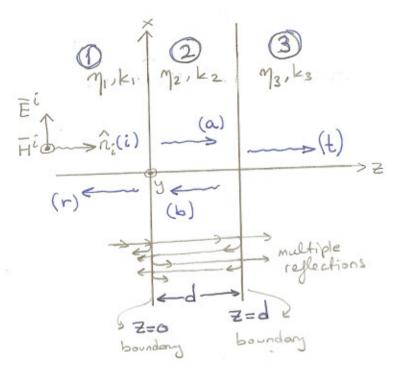
## Case 4: Multiple Reflections under normal incidence

Consider the following problem with 3 lossless dielectric media:



## At steady state:

- (i): Incident u.p.w. in 1)
- (r): Resultant reflected u.p.w. in 1)
- (a): Resultant u.p.w propagating
- (b): Resultant u.p.w propagating
  - (t): Resultant u.p.w transmitted

$$\begin{aligned}
E^{i} &= \hat{a}_{x} E_{1} e^{-jk_{1}z} \\
E^{r} &= \hat{a}_{x} E_{2} e^{jk_{1}z} \end{aligned}$$

$$\begin{aligned}
E^{r} &= \hat{a}_{x} E_{3} e^{jk_{2}z} \\
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$$\begin{aligned}
&= \hat{a}_{x} E_{3} e^{jk_{2}z} \\
&= \hat{a}_{x} E_{4} e^{jk_{2}z} \end{aligned}$$

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$$\begin{aligned}
&= \hat{a}_{x} E_{3} e^{jk_{2}z} \\
&= \hat{a}_{x} E_{4} e^{jk_{2}z} \end{aligned}$$

$$\begin{aligned}
&= \hat{a}_{x} E_{5} e^{jk_{3}z} \end{aligned}$$

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$$\end{aligned}$$

Apply the B.C.s for Etange and Htot at z=0 and z=d

$$E_{1}+E_{2}=E_{3}+E_{4}...(I)$$

$$\frac{1}{\eta_{1}}(E_{1}-E_{2})=\frac{1}{\eta_{2}}(E_{3}-E_{4})...(II)$$

$$E_{3}=\int_{0}^{1}k_{2}d+E_{4}=\int_{0}^{1}E_{2}d=E_{5}=\int_{0}^{1}k_{3}d...(II)$$

$$\frac{1}{\eta_{2}}(E_{3}=\int_{0}^{1}k_{2}d-E_{4}=\int_{0}^{1}k_{2}d)=\frac{1}{\eta_{3}}(II)$$

$$\frac{1}{\eta_{2}}(E_{3}=\int_{0}^{1}k_{2}d-E_{4}=\int_{0}^{1}k_{2}d)=\frac{1}{\eta_{3}}(II)$$

Equations I, II, II and II can be simultaneously solved to determine.

The unknowns Ez, Ez, Ez, Ey and E5 in terms of the known constant E1.

Define: 
$$\Gamma \triangleq \frac{E_2}{E_1}$$
 : effective reflection (Note that  $\Gamma \neq \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$  any more)

Special Case: Quarter wave transformer

Let  $d = \frac{\lambda_2}{4}$  (The second medium has the thickness of quarter wavelength  $\lambda_2/4$  where  $\lambda_2 = \frac{2\pi}{k_1}$ )

$$\Rightarrow \text{ in equations} \qquad k_2 d = \frac{2\pi}{\lambda_2} d = \frac{2\pi}{\lambda_2} \frac{\lambda_2}{4} = \frac{\pi}{2}$$

$$d = \lambda_2 \frac{\lambda_2}{4}$$

$$\Rightarrow \hat{f}_{2}^{\dagger k_{2} d} = \hat{f}_{1}^{\dagger 1 1 / 2} = \hat{f}_{1}^{\dagger}$$

Then, equations I-IX can be written as:

 $T-\overline{W}$  can Divide eqn. T and  $\overline{H}$  side by side:  $\frac{E_1+E_2}{E_1-E_2}=\frac{\eta_2}{\eta_1}\frac{E_3+E_4}{E_3-E_4} \Rightarrow replace using \overline{M}$   $(E_3-E_4)$ 

$$(I) \quad E_1 - E_2 = \frac{\eta_1}{\eta_2} (E_3 - E_4)$$

$$(\overline{\mathbb{D}})$$
  $E_3 - E_4 = j E_5 e^{jk_3 \lambda_2 / 4} = j E_5'$ 

(D) 
$$E_3 + E_4 = j \frac{M_2}{M_3} E_5'$$

$$\frac{E_{1}+E_{2}}{E_{1}-E_{2}} = \frac{\eta_{2}}{\eta_{1}} \frac{j\frac{\eta_{2}}{\eta_{3}}E_{5}'}{jE_{5}'} = \frac{\eta_{2}^{2}}{\eta_{1}\eta_{3}}$$

$$\frac{E_{1}\left(1+\frac{E^{2}}{E_{1}}\right)}{E_{1}\left(1-\frac{E^{2}}{E_{1}}\right)} = \frac{1+\Gamma'}{1-\Gamma'} = \frac{M^{2}}{M_{1}M_{3}}$$

Solve for reflection coefficient [ intermio] m, mz and m3.

To have no reflections in medium (D,i,e.for Ez=0 or T=0

Let 
$$p=0$$
 in  $=$   $\frac{1+0}{1-0} = \frac{\eta^2}{\eta_1 \eta_3} \implies \eta_2^2 = \eta_1 \eta_3$  or  $\eta_2 = \sqrt{\eta_1 \eta_3}$  Geometric mean

Selecting 
$$\begin{cases} d = \frac{\Lambda_2}{4} \end{cases} \Rightarrow \Gamma = 0$$
 I no reflection  $M_2 = \sqrt{\eta_1 \eta_3}$  (or  $E_2 = 0$ ) I condition is ensured

Quarter-Wave Transformer where M, 7 M3 , poneral. In other words, a slab of thickness  $d=\frac{2z}{4}$  and intrinsic impedance  $\eta_2 = \sqrt{\eta_1 \eta_3}$  acts as an impedance transformer (or as a matching layer) between media (1) and (3) to obtain zero reflection in medium (1).

Example: Let,  $\mu_1 = \mu_2 = \mu_3 = \mu_3$  (all non-magnetic media)  $\frac{\lambda_2}{\lambda_1} = \frac{2\Pi}{k_2} = \frac{k_1}{k_2} = \frac{\omega\sqrt{\epsilon_1\mu_0}}{\omega\sqrt{\epsilon_2\mu_0}} = \sqrt{\frac{\epsilon_1}{\epsilon_2}}$ 

Then )  $d = \frac{\lambda_2}{4} = \frac{\lambda_1}{4} \sqrt{\frac{\epsilon_1}{\epsilon_2}}$  for the most ching layer in (2)

Also,  $\eta_z^2 = \eta_1 \eta_3 \implies f_{\epsilon_z}^0 = \sqrt{\frac{\mu_0}{\epsilon_1} \frac{\mu_0}{\epsilon_3}} \implies \epsilon_z = \sqrt{\frac{\epsilon_1 \epsilon_3}{\epsilon_1}}$ 

Exercise: Show that selecting  $d = \frac{A_2}{2}$  and  $\eta = \frac{M_3}{3}$ is another way of obtaining  $\Gamma = 0$ .

Note: It can be shown for this 3-region, normal incidence problem that

 $\Pi = \frac{E^2}{E_1} \triangleq \frac{\text{Meg} - \text{M}_1}{\text{Meg} + \text{M}_1} \quad \text{where } \text{Meg} = \frac{\text{M}_2}{2} \cdot \frac{\text{M}_3 + \text{j} \, \text{M}_2 \, \text{tan}(\beta_2 d)}{\text{Meg} + \text{M}_1}$ 

Example: A uniform plane wave with free-space would be 20 = 3 cm is normally incident on a fiberglass slab which has 6r = 4.9,  $\mu = \mu_0$ ;  $\sigma = 0$ .

b) What percentage of incident power will be reflected back from the fiberglass if the frequency of the incident wave is decreased by 10%, keeping the thickness (d) found in part (a) uncharged?

Use d= 2 to provide P=0.

Find 
$$\lambda_2$$
:  $\lambda_z = \frac{2\Pi}{k_z} = \frac{2\Pi}{k_0 \sqrt{\epsilon_r}} = \frac{\lambda_0}{\sqrt{\epsilon_r}} = \frac{3cm}{\sqrt{4.9}} \approx 1.355 cm$ .

$$(\gamma_0 = \frac{2\pi}{k_0} = \frac{2\pi}{\omega \sqrt{\epsilon_0 \mu_0}} = 3 \text{ cm} \cdot \text{ is given in free space})$$

(b) 
$$f_{\text{new}} = 0.9 \, f_{\text{old}} \implies \lambda_{2_{\text{new}}} = \frac{\lambda_{2_{\text{old}}}}{0.9} = \frac{1.355}{0.9} \approx 1.506 \, \text{cm} \cdot \text{in fiberglass}$$

$$\Rightarrow Using \quad \eta_1 = \eta_3 = \eta_0 = 120 \text{ Tr} (\Omega) \\ \text{and} \quad \eta_2 = \sqrt{\frac{\mu_2}{e_2}} = \frac{\eta_0}{\sqrt{4g}} (\Omega) \\ \Rightarrow \int_{eq}^{eq} = \eta_2 \frac{\eta_0 + j \eta_2 \tan(\beta_2 d)}{\eta_2 + j \eta_0 \tan(\beta_2 d)} = \dots$$

$$\Rightarrow \int = \frac{M_{eq} - M_o}{M_{eq} + M_o} \approx 0.263 \frac{2113.4}{}$$

$$\frac{P_{eq} \cong 120 \, \Pi \left(0.729 + j \, 0.377\right) \left(\Omega\right)}{P_{ao}^{ref}} = \left| \frac{17}{2} \cong 0.069 \right| \left(\frac{6.9 \% \text{ of the incident power will be reflected back to } 0\right)}{P_{ao}^{ref}}$$