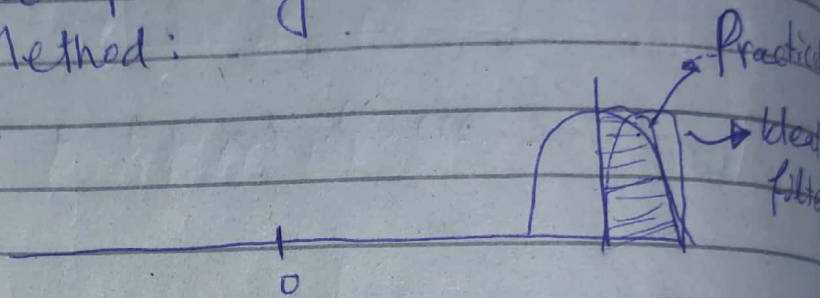


Com Sys After Mids:-

29/11/2023

★ Generation of SSB

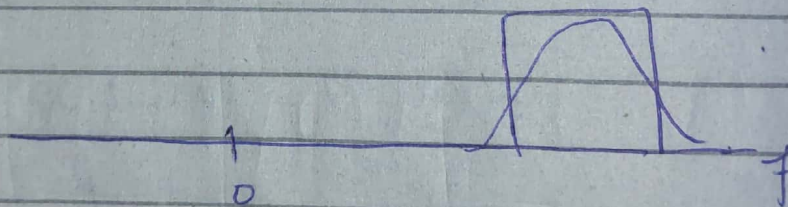
ii) Selective Filtering Method:



Can we do this?

No.

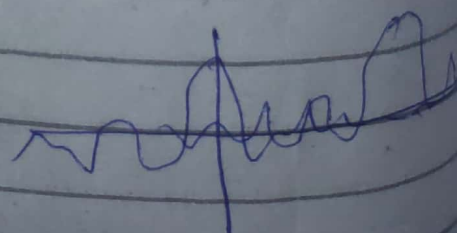
Why?



Butterworth filter

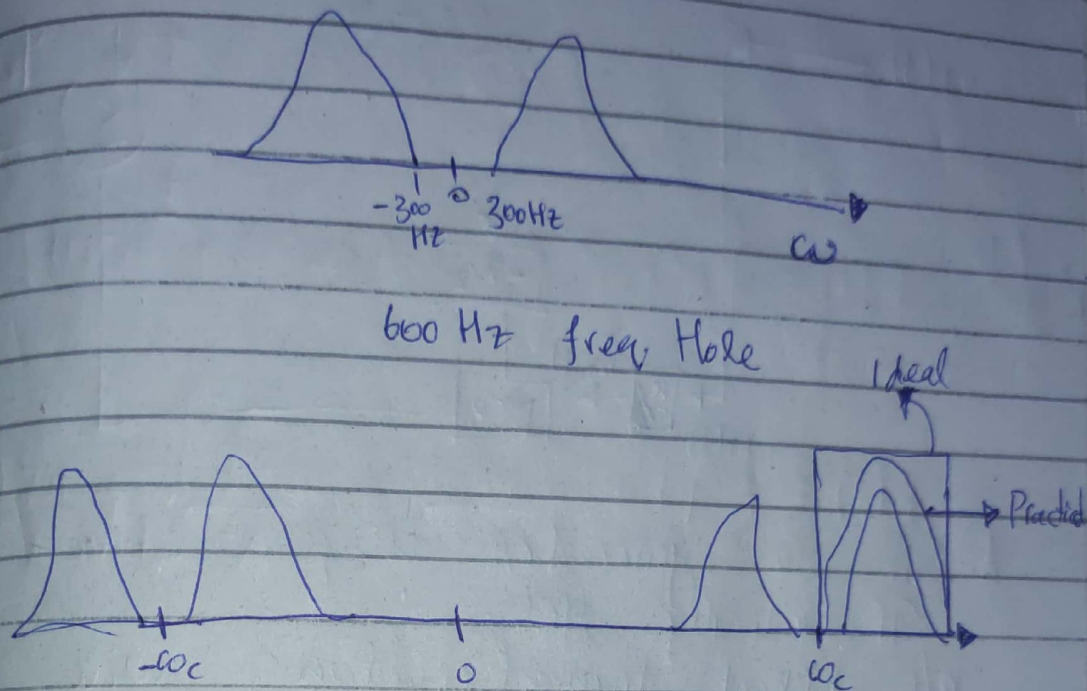
$$H(\omega) = \frac{1}{\sqrt{1 + \left(\frac{\omega}{2\lambda B}\right)^{2n}}}$$

$$\text{rect}\left(\frac{\omega}{2W}\right)$$



★ Speech Signal

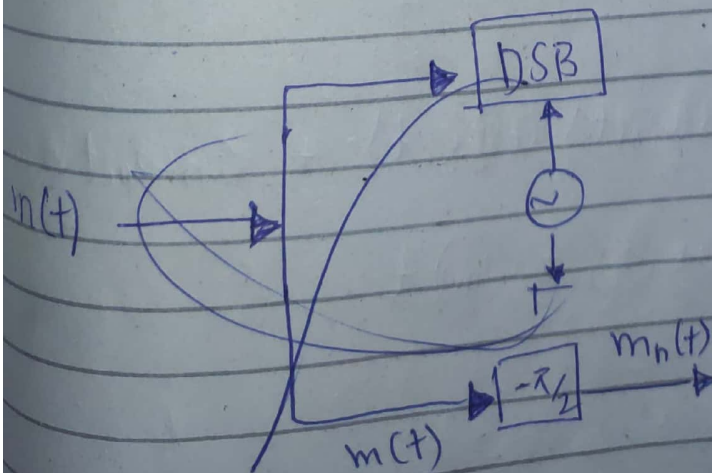
0.3 KHz to 3.4 KHz

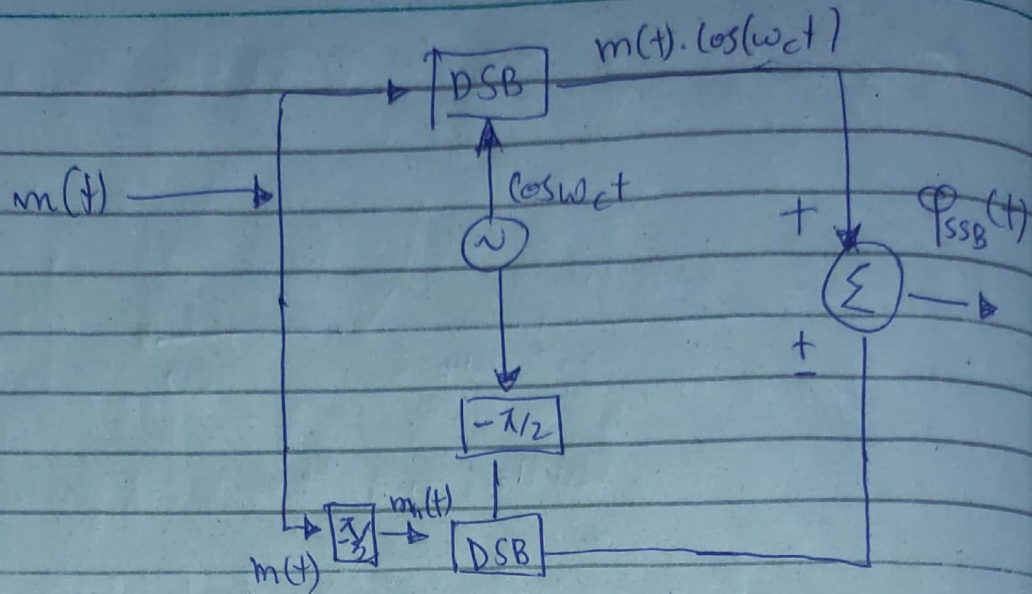


Speech signal can be isolated by practical filter bcoz freq. Hole

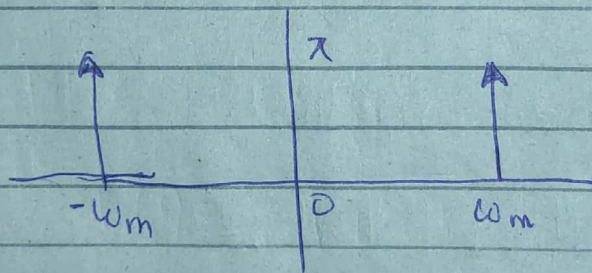
New possible method.

(ii) Phase Shift Method :-





★ Can we generate using above diagram?
 Theoretically yes.
 b/c hilbert transformation will
 applying constant transformation on
 every freq. component (ideal case).
 $m(t) = \cos(\omega_m t)$

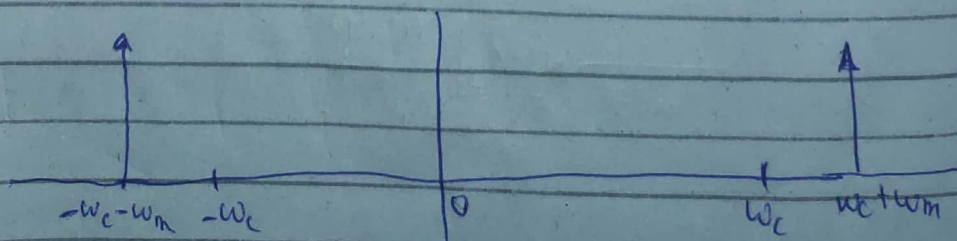


$$m_n(t) = \cos(\omega_m t - \frac{\pi}{2})$$

$$= \sin \omega_m t$$

$$\phi_{SSB}(t) = \cos(\omega_m t) \cos(\omega_c t) + \sin \omega_m t \sin \omega_c t$$

$$= \cos(\omega_c \pm \omega_m) t$$



Multiplying $\phi_{SSB}(t)$ with $\cos \omega_c t$

$$\phi_{SSB}(t) = m(t) \cos^2 \omega_c t + m_n(t) \sin \omega_c t \cos \omega_c t$$

$$\phi_{SSB}(t) = \frac{m(t)}{2} + \frac{m(t) \cos(2\omega_c t)}{2} + \frac{m_n(t) \sin 2\omega_c t}{2}$$

$$= \underbrace{M(\omega)}$$

Low Pass filter, Coherent Detection

Now we will send carrier along.

$$\phi_{SSB}(t) = \underbrace{A \cdot \cos \omega_c t + m(t) \cdot \cos \omega_c t + m_n(t) \cdot \sin \omega_c t}_{+c}$$

$$|| = (A + m(t)) \cdot \cos \omega_c t + m_n(t) \cdot \sin \omega_c t$$

$$|| = E(t) \cdot \cos(\omega_c t + \theta)$$

$$\text{as } \frac{a+ib}{\sqrt{a^2+b^2}}$$

$$\text{Now if } E(t) = \sqrt{[A+m(t)]^2 + m_n^2(t)}$$

Similar to

$$a_n \cdot \cos n\omega_c t + b_n \cdot \sin n\omega_c t$$

$$c_n = \sqrt{a_n^2 + b_n^2}$$

Now

$$E(t) = \left(A^2 + m^2(t) + 2 \cdot A \cdot m(t) + m_n^2(t) \right)^{1/2}$$

$$E(t) = A \left[1 + \frac{2m(t)}{A} + \frac{m^2(t)}{A^2} + \frac{m_n^2(t)}{A^2} \right]^{1/2}$$

if $m(t) \ll A$
then

$$E(t) \approx A \left[1 + \frac{2m(t)}{A} \right]^{1/2}$$

Now using binomial theorem

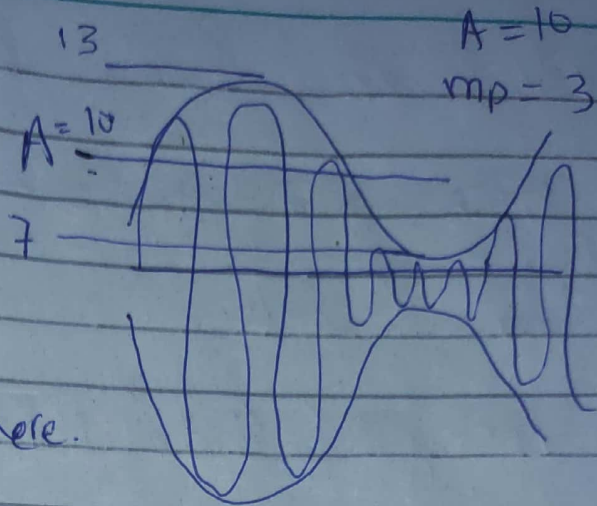
$$E(t) \approx A \left[1 + \frac{1}{2} \times \frac{2m(t)}{A} \right]$$

$$E(t) \approx A + m(t)$$

Now put in above equations

$$P_{SSB}(t) = [A + m(t)] \cos(\omega_c t + \theta)$$

We are using extra power here.



$$\eta = \frac{M^2}{2+M^2} = \frac{1}{3} \times 100 = 33.33\%$$

8/12/2023

$$\begin{aligned} \phi_{\text{DSB-SC}}(t) &= m(t) \cdot \cos(\omega_c t) \\ \phi_{\text{DSB+SC}}(t) &= [A + m(t)] \cos(\omega_c t) \end{aligned} \quad \left. \vphantom{\begin{aligned} \phi_{\text{DSB-SC}}(t) &= m(t) \cdot \cos(\omega_c t) \\ \phi_{\text{DSB+SC}}(t) &= [A + m(t)] \cos(\omega_c t) \end{aligned}} \right\} 2B\text{Hz}$$

$$\phi_{\text{QAM}}(t) = m_1(t) \cos(\omega_c t) + m_2(t) \sin(\omega_c t)$$

$$\phi_{\text{SSB}}(t) = m(t) \cdot \cos(\omega_c t) \mp m_n(t) \sin(\omega_c t)$$

- (i) Selective Filtering Method
- (ii) Phase shift

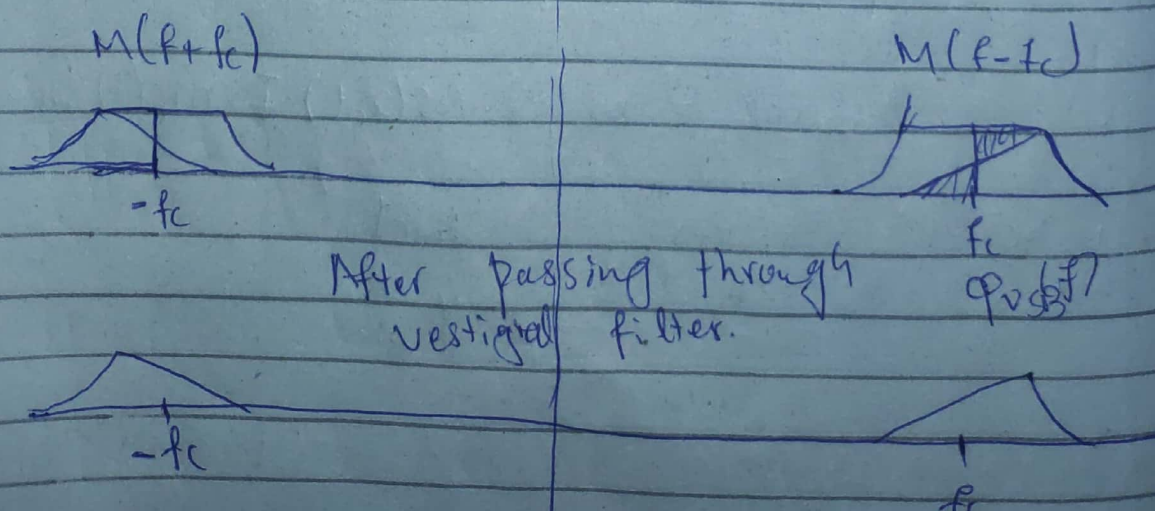
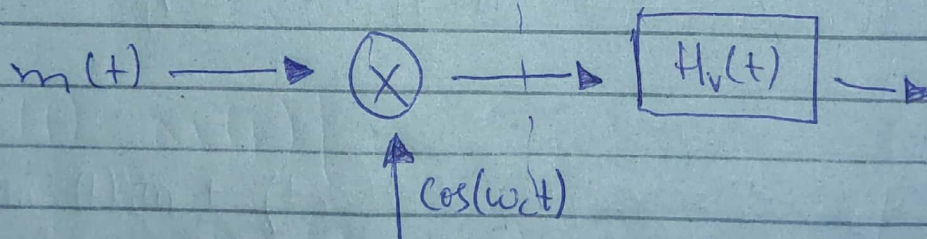
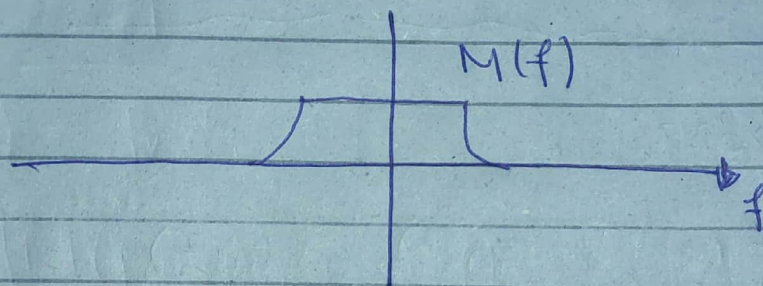
We have two extremes here

$$DSB \rightarrow 2B \text{ Hz} \quad SSB \rightarrow B \text{ Hz}$$

Now comes:

★ Vestigial Side Band Modulation:-

$$B_{HE} < B_T < 2B \text{ Hz}$$



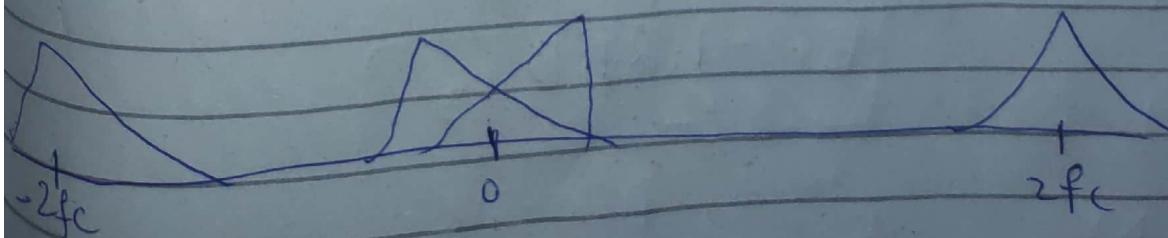
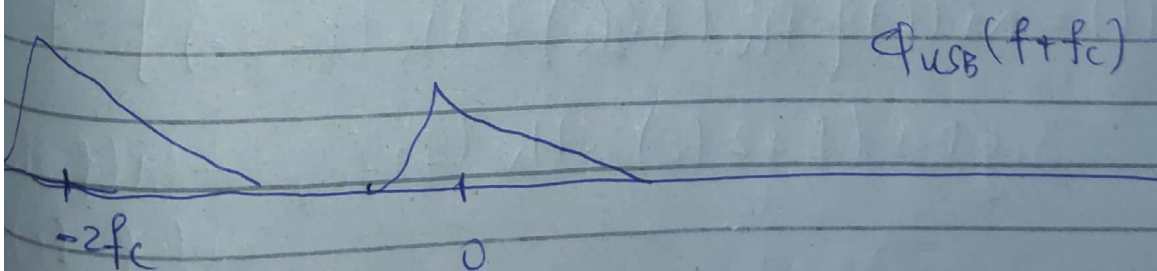
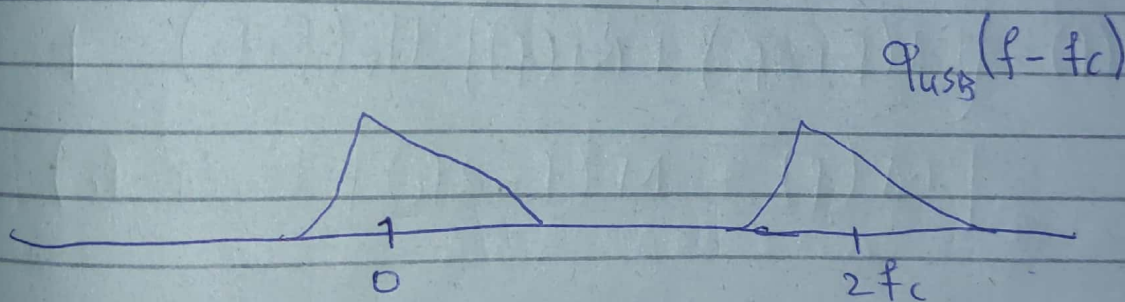
W Demodulation.

$$\varphi(t)_{\text{DSB-SC}} = m(t) \cdot \cos(\omega_c t) \quad \text{Modulation}$$

Multiply $\cos(\omega_c t)$ at receiver's end.

$$s(t) = \varphi_{\text{USB}}(t) \cdot \cos(\omega_c t) \quad \text{demodulation.}$$

$$s(f) = \varphi_{\text{USB}}(f - f_c) + \varphi_{\text{USB}}(f + f_c)$$



Now at sender's end we have

$$P_{VSB}^{(f)} = [M(f + f_c) + M(f - f_c)] H_v(f)$$

$$\begin{aligned} \text{Now } P_{VSB}(f + f_c) &= [M(f + 2f_c) + M(f)] H_v(f + f_c) \\ P_{VSB}(f - f_c) &= [M(f) + M(f - 2f_c)] H_v(f - f_c) \end{aligned}$$

Now if we add these two, get

$$S(f) = P_{VSB}(f + f_c) + P_{VSB}(f - f_c)$$

$$S(f) = [M(f + 2f_c) + M(f)] H_v(f + f_c) + [M(f) + M(f - 2f_c)] H_v(f - f_c)$$

$$S(f) = M(f) [H_v(f + f_c) + H_v(f - f_c)] + M(f + 2f_c) H_v(f + f_c) + M(f - 2f_c) H_v(f - f_c)$$

Typical value for Bandwidth is;

$$B_T = 1.2 B \text{ Hz}$$

Now to recover $M(f)$ we

will pass it through Low Pass
filter.

$$M(f) = S(f) + H_{LPF}(f)$$

Hence.

$$M(f) = m(f) [H_v(f+f_c) + H_v(f-f_c)]$$

$H_{LPF}(f)$

$$0 = H_v(f+f_c) +$$

$$H_{LPF}(f) = \frac{1}{H_v(f+f_c) + H_v(f-f_c)}$$

* Carrier Acquisition:-

$$m(t) \cdot \cos \omega_c t \cdot \cos ((\omega_c + \Delta \omega)t + \delta)$$

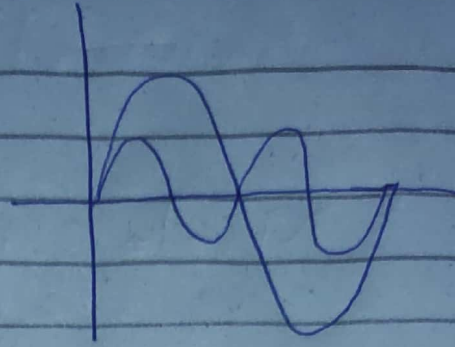
Now $\cos \alpha \cdot \cos \beta = \cos(\alpha + \beta) + \cos(\alpha - \beta)$

$$m(t) \cdot \cos(\Delta \omega t + \delta) + m(t) \cdot \cos(2\omega_c t + \Delta \omega t + \delta)$$

By passing through LPF

$$m(t) \cdot \cos(\Delta \omega t + \delta)$$

$$f = \frac{d\phi(t)}{dt}$$



Case

① Now if $\Delta\omega = 0$, $\delta = \text{const.}$

$$m(t) \cdot \cos(\delta)$$

e.g.

Hence, shape of $m(t)$ will not be changed. Hence it is distortionless.

Case ② $\Delta\omega = \text{same value, } \delta = 0$

$$m(t) \cdot \cos(\Delta\omega t)$$

Signal will be distorted.

So, we need carrier acquisition.

Carrier Acquisition:-

(i) Pilot Signal:-

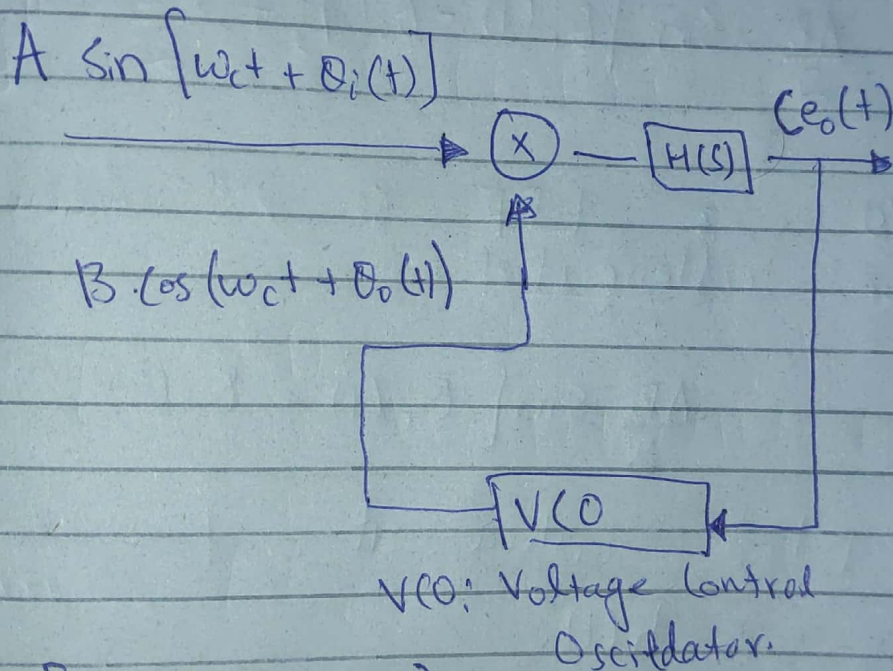
DSB-SC

$$[A + m(t)] \cos \omega_c t$$

- (ii) Phase Loop Lock:-
 (iii) Squaring Method:-

Phase Loop Lock:-

system. This is a feedback



$[\theta_i(t) - \theta_o(t)] \propto e_o$
 will create voltage

$$\omega_i = \omega_c + C \cdot e_o(t) \quad \text{--- (i)}$$

$$\phi(t) = \omega_c t + \theta_o(t)$$

$$\frac{d}{dt} \phi(t) = \frac{d}{dt} (\omega_c t) + \frac{d}{dt} (\theta_o(t))$$

$$\omega_i = \omega_c + \dot{\theta}_o(t) \quad \text{--- (ii)}$$

Compare (i) and (ii)

$$\dot{\theta}_o(t) = C \cdot e_o(t)$$

Now output of multiplier B:

$$A \cdot \sin(\omega_c t + \theta_i(t)) \cdot B \cdot \cos[\omega_c t + \theta_o(t)]$$

$$\frac{AB}{2} \cdot \sin[\theta_i(t) - \theta_o(t)] + \frac{AB}{2} \sin[2\omega_c t + \theta_i(t) + \theta_o(t)]$$

H(s) is a LPF so 2nd term will be attenuated.

$$\frac{AB}{2} \sin[\theta_i(t) - \theta_o(t)]$$

Now when it passes through $h(t)$.

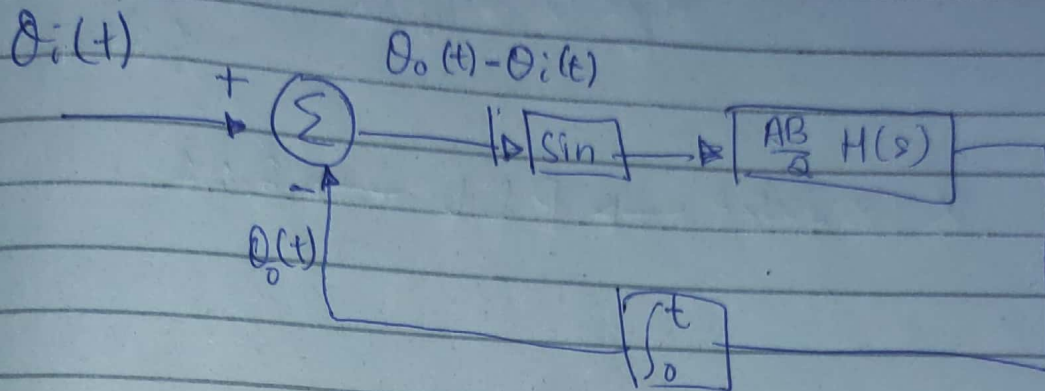
$$\frac{AB}{2} [h(t) * \sin[\theta_i(t) - \theta_o(t)]]$$

$$C e_o(t) = \frac{AB}{2} \int_0^t h(t-x) \cdot \sin[\theta_i(x) - \theta_o(x)] dx$$

$$\text{Put } C e_o(t) = \dot{\theta}_o(t)$$

$$\int \dot{\theta}_o(t) = \frac{AB}{2} \int_0^t \text{---} dx$$

$$\theta_o(t) =$$



(iii) Squaring Method:-

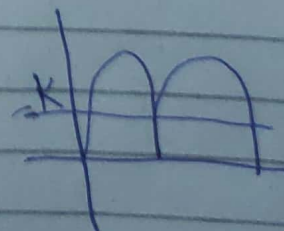
$$m(t)^2 (\cos \omega_c t)$$

$$\frac{m^2(t) \cdot [1 + \cos(2\omega_c t)]}{2}$$

$$\frac{m^2(t)}{2} + \frac{m^2(t) \cos(2\omega_c t)}{2}$$

Let $\frac{m^2(t)}{2} = K + \phi(t)$

Average value



$$\frac{m^2(t)}{2} + \frac{[K + \phi(t)] \cos(2\omega_c t)}{2}$$

$m(t) \rightarrow B \text{ Hz}$
 $m^2(t) \rightarrow 2B \text{ Hz}$

$$\frac{m^2(t)}{2} + \frac{K \cos 2\omega_c t}{2} + \frac{\phi(t) \cos 2\omega_c t}{2}$$

High Quality Q Narrowband
filter

$K \cos 2\omega_c t \rightarrow PLL \rightarrow 2:1$