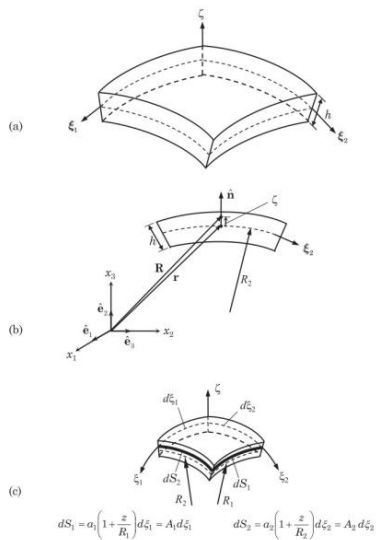




# NONLINEAR BENDING OF SHELLS

- Shells are much like plates except that they are curved.
- FEM models of shells are developed using (1) shell theory or (2) 2-D equations obtained from a degenerated 3D elasticity model
- Shell theory are developed, are originally based on Kirchhoff-Love kinematic hypothesis
- Some group of shell theories is based on order magnitude on strains and rotations in full nonlinear equations (called finite rotation theories).
  - ▶ Strains and rotations about the normal to the surface are assumed to be of order  $\epsilon \ll 1$
  - ▶ Rotations about tangents to the surface are organised in a consistent classification where for each range of magnitude of rotations specific shell equations are obtained.
- Shells can be synclastic or anticlastic. A curved surface is developable if it can be developed to a plane without stretching. Nondevelopable requires cutting or deforming. These are stronger than developable because they need additional forces to collapse to planar surfaces.



**Fig. 8.2.1:** (a) Shell geometry. (b) Position vector of a point and coordinates on the middle surface. (c) Position vectors of points on the middle surface and above the middle surface.

- Take a curved shell element of uniform thickness. Here  $(\xi_1, \xi_2, \zeta)$  which denote the curvilinear coordinates such that  $\xi_1, \xi_2$  curves are the lines of crvature of the middle surface ( $\zeta = 0$ ).
- The position vector of a point  $(\xi_1, \xi_2, 0)$  is denote by  $\mathbf{r}$  and any other arbitrary point is denoted by  $\mathbf{R}$
- A differential line element on the middle suface can be written as

$$d\mathbf{r} = \frac{\partial \mathbf{r}}{\partial \xi_a} d\xi_a = \mathbf{g}_a d\xi_a, \quad \mathbf{g}_a = \frac{\partial \mathbf{r}}{\partial \xi_a} \quad (a = 1, 2) \quad (1)$$

where the vectors  $\mathbf{g}_1$  and  $\mathbf{g}_2$  are tangent to the  $\xi_1, \xi_2$  coordinates lines as shown.

- The components of the metric tensor  $g_{ab}$ ,  $(a,b=1,2)$  are

$$\mathbf{g}_a \cdot \mathbf{g}_b = g_{ab}, \quad p_1 = \sqrt{g_{11}}, \quad p_2 = \sqrt{g_{22}}, \quad \mathbf{g}_1 \cdot \mathbf{g}_2 = p_1 p_2 \cos \chi \quad (2)$$

where  $\chi$  denotes the angle between the coordinate curves.<sup>1</sup>

- The normal vector is found as

$$\mathbf{n} = \frac{\mathbf{g}_1 \times \mathbf{g}_2}{p_1 p_2 \sin \chi} \quad (3)$$

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<sup>1</sup>Note that  $\mathbf{n}, p_1, p_2$  are functions of  $\xi_1, \xi_2$

- The square of the distance  $dS$ , say between points  $(\xi_1, \xi_2, 0)$  and  $(\xi_1 + d\xi_1, \xi_2 + d\xi_2, 0)$  on the middle surface is given by

$$(ds)^2 = d\mathbf{r} \cdot d\mathbf{r} = g_{ab} d\xi_a d\xi_b = p_1^2 (d\xi_1)^2 + p_2^2 (d\xi_2)^2 + 2a_1 a_2 \cos \chi d\xi_1 d\xi_2 \quad (4)$$

The RHS is called the first quadratic form of the surface which allows us to find infinitesimal lengths, angles and area. The terms  $p_1^2$ ,  $p_2^2$ ,  $p_1 p_2 \cos \chi$  are called the first fundamental quantities

- Let  $\mathbf{r} = \mathbf{r}(s)$  be the equation of a curve  $s$  on the surface. The unit vector tangent to the curve is

$$\hat{\mathbf{t}} = \frac{d\mathbf{r}}{ds} = \frac{\partial \mathbf{r}}{\partial \xi_a} \frac{\partial \xi_a}{\partial s} = \mathbf{g}_a \frac{\partial \xi_a}{\partial s} \quad (5)$$

Im not writing this because the conventions are too long. Please check the annotated book