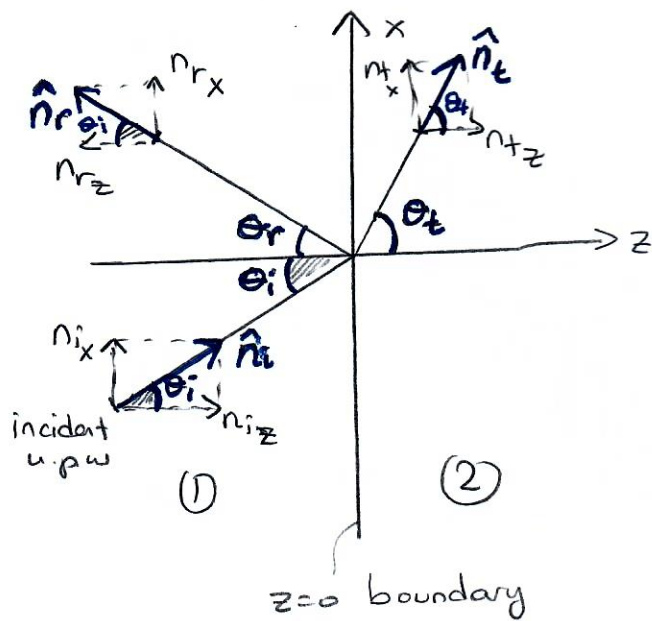


Example: Consider the following "oblique incidence" problem where the planar boundary is at  $z=0$ , and the medium parameters are given as

$$\sigma_1 = 0, \mu_1 = \mu_0, \epsilon_1 = 6\epsilon_0$$

$$\sigma_2 = 0, \mu_2 = \mu_0, \epsilon_2 = 2\epsilon_0$$



For a given incident  $\bar{E}^i$  phasor of a uniform plane wave (upw), determine:

- The angles  $\theta_i, \theta_r, \theta_t$ .
- Reflection and transmission coefficients  $\Gamma_{||}, T_{||}, \Gamma_{\perp}, T_{\perp}$ .
- Reflected  $\bar{E}^r$  phasor
- Transmitted  $\bar{E}^t$  phasor

Solution: The  $\bar{E}^i$  phasor of a u.p.w. is given as:

$$\bar{E}^i(x, z) = \left( \frac{\sqrt{3}}{2} \hat{a}_x + \hat{a}_y - \frac{1}{2} \hat{a}_z \right) e^{-jk_1 \left( \frac{1}{2}x + \frac{\sqrt{3}}{2}z \right)} = \bar{E}_1 e^{-j\bar{k}_i \cdot \bar{r}}$$

$$\begin{aligned} \textcircled{a} \quad e^{-j\bar{k}_i \cdot \bar{r}} &= e^{-jk_1 \hat{n}_i \cdot \bar{r}} = e^{-jk_1 (\sin \theta_i \hat{a}_x + \cos \theta_i \hat{a}_z) \cdot (x \hat{a}_x + y \hat{a}_y + z \hat{a}_z)} \\ &= e^{-jk_1 (\sin \theta_i x + \cos \theta_i z)} = e^{-jk_1 \left( \frac{1}{2}x + \frac{\sqrt{3}}{2}z \right)} \end{aligned}$$

$$\Rightarrow \sin \theta_i = \frac{1}{2}, \cos \theta_i = \frac{\sqrt{3}}{2} \Rightarrow \boxed{\theta_i = 30^\circ}$$

$$\text{Snell's Law of Reflection: } \theta_r = \theta_i \Rightarrow \boxed{\theta_r = 30^\circ}$$

$$\text{Snell's Law of Refraction: } k_1 \sin \theta_i = k_2 \sin \theta_t \Rightarrow \sin \theta_t = \frac{k_1}{k_2} \sin \theta_i = \frac{1}{2}$$

$$\Rightarrow \sin \theta_t = \frac{\sqrt{\mu_0 6\epsilon_0}}{\sqrt{\mu_0 2\epsilon_0}} \cdot \frac{1}{2} = \frac{\sqrt{3}}{2} \Rightarrow \boxed{\theta_t = 60^\circ}$$

(b) For parallel polarization:

$$\Gamma_{||} = \frac{\eta_2 \cos \theta_t - \eta_1 \cos \theta_i}{\eta_2 \cos \theta_t + \eta_1 \cos \theta_i} \quad \text{where } \eta_1 = \sqrt{\frac{\mu_1}{\epsilon_1}} = \sqrt{\frac{\mu_0}{6\epsilon_0}} = \frac{120\pi}{\sqrt{6}} (\Omega)$$

$$\eta_2 = \sqrt{\frac{\mu_2}{\epsilon_2}} = \sqrt{\frac{\mu_0}{2\epsilon_0}} = \frac{120\pi}{\sqrt{2}} (\Omega)$$

$$= \frac{\frac{120\pi}{\sqrt{2}} \frac{1}{2} - \frac{120\pi}{\sqrt{6}} \frac{\sqrt{3}}{2}}{\frac{120\pi}{\sqrt{2}} \frac{1}{2} + \frac{120\pi}{\sqrt{6}} \frac{\sqrt{3}}{2}} = \frac{\frac{1}{\sqrt{2}} - \frac{1}{\sqrt{2}}}{\frac{1}{\sqrt{2}} + \frac{1}{\sqrt{2}}} = 0 \Rightarrow \boxed{\Gamma_{||} = 0}$$

$$\text{As } 1 + \Gamma_{||} = T_{||} \left( \frac{\cos \theta_t}{\cos \theta_i} \right) \Rightarrow 1 + 0 = T_{||} \frac{\cos 60^\circ}{\cos 30^\circ} = T_{||} \frac{\frac{1}{2}}{\frac{\sqrt{3}}{2}} = \frac{1}{\sqrt{3}}$$

$$\Rightarrow \boxed{T_{||} = \sqrt{3}}$$

For perpendicular polarization:

$$\Gamma_{\perp} = \frac{\eta_2 \cos \theta_i - \eta_1 \cos \theta_t}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t} = \frac{\frac{120\pi}{\sqrt{2}} \frac{\sqrt{3}}{2} - \frac{120\pi}{\sqrt{6}} \frac{1}{2}}{\frac{120\pi}{\sqrt{2}} \frac{\sqrt{3}}{2} + \frac{120\pi}{\sqrt{6}} \frac{1}{2}} = \frac{\frac{\sqrt{3}}{\sqrt{2}} - \frac{1}{\sqrt{6}}}{\frac{\sqrt{3}}{\sqrt{2}} + \frac{1}{\sqrt{6}}}$$

$$= \frac{\frac{\sqrt{3}\sqrt{3}}{\sqrt{6}} - \frac{1}{\sqrt{6}}}{\frac{\sqrt{3}\sqrt{3}}{\sqrt{6}} + \frac{1}{\sqrt{6}}} = \frac{3-1}{3+1} = \frac{2}{4} = \frac{1}{2} \Rightarrow \boxed{\Gamma_{\perp} = \frac{1}{2}}$$

$$\text{As } T_{\perp} = 1 + \Gamma_{\perp} = 1 + \frac{1}{2} = \frac{3}{2} \Rightarrow \boxed{T_{\perp} = \frac{3}{2}}$$

(c) For the incident up.w,  $\vec{E}^i = \underbrace{\vec{E}_1}_{\vec{E}_{||} + \vec{E}_{\perp}} e^{-j\vec{k}_i \cdot \vec{r}} = (\vec{E}_{||} + \vec{E}_{\perp}) e^{-j\vec{k}_i \cdot \vec{r}}$

$$\vec{E}_1 = \frac{\sqrt{3}}{2} \hat{a}_x + \hat{a}_y - \frac{1}{2} \hat{a}_z = \underbrace{\left( \frac{\sqrt{3}}{2} \hat{a}_x - \frac{1}{2} \hat{a}_z \right)}_{// \text{ components}} + \underbrace{\hat{a}_y}_{\perp \text{ component}}$$

With respect to the plane of incidence (POI) which is the (x-z) plane here!

Therefore, 
$$\begin{cases} \bar{E}_{1//} = \frac{\sqrt{3}}{2} \hat{a}_x - \frac{1}{2} \hat{a}_z = \underbrace{(1)}_{E_{1//}} \underbrace{\left(\frac{\sqrt{3}}{2} \hat{a}_x - \frac{1}{2} \hat{a}_z\right)}_{\hat{u}_{1//} = \text{unit vector}} \\ \bar{E}_{1\perp} = \hat{a}_y = \underbrace{(1)}_{E_{1\perp}} \underbrace{\hat{a}_y}_{\hat{u}_{1\perp} = \text{unit vector}} \end{cases}$$

Then, 
$$\bar{E}^r = \bar{E}_2 e^{-jk_r \cdot \bar{r}} = (\bar{E}_{2//} + \bar{E}_{2\perp}) e^{-jk_1 \hat{n}_r \cdot \bar{r}}$$

As  $\rho_{//} = 0 \Rightarrow \bar{E}_{2//} = 0 \Rightarrow \bar{E}^r$  has only  $(\perp)$  component.

$$\bar{E}_2 = \bar{E}_{2\perp} = E_{2\perp} \underbrace{\hat{u}_{2\perp}}_{=\hat{a}_y} \text{ where } E_{2\perp} = \underbrace{\rho_{\perp}}_{\frac{1}{2}} \underbrace{E_{1\perp}}_1 \Rightarrow \boxed{E_{2\perp} = \frac{1}{2}}$$

$$\Rightarrow \boxed{\bar{E}_2 = \frac{1}{2} \hat{a}_y} \text{ and } \bar{E}^r = \bar{E}_2 e^{-jk_1 \hat{n}_r \cdot \bar{r}}$$

$$\hat{n}_r = \underbrace{\sin \theta_r}_{\sin 30^\circ = \frac{1}{2}} \hat{a}_x - \underbrace{\cos \theta_r}_{\cos 30^\circ = \frac{\sqrt{3}}{2}} \hat{a}_z = \frac{1}{2} \hat{a}_x - \frac{\sqrt{3}}{2} \hat{a}_z$$

$$\Rightarrow \boxed{\hat{n}_r \cdot \bar{r} = \frac{1}{2} x - \frac{\sqrt{3}}{2} z} \Rightarrow \boxed{\bar{E}^r = \hat{a}_y \frac{1}{2} e^{-jk_1 \left(\frac{1}{2} x - \frac{\sqrt{3}}{2} z\right)}}$$

① For the transmitted field, we have

$$\bar{E}^t = \bar{E}_3 e^{-jk_t \cdot \bar{r}} = (\bar{E}_{3//} + \bar{E}_{3\perp}) e^{-jk_2 \hat{n}_t \cdot \bar{r}}$$

where 
$$\hat{n}_t = \underbrace{\sin \theta_t}_{\sin 60^\circ = \frac{\sqrt{3}}{2}} \hat{a}_x + \underbrace{\cos \theta_t}_{\cos 60^\circ = \frac{1}{2}} \hat{a}_z \Rightarrow \boxed{\hat{n}_t = \frac{\sqrt{3}}{2} \hat{a}_x + \frac{1}{2} \hat{a}_z}$$

$$\Rightarrow \boxed{\hat{n}_t \cdot \bar{r} = \frac{\sqrt{3}}{2} x + \frac{1}{2} z}$$



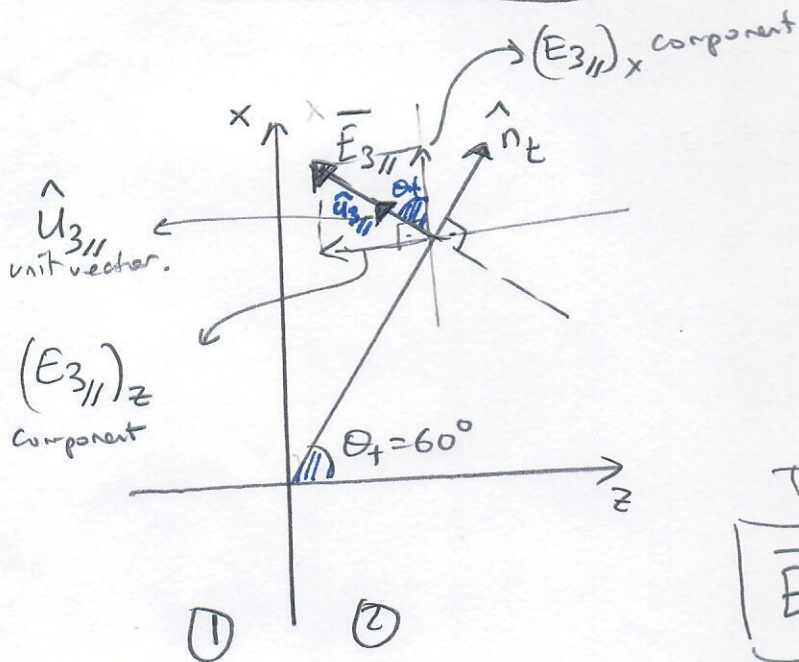
$$\bar{E}_{3\perp} = E_{3\perp} \hat{u}_{3\perp} \text{ where } E_{3\perp} = \underbrace{T_{\perp}}_{3/2} \underbrace{E_{1\perp}}_1 = \frac{3}{2}$$

$$\Rightarrow \boxed{\bar{E}_{3\perp} = \frac{3}{2} \hat{a}_y}$$

$$\bar{E}_{3\parallel} = E_{3\parallel} \hat{u}_{3\parallel} \text{ where } E_{3\parallel} = \underbrace{T_{\parallel}}_{\sqrt{3}} \underbrace{E_{1\parallel}}_1 = \sqrt{3}$$

unit vector in the direction of  $\bar{E}_{3\parallel}$

$$\Rightarrow \boxed{\bar{E}_{3\parallel} = \sqrt{3} \hat{u}_{3\parallel}}$$



$$\text{Here } \hat{u}_{3\parallel} = \hat{a}_x \underbrace{\cos \theta_t}_{\cos 60^\circ} - \hat{a}_z \underbrace{\sin \theta_t}_{\sin 60^\circ}$$

$$\boxed{\hat{u}_{3\parallel} = \frac{1}{2} \hat{a}_x - \frac{\sqrt{3}}{2} \hat{a}_z}$$

Then,

$$\boxed{\bar{E}_{3\parallel} = \sqrt{3} \left( \frac{1}{2} \hat{a}_x - \frac{\sqrt{3}}{2} \hat{a}_z \right)}$$

$$\text{Then, } \bar{E}^t = (\bar{E}_{3\parallel} + \bar{E}_{3\perp}) e^{-jk_2 \left( \frac{\sqrt{3}}{2} x + \frac{1}{2} z \right)}$$

$$\boxed{\bar{E}^t = \left( \frac{\sqrt{3}}{2} \hat{a}_x + \frac{3}{2} \hat{a}_y - \frac{3}{2} \hat{a}_z \right) e^{-jk_2 \left( \frac{\sqrt{3}}{2} x + \frac{1}{2} z \right)}}$$

$$\text{Finally, check if } (\bar{E}_{\text{tang}}^i + \bar{E}_{\text{tang}}^r) \Big|_{z=0} \stackrel{?}{=} \bar{E}_{\text{tang}}^t \Big|_{z=0}$$

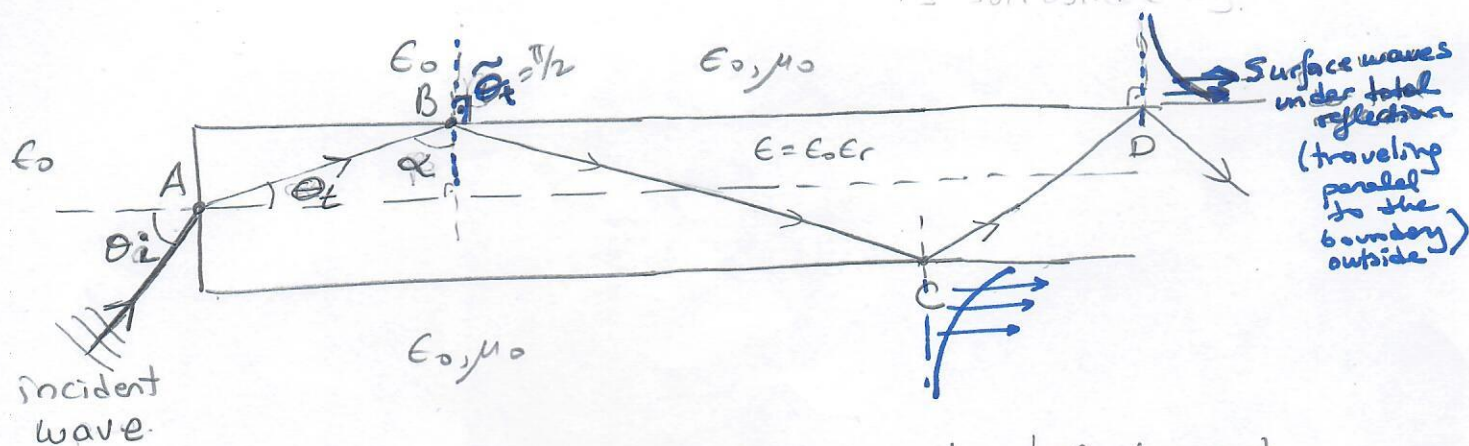
(x and y components are tangential wrt z=0 boundary)

$$\left( \frac{\sqrt{3}}{2} \hat{a}_x + \hat{a}_y \right) e^{-jk_1 \frac{x}{2}} + \frac{1}{2} \hat{a}_y e^{-jk_1 \frac{x}{2}} \stackrel{?}{=} \left( \frac{\sqrt{3}}{2} \hat{a}_x + \frac{3}{2} \hat{a}_y \right) e^{-jk_2 \frac{\sqrt{3}}{2} x}$$

As  $k_1 \sin \theta_i = k_2 \sin \theta_t \Rightarrow \frac{k_1}{2} = k_2 \frac{\sqrt{3}}{2} \Rightarrow$  exponentials are cancelled and equality is shown!  
BC is satisfied ✓



Example: Consider a dielectric rod with  $\epsilon = \epsilon_r \epsilon_0$ ,  $\mu = \mu_0$ ,  $\sigma = 0$ .  
 Assume the outside medium is air. (optical fiber)  
 is surrounded by air.



at point A: Wave enters from air to dielectric rod

Apply Snell's Law  $\sqrt{\epsilon_0 \mu_0} \sin \theta_i = \sqrt{\epsilon_0 \epsilon_r \mu_0} \sin \theta_t$

$$\Rightarrow \boxed{\sin \theta_t = \frac{1}{\sqrt{\epsilon_r}} \sin \theta_i} \quad (1)$$

at points B, C, D etc., "total reflection" must occur to keep the wave escaping from the rod into air!

So, we need  $\alpha \geq \theta_c$  where  $\boxed{\sin \theta_c = \frac{1}{\sqrt{\epsilon_r}}} \quad (2)$   
 ( $\sin \alpha \geq \sin \theta_c$ )

(Apply Snell's Law for  $\alpha = \theta_c$ ,  $\theta_t = \frac{\pi}{2}$ )  $\Rightarrow \sqrt{\mu_0 \epsilon_0 \epsilon_r} \sin \theta_c = \sqrt{\mu_0 \epsilon_0} \sin \frac{\pi}{2}$

But,  $\alpha = \frac{\pi}{2} - \theta_t \Rightarrow \sin \alpha = \sin(\frac{\pi}{2} - \theta_t) = \cos \theta_t$

For "total reflection", we need  $\boxed{\sin \alpha = \cos \theta_t \geq \sin \theta_c = \frac{1}{\sqrt{\epsilon_r}}}$

$$\cos \theta_t = \sqrt{1 - \sin^2 \theta_t} \stackrel{\text{use (1)}}{=} \sqrt{1 - \left(\frac{1}{\sqrt{\epsilon_r}} \sin \theta_i\right)^2} \geq \frac{1}{\sqrt{\epsilon_r}}$$

$$\Rightarrow 1 - \left(\frac{1}{\sqrt{\epsilon_r}} \sin \theta_i\right)^2 \geq \left(\frac{1}{\sqrt{\epsilon_r}}\right)^2 \Rightarrow \epsilon_r - \sin^2 \theta_i \geq 1$$

maximum acceptance angle  $\theta_{i, \max} = \sin^{-1}(\sqrt{\epsilon_r - 1})$

← or

$\Rightarrow \boxed{\epsilon_r \geq 1 + \sin^2 \theta_i}$   
 is needed to guide EM wave within the rod!