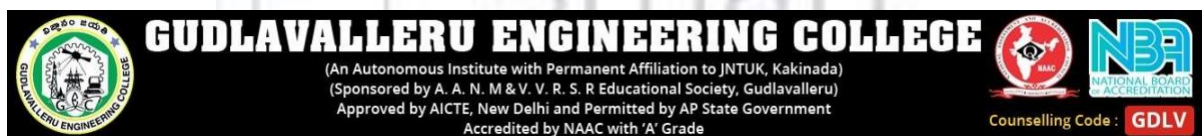


Internship Program Report

By

ALURI SUPRIYA
18481A0203



In association with



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Introduction

Internship program arranged by GUDLAVALLERU ENGINEERING COLLEGE in association with Smart Internz, Hyderabad for the benefit of 3rd year EEE batch 2018-2022 on Electrical Detailed design Engineering for Oil& Gas, Power and Utility industrial sectors.

Program organiser

Smart Bridge, Hyderabad.

Pioneer in organising Internships, knowledge workshops, debates, hackathons, Technical sessions and Industrial Automation projects.



Courtesy

Dr. Sri B. Dasu – HOD – EEE, GEC

Dr.G.Srinivasa Rao-Coordinator

Mr. Ramesh V - Mentor

Mr. Vinay Kumar - System Support

Mr. Harikanth – Softwar/Technical Support

Program details

Smart Internz program schedule: 4 weeks starting from 3rd May 2021

Daily schedule time shall be 4PM to 6.30PM

Mode of Classes: Online through ZOOM

Presenter: Mr Ramesh V

Internship program

We have been given the opportunity to learn and interact with industry experienced engineering specialist to learn the Electrical detailed design engineering for various industrial sectors.

3rd May 2021: Introduction to EPC Industry

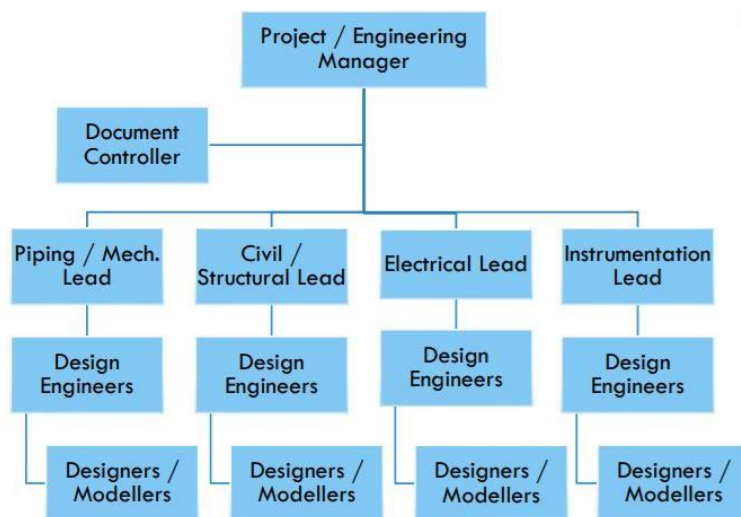
1	EPC Industry & Electrical Detailed Engineering	EPC Industry Engineering Procurement Construction	Introduction Types of Engineering Engineering role in procurement Engineering role during construction
---	--	---	---

Topic details:

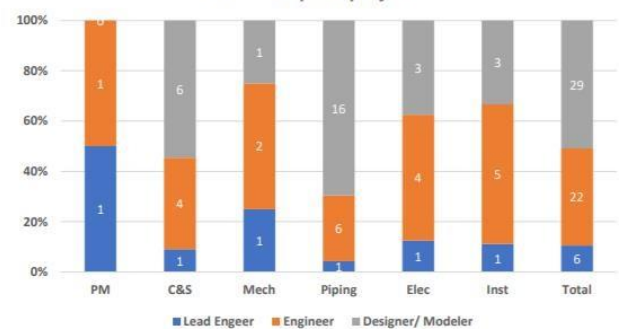
1B. ENGINEERING DEPARTMENT



Engineering Department Organization Chart



Engineering Manpower Distribution for typical a multi-discipline project



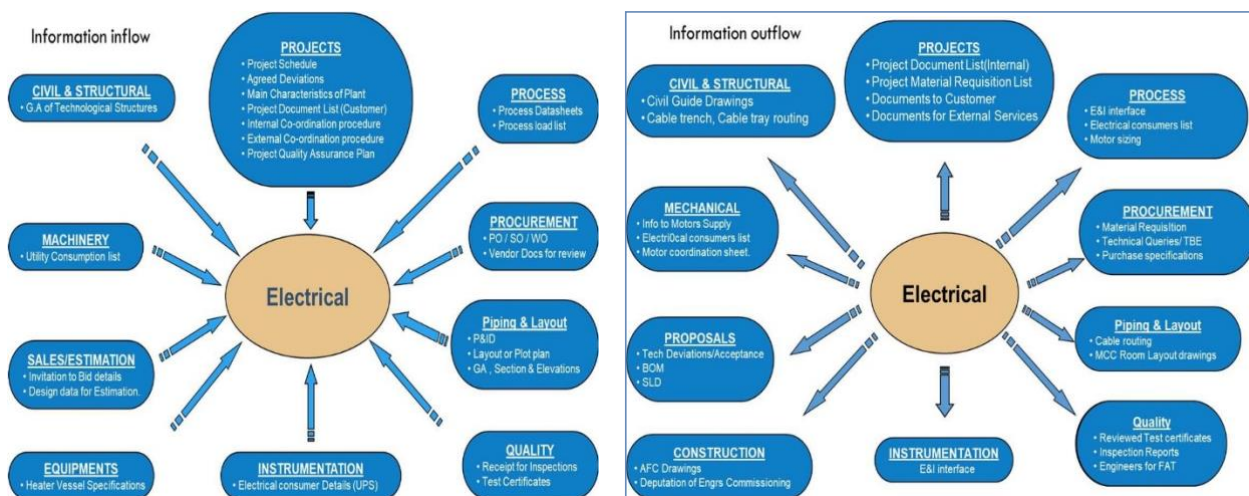
On this we have learnt about Engineering phases, Engineering deliverables (drawings & documents) list, Design Engineer role at various phases of project.

4th May2021: Engineering documentation for EPC projects

2	Electrical Design Documentation	Engineering Deliverables list Detailed Engineering work flow Document transmission Deliverables types	Sequence of deliverables Detailed engineering process Document submission and info exchange Different types of deliverables
---	---------------------------------	--	--

Topic details:

SEQUENCE OF DELIVERABLES



On this day we have gone through Deliverable list of details and work flow in electrical detailing .

This topic has given a detailed information of deliverables and its parts. And also gone through electrical information inflow and out flow in a neat manner which gives us an idea regarding electrical terminologies and abbreviations.

5th May2021: Engineering documentation for commands and formulae

3	Electrical Design Documentation	Ms word commands Ms excel formulae Auto cad basic commands
---	---------------------------------	--

Topic details:

MS Word,Excel and Auto cad COMMANDS.

Word Shortcut Keys

Command Name	Keys
All Caps	Ctrl+Shift+A
Apply List Bullet	Ctrl+Shift+L
Auto Format	Alt+Ctrl+K
Auto Text	F3
Bold	Ctrl+B
Cancel	ESC
Center Para	Ctrl+E
Change Case	Shift+F3
Clear	Del
Close or Exit	Alt+F4
Copy	Ctrl+C
Create Auto Text	Alt+F3
Cut	Ctrl+X
Double Underline	Ctrl+Shift+D
Find	Ctrl+F
Help	F1
Hyperlink	Ctrl+K
Indent	Ctrl+M
Italic	Ctrl+I
Justify Para	Ctrl+J
Merge Field	Alt+Shift+F
New Document	Ctrl+N
Open	Ctrl+O
Outline	Alt+Ctrl+O
Overtyping	Insert
Page	Alt+Ctrl+P
Page Break	Ctrl+Return
Paste	Ctrl+V
Paste Format	Ctrl+Shift+V
Print	Ctrl+P
Print Preview	Ctrl+F2
Redo	Alt+Shift+Backspace
Redo or Repeat	Ctrl+Y
Save	Ctrl+S
Select All	Ctrl+A
Small Caps	Ctrl+Shift+K
Style	Ctrl+Shift+S
Subscript	Ctrl+=
Superscript	Ctrl+Shift+=
Task Pane	Ctrl+F1
Time Field	Alt+Shift+T

Underline	Ctrl+U
Undo	Ctrl+Z
Update Fields	F9
Word Count List	Ctrl+Shift+G

Function Keys	
F1	Get Help or visit Microsoft Office Online.
F2	Move text or graphics.
F3	Insert an AutoText (AutoText: A storage location for text or graphics you want to use again, such as a standard contract clause or a long distribution list. Each selection of text or graphics is recorded as an AutoText entry and is assigned a unique name.) entry (after Microsoft Word displays the entry).
F4	Repeat the last action.
F5	Choose the Go To command (Edit menu).
F6	Go to the next pane or frame.
F7	Choose the Spelling command (Tools menu).
F8	Extend a selection.
F9	Update selected fields.
F10	Activate the menu bar.
F11	Go to the next field.
F12	Choose the Save As command (File menu).

In this session we learnt the basic fields of engineering such as MS WORD COMMANDS,MS EXCEL FORMULAE AND BASIC AUTOCAD PRINCIPLES. From these commands we have drawn powerplant sketches .

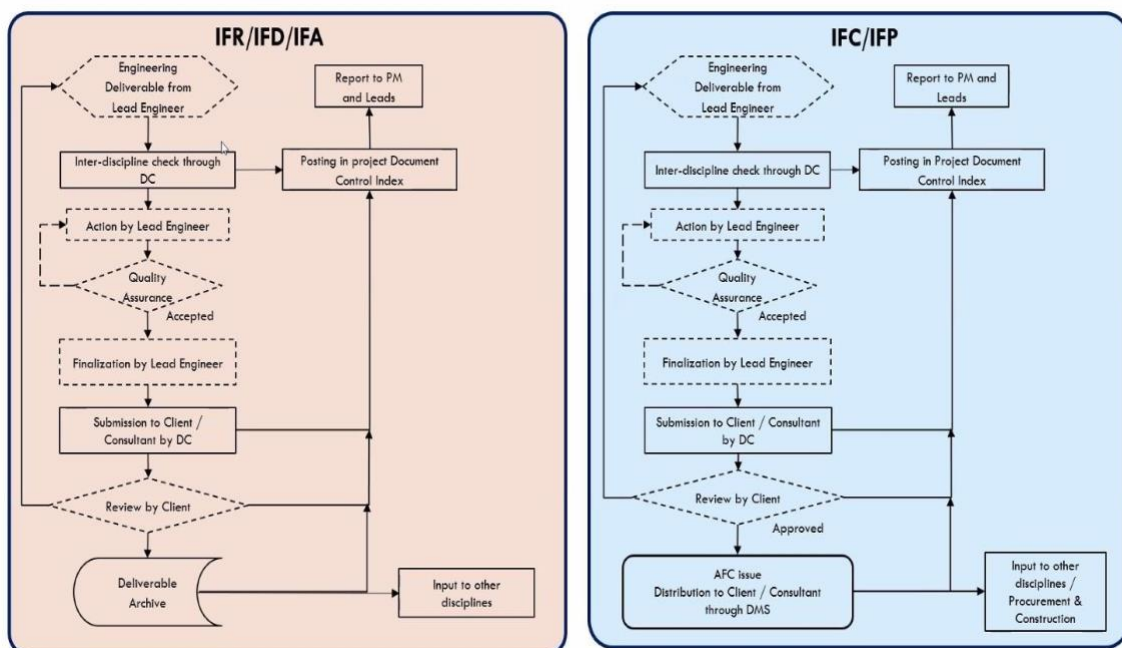
7th May2021: Engineering documentation for Electrical system design

- | | | |
|---|--|--|
| 4 | Electrical system design for a small small project | Overall plant description
Sequence of approach
Approach to detailed design |
|---|--|--|

Topic details: Overall plant description ,approach to detailed design.



1C. DETAILED ENGINEERING



Here we observed that how to do a project and Sequence of approach, Approach to detail design and Overall plant distribution system.

5	Electrical system design for typical diagrams	Load lists shedule Single line diagram	Power flow diagram Typical schematic diagram
---	---	---	---

Sl. No.	EQUIPMENT										REMARKS									
	Equipment No.	Description	Supply by	Value	Non-essential / Essential	Accounting	Estimated	Load factor	Efficiency	Power factor	MW + A/D				kVAH + kVAH				Remarks	
											Continuous		Intermittent and spares		Standby					
											Max	Min	Max	Min	Max	Min				
PROCESS LOADS																				
1	PD-3431	Portable MEG Injection Pump Package	LEWA	x	27.00	37.00	0.73	0.91	0.83						1	20.67	10.94		Portable Skid (Please refer Note-d)	
2	34-PM6A01	Batch Return Pump Motor	LEWA	x	25.45	31.00	0.82	0.93	0.81						1	27.37	19.81			
3	34-PM6A01B	Liquid Return Pump Motor	LEWA	x	25.45	31.00	0.82	0.93	0.81								27.37	19.81		
4	34-PM6A02	Booster Pump Motor (LRP Package)	LEWA	x	1.40	2.20	0.64	0.78	0.84							1	1.79	1.16		
5	34-PM6A02B	Booster Pump Motor (LRP Package)	LEWA	x	1.40	2.20	0.64	0.78	0.84									1.79	1.16	
6	34-PMF002A	Corrosion inhibitor injection Pump Motor	LEWA	x	6.45	11.00	0.59	0.90	0.77	1	7.17	5.94								
7	34-PMF002B	Corrosion inhibitor injection Pump Motor	LEWA	x	6.45	11.00	0.59	0.90	0.77							1	7.17	5.94		
8	34-PMF003A	Batch Corrosion inhibitor injection Pump Motor	RAM	x	133.50	160.00	0.83	0.96	0.80								139.06	104.30		
9	34-PMF003B	Batch Corrosion inhibitor injection Pump Motor	RAM	x	133.50	160.00	0.83	0.96	0.80								139.06	104.30		
10	34-PMF004A	KH Inhibitor Injection Pump Motor	LEWA	x	6.45	11.00	0.59	0.90	0.77	1	7.17	5.94							VSD for speed control	
11	34-PMF004B	KH Inhibitor Injection Pump Motor	LEWA	x	6.45	11.00	0.59	0.90	0.77										VSD for speed control	
12	34-PMF005A	Scale Inhibitor Injection Pump Motor	FUTURE	x	3.00	4.00	0.75	0.85	0.81	1	3.53	2.56							Future	
13	34-PMF005B	Scale Inhibitor Injection Pump Motor	FUTURE	x	3.00	4.00	0.75	0.85	0.81										Future	
14	34-KM002A	Nitrogen Compressor Motor	GENERON	x	30.00	37.50	0.80	0.90	0.80	1	33.33	25.00								
15	34-KM002B	Nitrogen Compressor Motor	GENERON	x	30.00	37.50	0.80	0.90	0.80	1	33.33	25.00								
16	34-KM003A	Nitrogen Compressor Motor	GENERON	x	30.00	37.50	0.80	0.90	0.80								33.33	25.00		
17	34-KM003A	Afterscooler for Nitrogen Compressor	GENERON	x	1.15	2.50	0.48	0.78	0.80							1	1.47	1.11		
18	34-KM003B	Afterscooler for Nitrogen Compressor	GENERON	x	1.15	2.50	0.48	0.78	0.80							1	1.47	1.11		
19	34-KM003C	Afterscooler for Nitrogen Compressor	GENERON	x	1.15	2.50	0.48	0.78	0.80									1.44	1.08	
20	34-HM002	Nitrogen Heater		x	6.20	1.00	6.20	0.90	1.00											
21	34-PMF010A	Hydraulic Fluid Pump - Wellhead HPV - Very High Pressure	FRAMIS	x	0.19	0.55	0.35	0.80	0.70											

Page 8 of 22

11th May2021: Classification of Transformers and Generators

6	Classification of Transformers and Generators	Different types of Transformers	Different types of Generators
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Topic Details: Classification of Transformers and Generators.



1 Ph. Pad mounted 3 Ph Pole mounted Commercial/ 3 Ph Oil filled (ONAN) Distribution Residential lighting Residential/ street lighting type for industrial & commercial.



415V Diesel generator sets for standby / 240V 1 ph diesel generator set for lighting and small power only Emergency power supply.

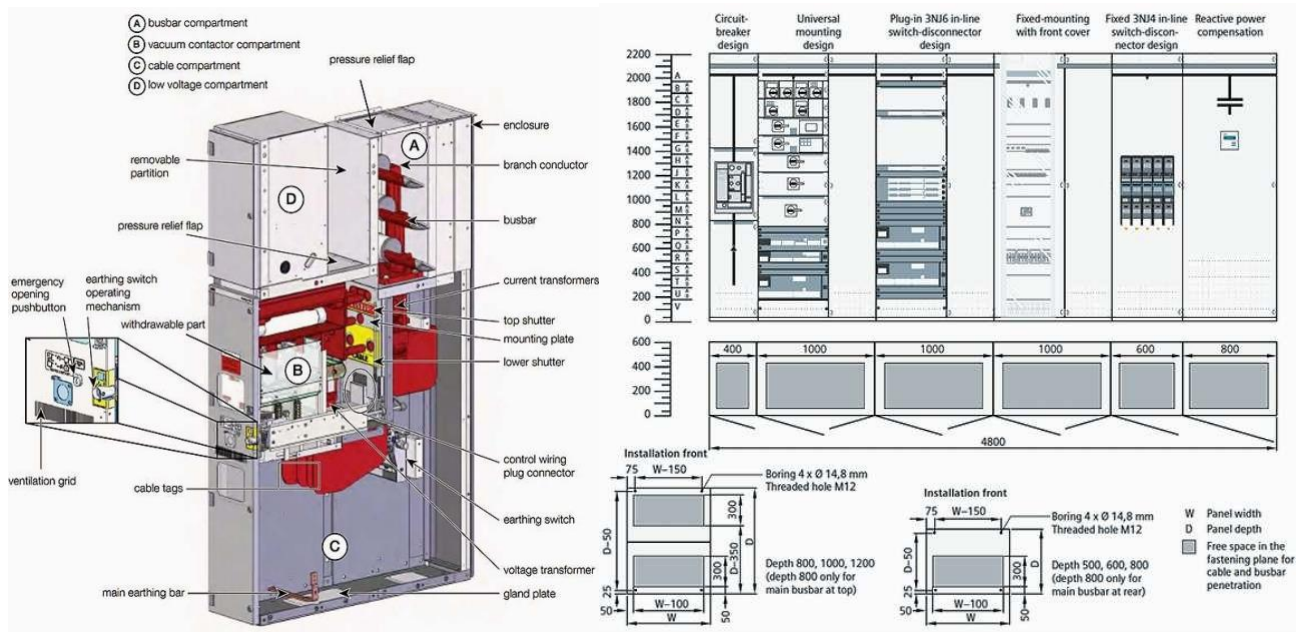
Transformer shall include a primary disconnect on the incoming power source. The disconnect means shall be either a breaker or a load break primary switch that is fused. Transformers are sized to carry the peak running load of all busses connected to them. In addition, feeders to and from power transformers shall be rated to carry full current at the maximum rating.

The packaged combination of a diesel engine, an alternator and various ancillary devices such as base, canopy, sound attenuation, control systems, circuit breakers, jacket water heaters, starting systems etc., is referred to as a Diesel Generating Set or a DG Set in short.

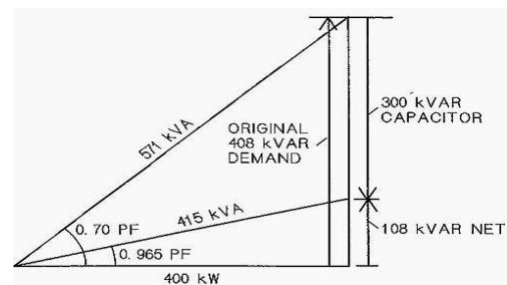
12th May2021: Classification of Switchgears construction and power factor improvement

7	Classification of Switchgears construction and power factor improvement	Different types of Switchgears Assembles	Power factor improvement
---	---	--	--------------------------

Topic details: Classification of Switchgear construction Features.



Switchgear includes switching & protecting devices like fuses, switches, CTs, VTs, relays, circuit breakers, etc. This device allows operating devices like electrical equipment, generators, distributors, transmission lines, etc.



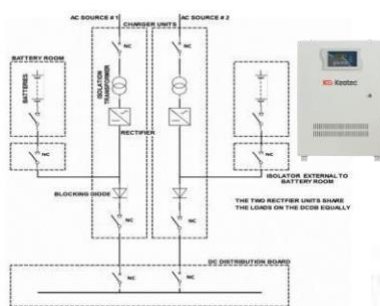
Power factor defined as the ratio of real power to volt-amperes and is the cosine of the phase angle between the voltage and current in an AC circuit.

17th May2021: Detailing about UPS system and Busducts.

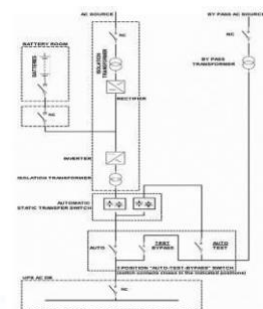
8	Detailing about UPS system and Busducts	Uninterruptible power supply system	Busducts of the system
---	---	-------------------------------------	------------------------

Topic details: Power distribution of UPS system and Busducts.

UPS systems are designed to provide continuous power to a load, even with an interruption or loss of utility supply power. UPS generally involves a balance of cost Vs need.



110V or 220V DC
UPS System



110V or 230V
AC UPS System

Busducts are classified into various types depending on its application via phase separated Busducts, segregated phase busducts, non-segregated phase busducts.

Phase Separated
busduct



18th May2021: Detailing about Motor Starters and Sizing of motors.

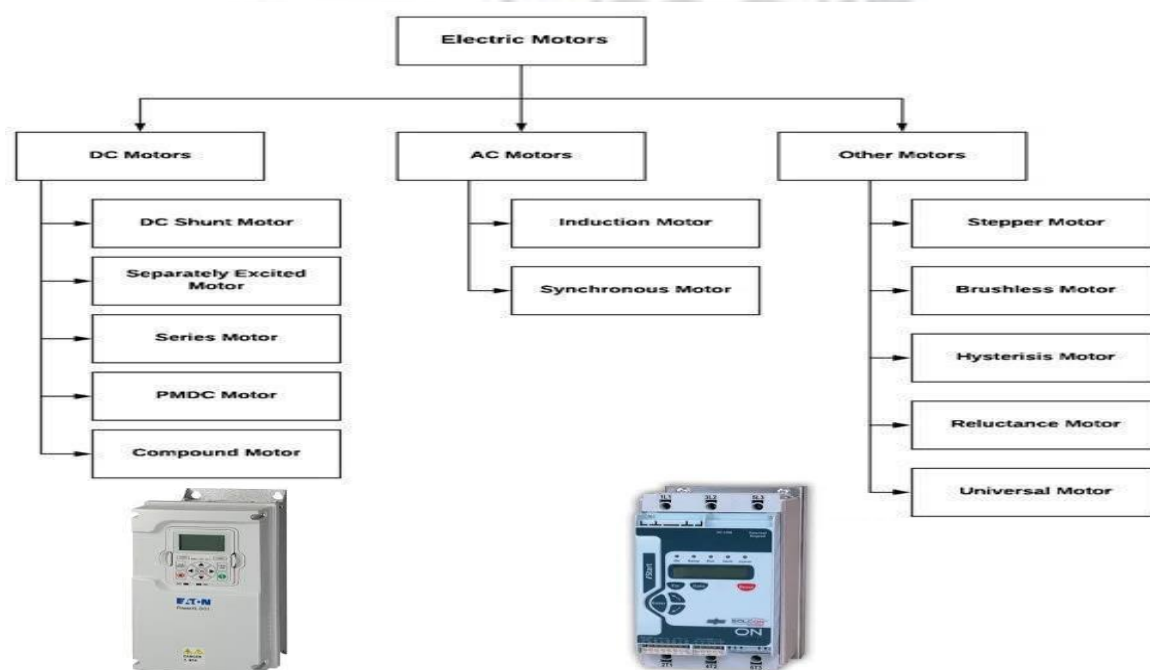
9	Detailing about Motor Starters and Sizing of motors	Motor starters and drives	Sizing and selection of motors
---	---	---------------------------	--------------------------------

Topic details: Detailing about Motor Starter and Sizing of motors and their selection.

The principal function of a motor starter is to start and stop the respective motor connected with specially designed electromechanical switches which are similar in some ways to relays. The main difference between a relay and a starter is that a starter has overload protection for the motor that is missing in a relay.

Different types of motor starters are as follows:

- Direct-On-Line Starter
- Rotor Resistance Starter
- Stator Resistance Starter
- Auto Transformer Starter
- Star Delta Starter



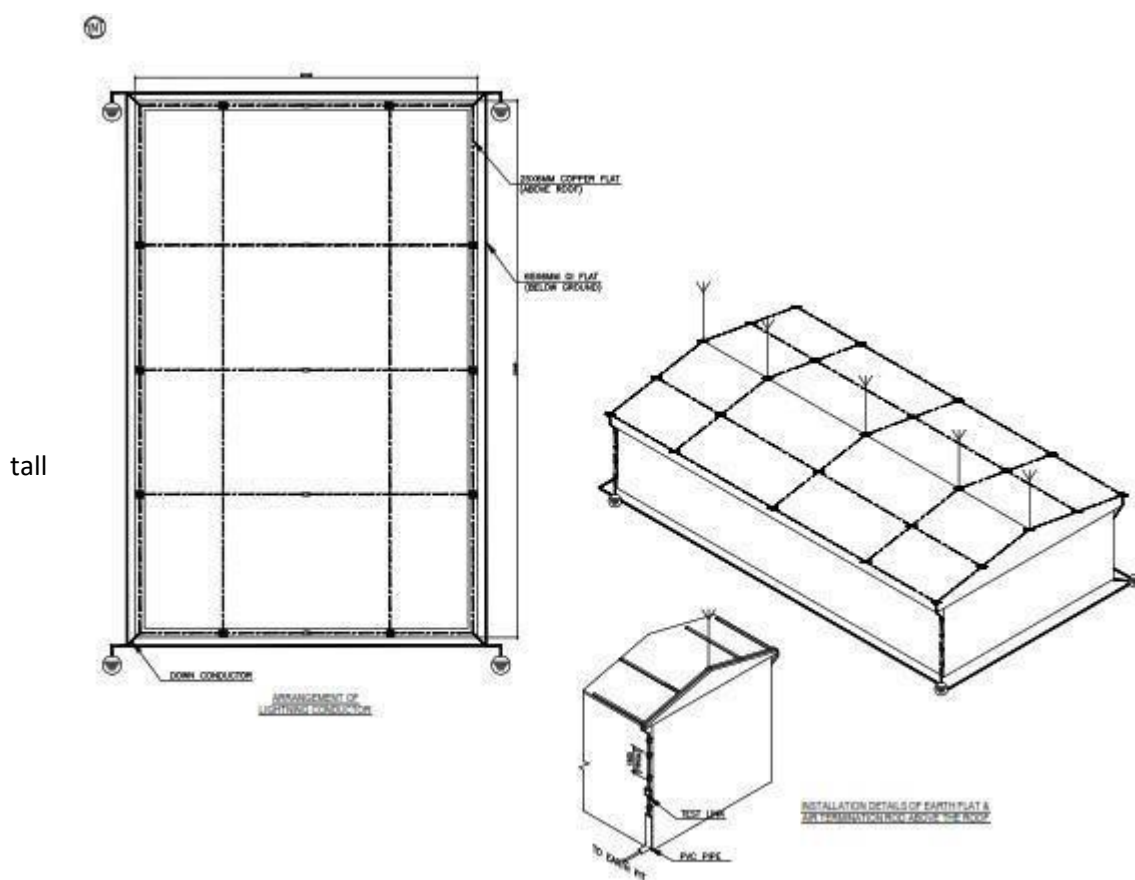
- Starting method – soft starter, Auto transformer, Star/Delta
- Speed variation – Constant speed, variable speed for VFD
 - Frame Size – 56 to 280
- Insulation class & Temp rise – A, E, B, F & H
- Protection – Protection based on voltage & KW rating
- Cable entry, size & termination – Cable sizing based on starting/running voltage drop and short circuit current Vibration – monitoring based on KW rating.

19th May2021: Describing about Earthing system and Lighting Protection.

10	Describing about Earthing system and Lighting Protection.	Plant Earthing system	Lighting Protection materials
----	---	-----------------------	-------------------------------

Topic details: Describing about Earthing system and Lighting Protection.

The purpose of earthing is to prevent damage to people and prevent or limit plant damage. Various earthing systems are provided with each earthing system is isolated from the other.



Lightning protection required for high rise structures and important buildings against lightning currents during thunder storms. Primarily Lightning protection system calculations are done based on soil resistivity, conductor material, coverage structure / Building to determine whether lightning protection is required or not.

20th May2021: Lighting or illumination systems and calculations.

11 Lighting or Illumination systems and Calculations

Lighting or illumination systems

Lighting calculations

Topic details: Lighting or Illumination systems and Calculations.

All outdoor lighting fittings shall be connected with armoured PVC cable of suitable no. of cores and size. Necessary type and no. of junction boxes shall be provided for branch connections. Indoor light fittings shall be connected with FRLS PVC wires laid in cable trunks or conduits.



Inputs required: Equipment and cable routing layouts, lighting calculations, Design basis for type of light fittings to be used, required lux levels

Lighting calculations software: Dialux, Chalmrite, Calculux, Relux, Luxicon, CG Lux

Applicable Standards: IS 6665: Code of practice for industrial lighting, IS 3646: Code of practice for interior illumination, IEC 60598: Luminaires, IEC 62493: Assessment of lighting equipment related to human exposure to electromagnetic field

Deliverables: Indoor Lighting layouts, socket outlet layouts, Street lighting and area lighting layouts. BOQ.

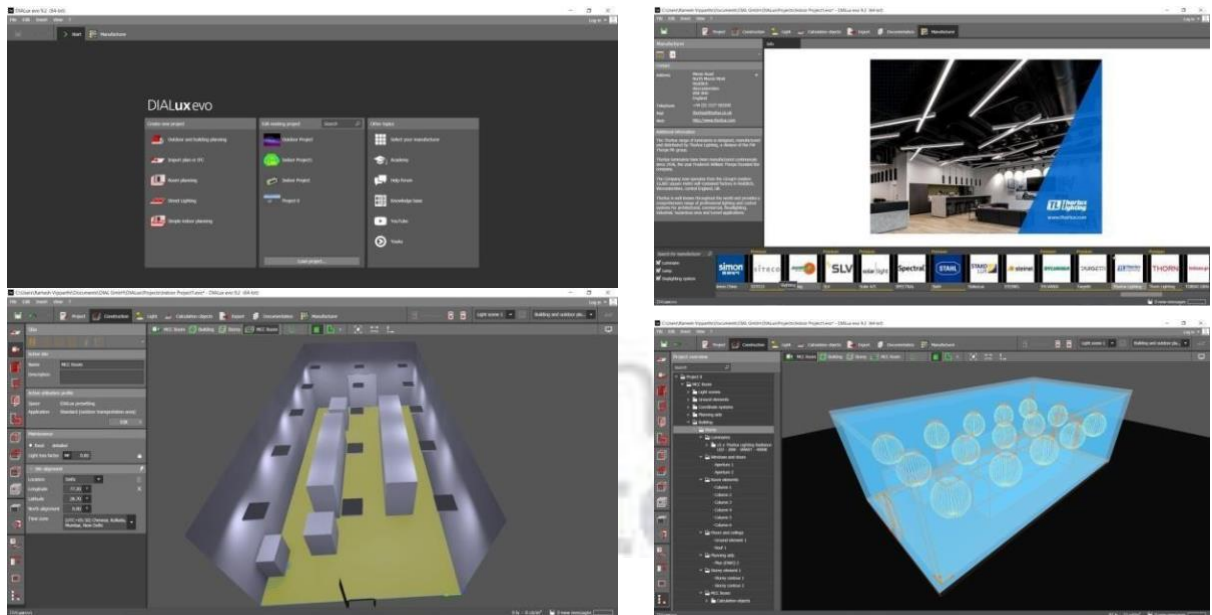
Types of light fittings: Industrial, flame proof type (EX d), increased safety type (Ex e).

21th May 2021: Lighting or illumination systems using DIALUX software.

12	Lighting or Illumination using DIALUX software	Lighting or illumination systems	Operation of dialux software
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Topic details: Lighting or Illumination Calculations using DIALUX software.

Here we are using this Dialux evo 5.9.2 software windows to construct the power plant and we can perform the operation from this software.



We have the indoor calculations and outdoor calculations too.

Results

	Symbol	Calculated	Target	Check	Index
Workplane	$E_{\text{perpendicular}}$	264 lx	≥ 500 lx	✗	50
	ϕ	0.077	-	-	50
Consumption values	Consumption	1300 kWh/a	max. 3400 kWh/a	✓	
Lighting power density	Room	4.82 W/m ²	-	-	
		1.83 W/m ² /100 lx	-	-	

Utilisation profile: DIALux presetting, Standard (office)

Luminaire list

pcs.	Manufacturer	Article No.	Article name	P	ϕ	Luminous efficacy
15	THORLUX	RAD16401	Radiance LED - 28W - SMART - 4000K	31.0 W	4130 lm	133.2 lm/W

Indoor calculation

Piperack

Luminaire list

Φ_{total}	P_{total}	Luminous efficacy
15850 lm	360.0 W	44.0 lm/W

5	CEAG	122658811	eLLK 92018/18 CG-S	72.0 W	3170 lm	44.0 lm/W
		03				

outdoor calculations

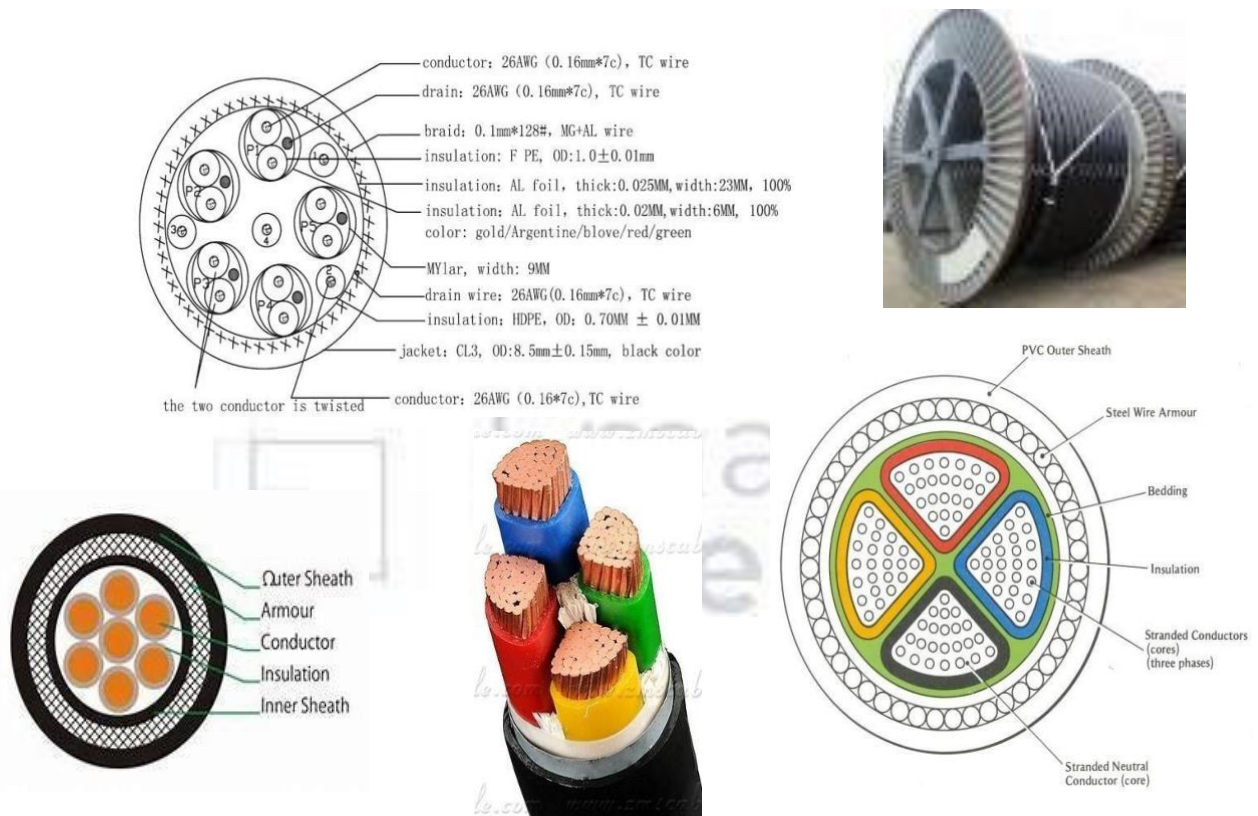
24th May2021: Cabling and their calculations and types.

13 Cabling and their types and calculations

Cabling calculations

Types of cabling materials

Topic details: Cabling and their types and calculations .



Electrical cables must be properly supported to relieve mechanical stresses on the conductors, and protected from harsh conditions such as abrasion which might degrade the insulation.

Cables generally laid in the cable trays above ground, direct buried underground and in metallic or PVC conduits. Derating factors may be applicable for each type of cable laying conditions.

Cable trays shall be generally loaded 60 to 70% leaving space for future use. Underground cabling shall be done in concrete cable trenches with cable trays in paved areas and directly buried with mandatory gap of 300mm between different systems of cables.

25th May2021: Cabling calculations and Cable gland selection.

14	Cabling calculations and cable gland Selection	Cabling calculations	Cable gland selection
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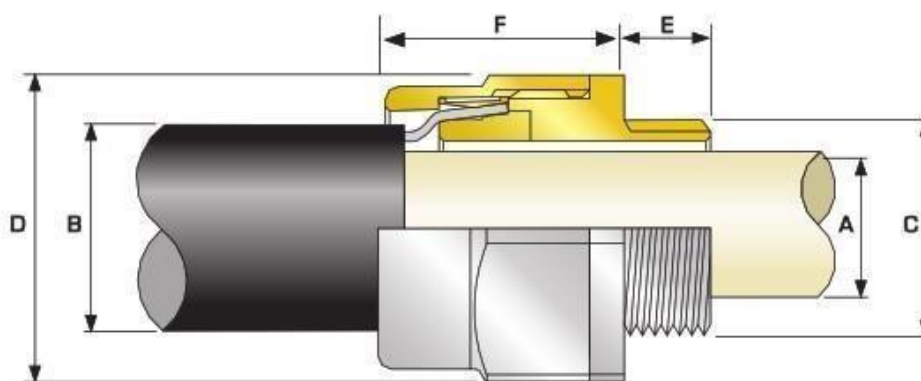
Topic details: Cable sizing calculation and cable gland selection.

Inputs required: Load List, Design basis, Electrical equipment layout, cable schedule, vendor catalogues for cable tray.

Cable tray sizing shall be performed for each branch of cable tray routing up to the load point.

Results shall be checked with specified limits mentioned in design basis.

Cable gland:



Cable Gland Selection Table

Refer to illustration at the top of the page.

Cable Gland Size	Available Entry Threads "C" (Alternate Metric Thread Lengths Available)		Cable Bedding Diameter "A"	Overall Cable Diameter "B"	Armour Range		Across Flats "D"	Across Corners "D"	Protrusion Length "F"
	Metric	Thread Length (Metric) "E"	Max	Max	Min	Max	Max	Max	
20S16	M20	10.0	8.7	13.2	0.8	1.25	24.0	26.4	35.2
20S	M20	10.0	11.7	15.9	0.8	1.25	24.0	26.4	32.2
20	M20	10.0	14.0	20.9	0.8	1.25	30.5	33.6	30.6
25	M25	10.0	20.0	26.2	1.25	1.6	36.0	39.6	36.4
32	M32	10.0	26.3	33.9	1.6	2.0	46.0	50.6	32.6
40	M40	15.0	32.2	40.4	1.6	2.0	55.0	60.5	36.6
50S	M50	15.0	38.2	46.7	2.0	2.5	60.0	66.0	39.6
50	M50	15.0	44.1	53.1	2.0	2.5	70.1	77.1	39.1
63S	M63	15.0	50.0	59.4	2.0	2.5	75.0	82.5	52.0
63	M63	15.0	56.0	65.9	2.0	2.5	80.0	88.0	49.8
75S	M75	15.0	62.0	72.1	2.0	2.5	90.0	99.0	63.7
75	M75	15.0	68.0	78.5	2.5	3.0	100.0	110.0	57.3
90	M90	24.0	80.0	90.4	3.15	4.0	114.3	125.7	66.6

28 th May2021: Load calculations and Transformer sizing calculations

15 Load calculations
and TR
calculations

Load calculations

TR calculations

Topic details:

List of electrical load calculations.

Sl. No.	Equipment No.	Equipment Description	Breaker Rating	Breaker Type	Breaker No. of Poles	ELCB Rating	Absorbed Load	Motor / Load Rating	Load Factor (AI/BI)	Efficiency Factor (CI)	Power Factor at Load Factor (CI)	kVA = (AI/BI)		Consumed Load		kVAR = kVA x tan φ	
							(A) kVA	(B) kVA	(C) decimal	(D) decimal	cos φ	kW	kVAR	Continuous	Intermittent	Stand-by	
1	PU2315	Silica filter feed pump					12.47	15.00	0.83	0.85	0.73	14.67	13.74				
2	PU 2314-A	Absorbent/Neutral oil pump (W)					3.62	4.70	0.77	0.85	0.73	4.3	4.0				
3	PU 2314-B	Absorbent/Neutral oil pump (W)					3.11	3.70	0.84	0.85	0.73						
4	PU2305	Feed Pump (Separator)					12.58	15.00	0.84	0.85	0.73	14.8	13.9				3.7
5	M02305	M02305 (W)					12.68	15.00	0.85	0.85	0.73	14.9	14.0				3.4
6	M02309	M02309 (W)					12.68	15.00	0.85	0.85	0.73	14.9	14.0				3.4
7	BV2313	Blower					5.45	7.50	0.73	0.85	0.73	6.4	6.0				14.9
8	TK 2313B (I)	TK 2313B (I)					0.53	0.75	0.71	0.85	0.73						14.0
9	SC2311	Screw conveyor (I)					1.23	1.50	0.82	0.85	0.73						
10	AG 2324A	Criso acid tank agitator (W)					0.91	1.10	0.83	0.85	0.73	1.07	1.00				
11	AG 2324B	Criso acid tank agitator (W)					0.91	1.10	0.83	0.85	0.73						
12	AG 2309	Criso oil reaction vessel agitator					3.34	3.70	0.90	0.85	0.73	3.93	3.66				1.1
13	AG 2309	Upe oil reaction vessel agitator					1.21	1.50	0.81	0.85	0.73	1.42	1.33				1.0
14	AG 2310	Upe oil reaction vessel agitator					1.21	1.50	0.81	0.85	0.73	1.42	1.33				
15	AG 2314	Slope Absorbent Tank Agitator					2.12	3.00	0.71	0.85	0.73	2.49	2.34				
Maximum of normal running plant load:			66.0 kVA			61.6 kVAR	sqrt (kW ² + kVAR ²) =		90.4 kVA		TOTAL	65.40	61.23	2.07	1.94	19.65	16.39
Peak Load:			68.0 kVA			63.7 kVAR	sqrt (kW ² + kVAR ²) =		93.1 kVA		kVA	69.59	66.94	2.84		26.91	
Assumptions																	
Load factor, Efficiency and Power factor:																	
Load Rating (kW)																	
≤ 20																	
> 20 - ≤ 45																	
> 45 - ≤ 150																	
> 150																	

TR sizing calculations:

Calculation for Transformer Capacity

1.0 Example of calculation for Transformer Capacity

1.1 Calculation for consumed load

Consumed loads used for this example are as follows:

	kW	kVar	kVA	
a. Continuous load	56.86	53.2	77.89	--- (i)
b. Intermittent load / Diversity Factor	1.8	1.7	2.47	--- (ii)
c. Stand-by load required as consumed load	17.08	16.0	23.40	--- (iii)

Max. Consumed load = ((i) + 30% (ii) + 10% (iii)) =	59.1	55.3	80.97
Future expansion load (20% capacity)	11.8	11.1	16.19
Total Load =	70.9	66.4	97.16

1.2 Calculation for 3.3kV / 0.433 kV transformer capacity

Max. Consumed load	=	81.0 kVA
Spare capacity	=	16.2 kVA
Required capacity	=	97.2 kVA
Transformer rated capacity	=	120 kVA

1.3 Voltage regulation check

During starting or reacceleration of max. capacity motor (3400 kW), while all the other loads running, the voltage regulation is as follows:

$P_T =$	120 KVA	(%Z) =	4	& Ratio %R =	3.3
Hence, %R =					1.176 %
%X =					3.82 %
$P_H =$	15 KW having (K =	6	& C =	1	& Cos $\theta =$ 0.73 & Eff. = 0.85 & Cos $\theta_s =$ 0.25
$P_s =$					145.04 KVA
Cos $\theta_s =$ 0.25, Corresponding to Angle $\theta_s =$	75.522	Degrees for which Sin $\theta_s =$	0.97		
$P_H =$	57.35 KVA	& PB in kW is =	48.74	& P_H in Kvar =	30.39 ∴ Cos $\theta_s =$ 0.850
Cos $\theta_s =$ 0.85, Corresponding to Angle $\theta_s =$	31.803	Degrees, for which Sin $\theta_s =$	0.53		
$P_{c\phi} =$					85.001 KW
$P_{c\phi} =$					170.83 KVAR
$P_c =$					190.81 KVA
Cos $\theta_c =$	0.4455	, where as Sin $\theta_c =$	0.895		

Voltage Regulation = 6.3 %

Result During starting of max. capacity motor, while all other loads are running, the voltage regulation at Transformer secondary terminals is approx 6.30%1.4 Selection of rated capacity
120 kVA transformer selected.

29th May2021: DG set calculations.

16 DG set
Calculations

Topic details:

Transformer and DG set calculations,types ,sizing or selections

DG SIZING CALCULATIONS		
Design Data		
Rated Voltage	415	KV
Power factor (CosØ)	0.73	Avg
Efficiency	0.85	Avg
Total operating load on DG set in kVA at 0.73 power factor	78.6	
Largest motor to start in the sequence - load in KW	15	KW
Running kVA of last motor (CosØ= 0.91)	24	KVA
Starting current ratio of motor	6	(Considering starting method as Soft starter)
Starting KVA of the largest motor (Running kVA of last motor X Starting current ratio of motor)	145	KVA
Base load of DG set in KVA (Total operating load in kVA – Running kVA of last motor)	54	KVA
A Continuous operation under load -P1		
Capacity of DG set based on continuous operation under load P1	54	KVA
B Transient Voltage dip during starting of Last motor P2		
Total momentary load in KVA (Starting KVA of the last motor+Base load of DG set in KVA)	199	KVA
Subtransient Reactance of Generator (Xd'')	7.91%	(Assumed)
Transient Reactance of Generator (Xd')	10.065%	(Assumed)
$X_d''' = (X_d'' + X_d')/2$	0.089875	
Transient Voltage Dip	15%	(Max)
Transient Voltage dip during Soft starter starting of Last motor $P2 = \text{Total momentary load in KVA} \times X_d''' \times \frac{[1 - \text{Transient Voltage}]}{(\text{Transient Voltage Dip})}$	102	KVA
C Overload capacity P3		
Capacity of DG set required considering overload capacity		
Total momentary load in KVA	199	KVA
overcurrent capacity of DG (K) (Ref: IS/IEC 60034-1, Clause 9.3.2)	150%	
Capacity of DG set required considering overload capacity (P3) = $\frac{\text{Total momentary load in KVA}}{\text{overcurrent capacity of DG (K)}}$	133	KVA
Considering the last value amongst P1, P2 and P3		
Continuous operation under load -P1	54	KVA
Transient Voltage dip during Soft starter starting of Last motor P2	102	KVA
Overload capacity P3	133	KVA
Considering the last value amongst P1, P2 and P3	133	KVA

17	Calculation of Earthing and Lighting protection calculations	Earthing calculations	Lighting protection calculation
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Calculation of Earthing and Lighting protection calculations

Location	1	Mangalore
Building		Concrete, Industrial
Type of Building		Flat Roofs (a)
Building Length (L)	14	
Building breadth (W)	4	
Building Height (H)	5	
Risk Factor Calculation		
1 Collection Area (A_s)		
A _s	=	(L*W) + (2*L*H) + (2*W*H) + (3.14*H*H) 314.5
2 Probability of Being Struck (P)		
P	=	A _s * N _a * 10 ⁻⁶ 0.0005976
3 Overall weighing factor		
a) Use of structure (A)	=	1.2
b) Type of construction (B)	=	0.4
c) Contents or consequential effects (C)	=	0.8
d) Degree of isolation (D)	=	1.0
e) Type of country (E)	=	0.3
Wo - Overall weighing factor	=	A * B * C * D * E 0.115
4 Overall Risk Factor		
Po	=	P * Wo 6.884E-05
Pa	=	10 ⁻⁵
As per clause no. 3.7 of BS- 6651, suggested acceptable risk factor (Po) has been taken as 10 ⁻⁵		
Since Po > Pa lightning protection required.		
5 Air Terminations		
Perimeter of the building	=	2(L+W) 36 Mts.
6 Down Conductors		
Perimeter of building	=	36 Mts.
No. of down conductors based on perimeter	=	2 Nos.
Hence 2 nos. of Down conductors have been selected.		
Size of Down conductor	=	20 X 2.5 mm Galvanized Steel Strip
(As per BS6651, lightning currents have very short duration, therefore thermal factors are of little consequence in deciding the cross-section of the conductor. The minimum size of Down conductor is 20 X 2.5 mm Galvanized Steel Strip)		

	1	
Maximum line-to-ground fault in kA for 1 sec	12	
Earthing material (Earth rod & earth strip)	GI	
Depth of earth flat burial in meter	0.5	
Average depth / length of Earth rod in meters	4.0	
Soil resistivity Ω-meter	15	
Ambient temperature in deg C	50	
Plot dimensions (earth grid) L x B in meters	70	130
Number of earth rods in nos.	6	
 Earth electrode sizing:		
Ac - Required conductor cross section in sq.mm		
$I_{lg} = A_c \times \sqrt{\left[\frac{TCAP \times 10^{-4}}{t_c \times \alpha_r \times \rho_r} \right] \ln \left[\frac{K_o + T_m}{K_o + T_a} \right]}$		
αr - Thermal co-efficient of resistivity, at 20 oC	0.0032	
ρr - Resistivity of ground conductor at 20 oC	20.10	
Ta - Ambient Temperature is °C	50	
I _{L-4} - RMS fault current in kA = 50 KA	11	
t _c - Short circuit current duration sec	1	
Thermal capacity factor, TCAP J/(cm ³ .oC)	3.93	
Tm - Maximum allowable temperature for copper conductor, in oC	419	
K0 - Factor at oC	293	
The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:		
	11 = Ac *	0.123
Ac - Required conductor cross section in sq.mm		90
Earth rod dia in mm		11
Earth rod dia (including 25% corrosion allowance) in mm		13

5 th june 2021: Cable sizing and cable tray sizing calculations.

18 Cable sizing and cable tray sizing calculations

Cable sizing calculations

Cable tray calculation

Topic details: Cable sizing and cable tray sizing calculations for LV cables and MV/HV cables.

S.NO.	Description	Equipment No.	Description	Consumed Load KW	Load Rating KW	Voltage (V)	No. of ph	Full Load Current (A)	Motor Starting Current (A)	Load P.F. Running	SIN Φ Running	Motor P.F. Staring	SIN Φ Staring	Type	No. of Runs	No. of Cores	Size (mm ²)	Current Rating (A)	Derating factor k1	Derating factor k2	Derating factor k3	Derating factor k4	Overall Derating factor k
3	LV MCC	PU235	Silica filter feed pump	10.94	5.00	415	3	18.9	113.11	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882
4	LV MCC	PU234-A	Absoberent/Miscel oil pump (V)	3.5	3.70	415	3	5.5	32.87	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882
5	LV MCC	PU234-B	Absoberent/Miscel oil pump (S)	2.70	2.80	415	3	4.7	28.17	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882
6	LV MCC	PU235	Feed Pump (Dispersor)	10.94	5.00	415	3	19.0	114.15	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882
7	LV MCC	MCE25	MISER (V)	10.02	5.00	415	3	19.2	115.09	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882
8	LV MCC	MCE25	MISER (S)	10.02	5.00	415	3	19.2	115.09	0.8	0.6	0.8	0.5	2	1	4.0	10	66	0.98	0.9	1	1	0.882
9	LV MCC	BW230	Blower	4.74	5.00	415	3	8.2	49.46	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882
10	LV MCC	Rotary valve	TY 2202B (I)	0.43	0.50	415	3	0.8	4.80	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882
11	LV MCC	SC234	Sewer conveyor (I)	1.07	1.50	415	3	1.9	11.16	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882
12	LV MCC	AG 2324A	Chitic acid tank lighter (V)	0.75	1.00	415	3	1.4	8.24	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882
13	LV MCC	AG 2324B	Chitic acid tank lighter (S)	0.75	1.00	415	3	1.4	8.24	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882
14	LV MCC	AG 2325	Chitic acid reaction vessel lighter	2.30	3.00	415	3	5.0	30.26	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882
15	LV MCC	AG 2326	Lys oil reaction vessel lighter	1.05	1.50	415	3	1.8	10.96	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882
16	LV MCC	AG 2320	Lys oil reaction vessel lighter	1.05	1.50	415	3	1.8	10.96	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882
17	LV MCC	AG 2324	Soap Adsorbent Tank lighter	1.04	2.20	415	3	3.2	19.20	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882
18																							
19																							

Cable Tray calculations:

LT CABLES									
CABLE TRAY: FROM									
Sr. No.	Cable Route (From-To)	LT-4		TO		LT-5		Self Weight of Cable (Kg/Mt)	Total Weight of Cable (Kg/Mt)
		Type & Cable Size	Size of Cable (mm ²)	No. of Cable	Overall Diameter of each Cable (mm)	Sum of Cable OD (mm)			
1	LV MCC	4	6	1	18	18	3.95	0.7	
2	PU2315- VFD	4	6	1	18	18	0.37	0.7	
3	PU2315- VFD	5	1.5	1	15	15	3.95	0.4	
4	LV MCC	4	2.5	1	16	16	0.37	0.5	
5	LV MCC	5	1.5	1	15	15	3.95	0.4	
6	LV MCC	4	2.5	1	16	16	0.37	0.5	
7	PU 2314 -B- VFD	4	2.5	1	16	16	0.37	0.5	
8	PU 2314 -B- VFD	5	1.5	1	15	15	0.9	0.4	
9	LV MCC	4	6	1	18	18	2.9	0.7	
10	PU2305- VFD	4	6	1	18	18	1.2	0.7	
11	PU2305- VFD	5	1.5	1	15	15	1.2	0.4	
12	LV MCC	4	6	1	18	18	1.2	0.7	
13	LV MCC	5	1.5	1	15	15	1.45	0.4	
14	LV MCC	4	10	1	18	18	2	0.9	
15	LV MCC	5	1.5	1	15	15	2.4	0.4	
16	LV MCC	4	6	1	18	18	2.4	0.7	
17	BW2313- VFD	4	6	1	18	18	0.85	0.7	
18	BW2313- VFD	5	1.5	1	15	15	0.85	0.4	
19	LV MCC	4	6	1	18	18	0.85	0.7	
20	LV MCC	5	1.5	1	15	15	1	0.4	
21	LV MCC	4	6	1	18	18	0.85	0.7	
Total				21		348	33.91	11.9	
Calculation									
Maximum Cable Diameter:				18	mm	Result			
Consider Spare Capacity of Cable Tray:				30%		Selected Cable Tray width:			
Distance between each Cable:				0	mm	Selected Cable Tray Depth:			
Calculated Width of Cable Tray:				452	mm	Selected Cable Tray Weight:			
Calculated Area of Cable Tray:				8143	Sq.mm	Selected Cable Tray Size:			
No of Layer of Cables in Cable Tray:				2		Required Cable Tray Size:			
Selected No of Cable Tray:				1	Nos.	Required Nos of Cable Tray:			
Selected Cable Tray Width:				300	mm	Required Cable Tray Weight:			
Selected Cable Tray Depth:				150	mm	Type of Cable Tray:			
Selected Cable Tray Weight Capacity:				150	Kg/Meter	Cable Tray Width Area Remar			
Type of Cable Tray:				Ladder		Cable Tray Area Remaining:			
Total Area of Cable Tray:				15000	Sq.mm				

Conclusion:

We have been taught many aspects of engineering activities during the EPC stages for all electrical and related other disciplines also.

Feedback:

Smart Bridge

They conduct summer internships, work shops, debates, hackthons, technical sessions.

Method of conducting program

Online virtual program with presentation slides and explanation on the topic and practical usage of topic and with some examples.

Program highlights

It is for the detailed design of any industrial sectors.

Material

The material was good .

Benefits

It has been given the opportunity to learn and interact with industry experienced engineering specialist to learn the Electrical detailed design engineering for various industrial sectors.

ASSIGNMENT - 1

ELECTRICAL LOAD CALCULATIONS LV MCC

[illegible]

ASSIGNMENT - 2
Calculation for Transformer Capacity

Example of calculation for Transformer Capacity
Calculation for consumed load

Consumed loads used for this example are as follows :

	kW	kVar	kVA	
a. Continuous load	56.86	53.2	77.89	--- (i)
b. Intermittent load / Diversity Factor	1.8	1.7	2.47	--- (ii)
c. Stand-by load required as consumed load	17.08	16.0	23.40	--- (iii)
Max. Consumed load = ((i) + 30% (ii) + 10% (iii)) =	59.1	55.3	80.97	
Future expansion load (20% capacity)	11.8	11.1	16.19	
Total Load =	70.9	66.4	97.16	

Calculation for 3.3kV / 0.433 kV transformer capacity

Max. Consumed load	=	81.0 kVA
Spare capacity	=	16.2 kVA
Required capacity	=	97.2 kVA
Transformer rated capacity	=	120 kVA

1.3 Voltage regulation check

During starting or reacceleration of max. capacity motor (3400 kW) , while all the other loads running , the voltage regulation is as follows :

$$P_T = 120 \text{ KVA} \quad (\%Z) = 4 \quad \& \text{ Ratio X/R} = 3.3$$

$$\text{Hence, } \%R = 1.176 \%$$

$$\%X = 3.82 \%$$

$$P_M = 15 \text{ KW having (K = 6 \& C = 1 \& Cos } \theta = 0.73 \& \text{ Eff.h} = 0.85 \& \text{ Cos } \theta_s = 0.25$$

$$P_s = 145.044 \text{ KVA}$$

$$\text{Cos } \theta_s = 0.25, \text{Corresponding to Angle } \theta_s = 75.5225 \text{ Degrees for which Sin } \theta_s = 0.97$$

$$P_B = 57.35 \text{ KVA} \quad \& \text{ PB in KW is } 48.74 \quad \& \quad P_B \text{ in Kvar} = 30.39 \quad \backslash \text{ Cos } \theta_B = 0.850$$

$$\text{Cos } \theta_B = 0.85, \text{Corresponding to Angle } \theta_s = 31.8026 \text{ Degrees, for which Sin } \theta_s = 0.53$$

$$P_{CP} = 85.0011 \text{ KW}$$

$$P_{CQ} = 170.829 \text{ KVAR}$$

$$P_C = 190.808 \text{ KVA}$$

$$\text{Cos } \theta_c = 0.44548, \text{ where as Sin } \theta_c = 0.895$$

$$\text{Voltage Regulation } e = 6.3 \%$$

Result: During starting of max. capacity motor, while all other loads are running , the voltage regulation at Transformer secondary terminals is approx 6.30%

1.4 Selection of rated capacity

120 kVA transformer selected.

Assignment - 3

DG SIZING CALCULATIONS		
Design Data		
Rated Voltage	415	KV
Power factor (Cos ϕ)	0.73	Avg
Efficiency	0.85	Avg
Total operating load on DG set in kVA at 0.73 power factor	78.6	
Largest motor to start in the sequence - load in KW	15	KW
Running kVA of last motor (Cos ϕ = 0.91)	24	KVA
Starting current ratio of motor	6	(Considering starting method as Soft starter)
Starting KVA of the largest motor (Running kVA of last motor X Starting current ratio of motor)	145	KVA
Base load of DG set in KVA (Total operating load in kVA – Running kVA of last motor)	54	KVA
A Continuous operation under load -P1		
Capacity of DG set based on continuous operation under load P1	54	KVA
B Transient Voltage dip during starting of Last motor P2		
Total momentary load in KVA (Starting KVA of the last motor+Base load of DG set in KVA)	199	KVA
Subtransient Reactance of Generator (Xd'')	7.91%	(Assumed)
Transient Reactance of Generator (Xd')	10.065%	(Assumed)
$X_d''' = (X_d'' + X_d') / 2$	0.089875	
Transient Voltage Dip	15%	(Max)
Transient Voltage dip during Soft starter starting of Last motor $P2 = \text{Total momentary load in KVA} \times X_d''' \times \frac{(1 - \text{Transient Voltage Dip})}{(\text{Transient Voltage Dip})}$	102	KVA
C Overload capacity P3		
Capacity of DG set required considering overload capacity		
Total momentary load in KVA	199	KVA
overcurrent capacity of DG (K) (Ref: IS/IEC 60034-1, Clause 9.3.2)	150%	
Capacity of DG set required considering overload capacity (P3) = $\frac{\text{Total momentary load in KVA}}{\text{overcurrent capacity of DG (K)}}$	133	KVA
Considering the last value amongst P1, P2 and P3		
Continuous operation under load -P1	54	KVA
Transient Voltage dip during Soft starter starting of Last motor P2	102	KVA
Overload capacity P3	133	KVA
Considering the last value amongst P1, P2 and P3	133	KVA
Hence, Existing Generator 133 KVA is adequate to cater the loads as per re-scheduled loads		
NOTE:VOLTAGE DIP CONSIDERED - 15%		

Assignment - 4

Lightning Calculations

	1
Location	Mangalore
Building	Concrete, Industrial
Type of Building	Flat Roofs (a)
Building Length (L)	14
Building breadth (W)	4
Building Height (H)	5

Risk Factor Calculation

1 Collection Area (A_c)

$$A_c = (L*W) + (2*L*H) + (2*W*H) + (3.14*H*H) = 314.5$$

2 Probability of Being Struck (P)

$$P = A_c * N_g * 10^{-6} = 0.00059755$$

3 Overall weighing factor

a) Use of structure (A)	=	1.2
b) Type of construction (B)	=	0.4
c) Contents or consequential effects (C)	=	0.8
d) Degree of isolation (D)	=	1.0
e) Type of country (E)	=	0.3
Wo - Overall weighing factor	=	$A * B * C * D * E$
	=	0.115

4 Overall Risk Factor

Po	=	$P * Wo$
Po	=	6.88378E-05
Pa	=	10^{-5}

As per clause no. 9.7 of BS- 6651, suggested acceptable risk factor (Po) has been taken as 10^{-5}
 Since Po > Pa lightning protection required.

5 Air Terminations

Perimeter of the building	=	$2(L+W)$	
	=	36	Mts.

6 Down Conductors

Perimeter of building	=	36	Mts.
No. of down conductors based on perimeter	=	2	Nos.

Hence 2 nos. of Down conductors have been selected.

Size of Down conductor = 20 X 2.5 mm Galvanized Steel Strip
 (As per BS6651, lightning currents have very short duration, therefore thermal factors are of little consequence in deciding the cross-section of the conductor. The minimum size of Down conductors - 20mm X 2.5 mm Galvanized Steel Strip)

S.NO.	Description	Equipment No.	Description	Consumed Load KW	Load Rating KW	Voltage (V)	No. of ph	Full Load Current (A)	Motor Starting Current (A)	Load P.F. Running	SIN Φ Running	Motor P.F Staring	SIN Φ Staring	Type	No. of Runs	No. of Cores	Size (mm2)	Current Rating (A)	Derating factor k1	Derating factor k2	Derating factor k3	Derating factor k4	Overall Derating factor k	Derated Current (A)	Cable Length (M)	Cable Resistance (Ohms/kM)	Cable Reactance (Ohms/kM)	Voltage drop (Running) (V)	Voltage drop (Running) (%)	Voltage drop (Starting) (V)	Voltage drop (starting) (%)	Cable size result	OD of Cable (mm)	Gland size
3	LV MCC	PU2315	Silica filter feed pump	10.84	15.00	415	3	18.9	113.11	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	95	3.9400	0.0902	9.94	2.40	59.50	14.34	OK	18	20
4	LV MCC	PU 2314-A	Absorbent/Neutral oil pump (W)	3.15	3.34	415	3	5.5	32.87	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	95	9.4800	0.1007	6.89	1.66	41.29	9.95	OK	16	20s
5	LV MCC	PU 2314 -B	Absorbent/Neutral oil pump (S)	2.70	3.00	415	3	4.7	28.17	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	60	9.4800	0.1007	3.73	0.90	22.35	5.39	OK	16	20s
6	LV MCC	PU2305	Feed Pump (Separator)	10.94	11.00	415	3	19.0	114.15	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	85	3.9400	0.0902	8.98	2.16	53.73	12.95	OK	18	20s
7	LV MCC	MX2305	MIXER (W)	11.03	15.00	415	3	19.2	115.09	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	75	3.9400	0.0902	7.99	1.92	47.80	11.52	OK	18	20s
8	LV MCC	MX 2308	MIXER (S)	11.03	15.00	415	3	19.2	115.09	0.8	0.6	0.8	0.5	2	1	4.0	10	66	0.98	0.9	1	1	0.882	58.2	105	2.3400	0.0852	6.71	1.62	40.07	9.66	OK	18	20s
9	LV MCC	BW 2313	Blower	4.74	5.54	415	3	8.2	49.46	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	100	3.9400	0.0902	4.58	1.10	27.39	6.60	OK	18	20s
10	LV MCC	Rotary valve	TK 2313B (I)	0.46	0.30	415	3	0.8	4.80	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	100	3.9400	0.0902	0.44	0.11	2.66	0.64	OK	18	20s
11	LV MCC	SC2314	Screw conveyor (I)	1.07	1.00	415	3	1.9	11.16	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	75	3.9400	0.0902	0.77	0.19	4.64	1.12	OK	18	20
12	LV MCC	AG 2324A	Citric acid tan agitator (W)	0.79	1.10	415	3	1.4	8.24	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	110	9.4800	0.1007	2.00	0.48	11.99	2.89	OK	16	20s
13	LV MCC	AG 2324B	Citric acid tank agitator (S)	0.79	1.10	415	3	1.4	8.24	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	75	3.9400	0.0902	0.57	0.14	3.42	0.82	OK	18	20
14	LV MCC	AG 2305	Citric oil reaction vessel agitator	2.80	3.34	415	3	5.0	30.26	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	105	3.9400	0.0902	2.94	0.71	17.59	4.24	OK	18	20
15	LV MCC	AG 2309	Lye oil reaction vessel agitator		1.30	415	3	1.8	10.96	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	85	9.4800	0.1007	2.06	0.50	12.31	2.97	OK	16	32
16	LV MCC	AG 2310	Lye oil reaction vessel agitator	1.05	1.30	415	3	1.8	10.96	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	95	9.4800	0.1007	2.30	0.55	13.76	3.32	OK	16	20s
17	LV MCC	AG 2314	Soap Adsorbant Tank Agitator	1.84	2.34	415	3	3.2	19.20	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	65	9.4800	0.1007	2.75	0.66	16.50	3.98	OK	16	20s
18																																		
19																																		
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27																																		

Basis:

- Overall derating factor $k = k_1 \times k_2 \times k_3 \times k_4$

K1=Rating factor for variation in air/ground temperature

K2=Rating factor for depth of laying

K3=Rating factor for spacing between two circuits

K4=Rating factor for variation in thermal resistivity of the soil
- LT Motors : Running Voltage Drop = 3%, Starting Voltage Drop = 15%
- Cable type:

TYPE 1: Al Conductor, XLPE Insulated, Armoured, PVC outer sheathed

TYPE 2: Cu Conductor, XLPE Insulated, Armoured, PVC outer sheathed
- Effect of Frequency Variation $\pm 5\%$
- Combined Effect of Voltage & Frequency Variation $\pm 10\%$

Assignment -6,
CABLE TRAY

LT CABLES

CABLE TRAY: FROM									
LT-4									
TO									
LT-5									
Sr. No.	Cable Route (From-To)	Type & Cable Size	Size of Cable (mm ²)	No. of Cable	Overall Diameter of each Cable (mm)	Sum of Cable OD (mm)	Self Weight of Cable (Kg/Mt)	Total Weight of Cable (Kg/Mt)	Remarks
1	LV MCC	4	6	1	18	18	3.95	0.7	
2	PU2315- VFD	4	6	1	18	18	0.37	0.7	
3	PU2315- VFD	5	1.5	1	15	15	3.95	0.4	
4	LV MCC	4	2.5	1	16	16	0.37	0.5	
5	LV MCC	5	1.5	1	15	15	3.95	0.4	
6	LV MCC	4	2.5	1	16	16	0.37	0.5	
7	PU 2314 -B- VFD	4	2.5	1	16	16	0.9	0.5	
8	PU 2314 -B- VFD	5	1.5	1	15	15	0.9	0.4	
9	LV MCC	4	6	1	18	18	2.9	0.7	
10	PU2305- VFD	4	6	1	18	18	1.2	0.7	
11	PU2305- VFD	5	1.5	1	15	15	1.2	0.4	
12	LV MCC	4	6	1	18	18	1.2	0.7	
13	LV MCC	5	1.5	1	15	15	1.45	0.4	
14	LV MCC	4	10	1	18	18	2	0.9	
15	LV MCC	5	1.5	1	15	15	2.4	0.4	
16	LV MCC	4	6	1	18	18	2.4	0.7	
17	BW2313- VFD	4	6	1	18	18	0.85	0.7	
18	BW2313- VFD	5	1.5	1	15	15	0.85	0.4	
19	LV MCC	4	6	1	18	18	0.85	0.7	
20	LV MCC	5	1.5	1	15	15	1	0.4	
21	LV MCC	4	6	1	18	18	0.85	0.7	
Total				21		348	33.91	11.9	

Calculation

Maximum Cable Diameter:	18	mm
Consider Spare Capacity of Cable Tray:	30%	
Distance between each Cable:	0	mm
Calculated Width of Cable Tray:	452	mm
Calculated Area of Cable Tray:	8143	Sq.mm
No of Layer of Cables in Cable Tray:	2	
Selected No of Cable Tray:	1	Nos.
Selected Cable Tray Width:	300	mm
Selected Cable Tray Depth:	50	mm
Selected Cable Tray Weight Capacity:	150	Kg/Meter
Type of Cable Tray:	Ladder	
Total Area of Cable Tray:	15000	Sq.mm

Result

Selected Cable Tray width:	O.K	
Selected Cable Tray Depth:	O.K	
Selectrd Cable Tray Weight:	O.K	Including Spare Capacity
Selected Cable Tray Size:	O.K	Including Spare Capacity
Required Cable Tray Size:	300 x 50	mm
Required Nos of Cable Tray:	1	No
Required Cable Tray Weight:	150.00	Kg/Meter/Tray
Type of Cable Tray:	Ladder	
Cable Tray Width Area Remaning	25%	
Cable Tray Area Remaning:	46%	

Assignment - 7

Earthing calculations inputs

Maximum line-to-ground fault in kA for 1 sec	12
Earthing material (Earth rod & earth strip)	GI
Depth of earth flat burial in meter	0.5
Average depth / length of Earth rod in meters	4.0
Soil resistivity Ω-meter	15
Ambient temperature in deg C	50
Plot dimensions (earth grid) L x B in meters	70 130
Number of earth rods in nos.	6

$$I_{lg} = A_c \times \sqrt{\left[\frac{TCAP \times 10^{-4}}{t_c \times \alpha_r \times \rho_r} \right] \times \ln \left[\frac{K_0 + T_m}{K_0 + T_a} \right]}$$

pr - Resistivity of ground conductor at 20 oC	0.0032
Ta - Ambient Temperature is °C	20.10
I _{lg} - RMS fault current in kA = 50 KA	50
tc - Short circuit current duration sec	11
Thermal capacity factor, TCAP J/(cm3.oC)	1
Tm - Maximum allowable temperature for copper conductor, in oC	3.93
K0 - Factor at oC	419
The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:	293
11 = Ac *	0.123
Earth rod dia in mm	90
Earth rod dia (including 25% corrosion allowance) in mm	11
	13

IEEE
Std 80-2000

IEEE GUIDE FOR SAFETY

Table 1—Material constants

Description	Material conductivity (%)	α _r factor at 20 °C (1/°C)	K ₀ at 0 °C (°C)	Fusing* temperature T _m (°C)	ρ _r 20 °C (μΩ-cm)	TCAP thermal capacity [J/(cm ³ ·°C)]
Copper, annealed soft-drawn	100.0	0.00393	234	1083	1.72	3.42
Copper, commercial hard-drawn	97.0	0.00381	242	1084	1.78	3.42
Copper-clad steel wire	40.0	0.00378	245	1084	4.40	3.85
Copper-clad steel wire	30.0	0.00378	245	1084	5.86	3.85
Copper-clad steel rod ^b	20.0	0.00378	245	1084	8.62	3.85
Aluminum, EC grade	61.0	0.00403	228	657	2.86	2.56
Aluminum, 5053 alloy	53.5	0.00353	263	652	3.22	2.60
Aluminum, 6201 alloy	52.5	0.00347	268	654	3.28	2.60
Aluminum-clad steel wire	20.3	0.00360	258	657	8.48	3.58
Steel, 1020	10.8	0.00160	605	1510	15.90	3.28
Stainless-clad steel rod ^c	9.8	0.00160	605	1400	17.50	4.44
Zinc-coated steel rod	8.6	0.00320	293	419	20.10	3.93
Stainless steel, 304	2.4	0.00130	749	1400	72.00	4.03

*From ASTM standards.

^bCopper-clad steel rods based on 0.254 mm (0.010 in) copper thickness.

^cStainless-clad steel rod based on 0.508 mm (0.020 in) No. 304 stainless steel thickness over No. 1020 steel core.