

DM systems are subjected to 2 types of quantizing error -

1) slope - overload distortion.

2) Granular noise.

Let  $q(nT_s)$  denote the quantizing error.

from DPCM wkt i/p to prediction filter is

$$u(nT_s) = x(nT_s) + q(nT_s) \quad \text{--- (1)}$$

from DM wkt  $\Rightarrow$

$$e(nT_s) = x(nT_s) - u(nT_s - T_s) \quad \text{--- (2)}$$

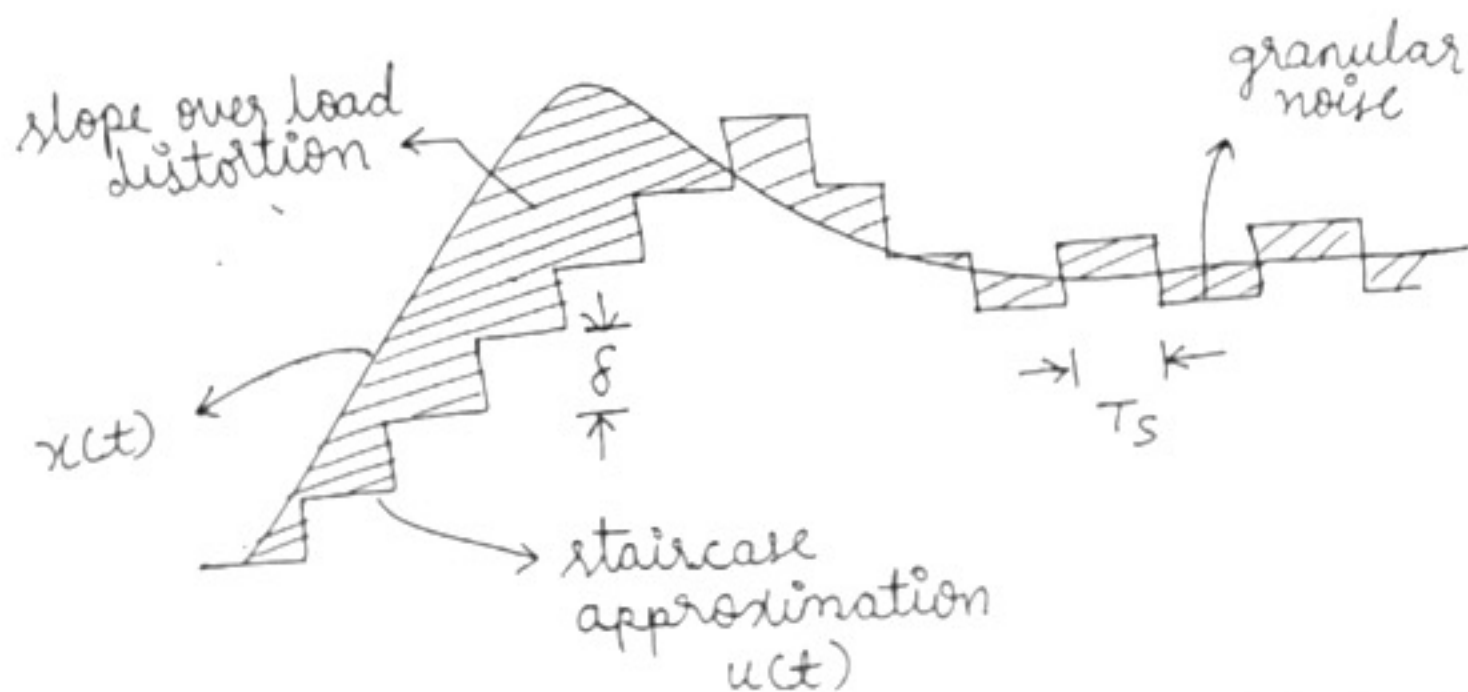
Put (1) in (2)  $\Rightarrow$

$$e(nT_s) = x(nT_s) - x(nT_s - T_s) - q(nT_s - T_s) \quad \text{--- (3)}$$

Thus except for quantization error  $q(nT_s - T_s)$ , the quantizer i/p is a first backward difference of i/p signal, which may be viewed as a digital approximation to the derivative of the i/p signal.

If we consider the maximum slope of original i/p waveform  $x(t)$ , it is clear that in order for sequence of samples  $u(nT_s)$  to increase as fast as the input sequence of samples  $x(nT_s)$  in a region of maximum slope of  $x(t)$ , we require the condition below to be satisfied  $\Rightarrow$

$$\frac{\delta}{T_s} \geq \max \left| \frac{dx(t)}{dt} \right| \quad \text{--- (4)}$$



The staircase approximation  $u(t)$  falls behind  $x(t)$  because the step size  $\delta$  is too small to trace the i/p signal  $x(t)$ . This condition is called slope-overload distortion - quantisation error.

"If the step size  $\delta$  is too large relative to the local slope characteristics of i/p waveform  $x(t)$ , it causes the staircase approximation  $u(t)$  to hunt around a relatively flat segment of the i/p waveform & this phenomenon is called as granular noise".

Thus we require a large step size to accommodate a wide dynamic range, whereas a small step size is required for the accurate representation of relatively low-level signals.

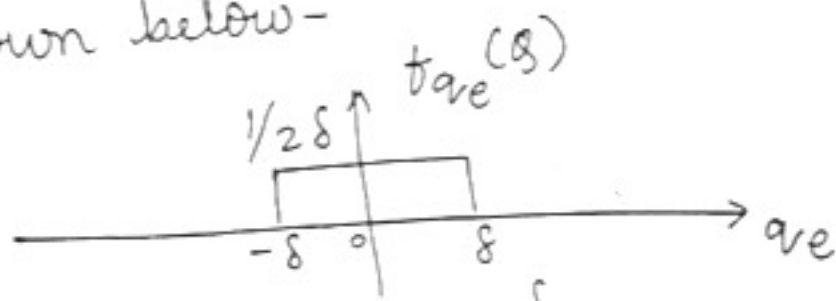
$\therefore$  choice of optimum step size is very important to minimize the quantizing error in a linear delta modulator which is comprised b/w slope overload distortion & granular noise.

If slope overload distortion is not there, then max<sup>m</sup> quantisation error is  $\pm \delta$ .

$\therefore$  let this be uniformly distributed with variance  $\frac{\delta^2}{3}$ . At the receiver, a LPF is designed with a bandwidth ' $\omega$ ' Hz, ( $\omega_m \leq \omega$ )

$$\therefore (\text{Avg o/p noise power}) = \frac{\omega}{\omega_s} \times \frac{\delta^2}{3}$$

In delta modulation (DM) the quantisation error varies between  $[-\delta \text{ \& } \delta]$  & its pdf is as shown below-



$$\text{variance } \sigma_{q_e}^2 = \int_{-\delta}^{\delta} q_e^2 f_{q_e}(q) dq_e$$

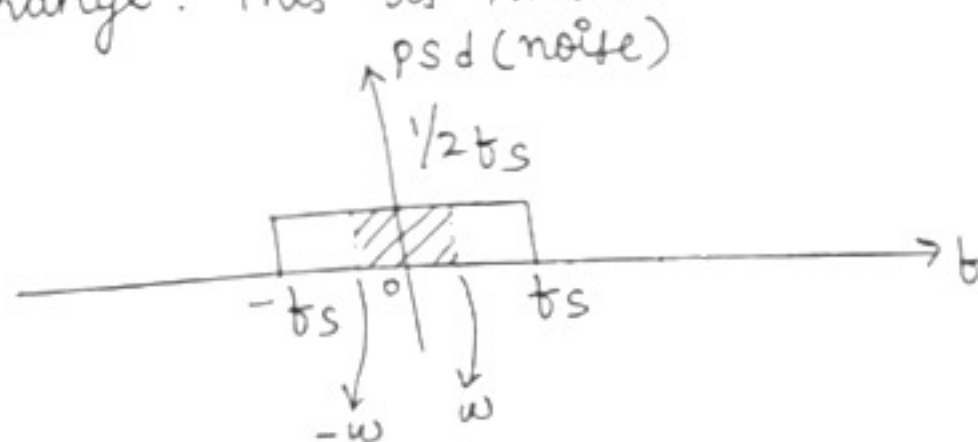
$$\sigma_{q_e}^2 = \frac{1}{2\delta} \left[ \frac{q_e^3}{3} \right]_{-\delta}^{\delta}$$

$$\sigma_{q_e}^2 = \frac{1}{2\delta} \left[ \frac{\delta^3}{3} - \left( \frac{-\delta^3}{3} \right) \right]$$

$$\sigma_{q_e}^2 = \frac{2\delta^3}{2\delta \cdot 3}$$

$$\sigma_{q_e}^2 = \frac{\delta^2}{3}$$

This noise power is uniformly distributed over  $-b_s$  to  $b_s$  range. This is shown in below figure-



ie average o/p noise power  $= \left( \frac{w}{b_s} \right) \times \frac{\delta^2}{3}$

$$N = \frac{w \delta^2}{3 b_s}$$

$\therefore (SNR)_{\text{omax}} = \frac{\text{signal power}}{\text{noise power}}$

$$(SNR)_{\text{omax}} = \frac{\frac{\delta^2}{8 \pi^2 f_m^2 T_s^2}}{\frac{w \delta^2}{3 b_s}}$$

$$(SNR)_{\text{omax}} = \frac{\cancel{\delta^2}}{8 \pi^2 f_m^2 T_s^2} \times \frac{3 b_s}{w \cancel{\delta^2}}$$

$$(SNR)_{\text{omax}} = \frac{3}{8 w T_s^3 \pi^2 f_m^2}$$

(post-filtered)  
(o/p SNR)  $\Rightarrow$   $(SNR)_{\text{omax}} = \frac{3}{8 \pi^2 w f_m^2 T_s^3}$

At no slope overload distortion, the o/p SNR is inversely proportional to cube of sampling interval  $T_s$ .