

## Double-Sideband Amplitude Modulation

- Amplitude of the carrier is varied in proportion to the baseband(message) signal.
- Modulation:**

$$\begin{aligned} \text{message signal} &: m(t) \\ \text{carrier signal} &: \cos(\omega_c t) \\ \text{modulated signal} &: m(t)\cos(\omega_c t) = \frac{1}{2}m(t)e^{-j\omega_c t} + \frac{1}{2}m(t)e^{j\omega_c t} \\ \text{Spectrum} &: M(\omega) \rightarrow \frac{1}{2}[M(\omega + \omega_c) + M(\omega - \omega_c)] \end{aligned}$$

- Demodulation: Synchronous/Coherent demodulation**

$$\begin{aligned} m(t)\cos(\omega_c t) \times \cos(\omega_c t) &= \frac{1}{2}m(t)\cos(2\omega_c t) + \frac{1}{2}m(t) \\ \text{spectrum} &: \frac{1}{4}[M(\omega + 2\omega_c) + M(\omega - 2\omega_c)] + \frac{1}{2}M\omega \end{aligned}$$

## Amplitude Modulation

- Motivation:** coherent demodulation of DSB-SC requires the receiver to generate a carrier. To simplify receiver, we use AM.
- Modulation:**

$$\begin{aligned} \text{Message signal} &: m(t) \\ \text{Carrier signal} &: \cos(\omega_c t) \\ \text{Modulated signal} &: (A + m(t))\cos(\omega_c t) \\ \text{Spectrum} &: M(\omega) \rightarrow \frac{1}{2}[M(\omega + \omega_c) + M(\omega - \omega_c)] + \frac{A}{2}[\delta(\omega + \omega_c) + \delta(\omega - \omega_c)] \end{aligned}$$

Drawback: Extra transmit power

- Demodulation: Envelope detector**

To ensure correct envelope detector, we must have

$$\begin{aligned} A + m(t) &> 0 \quad \text{for all } t \\ \text{Define : } \mu - \text{Modulation index, } \mu &= \frac{m_p}{A} \end{aligned}$$

Envelope detection requires that

$$0 \leq \mu \leq 1$$

- Side Band and Carrier Power**

- Advantage of envelope detection is achieved under the expense of extra energy

$$\phi_{AM}(t) = A\cos(\omega_c t) + m(t)\cos(\omega_c t), \text{ where } A\cos\omega_c t \rightarrow \text{carrier}, m(t)\cos\omega_c t \Rightarrow \text{sideband}$$

$$P_c = \frac{1}{T} \int_{\frac{T_c}{2}}^{\frac{T_c}{2}} A^2 \cos^2 \omega_c t dt = \frac{A^2}{2}, P_s = \frac{1}{2} \overline{m^2(t)} = \frac{1}{2} P_m$$

- Power efficiency is as follows

$$\eta = \frac{P_s}{P_c + P_s} = \frac{\overline{m^2(t)}}{A^2 + \overline{m^2(t)}} \leq \frac{1}{3}$$

Given that when  $m(t) = \cos\omega_m t$ ,  $\eta$  reaches maximum

## Quadrature Amplitude Modulation

- Motivation:**

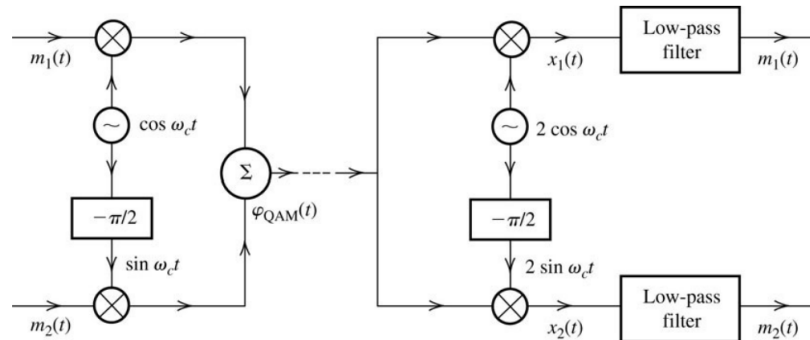
Using DSB-SC,

$$\begin{aligned} \text{if } m(t) \text{ real} &\rightarrow M(\omega) = M^*(-\omega) \\ \text{Modulated signal } \Phi(t) \text{ real} &\rightarrow \Phi(\omega) = \Phi^*(-\omega) \end{aligned}$$

We can tell that **only half** of the frequency spectrum of **message signal** and **one fourth** of the frequency spectrum of the **modulated signal** carries information.

- **Modulation:**

$$\begin{aligned} \text{baseband signals : } m_1(t), m_2(t) \\ \text{Modulated signal : } \Phi(t) &= m_1(t)\cos\omega_c t + m_2(t)\sin\omega_c t \\ \text{Spectrum : } \Phi(\omega) &= \frac{1}{2}(M_1(\omega - \omega_c) + M_1(\omega + \omega_c)) + \frac{j}{2}(M_1(\omega - \omega_c) - M_1(\omega + \omega_c)) \end{aligned}$$



- **Demodulation**

$$\begin{aligned} \text{Channel 1 : } \Phi(t)2\cos\omega_c t &= 2m_1(t)\cos^2\omega_c t + 2m_2(t)\cos\omega_c t\sin\omega_c t = m_1(t) + m_1(t)\cos 2\omega_c t + m_2(t)\sin 2\omega_c t \\ \text{Channel 2 : } \Phi(t)2\sin\omega_c t &= 2m_1(t)\sin\omega_c t\cos\omega_c t + 2m_2(t)\sin^2\omega_c t = m_1(t)\sin 2\omega_c t - m_2(t)\cos 2\omega_c t + m_2(t)\sin 2\omega_c t \end{aligned}$$

- **Complex View of Modulation:**

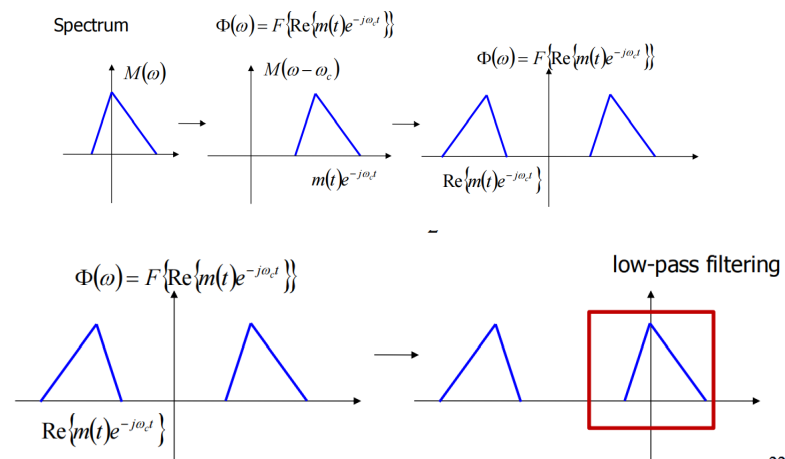
$$\text{Message signal : } m(t) = m_1(t) + jm_2(t) \rightarrow M(\omega) \neq M^*(-\omega)$$

- This implies that both positive and negative spectra carry information.

$$\begin{aligned} \text{Carrier signal : } \cos\omega_c t &= \text{Re}\{e^{-j\omega_c t}\} \\ \text{Modulated signal : } \text{Re}\{m(t)e^{-j\omega_c t}\} &= m_1(t)\cos\omega_c t + m_2(t)\sin\omega_c t \\ \text{Spectrum : } \Phi(\omega) &= F\{\text{Re}\{m(t)e^{-j\omega_c t}\}\} \end{aligned}$$

- **Demodulation:**

$$\Phi(t) \rightarrow \Phi(t)e^{j\omega_c t} \Rightarrow \Phi(\omega) \rightarrow \Phi(\omega + \omega_c) \rightarrow \text{lowpass filter} \rightarrow \frac{1}{2}M(\omega)$$



## Single Sideband Modulation

- **Modulation:**

$$\begin{aligned} \text{Step 1 : } m(t)\cos\omega_c t &\rightarrow \Phi(\omega) = \frac{1}{2}[M(\omega + \omega_c) + M(\omega - \omega_c)] \\ \text{Step 2 : } &\text{Bandpass filter to remove either the LSB or USB.} \end{aligned}$$

- **Hilbert Transform**

$$\text{Hilbert transform : } H(\omega) = -j \operatorname{sgn}(\omega) = \begin{cases} j & \omega \leq 0 \\ -j & \omega > 0 \end{cases}$$

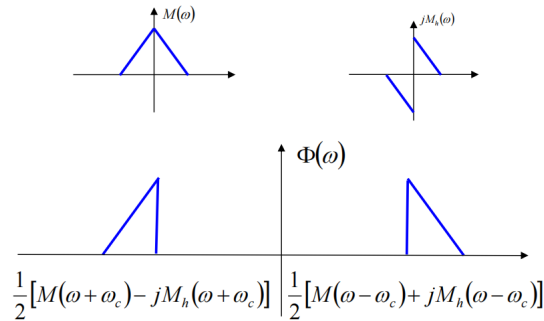
$$H(\omega) \xleftrightarrow{F} h(t) = F^{-1}(-j \operatorname{sgn}(\omega)) = \frac{1}{\pi t}$$

- SSB Modulation via Hilbert Transform

- Modulation:

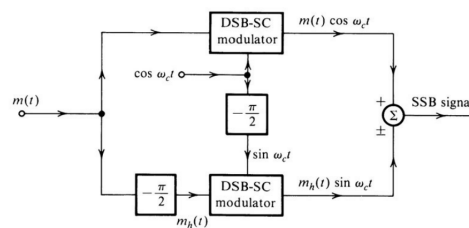
$$\Phi(t) = m(t) \cos \omega_c t + m_h(t) \sin \omega_c t, m_h(t) = m(t) * h(t), h(t) : \text{Hilbert transform}$$

$$\Rightarrow \Phi(\omega) = \frac{1}{2} [M(\omega + \omega_c) - jM_h(\omega + \omega_c)] + \frac{1}{2} [M(\omega - \omega_c) + jM_h(\omega - \omega_c)]$$



- Modulation Using Phase Shift:

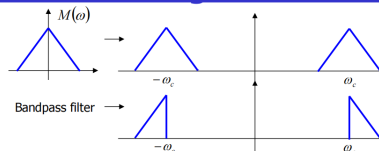
### Phase Shift SSB Modulator



- Modulation Using Selective Filtering:



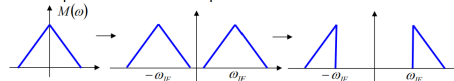
### Selective Filtering SSB Modulator



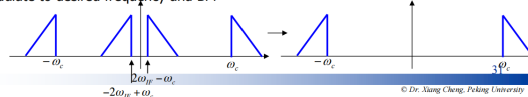
**Problem:** Sharp frequency cut off is very difficult to implement at high frequency

**Solution:** Two-step approach.

1. Modulate to a pre-determined low freq. carrier and BPF



2. Modulate to desired frequency and BPF



- Demodulation:

- 1. Coherent Demodulation:

$$\Phi(t) \cos \omega_c t = m(t) \cos^2 \omega_c t + m_h(t) \sin \omega_c t \cos \omega_c t = \frac{1}{2} m(t) + \frac{1}{2} [m(t) \cos 2\omega_c t + m_h(t) \sin 2\omega_c t]$$

- 2. Envelope Demodulation:

$$\begin{aligned}
& \text{Acquirements : } A \gg m^2(t) + m_h^2(t) \\
\Phi(t) + A \cos \omega_c t &= (A + m(t)) \cos \omega_c t + m_h(t) \sin \omega_c t = K(t) [\cos \theta_t \cos \omega_c t + \sin \theta_t a \sin \omega_c t] \\
K^2(t) &= (A + m(t))^2 + m_h^2(t) = A^2 \left[ 1 + \frac{2m(t)}{A} + \frac{m^2(t) + m_h^2(t)}{A^2} \right] \\
\Rightarrow \text{Envelope} &\approx \sqrt{1 + \frac{2m(t)}{A}} - 1 \approx \frac{m(t)}{A}
\end{aligned}$$

## Vestigial Sideband Modulation

- **Motivation:**

It's hard to implement a bandpass filter with sharp edges.

- **Modulation:**

$$\Phi_{VSB}(\omega) = [M(\omega - \omega_c) + M(\omega + \omega_c)]H_i(\omega), H_i(\omega) : \text{transmitter shaping filter.}$$

- **Demodulation:**

pass  $2\Phi_{VSB}(t) \cos \omega_c t$  through  $H_o(\omega), H_o(\omega) : \text{receiver shaping filter.}$

*Spectrum* :  $[\Phi_{VSB}(\omega + \omega_c) + \Phi_{VSB}(\omega - \omega_c)]H_o\omega = M(\omega)[H_i(\omega) + H_i(\omega - \omega_c)]H_o(\omega) + \text{high frequency term.}$

*Thus we require* :  $[H_i(\omega + \omega_c) + H_i(\omega - \omega_c)]H_o(\omega) = 1$

To simplify the filter used by the receiver, we want that

$$\begin{aligned}
H_i(\omega - \omega_c) + H_i(\omega + \omega_c) &= 1 \quad \text{for } |\omega_c| < 2\pi B \\
\Rightarrow H_o(\omega) &= 1
\end{aligned}$$

so that for the receiver, he only needs to do lowpass