

Chapter 1

Recall of Thermodynamics

1.1 A short recap of thermodynamics definitions

The systems we are considering are

1. In equilibrium with an external bath at fixed temperature T .
2. Made by a (large) number N of degrees of freedom. For instance, we remind that $1 \text{ mol} \approx N_A \sim 10^{23}$ elementary units.

Thermodynamic is a macroscopic theory of matter at equilibrium. It starts either from experimental observations or from *axiomatic assumptions* and establishes rigorous relations between macroscopic variables (**observables**) to describe systems at equilibrium. One of the first important concept is the one of **extensive variables**. For instance, the extensive variables that characterize the system at equilibrium are the internal energy U , volume V , number of particles N and magnetization \vec{M} that "scale with the system". In general, the extensive variable are additive.

In thermodynamic, it is important the concept of walls and thermodynamic constraints that are necessary for a complete definition of a thermodynamic system. With their presence or absence it is possible to control and redistribute the thermodynamic variables for changing the system. The typical walls are:

- **Adiabatic walls:** no heat flux. If it is removed we obtain a *diathermic walls*.
- **Rigid walls:** no mechanical work. If it is removed we obtain a *flexible or mobile walls*.
- **Impermeable walls:** no flux of particles (the number of particles remain constraints). If it is removed we obtain a *permeable walls*.

1.2 Equilibrium states

Consider a system in an equilibrium state, if the system changes our aim is to study the next equilibrium state of the system. Therefore we move from a system in equilibrium to another. The fundamental problem of thermodynamics is how to characterize the new system.

Now, we define the concept of **equilibrium states**. Consider macroscopic states that are fully described by *extensive* variables such as the internal energy U , the volume V , the number of particles N , the magnetization \vec{M} , etc If these variables are time independent, the system is in a *steady state*. If moreover there are no macroscopic currents, the system is at *equilibrium*. Therefore, we describe a system by characterizing all the extensive variables at equilibrium.

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Suppose that the system changes slow in time, it goes from an equilibrium state to another one and the transformation is so slow that in each Δt the system is at equilibrium. Therefore, consider a sequence of equilibrium states, the **quasi-static transformation** are described by the 1st Law of Thermodynamic:

$$dU = \delta Q - \delta W \quad (1.1)$$

The variation of the internal energy of the systems depends by two factors, δw that is the work done by the system during a *quasi-static process* (infinitively slow), and δQ that is the heat absorbed by the system during the process. Remember that we write dU because it is a differential quantity, while the other quantities with the δ are only small quantities. Therefore, dU is a function of state, the other are not.

Remark. The convention is $\delta Q > 0$ if the heat is absorbed by the system, and $\delta W > 0$ if the work is done by the system.

For example, for a simple fluid with a given pressure if we change the volume, the work done by the systems is $\delta W = P dV$. For a magnetized system, we have $\delta W = -\vec{H} \cdot d\vec{M}$.

In conclusion, starting from an equilibrium state and removing some constraints (i.e. wall properties), we want to find the new equilibrium state compatible with the new constraints.

Suppose a system with adiabatic rigid impermeable constraints. The system on the left is characterized by V_1, N_1, U_1 , the one on the right by V_2, N_2, U_2 . There are many ways for solving this problem. We use the most general way, that is by using the *maximum entropy principle*. If exists a function S of the extensive variables of the system that is defined for all equilibrium states, we call it **entropy** and the fundamental relation is

$$S = S(U, V, N) \quad (1.2)$$

The new values taken by the extensive parameters when a constraint has been removed are the ones that *maximize* S . It means $dS = 0$ and $d^2S < 0$, given the remaining constraint.

The properties of S are:

1. S is an additive function with respect to the subsystems in which the system is partitioned:

$$S = \sum_{\alpha} S^{(\alpha)} \quad (1.3)$$

2. S is differentiable and *monotonically increasing* with respect to the internal energy U . It means that $(\frac{\partial S}{\partial U})_{V,N} > 0$.

3. For each subsystem (α) we have:

$$S^{(\alpha)} = S^{(\alpha)}(U^{(\alpha)}, V^{(\alpha)}, N^{(\alpha)}) \quad (1.4)$$

This fundamental relation holds for each subsystem.

4. S is an *homogeneous function* of 1st order with respect to the extensive parameters, namely:

$$S(\lambda U, \lambda V, \lambda N) = \lambda S(U, V, N), \quad \forall \lambda > 0 \quad (1.5)$$

It means that S is an extensive quantity.

Remark. Since S is monotonically increasing in U , the following inequality holds:

$$\left(\frac{\partial S}{\partial U}\right)_{V,N} > 0$$

Therefore, we have $\left(\frac{\partial S}{\partial U}\right)_{V,N} \neq 0$ and it can be inverted locally.

Afterwards, $S = S(U, V, N)$ inverted in U gives the second fundamental relation

$$U = U(S, V, N) \quad (1.6)$$

It means that, we can look at S or U and, when these quantities are known, all the informations about the system can be obtained.

By taking the differential of the fundamental relation

$$U = U(S, V, N_1, \dots, N_r) \quad (1.7)$$

one gets

$$dU = \underbrace{\left(\frac{\partial U}{\partial S}\right)_{V,N_j}}_{\substack{T \\ \text{absolute} \\ \text{temperature}}} dS + \underbrace{\left(\frac{\partial U}{\partial V}\right)_{S,N_j}}_{\substack{-P \\ \text{pressure}}} dV + \sum_{j=1}^r \underbrace{\left(\frac{\partial U}{\partial N_j}\right)_{S,V}}_{\substack{\mu_j \\ \text{electrochemical} \\ \text{potential}}} dN_j \quad (1.8)$$

1.3 Equations of states

Now, we define another set of variables that are called **intensive variables**. The term *intensive* means that it is independent of the size of the system, namely that the value of the variable relative to a subsystem is equal to that of the whole system. The intensive variables are themselves functions of S, V, N , and examples of intensive variables are the pressure, P , and the temperature of the system, T .

The **state equations** are defined as:

$$T = T(S, V, N_1, \dots, N_r) \quad (1.9a)$$

$$P = P(S, V, N_1, \dots, N_r) \quad (1.9b)$$

$$\mu_j = \mu_j(S, V, N_1, \dots, N_r) \quad (1.9c)$$

Remark. If all the state equations are known, the fundamental relation is determined a part from a constant. It means that the coefficients of the differential (1.8) are known.

Example 1. Suppose an *ideal* gas, for which is valid the relation

$$PV = NK_b T \quad (1.10)$$

The *Van-Der Waals equation* of the state is

$$\left(P + \frac{\alpha N^2}{V^2}\right)(V - Nb) = NK_b T \quad (1.11)$$

Another equation of state for magnetic systems is the *Curie Law*:

$$M = \frac{CH}{T} \quad (1.12)$$

We compute $\left(\frac{\partial U}{\partial M}\right)_{S,N} = H$.

The state equations are homogenous functions of *zero* degree:

$$T(\lambda S, \lambda V, \lambda N) \stackrel{0}{=} T(S, V, N) \quad (1.13)$$

At equilibrium the temperature of a subsystem is equal to the one of the whole system. Similarly

$$P(\lambda S, \lambda V, \lambda N) = P(S, V, N) \quad (1.14)$$

Now, we keep S parameter separates from the other that are substituted by *generalized displacements*, as $(V, N_1, \dots, N_r) \rightarrow X_j$. The fundamental relation is

$$U = U(S, X_1, \dots, X_{r+1}) \quad (1.15)$$

We define:

$$\left(\frac{\partial U}{\partial S} \right) \equiv T \quad (1.16a)$$

$$\left(\frac{\partial U}{\partial X_j} \right) \equiv P_j \quad (1.16b)$$

The differential is written as the following:

$$dU = T dS + \sum_{j=1}^{r+1} P_j dX_j \quad (1.17)$$

where $P_1 = -P$ is the *pressure* and $X_1 = V$ is the volume.

From the equilibrium condition, $dU = 0$, one can get a relation between intensive variables in differential form as the **Gibbo-Duhem relation**:

$$S dT + \sum_{j=1}^{r+1} X_j dP_j = 0 \quad (1.18)$$

For a one-component simple fluid system, the equation (1.18) simplifies into

$$S dT - V dP + N d\mu = 0 \quad (1.19)$$

and dividing by the number of moles N

$$d\mu = -s dT + v dP \quad (1.20)$$

that is the Gibbs-Duhem relation in *molar form*.

For a magnetic system we have $dU = T dS + \vec{\mathbf{H}} \cdot d\vec{\mathbf{M}} + \mu dN$.

Remark. Note that $\mu = \mu(T, P)$ is a relation between intensive variables.

To summarize, the fundamental relations are $S = S(U, V, N_1, \dots, N_r)$ or $S = S(U, \vec{\mathbf{M}}, N_1, \dots, N_r)$ for magnetic systems. In the energy representation we have $U = U(S, V, N_1, \dots, N_r)$ or $U = U(S, \vec{\mathbf{M}}, N_1, \dots, N_r)$.

1.4 Legendre transform and thermodynamic potentials

In many situations it is convenient to change some extensive variables with their conjugate intensive ones that became independent and free to vary. We have new thermodynamic potentials. It works as following; suppose we have a function as

$$Y = Y(X_0, X_1, \dots, X_k, \dots, X_{r+1}) \quad (1.21)$$

such that Y is *strictly convex* in say, X_k ($\frac{\partial^2 Y}{\partial X_k^2} > 0$) and smooth. The idea is to find a transformation such that $Y = Y(X_0, X_1, \dots, P_k, \dots, X_{r+1})$, where

$$X_k \rightarrow P_k \equiv \frac{\partial Y}{\partial X_k} \quad (1.22)$$

i.e. P_k substitutes X_k as a new independent variable. In mathematic this is called *Legendre transform*.

Thermodynamic potentials are extremely useful tools, whose name derives from an analogy with mechanical potential energy: as we will later see, in certain circumstances the work obtainable from a macroscopic system is related to the change of an appropriately defined function, the thermodynamic potential. They are useful because they allow one to define quantities which are experimentally more easy to control and to rewrite the fundamental thermodynamic relations in terms of them.

Mathematically all the thermodynamic potentials are the result of a Legendre transformation of the internal energy, namely they are a rewriting of the internal energy so that a variable has been substituted with another.

Example 2. Suppose we want to replace the entropy S with its conjugate derivative

$$T = \frac{\partial U}{\partial S}$$

One starts from the fundamental relation

$$U = U(S, V, N_1, \dots)$$

and transforms U such that S is replaced by T as new independent variable. Let us consider the transformation

$$A \equiv U - S \frac{\partial U}{\partial S} = U - TS$$

By differentiating A we get

$$dA = dU - T dS - S dT$$

On the other hand

$$dU = T dS + \sum_j P_j dX_j$$

It implies that

$$dA = -S dT + \sum_j P_j dX_j$$

For such a system we have $A = A(T, V, N_1, \dots, N_r)$. It is a function of T instead of S , as wanted. Similarly for a magnetic system $A = A(T, \vec{M}, N_1, \dots, N_r)$.

Helmholtz free energy

The **Helmholtz free energy** is defined as:

$$A \equiv U - TS \quad (1.23)$$

In terms of heat and mechanical work, since $dU = \delta Q - \delta W$:

$$dA = dU - d(TS) = \delta Q - T dS - S dT - \delta W \quad (1.24)$$

Hence,

$$\delta W = (\delta Q - T dS) - S dT - dA \quad (1.25)$$

On the other hand, for a *reversible transformation* we have $\delta Q = T dS$, which implies

$$\delta W = -S dT - dA \quad (1.26)$$

If the reversible transformation is also *isothermal*, $dT = 0$ and we obtain $dA = dW$. It is reminiscent of a potential energy.

Remark. For an isothermal but *not reversible* (spontaneous) process we know the 2nd Law of Thermodynamics

$$\delta Q \leq T dS \quad (1.27)$$

which implies

$$(\delta W)_{irr} = \delta Q - T dS - dA \leq -dA.$$

Hence, if $\delta W = 0$ and $dT = 0$, we have $dA \leq 0$. Therefore, in a spontaneous (irreversible) process, the thermodynamic system, as a function of T, V, N etc, evolves towards a *minimum* of the Helmholtz free energy $A = A(T, V, N_1, \dots, N_r)$.

In the case of a system with (P, V, T) we have:

$$dA = -S dT - P dV + \sum_j \mu_j dN_j \quad (1.28)$$

where

$$-S = \left(\frac{\partial A}{\partial T} \right)_{V, N_j} \quad (1.29a)$$

$$-P = \left(\frac{\partial A}{\partial V} \right)_{T, N_j} \quad (1.29b)$$

$$\mu_j = \left(\frac{\partial A}{\partial N_j} \right)_{T, V} \quad (1.29c)$$

For a magnetic system (\vec{H}, \vec{M}, T) :

$$dA = -S dT + \vec{H} \cdot d\vec{M} + \sum_j \mu_j dN_j \quad (1.30)$$

with

$$H_\alpha = \left(\frac{\partial A}{\partial M_\alpha} \right)_{T, \{N_j\}} \quad (1.31)$$

Hentalpy

The **Hentalpy** is the partial Legendre transform of U that replaces the volume V with the pressure P as independent variable.

Consider $U = U(S, V, N_1, \dots, N_r)$ and $-P = \frac{\partial U}{\partial V}$, we define the hentalpy as

$$H = U + PV \quad (1.32)$$

Remark. Note that the plus sign in the definition of the hentalpy is just because the minus of the P .

We have:

$$\begin{aligned} dH &= dU + P dV + V dP \\ &= T dS - P dV + \sum_j \mu_j dN_j + P dV + V dP \\ &= T dS + V dP + \sum_j \mu_j dN_j \end{aligned} \quad (1.33)$$

Finally, we obtain the relation $H = H(S, P, N_1, \dots, N_r)$.

Gibbs potential

The **Gibbs potential** is obtained by performing the Legendre transform of U to replace S and V with T and P .

Consider again $U = U(S, V, N_1, \dots, N_r)$ and $T = \frac{\partial U}{\partial S}$, $-P = \frac{\partial U}{\partial V}$, then we have:

$$G = U - TS + PV = A + PV \quad (1.34)$$

For a simple fluid system

$$\begin{aligned} dG &= dU - T dS - S dT + P dV + V dP \\ &= T dS - P dV + \sum_j \mu_j dN_j - T dS - S dT + P dV + V dP \\ &= -S dT + V dP + \sum_j \mu_j dN_j \end{aligned} \quad (1.35)$$

Hence, $G = G(T, P, N_1, \dots, N_r)$.

For a magnetic system, the Gibbs potential is defined as

$$G = A - \vec{\mathbf{M}} \cdot \vec{\mathbf{H}} \quad (1.36)$$

and

$$\begin{aligned} dG &= dA - d\vec{\mathbf{M}} \cdot \vec{\mathbf{H}} = d(U - TS) - d(-\vec{\mathbf{M}} \cdot \vec{\mathbf{H}}) \\ &= dU - T dS - S dT - d\vec{\mathbf{M}} \cdot \vec{\mathbf{H}} - \vec{\mathbf{M}} \cdot d\vec{\mathbf{H}} \\ &= T dS + \vec{\mathbf{H}} \cdot d\vec{\mathbf{M}} - T dS - S dT - d\vec{\mathbf{M}} \cdot \vec{\mathbf{H}} - \vec{\mathbf{M}} \cdot d\vec{\mathbf{H}} \\ &= -S dT - \vec{\mathbf{M}} \cdot d\vec{\mathbf{H}} \end{aligned} \quad (1.37)$$

and finally $G = G(T, \vec{\mathbf{H}})$ and also

$$S = -\left(\frac{\partial G}{\partial T}\right)_{\vec{\mathbf{H}}} \quad (1.38a)$$

$$\vec{\mathbf{M}} = -\left(\frac{\partial G}{\partial \vec{\mathbf{H}}}\right)_T \quad (1.38b)$$