

# Lecture No. 59

## Single Phase Induction Motor (Characteristics)

Lecture delivered by:



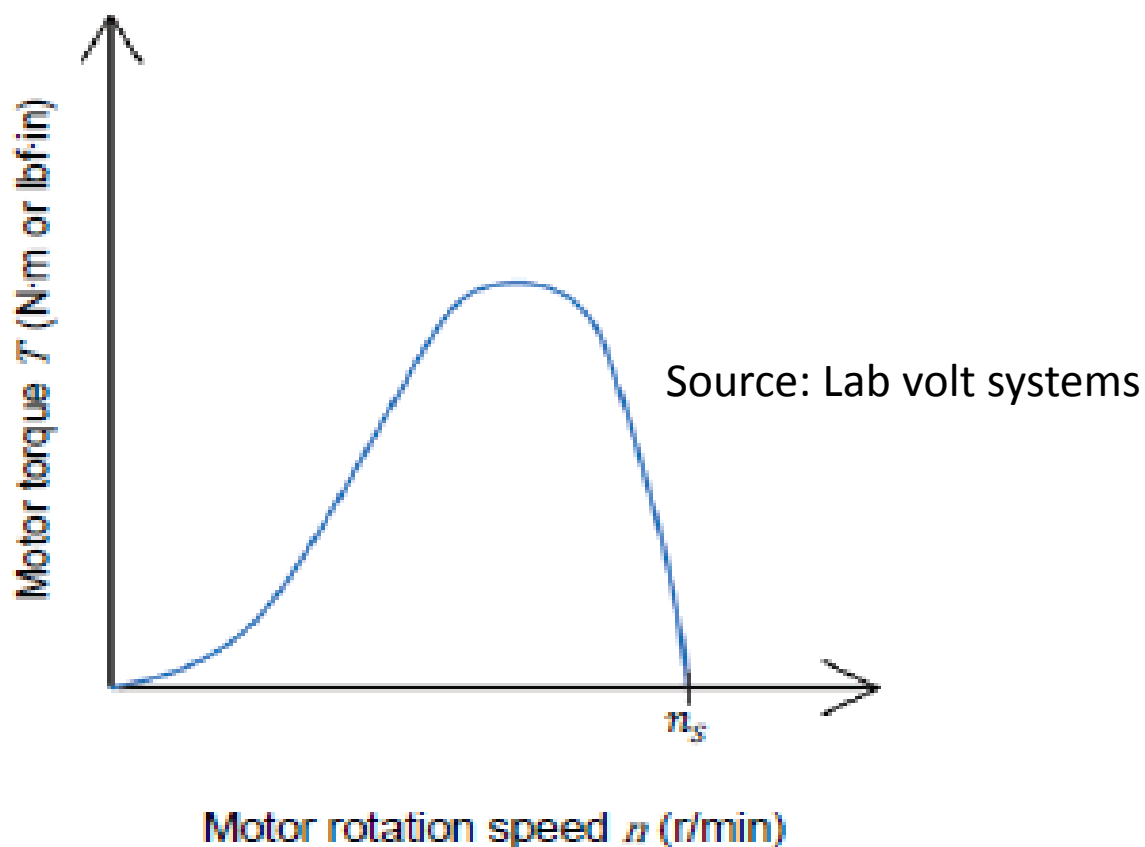
# Objectives

At the end of this lecture, student will be able to:

- Explain the Torque-Speed Characteristics
- Classify Single Phase Induction Motors based on construction and operation
- Discuss the need for Auxiliary winding



# Torque-Versus-Rotation Speed Curve of a Single-Phase Induction Motor



# Why low torque at low speeds?

- Forces created due to R.M.F cancel each other and the resulting force acting on the rotor is weak. Thus, single-phase induction motor must be started manually.
- When motor is starting , low torque is obtained at low speeds.



# Types of Induction Motor starting

Single-phase capacitor-start,

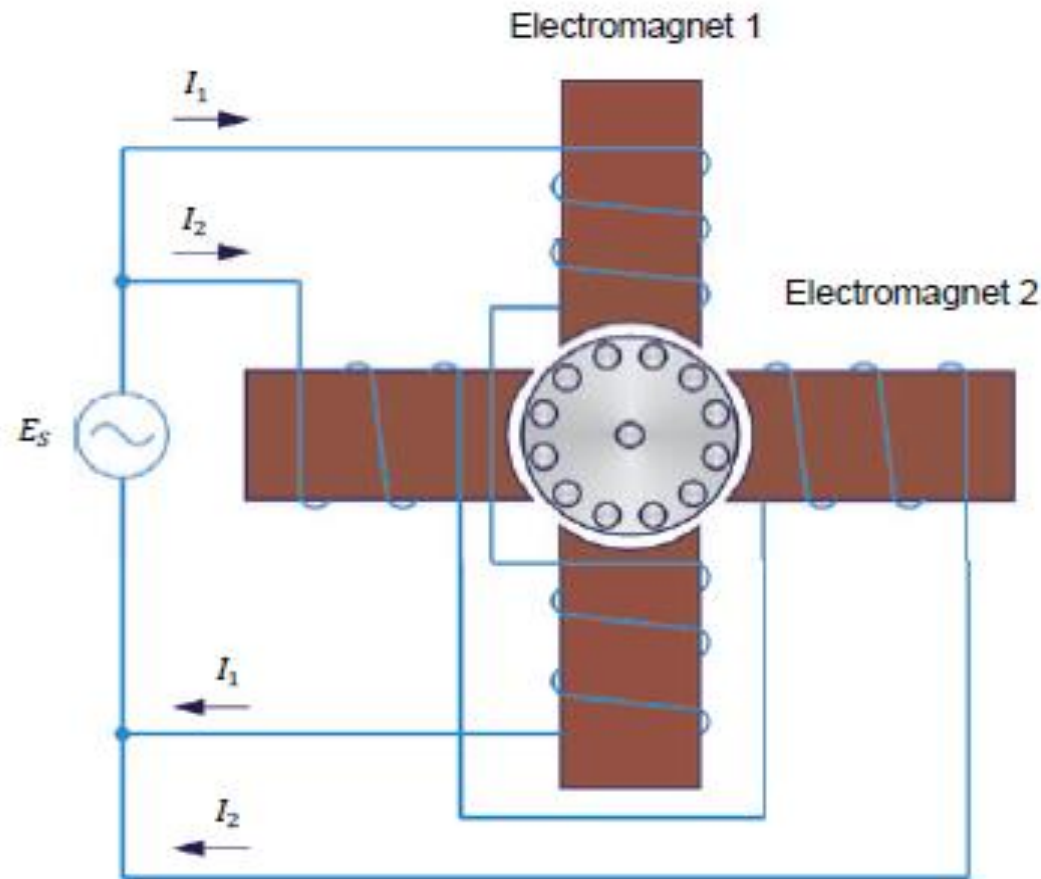
Capacitor-run

Split-phase and shaded-pole types

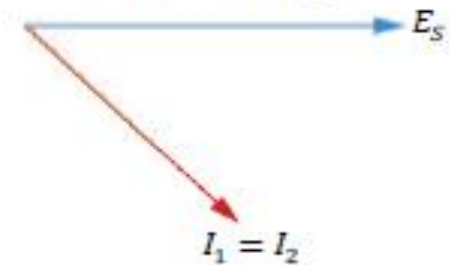
Small poly-phase induction motors.



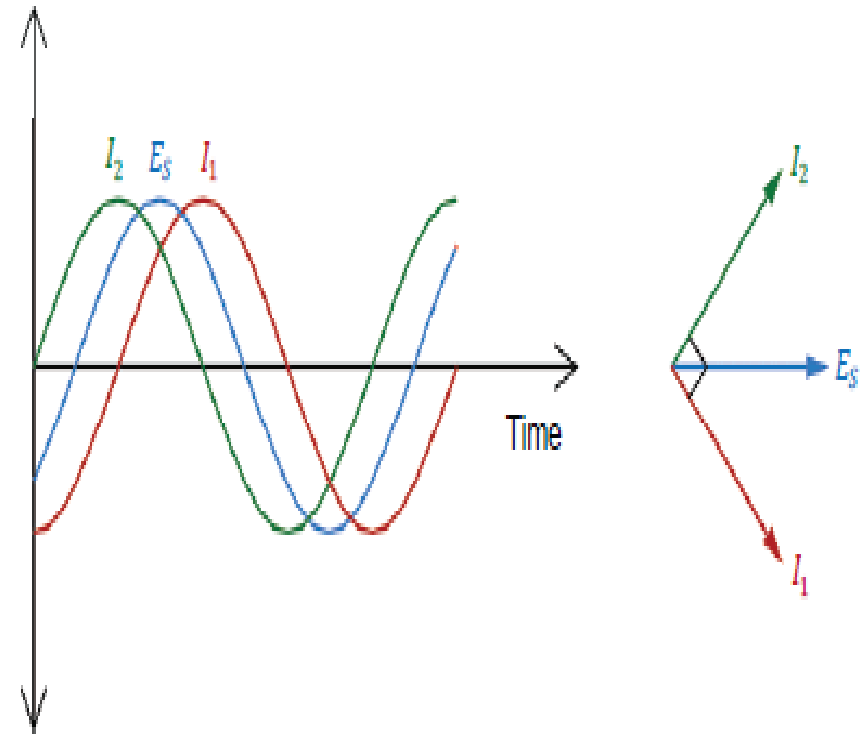
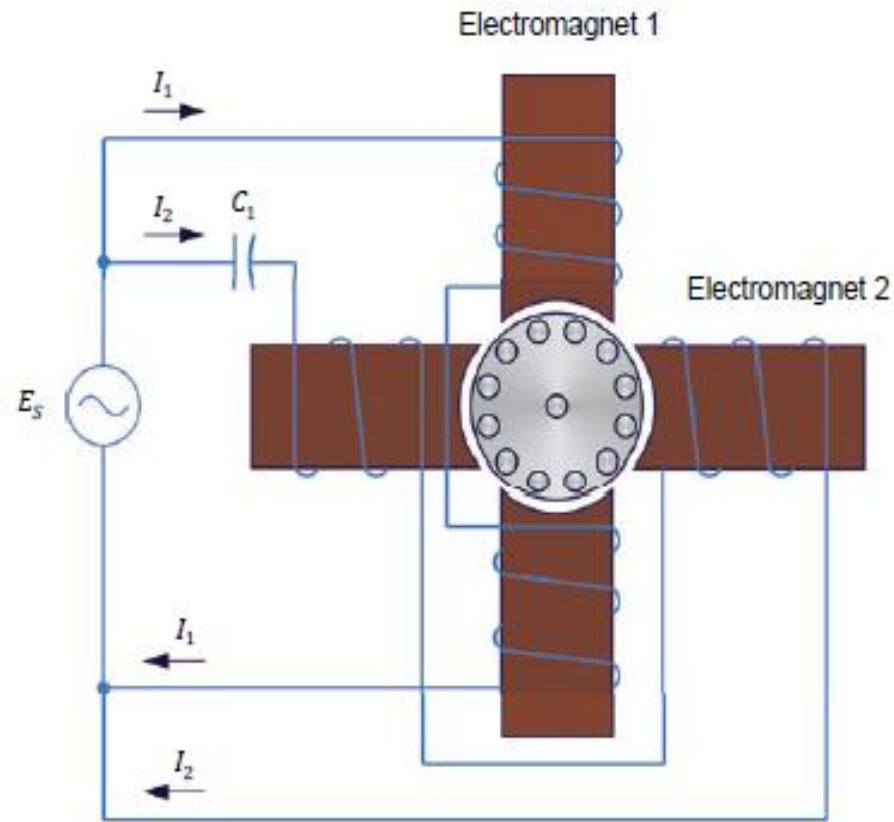
# Single Phase Induction Motor with Two Electromagnets



Voltage and current phasors when the motor is starting



# Addition of Capacitance to Induction Motor



Waveforms and phasors when the motor is starting



Note: Adding capacitors develop starting torque

# Parameters of Induction Motor

- Rotation rate of stator magnetic field, referred as synchronous speed is given by,

$$n_s = \frac{120 \times f}{p}$$

where ***f*** is the motor supply's frequency in Hertz and ***P*** is the number of magnetic poles





# Parameters of Induction Motor

- Slip, is defined as the difference between synchronous speed and operating speed, at the same frequency, expressed in rpm or in percent or ratio of synchronous speed.

$$s = \frac{n_s - n_r}{n_s}$$

Where  $n_s$  is stator electrical speed,  $n_r$  is rotor mechanical speed



# Parameters of Induction Motor

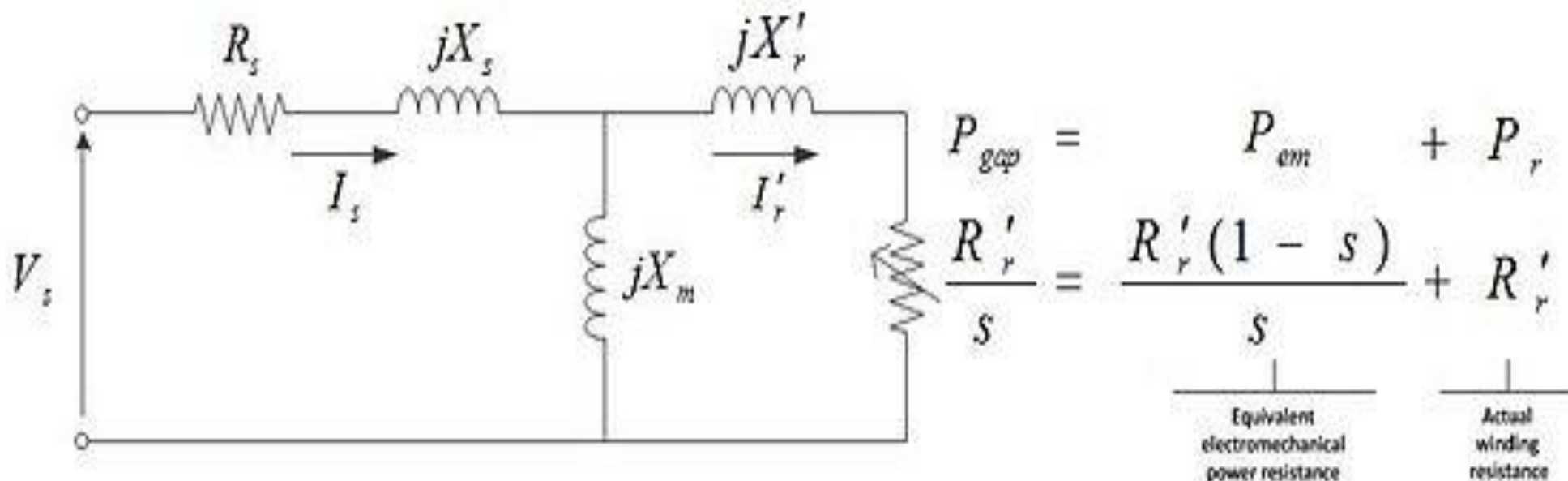
- **Power factor** of induction motors varies with load, typically from around 0.85 or 0.90 at full load to as low as 0.35 at no-load
- **Full load motor efficiency** varies from about 85 to 97%,
  - ✓ Friction and windage, 5% – 15%
  - ✓ Iron or core losses, 15% – 25%
  - ✓ Stator losses, 25% – 40%
  - ✓ Rotor losses, 15% – 25%
  - ✓ Stray load losses, 10% – 20%.

Source:

1. Liang, Xiaodong; Ilochonwu, Obinna (Jan 2011). "Induction Motor Starting in Practical Industrial Applications". IEEE Transactions on Industry Applications 47 (1): 271–280.
2. U.S. DOE (2008). "Improving Motor and Drive System Performance: A Sourcebook for Industry"



# Steinmetz Equivalent Circuit



- Stator resistance and leakage reactance ( $R_s, X_s$ )
- Rotor resistance, leakage reactance, and slip ( $R'_r, X'_r$  and  $s$ ).
- Magnetizing reactance ( $X_m$ ).

Source: Alger, Philip L. et al (1949). "Induction Machines' sub-section of Sec. 7 - Alternating-Current Generators and Motors". In Knowlton, A.E. *Standard Handbook for Electrical Engineers* (8th ed.). McGraw-Hill. p. 705.



# Steinmetz Equivalent Circuit

- Basic Electrical Equations

- ✓  $\omega_r = \frac{2\pi n_s}{60} = \frac{4\pi f_s}{p}$

- ✓ Motor input equivalent impedance

$$Z_m = R_s + jX_s + \frac{(\frac{R_s}{s} + jX_r')(jX_m)}{\frac{R_r'}{s} + j(X_r' + X_m)}$$

- ✓ Stator current

$$I_s = V_s / Z_m = V_s / (R_s + jX_s + \frac{(\frac{R_s}{s} + jX_r')(jX_m)}{\frac{R_r'}{s} + j(X_r' + X_m)})$$

- ✓ Rotor current referred to the stator side in terms of stator current

$$I_r' = \frac{jX_m}{\frac{R_r'}{s} + j(X_r' + X_m)} I_s$$



# Steinmetz equivalent circuit

- From Steinmetz equivalent circuit, we have

$$\frac{R'_r}{s} = \frac{R'_r(1-s)}{s} + R'_r$$

- Air gap power is equal to electromechanical power output plus rotor copper losses

$$P_{gap} = P_{em} + P_r$$

$$P_r = 3R'_r I_r'^2$$

$$P_{gap} = \frac{3R'_r I_r'^2}{s}$$

$$P_{em} = \frac{3R'_r I_r'^2(1-s)}{s}$$

$$P_{em} = P_{gap}(1-s)$$



# Power Equations

- Expressing electromechanical power output in terms of rotor speed

$$P_{em} = \frac{3R'_r I_r'^2 n_r}{sn_s}$$

$$P_{em} = \frac{3R'_r I_r'^2 n_r}{746sn_s}$$

$$T_{em} = \frac{P_{em}}{\omega_r} = \frac{\frac{P_r}{s}}{\omega_r} = \frac{3I_r'^2 R'_r}{\omega_r s}$$



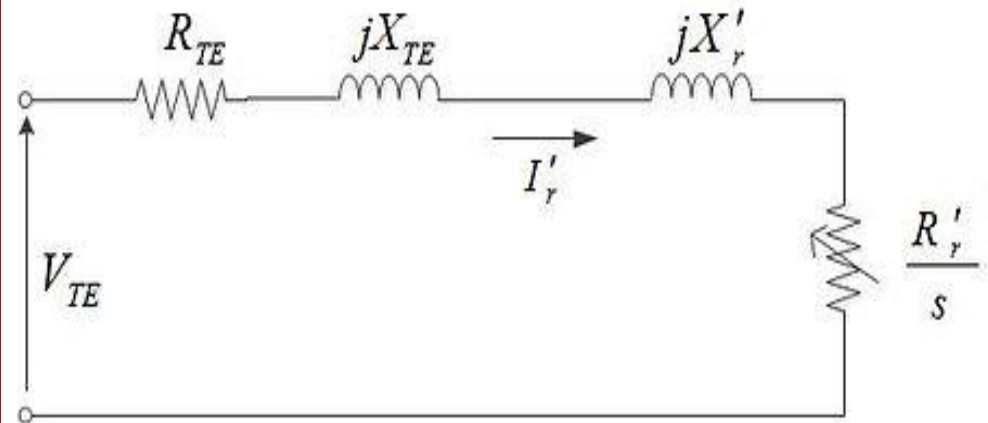
# Thevenin Equivalent Circuit

- Since,  $R_s^2 \gg (X_s + X_m)^2$   $X_s \ll X_m$   
and  $K_{TE} = \frac{X_m}{X_s + X_m}$

$$V_{TE} \approx Z_{TE} V_s$$

$$Z_{TE} \approx K_{TE}^2 R_s + jX_s$$

$$T_{em} = \frac{3V_{TE}^2}{(R_{TE} + \frac{R'_r}{s})^2 + (R_{TE} + X'_r)^2} \cdot \frac{R'_r}{s} \cdot \frac{1}{\omega_s} (N.m)$$



$$V_{TE} = \frac{X_m}{\sqrt{R_s^2 + (X_s + X_m)^2}} V_s$$

$$Z_{TE} = R_{TE} + jX_{TE} = \frac{jX_m(R_s + jX_s)}{R_s + j(X_s + X_m)}$$



Source: Özyurt, Ç.H. (2005). *Parameter and Speed Estimation of Induction Motors from Manufacturers Data and Measurements*. Middle East Technical University. pp. 33–34.

# Summary

- Auxiliary windings are connected with capacitors in series
- Current in the auxiliary winding causes magnetic field to rotate thereby providing starting torque

