Boundary Conditionsin lattice Boltzmann method

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Outline

- Introduction
 - Boundary Value Problems
- 2 Motivation
 - Navier-Stokes Boundary Conditions
- 3 Lattice Boltzmann Boundary Conditions
 - Problem definition
 - Boundaries in LBM
 - Particulate dynamics
 - Using Chapman-Enskog
- Summary



Outline

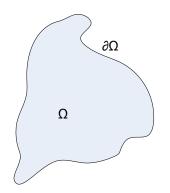
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 $\bullet \ \, \mathsf{Boundary} \,\, \mathsf{Value} \,\, \mathsf{Problem} \,\, \left\{ \begin{array}{c} \mathsf{Partial} \,\, \mathsf{Differential} \,\, \mathsf{Equation} \\ \mathsf{Boundary} \,\, \mathsf{Condition} \end{array} \right.$

Boundary Value Problem { Partial Differential Equation Boundary Condition

e.g. Poisson equation:

$$\begin{cases} \frac{\partial^2 \varphi}{\partial x^2} + \frac{\partial^2 \varphi}{\partial y^2} = f(x, y), & \text{in } \Omega \\ \varphi = \varphi_b, & \text{on } \partial \Omega \end{cases}$$



Types of Boundary Conditions

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→ Neumann Boundary Condition

$$\hat{\mathbf{n}} \cdot \nabla \varphi = \frac{\partial \varphi}{\partial n} = \varphi_b$$
 on $\partial \Omega$

→ Robin Boundary Condition

$$g\varphi + h\frac{\partial\varphi}{\partial n} = \varphi_b$$
 on $\partial\Omega$



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Steady isothermal and incompressible Navier-Stokes equations

$$\begin{cases} (\mathbf{u} \cdot \nabla)\mathbf{u} = -\nabla p + \nu \triangle \mathbf{u} + \mathbf{a} \\ \nabla \cdot \mathbf{u} = 0 \end{cases} \text{ in } \Omega$$

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Boundary Condition on solid walls

$$\mathbf{u} = \mathbf{u}_b \quad \text{on } \partial \Omega$$

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Boundary Condition on fluid boundaries

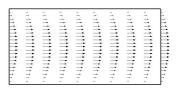
$$\mathbf{u} = \mathbf{u}_{in}$$
 on $\partial \Omega$

or

$$\begin{cases} -p + \nu \frac{\partial u_n}{\partial n} = (F_n)_{in} \\ \nu \frac{\partial u_t}{\partial n} = (F_t)_{in} \end{cases} \text{ on } \partial \Omega$$

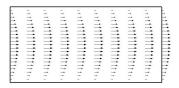
Periodic or Cyclic Boundary Conditions

$$\mathbf{u}(x,y) = \mathbf{u}(x+L,y)$$
 in $\Omega \Rightarrow \mathbf{u}_{in} = \mathbf{u}_{out}$ on $\partial\Omega$



Periodic or Cyclic Boundary Conditions

$$\mathbf{u}(x,y) = \mathbf{u}(x+L,y)$$
 in $\Omega \Rightarrow \mathbf{u}_{in} = \mathbf{u}_{out}$ on $\partial\Omega$



Symmetry Boundary Conditions

$$\mathbf{u} \cdot \mathbf{n} = 0$$
 and $\frac{\partial \mathbf{u}}{\partial n} = 0$ on $\partial \Omega$



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$$f_{\alpha}(\mathbf{x} + \mathbf{c}_{\alpha}\Delta t, t + \Delta t) = f_{\alpha}(\mathbf{x}, t) - \omega(f_{\alpha} - f_{\alpha}^{(eq)})|_{(\mathbf{x}, t)}$$
 in Ω

Lattice Boltzmann method (LBM)

$$f_{\alpha}(\mathbf{x} + \mathbf{c}_{\alpha}\Delta t, t + \Delta t) = f_{\alpha}(\mathbf{x}, t) - \omega(f_{\alpha} - f_{\alpha}^{(eq)})|_{(\mathbf{x}, t)}$$
 in Ω

Hydrodynamic Boundary Conditions in LBM

$$f_{\alpha}(\mathbf{x} + \mathbf{c}_{\alpha}\Delta t, t + \Delta t) = f_{\alpha}(\mathbf{x}, t) - \omega(f_{\alpha} - f_{\alpha}^{(eq)})|_{(\mathbf{x}, t)}$$
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- Hydrodynamic Boundary Conditions in LBM
 - \rightarrow Solution on $\partial\Omega$ is specified for f_{α} and NOT for $\{\rho, \mathbf{u}, \Pi\}$

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- Hydrodynamic Boundary Conditions in LBM
 - \rightarrow Solution on $\partial\Omega$ is specified for f_{α} and NOT for $\{\rho, \mathbf{u}, \Pi\}$
 - $\to f_{\alpha}$ set in a higher DoF system than $\{\rho, \mathbf{u}, \mathbf{\Pi}\}$, hence:
 - \circ Trivial: $f_{\alpha} \longrightarrow \{\rho, \mathbf{u}, \mathbf{\Pi}\}$
 - \circ Complex: $\{\rho, \mathbf{u}, \mathbf{\Pi}\} \longrightarrow f_{\alpha}$

Problem definition

Boundaries in LBM

Particulate dynamics

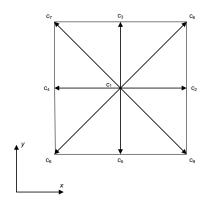
Using Chapman-Enskog

Introduction and motivation

$$f_{\alpha}(\mathbf{x} + \mathbf{c}_{\alpha}\Delta t, t + \Delta t) = f_{\alpha}(\mathbf{x}, t) - \omega(f_{\alpha} - f_{\alpha}^{(eq)})|_{(\mathbf{x}, t)}$$
 in Ω

- Hydrodynamic Boundary Conditions in LBM
 - \to Solution on $\partial\Omega$ is specified for f_{α} and NOT for $\{\rho,\mathbf{u},\Pi\}$
 - $\rightarrow f_{\alpha}$ set in a higher DoF system than $\{\rho, \mathbf{u}, \Pi\}$, hence:
 - \circ Trivial: $f_{\alpha} \longrightarrow \{\rho, \mathbf{u}, \mathbf{\Pi}\}$
 - \circ Complex: $\{\rho, \mathbf{u}, \mathbf{\Pi}\} \longrightarrow f_{\alpha}$
 - ightarrow Incorrect upscaling \longrightarrow Unwanted behavior, e.g. Knudsen layers

Lattice structure



• D2Q9 model

$$\mathbf{c}_1 = (0,0)$$

$$\mathbf{c}_2 = (1,0)$$

$$\mathbf{c}_3 = (0,1)$$

$$\mathbf{c}_4 = (-1,0)$$

$$\mathbf{c}_5 = (0,-1)$$

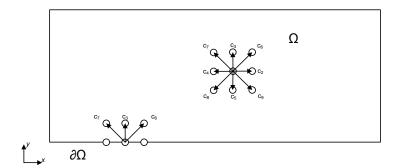
$$\mathbf{c}_6 = (1,1)$$

$$\mathbf{c}_7 = (-1,1)$$

$$\mathbf{c}_8 = (-1,-1)$$

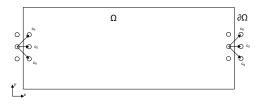
$$\mathbf{c}_9 = (-1,-1)$$

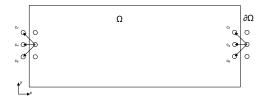
- \rightarrow **x** is a fluid node if \forall **c** so that $\mathbf{x} + \mathbf{c}\Delta t \in \{\Omega \bigcup \partial \Omega\}$
- \to **x** is a boundary node if \exists **c** so that **x** + **c** $\Delta t \notin \{\Omega \bigcup \partial \Omega\}$



Periodic Boundary Conditions

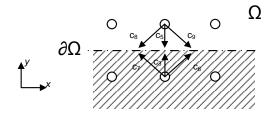
Periodicity \rightarrow $\mathbf{u}_{in} = \mathbf{u}_{out}$ on $\partial \Omega$





Symmetry Boundary Conditions

Symmetry
$$\rightarrow \mathbf{u} \cdot \mathbf{n} = 0$$
 and $\frac{\partial \mathbf{u}}{\partial n} = 0$ on $\partial \Omega$ (also called free-slip boundary)



A very intuitive idea:

A hard wall reflects particles back to where they originally came from

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A hard wall reflects particles back to where they originally came from

As a result:

- ightarrow There is no flux crossing the wall, i.e. the wall is impermeable
- → There is no relative transverse motion between fluid and wall, i.e. no-slip at the wall

REMEMBER: LBM algorithm can be operated in 2 steps:

→ Collision step:

$$\tilde{f}_{\alpha}(\mathbf{x},t) = f_{\alpha}(\mathbf{x},t) - \omega(f_{\alpha} - f_{\alpha}^{(eq)})|_{(\mathbf{x},t)}$$

 \rightarrow Streaming step:

$$f_{\alpha}(\mathbf{x} + \mathbf{c}_{\alpha}\Delta t, t + \Delta t) = \widetilde{f}_{\alpha}(\mathbf{x}, t)$$

The Bounceback method can be implemented following 2 reasonings:

Full-way bounceback:

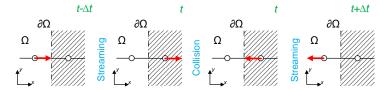
ightarrow inversion of particle velocity takes place during the **collision** step

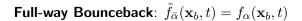
Half-way bounceback:

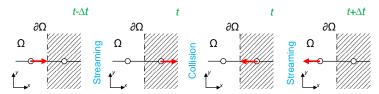
 \rightarrow inversion of particle velocity takes place during the streaming step



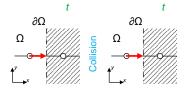
Full-way Bounceback: $\tilde{f}_{\bar{\alpha}}(\mathbf{x}_b,t)=f_{\alpha}(\mathbf{x}_b,t)$

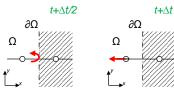




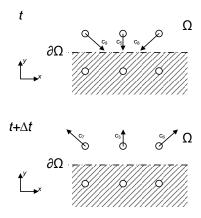


Half-way Bounceback: $f_{\bar{\alpha}}(\mathbf{x}_f, t + \Delta t) = \tilde{f}_{\alpha}(\mathbf{x}_f, t)$





Half-way bounceback in 2D:



Bounceback Boundary Conditions: summary

Pros

- → Mass is exactly conserved
- \rightarrow Stable for ω close to 2 (i.e. for high Re)
- \rightarrow Local
- → Flexibility in handling wall, edges, corners both in 2D and 3D
- ightarrow Very simple to implement from a programming viewpoint

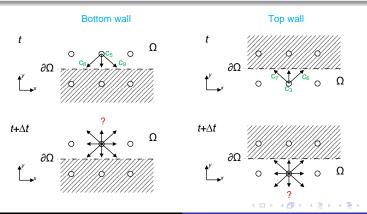
Cons

- \rightarrow Velocity accuracy may decrease from 2nd to 1st
- \rightarrow Pressure accuracy may decrease from 1st to 0th
- → In SRT model momentum is not exactly conserved (viscosity dependent slip velocity), which is equivalent to say the boundary location is not exactly defined (viscosity dependent slip length)

Bounceback Boundary Conditions: Exercise

Question:

Use the half-way bounceback scheme to find the unknown populations at $t+\Delta t$

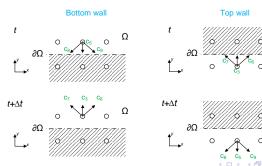


Bounceback Boundary Conditions: Exercise

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Solution:



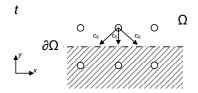
Momentum exchange

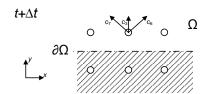
• Force (per unit volume):

$$\mathbf{F}|_{(t+\frac{\Delta t}{2})} = \frac{\Delta \mathbf{p}}{\Delta t}|_{(t+\frac{\Delta t}{2})} = \frac{1}{\Delta t}(\mathbf{p}(t+\Delta t) - \mathbf{p}(t))$$

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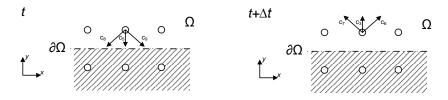
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 Momentum exchange (per unit volume) between the fluid/wall surface:

$$\Delta \mathbf{p}(\mathbf{x}, t + \frac{\Delta t}{2}) = \sum_{\alpha} \left[(\mathbf{c}_{\bar{\alpha}}) f_{\bar{\alpha}}(\mathbf{x}, t + \Delta t) - (\mathbf{c}_{\alpha}) \tilde{f}_{\alpha}(\mathbf{x}, t) \right]$$

Momentum exchange between the fluid/wall surface:

$$\Delta \mathbf{p}(\mathbf{x}, t + \frac{\Delta t}{2}) = -\sum_{\alpha} \mathbf{c}_{\alpha} \left[f_{\bar{\alpha}}(\mathbf{x}, t + \Delta t) + \tilde{f}_{\alpha}(\mathbf{x}, t) \right]$$

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Remember: Half-way Bounceback: $f_{\bar{\alpha}}(\mathbf{x}_f, t + \Delta t) = \tilde{f}_{\alpha}(\mathbf{x}_f, t)$

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$$\Rightarrow \Delta \mathbf{p}(\mathbf{x}, t + \frac{\Delta t}{2}) = -2 \sum_{\alpha} \mathbf{c}_{\alpha} \tilde{f}_{\alpha}(\mathbf{x}, t)$$

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$$\Rightarrow \Delta \mathbf{p}(\mathbf{x}, t + \frac{\Delta t}{2}) = -2 \sum_{\alpha} \mathbf{c}_{\alpha} \tilde{f}_{\alpha}(\mathbf{x}, t)$$

Force on the fluid due to the wall:

$$\mathbf{F}(\mathbf{x}, t + \frac{\Delta t}{2}) = -2 \frac{\Delta x}{\Delta t} \sum_{\mathbf{x}_b \in S} \sum_{\alpha} \mathbf{c}_{\alpha} \tilde{f}_{\alpha}(\mathbf{x}, t)$$

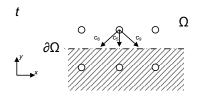


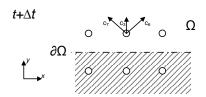
Transverse force on the fluid due to the bottom wall

$$F_x(\mathbf{x}, t + \frac{\Delta t}{2}) = -2\frac{\Delta x}{\Delta t} \sum_{\mathbf{x}_b \in S} \sum_{\alpha} (c_{\alpha})_x \tilde{f}_{\alpha}(\mathbf{x}, t)$$

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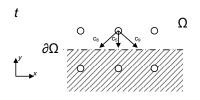
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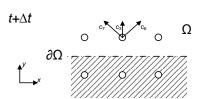




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Transverse force by **bottom wall**:

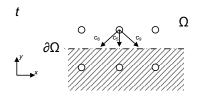
$$F_x(\mathbf{x}, t + \frac{\Delta t}{2}) = -2\frac{\Delta x}{\Delta t} \sum_{\mathbf{x}_b \in S} (\tilde{f}_9 - \tilde{f}_8)|_{(\mathbf{x}, t)}$$

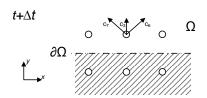
Normal force on the fluid due to the bottom wall

$$F_y(\mathbf{x}, t + \frac{\Delta t}{2}) = -2\frac{\Delta x}{\Delta t} \sum_{\mathbf{x}_b \in S} \sum_{\alpha} (c_{\alpha})_y \tilde{f}_{\alpha}(\mathbf{x}, t)$$

Normal force on the fluid due to the bottom wall

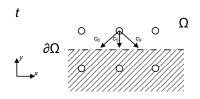
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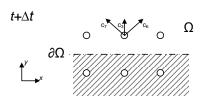




Normal force on the fluid due to the bottom wall

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Normal force by **bottom wall**:

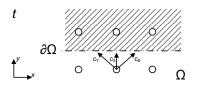
$$F_y(\mathbf{x}, t + \frac{\Delta t}{2}) = -2\frac{\Delta x}{\Delta t} \sum_{\mathbf{x}_b \in S} (\tilde{f}_5 + \tilde{f}_8 + \tilde{f}_9)|_{(\mathbf{x}, t)}$$

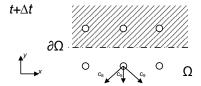
Momentum exchange: Exercise

Question:

Write the formulas of the transverse and normal forces at the top wall

Remember:





Momentum exchange: Exercise

Question:

Write the formulas of the transverse and normal forces at the top wall

Solution:

Transverse force by top wall:

$$F_x(\mathbf{x}, t + \frac{\Delta t}{2}) = -2\frac{\Delta x}{\Delta t} \sum_{\mathbf{x}_b \in S} (\tilde{f}_6 - \tilde{f}_7)|_{(\mathbf{x}, t)}$$

• Normal force by bottom wall:

$$F_y(\mathbf{x}, t + \frac{\Delta t}{2}) = -2\frac{\Delta x}{\Delta t} \sum_{\mathbf{x}_b \in S} (\tilde{f}_3 + \tilde{f}_6 + \tilde{f}_7)|_{(\mathbf{x}, t)}$$

Exercise I

Exercise I:

Poiseuille flow with bounceback walls

Motivation

 The solution of the Navier-Stokes not only requires the no-slip velocity condition on walls but also demands these equations to be valid near the wall

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- The solution of the Navier-Stokes not only requires the no-slip velocity condition on walls but also demands these equations to be valid near the wall
- Taking advantage of the Chapman-Enskog expansion...

$$f = f^{(0)}(\rho, \mathbf{u}) + \epsilon f^{(1)}(\nabla \mathbf{u}) + O(\epsilon^2)$$

Motivation

- The solution of the Navier-Stokes not only requires the no-slip velocity condition on walls but also demands these equations to be valid near the wall
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$$f = f^{(0)}(\rho, \mathbf{u}) + \epsilon f^{(1)}(\nabla \mathbf{u}) + O(\epsilon^2)$$

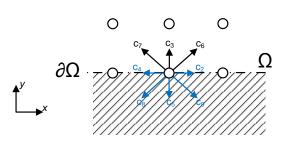
...it can be shown:

$$f_{\alpha}^{(0)} = w_{\alpha} \left(\rho + \frac{\mathbf{c}_{\alpha}}{c_s^2} \cdot \mathbf{u} + \frac{(\mathbf{c}_{\alpha} \mathbf{c}_{\alpha} - c_s^2 \mathbf{I})}{2c_s^4} : \mathbf{u} \mathbf{u} \right)$$

$$f_{\alpha}^{(1)} = -w_{\alpha} \frac{(\mathbf{c}_{\alpha} \mathbf{c}_{\alpha} - c_{s}^{2} \mathbf{I})}{\omega c_{s}^{2}} : (\nabla \mathbf{u} + (\nabla \mathbf{u})^{T})$$

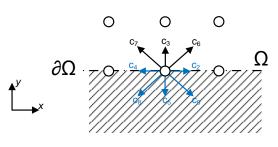
Zou He boundary condition

- ightarrow Boundary node and solid node coincide
- ightarrow Only unknown incoming populations are modified
- ightarrow Set ho or ${f u}$ in $f_{lpha}^{(0)}(
 ho,{f u})$
- ightarrow Construct $f_{lpha}^{(1)}$ from the symmetry requirement



• Known:

$$\rightarrow$$
 u = **0**
 \rightarrow $f_{\alpha} = (f_1, f_2, f_4, f_5, f_8, f_9)$

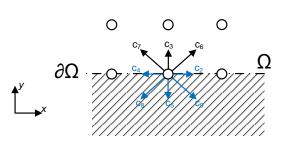


• Known:

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 u = **0**
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Unknown (4 variables):

$$ightarrow
ho$$
 $ightarrow f_{lpha} = (f_3, f_6, f_7)$



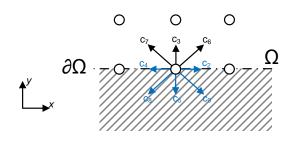
Known:

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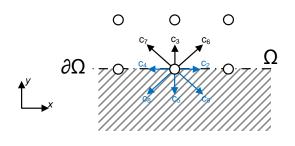
Unknown (4 variables):

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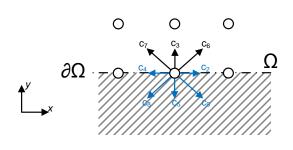
3 Equations (2 linearly independent):



- Symmetry of $f_{\alpha}^{(1)}$ (3 equations):
 - → Bounceback of non-equilibrium populations



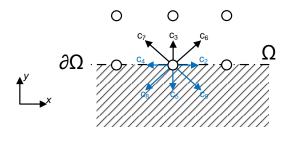
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- Introduce extra variable (problem overspecified):
 - ightarrow Transverse momentum correction N_{xy}



- Symmetry of $f_{\alpha}^{(1)}$ (3 equations):
 - Bounceback of non-equilibrium populations
- Introduce extra variable (problem overspecified):
 - ightarrow Transverse momentum correction N_{xy}
- Problem is well specified:
 - \rightarrow 6 eqs. and 6 unknowns



1) Computing ρ ...

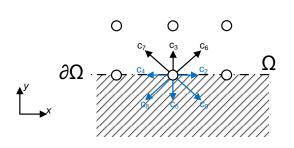


Population velocity set at boundary node:

$$\rightarrow C_{-} = \{\mathbf{c}_5, \mathbf{c}_8, \mathbf{c}_9\}$$

 Use the two velocity moments:

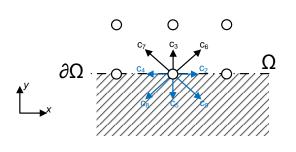
1) Computing ρ ...



 Relate the two velocity moments:

$$\begin{cases} \rho = \rho_+ + \rho_0 + \rho_- \\ u_y = \rho_+ - \rho_- \end{cases}$$

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 Relate the two velocity moments:

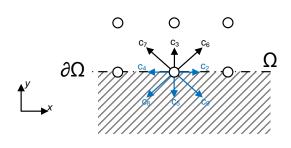
$$\begin{cases} \rho = \rho_+ + \rho_0 + \rho_- \\ u_y = \rho_+ - \rho_- \end{cases}$$

Solution:

$$\rho = u_y + \rho_0 + 2\rho_-$$

i.e.
$$\rho = u_y + (f_1 + f_2 + f_4) + 2(f_5 + f_8 + f_9)$$

2) Computing $\{f_3, f_6, f_7\}...$



 Non-equilibrium bounceback with transverse momentum correction:

$$f_3 - f_3^{(0)} = f_5 - f_5^{(0)}$$
$$f_6 - f_6^{(0)} = f_8 - f_8^{(0)} + N_{xy}$$

$$f_7 - f_7^{(0)} = f_9 - f_9^{(0)} - N_{xy}$$

2) Computing $\{f_3, f_6, f_7\}$...

Solution for the unknown incoming populations:

$$f_3 = f_5 + \frac{2}{3}u_y$$

$$f_6 = f_8 + \frac{1}{2}(f_4 - f_2) + \frac{1}{6}u_y + \frac{1}{2}u_x$$

$$f_7 = f_9 - \frac{1}{2}(f_4 - f_2) + \frac{1}{6}u_y - \frac{1}{2}u_x$$

Zou He boundary condition

Pros

- \rightarrow Local
- → Velocity is 2nd order accurate
- \rightarrow Pressure accuracy is (at worst) 1st order accurate
- → In SRT model momentum is conserved (up to 2nd order)

Cons

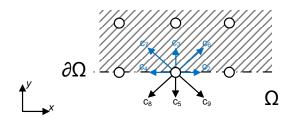
- \rightarrow Unstable when $\omega \longrightarrow 0$
- \rightarrow Mass is not exactly conserved (2nd order accurate)
- → Flexibility in handling wall, edges and corners or 2D and 3D domains are being modeled
- → Not so simple to implement (compared to bounceback)



Zou He boundary condition: Exercise

Question:

Use the Zou He procedure to find ρ and the unknown populations at the top wall



Zou He boundary condition: Exercise

Question:

Use the Zou He procedure to find ρ and the unknown populations at the top wall

Solution:

$$\rho = -u_y + (f_1 + f_2 + f_4) + 2(f_3 + f_6 + f_7)$$

$$f_5 = f_3 - \frac{2}{3}u_y$$

$$f_8 = f_6 + \frac{1}{2}(f_2 - f_4) - \frac{1}{6}u_y - \frac{1}{2}u_x$$

$$f_9 = f_7 - \frac{1}{2}(f_2 - f_4) - \frac{1}{6}u_y + \frac{1}{2}u_x$$

Exercise II

Exercise II:

Poiseuille flow Zou He walls

Outline

- Introduction
 - Boundary Value Problems
- 2 Motivation
 - Navier-Stokes Boundary Conditions
- 3 Lattice Boltzmann Boundary Conditions
 - Problem definition
 - Boundaries in LBM
 - Particulate dynamics
 - Using Chapman-Enskog
- Summary

BC scheme Bounceback Zou He

BC scheme	Bounceback	Zou He
Boundary location	Halfway	On node

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Coding simplicity	Yes	Not as simple