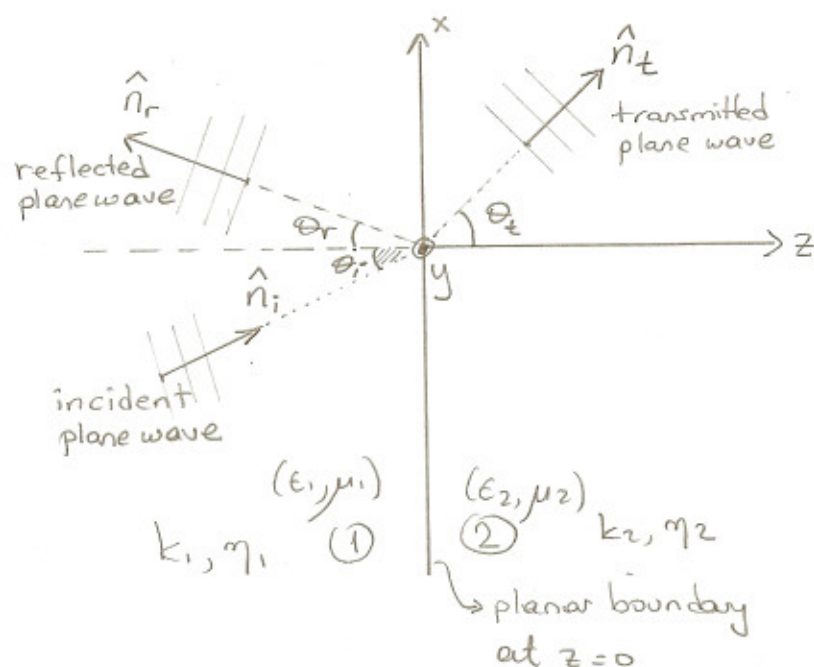


Reflection and Refraction (Transmission) of Plane Waves for OBLIQUE INCIDENCE at a Plane Boundary

Consider the planar boundary at $z=0$ between two lossless dielectrics:



Plane of Incidence (POI) is defined as the plane formed by

- the normal direction to the boundary, and
- the unit vector \hat{n}_i of the incident wave

For the picture shown (x, z) plane is the POI.

θ_i : angle of incidence	$0 \leq \theta_i \leq \frac{\pi}{2}$	
θ_r : " " reflection	$0 \leq \theta_r \leq \frac{\pi}{2}$	(by definition)
θ_t : " " transmission (refraction)	$0 \leq \theta_t \leq \frac{\pi}{2}$	

$$\begin{aligned}
 &\text{in medium (1)} \quad \begin{cases} \bar{E}^i = \bar{E}_1 e^{-j\bar{k}_i \cdot \bar{r}} \\ \bar{E}^r = \bar{E}_2 e^{-j\bar{k}_r \cdot \bar{r}} \end{cases} \quad \begin{aligned} &\text{with } \bar{k}_i = k_1 \hat{n}_i \quad (\text{for incident p.w.}) \\ &\text{with } \bar{k}_r = k_1 \hat{n}_r \quad (\text{for reflected p.w.}) \end{aligned} \\
 &\text{in medium (2)} \quad \begin{cases} \bar{E}^t = \bar{E}_3 e^{-j\bar{k}_t \cdot \bar{r}} \end{cases} \quad \text{with } \bar{k}_t = k_2 \hat{n}_t \quad (\text{for transmitted p.w.})
 \end{aligned}$$

where $k_1 = \omega \sqrt{\epsilon_1 \mu_1}$ and $k_2 = \omega \sqrt{\epsilon_2 \mu_2}$

Apply the B.C. at $z=0$ that $E_{\text{tang}}^{\text{total}}$ is continuous across the boundary.

$$(\bar{E}^i + \bar{E}^r)_{\text{tang}} \Big|_{z=0} = \bar{E}_{\text{tang}}^t \Big|_{z=0} \quad \text{for all } x, y !$$

$$\Rightarrow \left\{ \bar{E}_{1\text{tang}} e^{-j\bar{k}_i \cdot \bar{r}} + \bar{E}_{2\text{tang}} e^{-j\bar{k}_r \cdot \bar{r}} - \bar{E}_{3\text{tang}} e^{-j\bar{k}_t \cdot \bar{r}} \right\} \Big|_{z=0} = 0$$

$$\Rightarrow \left\{ \bar{E}_{1\text{tang}} e^{-j(k_{ix}x + k_{iy}y + k_{iz}z)} + \bar{E}_{2\text{tang}} e^{-j(k_{rx}x + k_{ry}y + k_{rz}z)} - \bar{E}_{3\text{tang}} e^{-j(k_{tx}x + k_{ty}y + k_{tz}z)} \right\} \Big|_{z=0} = 0$$

$$\bar{E}_{1\text{tang}} e^{-j(k_{ix}x + k_{iy}y)} + \bar{E}_{2\text{tang}} e^{-j(k_{rx}x + k_{ry}y)} - \bar{E}_{3\text{tang}} e^{-j(k_{tx}x + k_{ty}y)} = 0 \quad (*)$$

Note that for the incident, reflected and transmitted uniform planes, the vectors \bar{E}_1 , \bar{E}_2 and \bar{E}_3 are all constant vectors.

Therefore, their tangential (to the boundary) components are also constant vectors $\Rightarrow \bar{E}_{1\text{tang}}$, $\bar{E}_{2\text{tang}}$ and $\bar{E}_{3\text{tang}}$ are constant vectors.

As a result, the equation (*) above is satisfied for all possible (x, y) pairs on the $z=0$ boundary plane if and only if

$$(**) \quad k_{ix}x + k_{iy}y = k_{rx}x + k_{ry}y = k_{tx}x + k_{ty}y \quad \left(\begin{array}{l} \text{so the exponential} \\ \text{terms in } (*) \\ \text{can be cancelled} \\ \text{at } \underline{\underline{z=0}} \text{ plane} \end{array} \right)$$

But, we initially assumed that the propagation vector \bar{k}_i of the incident u.p.w. lies on the $(x-z)$ plane, so it has no y -component $\Rightarrow \underline{k_{iy} = 0}$

From $(**)$ \Rightarrow $\begin{cases} k_{ix} = k_{rx} = k_{tx} \\ k_{iy} = k_{ry} = k_{ty} = 0 \end{cases} (***)$
 and using $k_{iy} = 0$

which means, the propagation vectors \vec{k}_r and \vec{k}_t have no y-components.

Conclusion: Propagation vectors \vec{k}_i , \vec{k}_r and \vec{k}_t all lie in the plane of incidence (i.e., the (x-z) plane).

in medium ① $k_1 = \omega \sqrt{\epsilon_1 \mu_1}$

$$\begin{cases} \vec{k}_i = k_1 \hat{n}_i = k_1 (\underbrace{\sin \theta_i \hat{a}_x + \cos \theta_i \hat{a}_z}_{\hat{n}_i}) = \underbrace{k_1 \sin \theta_i \hat{a}_x}_{k_{ix}} + \underbrace{k_1 \cos \theta_i \hat{a}_z}_{k_{iz}} \\ \vec{k}_r = k_1 \hat{n}_r = \underbrace{k_1 \sin \theta_r \hat{a}_x}_{k_{rx}} - \underbrace{k_1 \cos \theta_r \hat{a}_z}_{k_{rz}} \end{cases}$$

in medium ② $k_2 = \omega \sqrt{\epsilon_2 \mu_2}$

$$\vec{k}_t = k_2 \hat{n}_t = \underbrace{k_2 \sin \theta_t \hat{a}_x}_{k_{tx}} + \underbrace{k_2 \cos \theta_t \hat{a}_z}_{k_{tz}}$$

We just found above in $(***)$

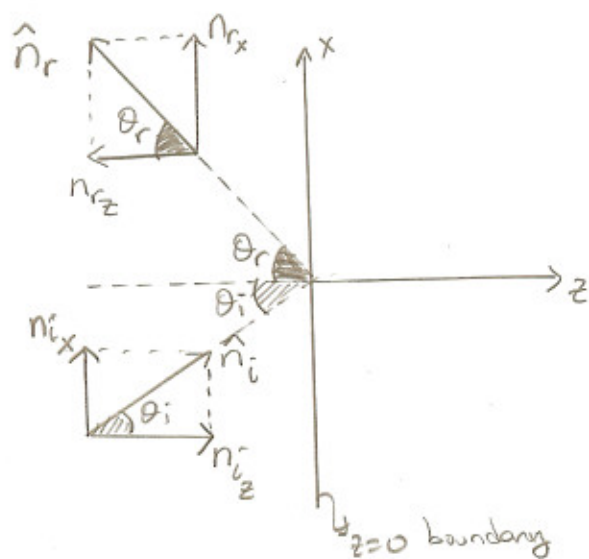
$$k_{ix} = k_{rx} = k_{tx}$$

$$\text{From } k_{ix} = k_{rx} \Rightarrow k_1 \sin \theta_i = k_1 \sin \theta_r$$

$$\Rightarrow \boxed{\theta_i = \theta_r} \text{ Snell's Law of Reflection}$$

Conclusion: Being independent from the medium parameters and frequency, the

angle of incidence must be equal to the angle of reflection.



Using $k_{ix} = k_{tx} \Rightarrow \boxed{k_1 \sin \theta_i = k_2 \sin \theta_t}$ Snell's Law of Refraction

insert $k_1 = \omega \sqrt{\mu_1 \epsilon_1}$ and $k_2 = \omega \sqrt{\mu_2 \epsilon_2}$ above,

$$\cancel{\omega} \sqrt{\mu_1 \epsilon_1} \sin \theta_i = \cancel{\omega} \sqrt{\mu_2 \epsilon_2} \sin \theta_t$$

$$\boxed{\sqrt{\mu_1 \epsilon_1} \sin \theta_i = \sqrt{\mu_2 \epsilon_2} \sin \theta_t}$$

or $\boxed{\frac{\sin \theta_t}{\sin \theta_i} = \sqrt{\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2}}}$ This ratio is independent of frequency.

For these lossless media, we can define:

$$v_1 = \frac{1}{\sqrt{\mu_1 \epsilon_1}} \text{ and } v_2 = \frac{1}{\sqrt{\mu_2 \epsilon_2}} \Rightarrow \boxed{\frac{\sin \theta_t}{\sin \theta_i} = \frac{v_2}{v_1}}$$

Index of refraction $= n \triangleq \frac{c}{v}$ in general where $c = 3 \times 10^8$ m/s, speed of light in vacuum ($c = \frac{1}{\sqrt{\epsilon_0 \mu_0}}$)

$$\left. \begin{aligned} n_1 &\triangleq \frac{c}{v_1} = \sqrt{\mu_1 \epsilon_1} \\ n_2 &\triangleq \frac{c}{v_2} = \sqrt{\mu_2 \epsilon_2} \end{aligned} \right\} \Rightarrow \frac{\sin \theta_t}{\sin \theta_i} = \frac{v_2}{v_1} = \frac{c/n_2}{c/n_1} = \frac{n_1}{n_2} \Rightarrow \boxed{n_1 \sin \theta_i = n_2 \sin \theta_t}$$

Consider two possible cases:

Case 1

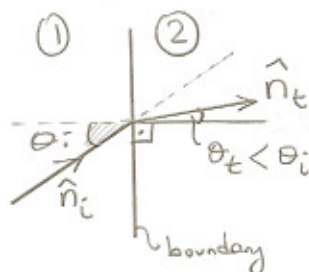
$\mu_1 \epsilon_1 < \mu_2 \epsilon_2$
(Second medium is denser)

$$\frac{\sin \theta_t}{\sin \theta_i} = \sqrt{\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2}} < 1$$

$$\Rightarrow \sin \theta_t < \sin \theta_i$$

$$\Rightarrow \boxed{\theta_t < \theta_i}$$

The transmitted wave will be bent closer to the normal of the boundary.



Case 2

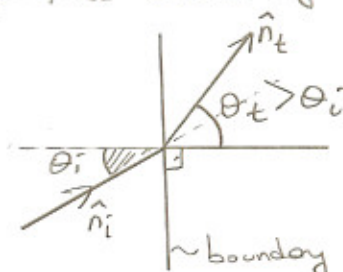
$\mu_1 \epsilon_1 > \mu_2 \epsilon_2$
(First medium is denser)

$$\frac{\sin \theta_t}{\sin \theta_i} = \sqrt{\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2}} > 1$$

$$\Rightarrow \sin \theta_t > \sin \theta_i$$

$$\Rightarrow \boxed{\theta_t > \theta_i}$$

The transmitted wave will be bent away from the normal of the boundary.



Question: How much can we increase θ_i (incidence angle) before θ_t becomes $\frac{\pi}{2}$ in case 2 where $\theta_t > \theta_i$?

θ_c : Critical Angle = Value of incidence angle θ_i for which $\theta_t = \frac{\pi}{2}$.

$$\sqrt{\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2}} = \frac{\sin \theta_t}{\sin \theta_i} \bigg|_{\theta_i = \theta_c} = \frac{\sin \frac{\pi}{2}}{\sin \theta_c} = \frac{1}{\sin \theta_c} \Rightarrow \boxed{\sin \theta_c = \sqrt{\frac{\mu_2 \epsilon_2}{\mu_1 \epsilon_1}}}$$

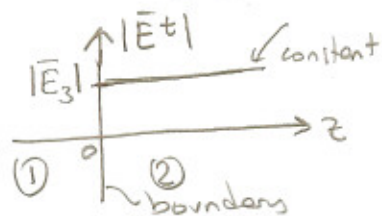
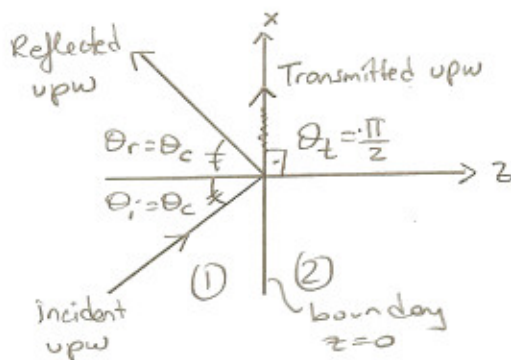
or $\theta_c = \sin^{-1} \left(\sqrt{\frac{\mu_2 \epsilon_2}{\mu_1 \epsilon_1}} \right)$

For $\theta_i = \theta_c$ when $\mu_1 \epsilon_1 > \mu_2 \epsilon_2$ (Case 2)

$$\Rightarrow \theta_t = \frac{\pi}{2} \Rightarrow \hat{n}_t = \hat{a}_x \Rightarrow \bar{k}_t = k_2 \hat{n}_t = k_2 \hat{a}_x$$

$$\Rightarrow \bar{k}_t \cdot \bar{r} = k_2 \hat{a}_x \cdot (x\hat{a}_x + y\hat{a}_y + z\hat{a}_z) = k_2 x$$

$$\Rightarrow \bar{E}^t = \bar{E}_3 e^{-j\bar{k}_t \cdot \bar{r}} = \underbrace{\bar{E}_3}_{\text{constant vector}} e^{-jk_2 x} \quad \left(\begin{array}{l} \text{a uniform plane wave} \\ \text{propagating in } (+x) \text{ direction} \\ \text{in medium (2) for } z > 0 \end{array} \right)$$



Note that $|\bar{E}^t| = |\bar{E}_3|$ for all $z > 0$

There exists a u.p.w in medium (2) propagating in $\hat{n}_t = \hat{a}_x$ direction with constant \bar{E} -phasor magnitude everywhere in $z > 0$ region.

Question: What happens (in case 2) if $\theta_i > \theta_c$?

$$\theta_i > \theta_c \Rightarrow \sin \theta_i > \sin \theta_c$$

$$\text{As } \sin \theta_c = \sqrt{\frac{\mu_2 \epsilon_2}{\mu_1 \epsilon_1}} \Rightarrow \sin \theta_i > \sqrt{\frac{\mu_2 \epsilon_2}{\mu_1 \epsilon_1}} \quad \left. \begin{array}{l} \sin \theta_t > \sqrt{\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2}} \sqrt{\frac{\mu_2 \epsilon_2}{\mu_1 \epsilon_1}} \\ \sin \theta_t > 1 \end{array} \right\}$$

$$\text{From Snell's Law of refraction} \Rightarrow \sin \theta_t = \sqrt{\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2}} \sin \theta_i$$

$$\boxed{\sin \theta_t > 1}$$

Conclusion: For $\left\{ \begin{array}{l} \mu_1 \epsilon_1 > \mu_2 \epsilon_2 \\ \theta_i > \theta_c \end{array} \right\} \Rightarrow \boxed{\sin \theta_t > 1}$ which is NOT possible for a real valued angle

$\Rightarrow \boxed{\theta_t \text{ must be a complex angle}}$

Consider the trigonometric identity

$$\cos^2 \theta_t + \sin^2 \theta_t = 1 \quad \text{which is valid for complex angles also!}$$

$$\cos \theta_t = \mp \sqrt{1 - \sin^2 \theta_t} = \mp \sqrt{\underbrace{-(\sin^2 \theta_t - 1)}_{>0}}$$

$< 0 \text{ as } \sin \theta_t > 1$

$$\cos \theta_t = \mp \underbrace{\sqrt{-1}}_j \sqrt{\sin^2 \theta_t - 1} = \mp j \sqrt{\sin^2 \theta_t - 1}$$

use Snell's Law
 $\sqrt{\mu_1 \epsilon_1} \sin \theta_i = \sqrt{\mu_2 \epsilon_2} \sin \theta_t$

$$\boxed{\cos \theta_t = \mp j \sqrt{\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2} \sin^2 \theta_i - 1}}$$

Conclusion: $\cos \theta_t$ is a purely imaginary number

$\Rightarrow \theta_t$ is indeed a complex quantity if $\theta_i > \theta_c$.

Hence, for the transmitted wave in medium (2):

$$\vec{E}^t = \vec{E}_3 e^{-j \vec{k}_t \cdot \vec{r}}$$

(Remember $\vec{k}_t = k_2 \hat{n}_t$
and $\hat{n}_t = \sin \theta_t \hat{a}_x + \cos \theta_t \hat{a}_z$)

$$= \vec{E}_3 e^{-j(k_2 \sin \theta_t x + k_2 \cos \theta_t z)}$$

$$= \vec{E}_3 e^{-jk_2 \sin \theta_t x} e^{-jk_2 \cos \theta_t z} \quad (\text{insert } \cos \theta_t \text{ expression})$$

$$= \vec{E}_3 e^{-jk_2 (\sin \theta_t) x} e^{-jk_2 (-j \sqrt{\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2} \sin^2 \theta_i - 1}) z}$$

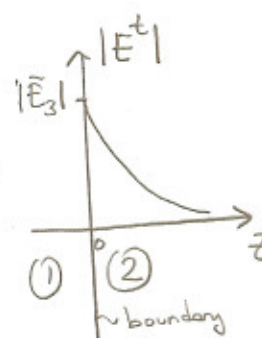
$$= \vec{E}_3 \underbrace{e^{-jk_2 \sin \theta_t x}}_{\text{Complex exponential}} \underbrace{e^{-k_2 \sqrt{\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2} \sin^2 \theta_i - 1} z}}_{\text{Real exponential (combine with } \vec{E}_3 = \text{constant amplitude vector)}}$$

Let $\left. \begin{aligned} \alpha_z &\triangleq k_2 \sqrt{\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2} \sin^2 \theta_i - 1} \\ \beta_x &\triangleq k_2 \sin \theta_t \end{aligned} \right\} \Rightarrow \boxed{\bar{E}^t = \bar{E}_3 e^{-\alpha_z z} e^{-j\beta_x x}}$

\swarrow Attenuation in z-direction \searrow Propagation in x-direction

$$\bar{E}^t = \bar{E}_3 e^{-\alpha_z z} e^{-j\beta_x x}$$

Amplitude of transmitted wave $|\bar{E}^t| = |\bar{E}_3| \underbrace{|e^{-\alpha_z z}|}_{e^{-\alpha_z z}} \underbrace{|e^{-j\beta_x x}|}_1 = \underbrace{|\bar{E}_3|}_{\text{constant vector}} e^{-\alpha_z z}$



$|\bar{E}^t|$ is kept constant if $\underline{z = \text{constant}}$ \Rightarrow "Constant Amplitude" surfaces are $z = \text{constant}$ planes.

Phase of transmitted wave $\angle \bar{E}^t = -\beta_x x$ is kept constant if $\underline{x = \text{constant}}$

\Rightarrow "Constant Phase" surfaces are $x = \text{constant}$ planes

Conclusion: In medium ②, we still have "plane wave" type transmitted electromagnetic field but it is now a NON-UNIFORM PLANE WAVE because the constant amplitude surfaces ($z = \text{const. planes}$) are not the same as constant phase surfaces ($x = \text{const. planes}$).

NOTES:

(*) The non-uniform plane wave in medium (2) can also be called "Surface Wave" if the attenuation parameter $\alpha_z = k_2 \sqrt{\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2} \sin^2 \theta_i - 1}$ is large enough. Then, the attenuation of the transmitted field in +z direction is sufficiently rapid, power associated with transmitted wave is concentrated in a region close to the boundary.

(*) The non-uniform plane wave solution in medium (2) is also called "Slow Wave" as: (remember $k_2 = \omega \sqrt{\mu \epsilon} = \frac{\omega}{v}$)

For $\theta_i \leq \theta_c$, the phase velocity = $v = \frac{\omega}{k_2}$
of the u.p.w in med. (2)

For $\theta_i > \theta_c$, the phase velocity = $v_{sw} = \frac{\omega}{\beta_x} = \frac{\omega}{k_2 \sin \theta_t}$
of the non-uniform pw
in medium (2)

As $\sin \theta_t > 1$ (for $\theta_i > \theta_c$) $\Rightarrow v_{sw} = \frac{\omega}{k_2 \sin \theta_t} < \frac{\omega}{k_2} = v$

i.e., $v_{sw} < v$ (Wave propagation is slower)

(*) When $\theta_i \geq \theta_c$, it is said that we have "Total Reflection" (TR) case where there is no wave propagation into the 2nd medium. Instead, propagation direction is parallel to the boundary.

(*) Remember that we have examined a "lossless" case. The parameter α_z in $\vec{E}^t = \vec{E}_3 e^{-\alpha_z z} e^{j\beta_x x}$ expression has nothing to do with the α parameter of lossy medium problems. The decay $e^{-\alpha_z z}$ is not due to medium loss ($\sigma_2 = 0$ is assumed at the beginning.)