07 5 11 ppm attributed CH₂ CH₂ respectively peak 5 29 5 32 ppm. 5 07 5 11 ppm attributed to the protons in NH and P-CH. The peaks at 6 5 8 2 ppm are attributed to the protons. Proton NH-P-CH peak 6 5 8 2 ppm attributed proton in the benzene ring. The 31P NMR spectra of DPO and Si-DF are shown in figure 3b. Benzene ring 31P NMR spectrum DPO-Si-DF shown figure 3b. Based on the 31P NMR spectrum of DPO, the peaks at 14 40 15 75 ppm are observed. Based 31P NMR spectrum DPO, peak 14 40 15 75 ppm observed. Molecule 2022 27 x peer review. H. W. L. E. T. H. E. P. P. E. A. K. S. A. R. E. A. B. B. S. E. N. T. T. H. E. S. A. E. W. W. A. V. A. V. E. N. U. M. M. B. E. R. E. F. R. O. R. I. S. D. F. F. N. A. N. D. E. W. N. E. P. W. E. A. P. K. E. A. A. K. R. S. E. A. B. R. E. S. E. O. O. R. F. B. V. 1. E. 1. D. A. T. 31. 50. 34. 85 ppm. The results from FTIR, 1H NMR and 31P NMR show that the flow served 31 50 34 85 ppm. Result FTIR, 1H NMR, 31P NMR show modifiers. Si-DF has been successfully synthesized. Flow modifier Si-DF successfully synthesized. Figure 3 1H NMR spectrum of Si-DF. 31P NMR spectra of Si-DF and DPO. Figure 3 1H NMR spectrum Si-DF. 31P NMR spectrum Si-DF. DPO 3 2 phase morphology. Highly filled polymer based composite. Disperse filler matrix. Key issue presenting challenge fabrication high performance composite. Display effect Si-DF dispersion. BN filler morphology. BN filler sample observed SEM. Figure 4 exists serious agglomeration. BN filler sample. BN pps 60 40. Figure 4a. BN pps 70 30. Figure 4b. Addition Si-DF morphology. BN filler present striking contrast. Obviously found BN filler exhibit homogeneous dispersion. Sample BN pps Si-DF 60 35 5. Figure 4a. BN pps Si-DF 70 25 5. Figure 4b. Figure 4 SEM image. BN pps 60 40. A1 BN pps Si-DF 60 35 5. A2 BN pps 70 30. B1 BN pps Si-DF 70 25 5. B2 previous work demonstrated fluorine containing flow modifier. PMFs low surface energy located. MH LLDPE interface. Highly filled. MH LLDPE composite. 80 20 weight improved dispersion. MH molecules. 2022 27 x peer review. 5 11. Figure 3 1H NMR spectrum Si-DF. B 31P NMR spectrum Si-DF. DPO 3 2 phase morphology. Highly filled polymer based composite. Disperse filler matrix. Key issue presenting challenge fabrication high performance composite. Molecules 2022 27 8066. Display effect Si-DF dispersion. BN filler morphology. 5 off 1 t1. He BN filler sample observed SEM. Figure 4 exists serious agglomeration. BN filler sample. BN pps 60 40. Figure 3 2 phase morphology. 4a BN pps 70 30. Figure 4b addition Si-DF morphology. 1 1 BN filler. Froser phirgehsley n fits l ead sptroilkyimnger c boansterdascto itp io oitbesv ihoouwslyto fdoiuspnedr stehtahte bfinlle frislilienrsth eexmhia btritix ai shomo. A key issue presenting a challenge in the fabrication of high performance composites. Geneous dispersion sample BN pps Si-DF 60 35 5. Figure 4a BN pps Si-DF 2. Display the effect of Si-DF on the dispersion of BN fillers. The morphology of the BN fillers. Si-DF 70 25 5. Figure 4b 2 in the sample is observed by SEM. Figure 4. Figure 4e 4. ESEM image. Aggeess 0 off bbn pppss 6600 4400 1 1 b bnn p ppp ssi id dff 6 06 03 53 55 5 2a 2 b nbn p ppsps 7 07 03 03 0 b 1b 1 bna npdpbsn pdpfs s7i0 2f5 57 0 b252 5 b2 int ohuerre pexriesvtiosseursio wusoargkg l owmee rdaetimonoonfsbttraftiellder tshinatt htehsea fmlupolerbinne pcpont a60in 4i0n g f filgouwre m4ao1 difiers andbn pps 70 30 figure 4b with the addition of Si-DF the morphology of the BN PMFs low surface energy located. MH LLDPE interface. Highly fillers presents a striking contrast. It is obviously found that BN filler exhibit a homogeneous filled. MH LLDPE composite. 80 20 weight improved dispersion. MH neous dispersion in the samples. BN pps Si-DF 60 35 5. Figure 4a and BN pps Si-DF 2 70 25 5. Figure 4b 2 in our previous work we demonstrated that the fluorine containing flow modifiers PMFs with low surface energy were located at the MH LLDPE interface in the highly filled. MH LLDPE composites. 80 20 by weight which improved the dispersion of MH particle. 23 meanwhile the distribution of flow modifiers can be estimated by evaluating the wetting coefficient ω. 24 herein young's model is used to calculate the ω of Si-DF. Additionally 1 ω 1 Si-DF is preferred to locate at the interface. The surface energy individual component pps BN Si-DF examined measuring contact angle. Interfacial energy

calculated using surface energy individual component using geometric mean equation harmonic mean equation 25 27 all of the data are listed in tables 2 and 3 respectively molecules 2022 27 8066 6 of 11 table 2 contact angles and surface energies of pps bn and si df contact angle γ_{yd} γ_p sample water diiodomethane mj m2 mj m2 mj m2 pps 90 37 24 76 46 99 46 63 0 36 bn 89 12 64 89 26 8 22 5 4 3 si df 98 45 51 20 34 08 33 78 0 3 table 3 preferential distribution of si df in the bn pps composites according to interfacial energies γ and wetting coefficients ω_a based on based on interfacial flow modifiers energy geometric mean harmonic mean ω_g ω_h distribution equation mj m2 equation mj m2 γ 6 52 11 75 bn pps γ si df pps 1 04 2 06 0 37 0 31 bn pps interface γ 3 47 5 74 si df bn as seen the values of ω for si df are 0 37 and 0 31 respectively as calculated geometric mean equation harmonic mean equation young model indicating that si df tends to locate at the interface between the bn fillers and pps matrix combining with the phase morphology and theoretical calculations it is concluded that the distribution of si df at the two phase interface is effectively able to reduce the formation of agglomeration in the matrix 3 3 thermal conductivity figure 5 presents the thermally conductive coefficient λ values of the pps matrix and bn pps composites the λ value of the pps matrix is 0 372 w k the composites reveal a dramatic enhancement in thermal conductivity in comparison with the pps matrix the λ values of bn pps 60 40 and bn pps 70 30 are 3 379 w k and 3 569 w k are approximately 9 and 9 6 times higher than that of the pps matrix respectively with the addition of si df the samples present higher thermal conductivity and the corresponding λ values are increased to 3 873 w k of bn pps si df 60 35 5 and 3 985 w k of bn pps si df 70 25 5 respectively this implies that efficient thermal transfer pathways could be formed at a high loading of bn fillers in the pps matrix by the introduction of si df 16 28 additionally it is believed that the homogeneous dispersion of bn fillers in the pps matrix is the key to the formation of thermal transfer pathways furthermore si df forms a protective layer on the bn surfaces which shows relatively lower interfacial molecule 2022 27 x peer review 7 11 thermal barriers with the pps matrix compared to the samples without si df resulting in higher λ values figure 5 thermal conductivity of pps matrix and bn pps composites figure 5 thermal conductivity pps matrix bn pps composite table 4 summarizes reported thermally conductive coefficient thermal conductivity enhancement bn pps composite noted bn pps composite higher bn filler content work show high thermally conductive coefficient highest thermal conductivity enhancement work provides relatively efficient facile method improve thermal conductivity bn pps composite table 4 comparison thermally conductive coefficient thermal conductivity enhancement bn pps composite thermally thermal filler loading conductive conductivity sample strategy year ref wt coefficient enhancement w k bn pps 60 2 638 822 3 hot compression 2017 15 surface modification bn pps 60 1 122 292 3 2017 16 hot compression bn pps 40 vol 2 45 880 hot compression 2017 18 bn pps 60 3 1 785 8 surface modification 2017 19 bn pps 60 2 7 610 5 melt blending 2017 19 bn pps 60 3 873 941 1 melt blending work bn pps 70 3 985 971 2 melt blending work 3 4 dielectric property key parameter electronic packaging material low dielectric constant conductive reducing signal propagation time electronic component important practical application dielectric constant frequency curve pps matrix bn pps composite displayed figure 6 pps matrix posse dielectric constant value 3 32 100 mhz seen dielectric constant value sample increased loading bn filler corresponding value increased 3 75 bn pps 60 40 3 98 bn pps 70 30 worth noting introduction si df beneficial decreasing dielectric constant sample sample bn pps si df 60 35 5 bn pps si df 70 25 5 dielectric constant value decreased 3 55 3 76 respectively lower dielectric constant attributed weakening interface polarization 29 30 si df improves dispersion bn filler also strengthens interaction bn filler pps matrix weakening polarization bn filler pps matrix resulting relatively lower dielectric constant value bn pps composite molecules 2022 27 8066 7 of 11 table 4 summarizes the reported thermally conductive coefficient and thermal conductivity enhancement for the bn pps composites it is noted that the bn pps composites with higher bn filler contents in this work show a high thermally conductive coefficient and the highest thermal conductivity enhancement this work provides a relatively more efficient and facile method to improve the thermal conductivity of bn pps composites table 4 comparison of thermally conductive coefficient and thermal conductivity enhancement in bn pps composites thermally thermal filler loading conductive conductivity sample strategy year ref wt coefficient

enhancement w k bn pps 60 2 638 822 3 hot compression 2017 15 surface modification bn pps 60 1
122 292 3 2017 16 hot compression bn pps 40 vol 2 45 880 hot compression 2017 18 bn pps 60 3 1
785 8 surface modification 2017 19 bn pps 60 2 7 610 5 meltblending 2017 19 bn pps 60 3 873 941 1
meltblending thiswork bn pps 70 3 985 971 2 meltblending thiswork 3 4 dielectricproperty key
parameter electronic packaging material low dielectric constant conducive reducing signal propagation
time electronic component veryimportantinpracticalapplications thedielectricconstant
frequencycurvesofthe ppsmatrixandbn ppscompositesaredisplayedinfigure6 theppsmatrixpossesses
adielectricconstantvalueof3 32at100mhz itcanbeseen thatthedielectricconstant
valueofthesamplesisincreasedastheloadingofofnfillers andthecorrespondingvalues areincreasedto3
75forbn pps 60 40 and3 98forbn pps 70 30 itisworthnotingthat theintroductionofsi
dfisbeneficialindecreasingthedielectricconstantofthesamples forsamplesbn pps si df 60 35 5 andbn pps
si df 70 25 5 thedielectricconstant valuesdecreasedto3 55and3 76 respectively
thelowerdielectricconstantsshouldbe attributedtotheweakeningofinterfacepolarization 29 30 si
dfnotonlyimprovesthe molecule 2022 27 x peer reviewdi
spersionofbnfillersbutalsostrengthenstheinteractionbetweenthebnfillersandpps8 11 matrix
weakeningthepolarizationbetweenthebnfillersandppsmatrix resultingin
relativelylowerdielectricconstantvaluesofthebn ppscomposites fif gi ug ru er e 6 6 dd ieie lele cc tt rr ii cc
cc oon n st ta nt fr fe req qu uen ec ny cycu cr uve rv eo sf p op f ppm sa mrix ata rn ixd ab nn bpp n pco
pm p co o mite p site 3 5 processability processability bn pps composite evaluated torque rheology test
31 figure 7 show torque v time curve bn pps composite expected stable torque value sample increased
loading bn filler pronounced decrease torque value bn pps composite addition si df observed sample bn
pps 60 40 bn pps 70 30 stable torque val ues 3 0 n 11 7 n 5 wt si df added corresponding value
decreased 2 1 n bn pps si df 60 35 5 2 5 n bn pps si df 70 25 5 respectively indicating si df obvious
advantage improving processability bn pps composite si df tends located interface effectively reduces
melt viscosity prevents bn filler aggregation de crease friction bn filler bn filler pps matrix figure 7 torque
versus time bn pps composite 3 6 mechanical property mechanical property critical composite
especially tensile strength toughness work tensile testing pps matrix bn pps composite con ducted
result shown figure 8 tensile strength pps matrix 38 mpa addition bn filler tensile strength sample
increased corresponding strength increased 48 mpa bn pps 60 40 43 mpa bn pps 70 30 tensile
strength slightly decreased sample si df tough ness sample evaluated calculating fracture work derived
areamolecules 2022 27 x peer review 8 11 figure 6 dielectric constant frequency curve pps matrix bn
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evaluated torque rheology test 3 5 processability 31 figure 7 show torque v time curve bn pps
composite expected statbhleep troorcqeusseabvialiltuyeosf obfn hpep ssacmomppeoss aitreess
iisnecvreaalusaetded wbiythth tehteorloquadeirnhgeoo lofg bynte stfil l3e1r figure 7 show torque v time
curve bn pps composite expected pronounced decrease torque value bn pps composite addition
thetabletorquevaluesofthesamplesareincreasedwiththeloadingofbnfillers si df observed sample bn pps
60 40 bn pps 70 30 stable torque val apronounceddecreaseinthetorquevaluesofthebn
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thetensilestrengthisslightlydecreasedforthesampleswithsi df thetoughness corresponding strength
increased 48 mpa bn pps 60 40 43 mpa bn pps
ofthesamplesisevaluatedbycalculatingthefractureworkderivedfromtheareaunder 70 30 tensile strength
slightly decreased sample si df tough thestress straincurve 32 33
theworkofthefractureoftheppsmatrixis13 66mj m3 ness sample evaluated calculating fracture work
derived area work fracture decreased loading bn filler sample bn pps 60 40 andbn pps 70 30
theworkofthefracturedecreasedto7 46mj m3and 5 53mj m3 respectively
thisisunderstandablebecausebnfillersaggregateeasilyand formagglomerationsintheppsmatrix
asexpected afteradding5wt ofsi df thework fracture sample increased 11 05 mj m3 bn pps si df 60 35 5
8 97mj m3ofbn pps si df 70 25 5 indicatingthatsi dpfhasanobviousadvantage
inimprovingthetoughnessofthehighlyfilledbn ppscomposites thisresultismainly ascribed distribution si df
si dpf tends located interface andformsa barrierlayer forbnfillers si
dfnotonlyreducetheagglomerationbut
alsotransferstheexternalforcereceivedbythesampletothesmallaggregateofbnfiller
whichisabletoactasthestressconcentrationpointstodissipatetheexternalenergy
thetoughnessofthesampleisachieved molecule 2022 27 x peer review 9 11 stress strain curve 32 33
work fracture pps matrix 13 66 mj m3 work fracture decreased loading bn filler sam ples bn pps 60 40
bn pps 70 30 work fracture decreased 7 46 mj m3 5 53 mj m3 respectively understandable bn filler
aggregate easily form agglomeration pps matrix expected adding 5 wt si df work fracture sample
increased 11 05 mj m3 bn pps si df 60 35 5 8 97 mj m3 bn pps si df 70 25 5 indicating si dpf obvious ad
vantage improving toughness highly filled bn pps composite result mainly ascribed distribution si df si
dpf tends located turface form barrier layer bn filler si df reduces agglomeration also transfer external
force received sample small aggregate bn molecules2022 27 8066 filler able act stress concentration
point dissipate external ener9goyf1 1 toughness sample achieved fif gi ugu rer e 8 8 t rt ar ia ni n t rt er
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4 conclusion aflurine containingflowmodifiersi dfwassuccessfullysynthesizedandapplied fluorine
containing flow modifier si df successfully synthesized applied
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electronic packaging material bn pps composite conven tionalmeltblendingtechniques si
dfwithlowsurfaceenergywasdominantlylocatedat tional melt blending technique si df low surface energy
dominantly located thebn ppsinterface leadingtotherelativelyhomogeneousdispersionofthebnfillers bn
pps interface leading relatively homogeneous dispersion bn fill
thussuccessfullyachievingssimultaneouslyhighthermalconductivity excellentdielectric er thus
successfully achieving simultaneously high thermal conductivity excellent die property processability
andtoughnessinbn ppscomposites solvingthewell known lepctoribcl epmropthearttiepso lpyrmoecer
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eimraptioorntaanldtleys itghniso fwfloorwk pmaovdedifi ethrse way constructing ideal electronic packaging material rational design flow modifier authorcontributions conceptualization b c methodology b c andx h software w z val aiudtahtioorn c oxn htr ibaunttiopn w c oinnvceespttiugaaltiioant iobn c b acn mxe hth ddoaltoagcyu rba tcio nan dx xh h w sroitfitnwga reo rwig izna l vdarlia ft dpatrieopna r axt ihon abn cd pw writ nign versetvigieawtioann dci ianngd b x c h v idsuaatali zcautrioanti opn w x shu p ewrvriistiinogn wo rzig ainlalla udtrhaoftr phreapvaerraetaiodna nbd ca g wrereidtintog therepvueibwli sahnedd eveirtsiiinogn obf cth e vmisaunauliszcartiipotr p w supervision w z au thor read agreed published version manuscript funding thisresearchwasfundedbyguangdongbasicandappliedbasicresearchfoundation 2021a1515110134 andtheopeningprojectofkeylaboratoryofpolymerprocessingengineer ing southchinauniversityoftechnology ministryofeducation kfk2102 institutionalreviewboardstatement notapplicable informedconsentstatement notapplicable dataavailabilitystatement thedatathatsupportthefindingsofthisstudyareavailablefromthe authorsuponreasonablerequest conflictsofinterest theauthorsdeclarenoconflictsofinterest sampleavailability samplesofthecompoundsareavailablefromtheauthors reference 1 shahil k balandin graphene multilayergraphenenanocompositesashighlyefficientthermalinterfacematerials nanolett 2012 12 861 867 crossref pubmed 2 han z fina thermalconductivityofcarbonnanotubesandtheirpolymernanocomposites areview prog polym sci 2011 36 914 944 crossref molecules2022 27 8066 10of11 3 lee g w park kim j lee j yoon h g enhancedthermalconductivityofpolymercompositesfilledwithhybrid filler compos partaappl sci manuf 2006 37 727 734 crossref 4 song h park k h kim b h choi w jun g h lee j kong b paik k w jeon enhancedthermalconductivity ofepoxy graphene compositesbyusingnon oxidizedgrapheneflakeswithnon covalentfunctionalization adv mater 2013 25 732 737 crossref pubmed 5 xu l chen g wang w li l fang x afacileassemblyofpolyimide graphene core shellstructurednanocomposites withbothhigh electricalandthermalconductivities compos partaappl sci manuf 2016 84 472 481 crossref 6 kim h jang j u yu j kim thermalconductivityofpolymercompositesbasedonthelengthofmulti walledcarbon nanotube compos partbeng 2015 79 505 512 crossref 7 gu j yang x lv z li n liang c zhang q functionalizedgraphitenanoplatelets epoxyresinnanocompositeswith highthermalconductivity int j heatmasstranf 2016 92 15 22 crossref 8 huang x zhi c jiang p golberg bando tanaka polyhedraloligosilsesquioxane modifiedboronnitridenanotube basedepoxynanocomposites anidealdielectricmaterialwithhighthermalconductivity adv funct mater 2013 23 1824 1831 crossref 9 han shi x yang x guo zhang j kong j gu j enhancedthermalconductivitiesofepoxynanocompositesvia incorporatingin situfabricatedhetero structuredsic bnnsfillers compos sci technol 2020 187 10944 crossref 10 guo xu g yang x ruan k zhang q gu j wu liu h guo z significantlyenhancedandprecisely mod eledthermalconductivityinpolyimidenanocompositeswithchemicallymodifiedgrapheneviainsitupolymeriz ation andelectrospinning hotpresstechnology j mater chem c2018 6 3004 3015 crossref 11 xie h zhu b k li j b wei x z xu z k preparation property polyimide aluminum nitride composite polym test 2004 23 797 801 crossref 12 jiang q wang x zhu hui qiu mechanical electrical thermal property aligned carbon nan otube polyimidecomposites compos partbeng 2014 56 408 412 crossref 13 guan x cao b cai j ye z lu x huang h liu zhao j designandsynthesisofpolysiloxanebasedsidechainliquid crystalpolymerforimprovingtheprocessabilityandtoughnessofmagnesiumhydrate linearlow densitypolyethylene composite polymers2020 12 911 crossref pubmed 14 cao b wang cai j xie w liu zhao j silicone fluorine functionalizedflowmodifierwithlowsurfaceenergyfor improvinginterfacesinhighlyfilledcomposites compos sci technol 2021 214 108984 crossref 15 gu j guo yang x liang c geng w tang l li n zhang q synergisticimprovementofthermalconductivitiesof polyphenylenesulfidecompositesfilledwithboronnitridehybridfillers compos partaappl sci manuf 2017 95 267 273 crossref 16 yang x tang l guo liang c zhang q kou k gu j improvementofthermalconductivitiesforppsdielectric nanocompositesviaincorporatingn h possfunctionalizedbnfillers compos partaappl sci manuf 2017 101 237 242 2 crossref 17 pan c kou k jia q zhang wu g ji improvedthermalconductivityanddielectricpropertiesofhbn ptf compositesviasurfacetreatmentbysilanecouplingagent compos partbeng 2017 111 83 90 crossref 18 jiang liu min p sui g bn mwcnt ppscore shellstructureparticlesandtheir3dseggregatedarchitecturecomposites withhighthermalconductivities

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Top Keywords

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areview: 0.0038593645215003474
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basedcompositeswithhighthermallyconductivecoefficients: 0.0038593645215003474
basedcompositeswithmagneticallyaligned: 0.0038593645215003474
basedepoxynanocomposites: 0.0038593645215003474
basedonthe31pnmr spectrumofdopo: 0.0038593645215003474
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cgotmhaptossi: 0.0038593645215003474
cgotmhperomsiatellsy: 0.0038593645215003474
chao: 0.0038593645215003474
characterizationofsi: 0.0038593645215003474
chasedfromshin: 0.0038593645215003474
chemical: 0.0038593645215003474
choi: 0.0038593645215003474
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citation: 0.0038593645215003474
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cnt: 0.0038593645215003474
coef: 0.0038593645215003474
combiningwiththephase morphology and theoretical calculations: 0.0038593645215003474
comparison: 0.0038593645215003474
comparison of thermally conductive coefficient and thermal conductivity enhancement in:
0.0038593645215003474
composites via surface treatment by silane coupling agent: 0.0038593645215003474
concentration: 0.0038593645215003474
conceptualization: 0.0038593645215003474
condition of the creative commons: 0.0038593645215003474
conductive: 0.0038593645215003474
conductive coefficient: 0.0038593645215003474
conductive coefficient of 33w: 0.0038593645215003474
confirmed: 0.0038593645215003474
conflicts of interest: 0.0038593645215003474
constructing: 0.0038593645215003474
contact: 0.0038593645215003474
contact angle: 0.0038593645215003474
contact angles and surface energies of pps: 0.0038593645215003474
containing flow: 0.0038593645215003474
containing flow modifiers: 0.0038593645215003474

containingthe: 0.0038593645215003474
content: 0.0038593645215003474
contrast: 0.0038593645215003474
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copyright: 0.0038593645215003474
correspondence: 0.0038593645215003474
couldbeformedatahighloadingofbnfillersintheppsmatrixbytheintroductionof: 0.0038593645215003474
covalentfunctionalization: 0.0038593645215003474
cp: 0.0038593645215003474
cpfo: 0.0038593645215003474
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creativecommons: 0.0038593645215003474
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critical: 0.0038593645215003474
crystalpolymerforimprovingtheprocessabilityandtoughnessofmagnesiumhydrate:
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cth: 0.0038593645215003474
cthoemcpolmexpitlye: 0.0038593645215003474
ctoveaffliuceiesnotf: 0.0038593645215003474
cucu: 0.0038593645215003474
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cλ: 0.0038593645215003474
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da6s: 0.0038593645215003474
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dataavailabilitystatement: 0.0038593645215003474
dbvea: 0.0038593645215003474
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ddrriieedd: 0.0038593645215003474
decreasesthefrictionbetweenthebnfillersandbetweenthebnfillersandtheppsmatrix:
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decreasing: 0.0038593645215003474
deisdpiesprseirosnio: 0.0038593645215003474
del: 0.0038593645215003474
deleovpemloepnmteonfti: 0.0038593645215003474
demonstrated: 0.0038593645215003474
denchevaandzlatandenchev: 0.0038593645215003474
densitypolyethylene: 0.0038593645215003474

deotopho: 0.0038593645215003474
derivedsicceramicaerogels: 0.0038593645215003474
design: 0.0038593645215003474
designandsynthesisofpolysiloxanebasedsidechainliquid: 0.0038593645215003474
deterioratingtheprocessabilityandtoughnessofthecomposites: 0.0038593645215003474
deur: 0.0038593645215003474
devel: 0.0038593645215003474
develophigh: 0.0038593645215003474
development: 0.0038593645215003474
dfanddopo: 0.0038593645215003474
dfare: 0.0038593645215003474
dfareshowninfigure3b: 0.0038593645215003474
dfatthetwo: 0.0038593645215003474
dff: 0.0038593645215003474
dfformsaprotectivelayeronthebnsurfaces: 0.0038593645215003474
dfhasbeensuccessfullysynthesized: 0.0038593645215003474
dfinthebn: 0.0038593645215003474
dfisbeneficialindecreasingthedialecticconstantofthesamples: 0.0038593645215003474
dfisdisplayedinfigure3a: 0.0038593645215003474
dfisobserved: 0.0038593645215003474
dfisperformedthroughtheaditionreactionofdopoandsi: 0.0038593645215003474
dfispreferredtolocateattheinterface: 0.0038593645215003474
dfnotonlyimprovesthe: 0.0038593645215003474
dfnotonlyreducetheagglomerationbut: 0.0038593645215003474
dfonthedispersionofbnfillers: 0.0038593645215003474
dfrfariesdt: 0.0038593645215003474
dftendstolocateattheinterfacebetweenthebnfillersandppsmatrix: 0.0038593645215003474
dfwassuccessfullysynthesizedandapplied: 0.0038593645215003474
dfwithlowsurfaceenergywasdominantlylocatedat: 0.0038593645215003474
dh: 0.0038593645215003474
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discussion: 0.0038593645215003474
displaytheeffectofsi: 0.0038593645215003474
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distributionofsi: 0.0038593645215003474
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dpfislocatedattheinterfacebetweenthebnfillersandthe: 0.0038593645215003474
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effectively: 0.0038593645215003474
effectofnanoparticlemobilityontoughnessofpolymernanocomposites: 0.0038593645215003474
efficientandfacilemethodtoimprovethethermalconductivityofbn: 0.0038593645215003474
efpfreoccteisvssealbyi: 0.0038593645215003474
eg: 0.0038593645215003474
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electromagnetic: 0.0038593645215003474
electronicpackagingmaterials: 0.0038593645215003474
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enabled: 0.0038593645215003474
enabledbylowsurfaceenergy: 0.0038593645215003474
ener9goyf1: 0.0038593645215003474
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enhancedthermalconductivitiesofepoxynanocompositesvia: 0.0038593645215003474
enhancedthermalconductivity: 0.0038593645215003474
enhancedthermalconductivityofpolymercompositesfilledwithhybrid: 0.0038593645215003474
eno: 0.0038593645215003474
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eoorf: 0.0038593645215003474
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epoxyresinnanocompositeswith: 0.0038593645215003474
epppps: 0.0038593645215003474
equippedwithanitrogeninlet: 0.0038593645215003474
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especially: 0.0038593645215003474
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exhibit: 0.0038593645215003474
expandedgraphite: 0.0038593645215003474
f2: 0.0038593645215003474
fabgne: 0.0038593645215003474
fabricationandmicrostructureevolutionofmonolithicbridgedpolysilsesquioxane:
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facile: 0.0038593645215003474
factorsaffectingthermalconductivitiesofthepolymersandpolymercomposites: 0.0038593645215003474
fang: 0.0038593645215003474
farotmthe: 0.0038593645215003474
fatnhde: 0.0038593645215003474
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figure1: 0.0038593645215003474
figure3: 0.0038593645215003474
figure4: 0.0038593645215003474
figure4a: 0.0038593645215003474
figure5: 0.0038593645215003474
figure5presentshethermallyconductivecoefficient: 0.0038593645215003474
filfilellresr: 0.0038593645215003474
filgouwre: 0.0038593645215003474

fill: 0.0038593645215003474
filledmh: 0.0038593645215003474
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fillerspresentsastrikingcontrast: 0.0038593645215003474
fina: 0.0038593645215003474
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first: 0.0038593645215003474
fitlhleersu: 0.0038593645215003474
fiwllehrichsh: 0.0038593645215003474
flask: 0.0038593645215003474
flowmodifiers: 0.0038593645215003474
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fopee: 0.0038593645215003474
forbnfillers: 0.0038593645215003474
force: 0.0038593645215003474
formagglomerationsintheppsmatrix: 0.0038593645215003474
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frequencycurvesofthe: 0.0038593645215003474
friction: 0.0038593645215003474
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funct: 0.0038593645215003474
functionalizedflowmodifierwithlowsurfaceenergyfor: 0.0038593645215003474
functionalizedgraphitenanoplatelets: 0.0038593645215003474
functionalpolymermaterials: 0.0038593645215003474
funding: 0.0038593645215003474
furthermore: 0.0038593645215003474
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polymer2015: 0.0038593645215003474
polymerization: 0.0038593645215003474
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ppscompositesaccordingtointerfacialenergies: 0.0038593645215003474
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ppscompositewiththeadition: 0.0038593645215003474
ppscore: 0.0038593645215003474
ppsmatrix: 0.0038593645215003474
ppsmatrixandbn: 0.0038593645215003474
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preferentialdistributionofsi: 0.0038593645215003474
preparationofbn: 0.0038593645215003474

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recyclable: 0.0038593645215003474
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shellstructurednanocomposites: 0.0038593645215003474
shellstructureparticlesandtheir3dseggregatedarchitecturecomposites: 0.0038593645215003474
shen: 0.0038593645215003474
shielding: 0.0038593645215003474
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shomo: 0.0038593645215003474
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shu: 0.0038593645215003474
significantlyenhancedandprecisely: 0.0038593645215003474
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silane: 0.0038593645215003474
silanesurfacemodificationofboronnitrideforhighthermalconductivitywithpolyphenylenesulfide:
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silanization: 0.0038593645215003474
silica: 0.0038593645215003474
siliconflameretardantsand: 0.0038593645215003474
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silttruastterdatiends: 0.0038593645215003474
sim: 0.0038593645215003474
simultaneousimprovementofprocessabilityandtoughness: 0.0038593645215003474
simultaneously: 0.0038593645215003474
sin: 0.0038593645215003474
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smodelisusedto calculatetheω: 0.0038593645215003474
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software: 0.0038593645215003474
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song: 0.0038593645215003474
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spectrometer: 0.0038593645215003474
speed: 0.0038593645215003474
spersionofbnfillersbutalsostrengthenstheinteractionbetweenthebnfillersandpps8:
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suchasboronnitride: 0.0038593645215003474
summarizes: 0.0038593645215003474
superiorchemicalresistance: 0.0038593645215003474
supervision: 0.0038593645215003474
surf: 0.0038593645215003474
surfacemodificationofmagnesiumhydroxidebywetprocessandeffectonthe: 0.0038593645215003474
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swaemreplmese: 0.0038593645215003474
switzerland: 0.0038593645215003474
swwilli: 0.0038593645215003474
synergisticimprovementofthermalconductivitiesof: 0.0038593645215003474
synthesisofsi: 0.0038593645215003474
synthesisrouteofsi: 0.0038593645215003474
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system: 0.0038593645215003474
t1e0dk: 0.0038593645215003474
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table2: 0.0038593645215003474
table3: 0.0038593645215003474
table4: 0.0038593645215003474
table4summarizesthereportedthermallyconductivecoefficientandthermalconduc:
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taenfosrilben: 0.0038593645215003474
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thebn: 0.0038593645215003474
thecompositesreveal: 0.0038593645215003474
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thedistributionofflowmodifierscanbeestimatedbyevaluating: 0.0038593645215003474
thefieldofelectroniccommunicationsduetoitsoutstandingthermaldimensionalstability:
0.0038593645215003474
thehec: 0.0038593645215003474
theintroductionofsi: 0.0038593645215003474
theirapplicationincycloaliphaticepoxysystems: 0.0038593645215003474
thelowerdielectricconstantshouldbe: 0.0038593645215003474
themixture: 0.0038593645215003474
themorphologyofthebn: 0.0038593645215003474
themorphologyofthebnfillers: 0.0038593645215003474
thepeakof: 0.0038593645215003474
thepeaksat: 0.0038593645215003474
thepeaksat14: 0.0038593645215003474
thepeaksat6: 0.0038593645215003474
thepps: 0.0038593645215003474
theppsmatrixhasarelativelylowthermally: 0.0038593645215003474
theppsmatrixpossesses: 0.0038593645215003474
therepvuiebwli: 0.0038593645215003474
theresultsfromftir: 0.0038593645215003474
thermalandmechanicalpropertiesofepoxycompositeswithabinaryparticlefillersystemconsisting:
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thermalbarrierswiththeppsmatrixcomparedtothesampleswithoutsi: 0.0038593645215003474
thermalconductivityofcarbonnanotubesandtheirpolymernanocomposites: 0.0038593645215003474
thermalconductivityofpolymer: 0.0038593645215003474
thermalconductivityofpolymercompositesbasedonthelengthofmulti: 0.0038593645215003474
thermalconductivityofppsmatrixandbn: 0.0038593645215003474
thermalstabilityofsiliconerubber: 0.0038593645215003474
thesampleprocessesalowerstabletorquevalue: 0.0038593645215003474
thesamplespresenthigherthermalconductivity: 0.0038593645215003474
thesi: 0.0038593645215003474
thestabletorque: 0.0038593645215003474
thestabletorquevaluesofthesamplesareincreasedwiththeloadingofbnfillers: 0.0038593645215003474
thestress: 0.0038593645215003474
thestrongpeakof: 0.0038593645215003474

thesurface: 0.0038593645215003474
thetensilestrengthisslightlydecreasedforthesampleswithsi: 0.0038593645215003474
thethermallyconductivecoeffi: 0.0038593645215003474
thetoughness: 0.0038593645215003474
thetoughnessofthesampleisachieved: 0.0038593645215003474
thetriggeredaldiminepolymerizationbetweenaminosiliconeoiland3: 0.0038593645215003474
thevaluesof ω : 0.0038593645215003474
thewettingcoefficient: 0.0038593645215003474
thework: 0.0038593645215003474
theworkofthefracturedecreasedto7: 0.0038593645215003474
theworkofthefractureoftheppsmatrixis13: 0.0038593645215003474
the λ : 0.0038593645215003474
the λ valueoftheppsmatrixis0: 0.0038593645215003474
thhiagth: 0.0038593645215003474
thisimpliesthatefficientthermaltransferpathways: 0.0038593645215003474
thisisunderstandablebecausebnfillersaggregateeasilyand: 0.0038593645215003474
thisresearchwasfundedbyguangdongbasicandappliedbasicresearchfoundation:
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thisresultismainly: 0.0038593645215003474
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thisworkprovidesarelativelymore: 0.0038593645215003474
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tothefabricationofidealelectronicpackagingmaterials: 0.0038593645215003474
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