

## ATTENUATORS:

An attenuator is a two port resistive network. It is used to reduce the signal level when used between a generator and load. Attenuators may be symmetrical (or) asymmetrical. They may provide fixed (or) variable attenuation. A fixed attenuator is also called pad. The attenuation is expressed in decibels.

$$\text{Attenuation in dB} = 20 \log_{10} \frac{P_1}{P_2}$$

Where  $P_1$  is the input power,  $P_2$  is o/p power.

for a properly matched N/W

$$P_1 = I_1^2 R_0 = \frac{V_1^2}{R_0}$$

$$P_2 = I_2^2 R_0 = \frac{V_2^2}{R_0}$$

where  $R_0$  is the characteristic resistance of the N/W

$$\text{Attenuation in dB} = 20 \log_{10} \frac{V_1}{V_2} = 20 \log_{10} \frac{I_1}{I_2}$$

Attenuation is also expressed in nepers as the natural logarithm of the voltage (or) current ratio.

$$\text{Attenuation in nepers} = \ln \frac{V_1}{V_2} = \ln \frac{I_1}{I_2} = \frac{1}{2} \ln \frac{P_1}{P_2}$$

$$\frac{V_1}{V_2} = \frac{I_1}{I_2} = N \text{ then } \frac{P_1}{P_2} = N^2$$

$$\text{Attenuation in dB} = 20 \log_{10} N$$

$$N = \text{antilog} \left( \frac{\text{dB}}{20} \right)$$

where  $N$  is the attenuation in nepers.

Relation b/w Decibel & Nepers

$$A \cdot N = \ln \frac{V_1}{V_2} \quad A \cdot D = 20 \log_{10} \frac{V_1}{V_2}$$

Changing the base of logarithm

$$A \cdot D = 20 \ln \frac{V_1}{V_2} = \frac{20}{2.303} \ln \frac{V_1}{V_2} = 8.686 \times \text{attenuation in nep}$$

$$A \cdot N = \frac{In P_1}{In P_2} = \frac{2.303}{2.303} \ln \frac{V_1}{V_2} = 0.115 \times \text{attenuation in dB}$$

## LATTICE ATTENUATOR

A lattice is a general type of symmetrical balanced and balanced N/W. Any symmetrical balanced (or) unbalanced N/W can be transformed into an equivalent lattice N/W.

The elements of a lattice attenuator can be specified in terms of characteristic impedance & propagation constant.

$$Z_0 = \sqrt{Z_{OC} Z_{SC}}$$

$$Z_{OC} = \frac{RA + RB}{2}$$

$$Z_0 = R_0 = \sqrt{\frac{RA + RB}{2} \times \frac{2RA RB}{RA + RB}} = \sqrt{RA RB}$$

Apply KVL to the loop.

$$V_1 = R_0 I_1 = RA(I_1 - I_2) + R_0(I_1 - I_2)$$

$$R_0 I_1 = RA(I_1 - I_2) + R_0 I_2$$

$$(R_0 - RA) I_1 = (RA + R_0) I_2$$

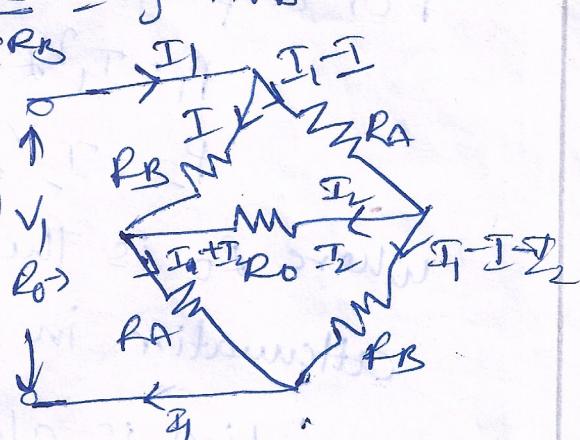
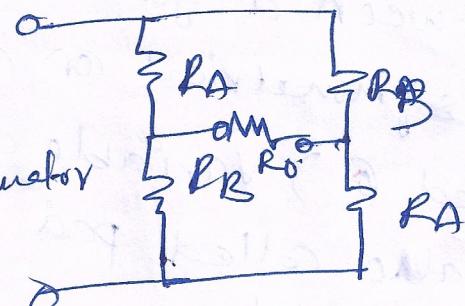
$$\frac{I_1}{I_2} = \frac{RA + R_0}{R_0 - RA} = \frac{1 + \frac{RA}{R_0}}{1 - \frac{RA}{R_0}}$$

$$N = e^{\alpha} = \frac{I_1}{I_2} = \frac{1 + RA/R_0}{1 - RA/R_0}$$

$$N \left(1 - \frac{RA}{R_0}\right) = 1 + \frac{RA}{R_0}$$

$$RA = R_0 \left(\frac{N-1}{N+1}\right)$$

$$RB = \frac{R_0 \frac{\alpha^2}{2} - \frac{\alpha^2}{2}}{RA} = R_0 \left(\frac{N+1}{N-1}\right) \frac{R_0(N-1)}{R_0(N+1)}$$



$$\begin{aligned} RA &= R_0 \tanh \frac{\alpha d}{2} \\ &= R_0 \left( \frac{e^{\alpha d/2} - e^{-\alpha d/2}}{e^{\alpha d/2} + e^{-\alpha d/2}} \right) \\ &= R_0 \left( \frac{e^\alpha - 1}{e^\alpha + 1} \right) \end{aligned}$$

$$Z_{R0} \left( \frac{N-1}{N+1} \right)$$

$$\begin{aligned} RB &= R_0 \coth \frac{\alpha d}{2} \\ &= R_0 \left( \frac{e^{\alpha d/2} + e^{-\alpha d/2}}{e^{\alpha d/2} - e^{-\alpha d/2}} \right) \\ &= R_0 \left( \frac{e^\alpha + 1}{e^\alpha - 1} \right) \\ &= R_0 \left( \frac{N+1}{N-1} \right) \end{aligned}$$

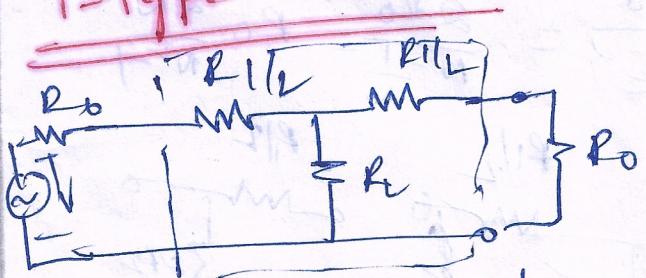
## Bisection theorem:-

A N/w said to have been bisected when the open-circuited & short-circuited i/p impedances of the two bisected networks are equivalent. Also, the square root of the product of these impedances is the characteristic impedance of the original whole N/w.

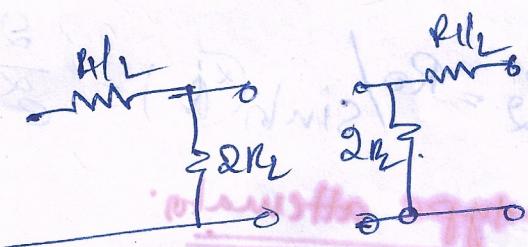
A bisection theorem states that 'any symmetrical balanced (or) unbalanced N/w can be transformed into an equivalent lattice network. The series arm of the lattice is equal to the short-circuited impedance of the bisected N/w and the diagonal arm is equal to the open-circuited impedance of the bisected N/w.

The lattice N/w  $R_A$  &  $R_B$  equations are used to find the ~~two~~ ~~other~~ equivalent lattice network for T&  $\pi$  networks using the bisection theorem.

## T-type attenuators:-



2. @ T-type attenuator



2⑥ bisection of T-type attenuator

from the bisection theorem, the series arm of the lattice N/w is equal to the short-circuited i/p resistance of the bisected network and the diagonal arm is equal to the open-circuited input resistance of the bisected network.

$$R_{OC} = R1/2 \quad R_{OC} = R1/2 + 2R2$$

$$R_A = R_{SC}, \quad R_B = R_{OC}$$

$$R_A = R_0 \left( \frac{N-1}{N} \right) \quad R_B = R_0 \left( \frac{N+1}{N-1} \right)$$

$$R_1 = 2R_A$$

$$= 2R_0 \left( \frac{N-1}{N+1} \right)$$

$$2R_2 = R_B - \frac{R_1}{2}$$

$$= R_0 \left( \frac{N+1}{N-1} \right) - \frac{2R_0 \left( \frac{N-1}{N+1} \right)}{2}$$

$$2R_2 = \frac{R_0 [(N+1)^2 - (N-1)^2]}{(N-1)(N+1)}$$

$$= R_0 \frac{[N^2 + 2N + 1 - N^2 + 1 + 2N]}{(N-1)(N+1)}$$

$$R_2 = \frac{R_0}{2} \times \frac{\frac{4N}{N^2-1}}{N^2-1} = \frac{2NR_0}{N^2-1} = \left( \frac{2N}{N^2-1} \right) R_0$$

(or) series & shunt arms of the

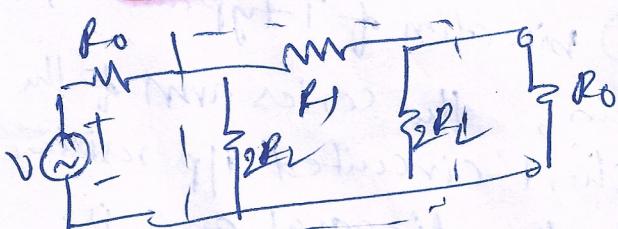
symmetrical T-Network can be given as

$$R_1 = R_0 \tanh \frac{\alpha}{2} = R_0 \left[ \frac{e^{d/2} - e^{-d/2}}{e^{d/2} + e^{-d/2}} \right] = R_0 \left( \frac{e^\alpha - 1}{e^\alpha + 1} \right)$$

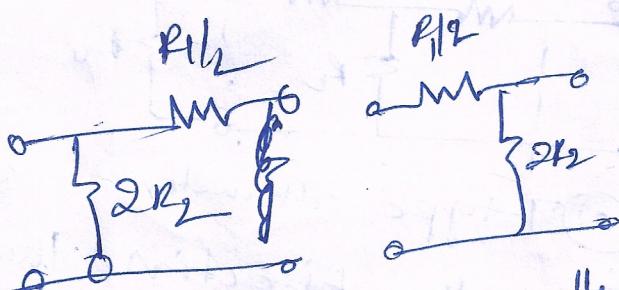
$$2R_0 = R_1 = 2R_0 \left( \frac{N-1}{N+1} \right) = R_0 \left( \frac{N-1}{N+1} \right)$$

$$R_2 = R_0 / \sinh \left( \frac{\alpha}{2} \right) = \frac{2R_0}{e^\alpha - e^{-\alpha}} = \frac{2R_0}{N-1} = R_0 \frac{2N}{N^2-1}$$

### II-type attenuator:



③ II-type attenuator



④ Bisection of II-type attenuator

From bisection theorem, the series arm of lattice N/W is equal to the short-circuited 1/p resistance of the bisected N/W & the diagonal arm is equal to the open-circuit 1/p resistance of the bisected N/W.

$$R_{SC} = \frac{R_1 R_2 \times \frac{R_1}{2}}{\frac{R_1}{2} + 2R_2} = R_{PA}$$

$$R_{SC} = \frac{R_1 R_2}{\frac{R_1}{2} + 2R_2} = R_A \Rightarrow R_A$$

$$R_{OC} = 2R_2 = R_B.$$

$$R_A = R_0 \left( \frac{N-1}{N+1} \right)$$

$$R_B = R_0 \left( \frac{N+1}{N-1} \right)$$

$$2R_2 = R_0 \left( \frac{N+1}{N-1} \right)$$

$$R_2 = \frac{R_0}{2} \left( \frac{N+1}{N-1} \right)$$

$$\frac{R_1 \times \frac{R_0}{2} \left( \frac{N+1}{N-1} \right)}{\frac{R_1}{2} + \frac{R_0}{2} \left( \frac{N+1}{N-1} \right)} = \frac{R_0 (N-1)}{N+1}$$

$$R_1 = R_0 \left( \frac{N-1}{2N} \right)$$

$$\frac{R_1 \times \frac{R_B}{2}}{\frac{R_1}{2} + \frac{R_B}{2}} = R_A$$

$$\frac{R_1 R_B / 2}{R_1 + 2R_B / 2} = R_A$$

$$R_1 R_B = R_1 R_A + 2R_A R_B$$

$$R_1 (R_B - R_A) = 2R_A R_B$$

$$R_1 = \frac{2R_A R_B}{R_B - R_A}$$

$$= 2 \times R_0 \left( \frac{N-1}{N+1} \right) \left( \frac{N-1}{N+1} \right)$$

$$= \frac{R_0 \left( \frac{N-1}{N+1} \right) \left( \frac{N-1}{N+1} \right)}{N^2 - 1}$$

$$= \frac{2R_0}{(N+1)^2 - (N-1)^2}$$

$$= 2R_0 \left( \frac{N^2 - 1}{N^2} \right)$$

$$R_1 = \frac{R_0}{2} \left( \frac{N^2 - 1}{2N} \right)$$

Series & shunt arms of T-type attenuator are given

$$R_1 = R_0 \sinh \alpha = R_0 \left( \frac{e^{\alpha} - e^{-\alpha}}{2} \right) = R_0 \frac{N-1/N}{2} = R_0 \left( \frac{N-1}{2N} \right) = R_0 \left( \frac{N-1}{2N} \right)^2$$

$$2R_2 = R_0 \coth \alpha / 2 = R_0 \left( \frac{e^{\alpha/2} + e^{-\alpha/2}}{e^{\alpha/2} - e^{-\alpha/2}} \right) = R_0 \left( \frac{e^{\alpha} + 1}{e^{\alpha} - 1} \right) = \left( \frac{N+1}{N-1} \right)$$

$$R_2 = \frac{R_0}{2} \left( \frac{N+1}{N-1} \right)$$

1. Design T-pad attenuator to give the attenuation of 60 dB and to work in a line of  $500\Omega$  impedance.

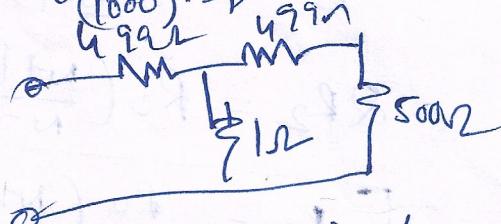
$$(N) \text{dB} = 60 \text{dB} \quad R_0 = 500\Omega$$

$$G_0 = 20 \log_{10}(N)$$

$$N = 1000$$

$$R_1 = 2R_0 \left( \frac{N-1}{N+1} \right) = 2 \times 500 \left( \frac{1000-1}{1000+1} \right) = 998\Omega$$

$$R_2 = R_0 \left( \frac{N+2}{N-1} \right) = 500 \left( \frac{2 \times 1006}{1000-1} \right) = 12\Omega$$



2. An attenuator is composed of symmetrical T-section having a series arm of  $175\Omega$  & shunt arm of  $350\Omega$ . find the characteristic impedance & attenuation in dB.

$$\frac{R_1}{2} = 175\Omega, \quad R_1 = 350\Omega, \quad R_2 = 350\Omega$$

$$R_1 = 2R_0 \left( \frac{N-1}{N+1} \right) = 350 \rightarrow ①$$

$$R_2 = R_0 \left( \frac{N+2}{N-1} \right) = 350 \rightarrow ②$$

divide eqn ② by ①.

$$\frac{2N(N^2-1)}{2(N-1)(N+1)} = 1$$

$$\frac{N}{N^2-1} = \frac{N-1}{N+1} \Rightarrow N^2(N-1)^2$$

$$\frac{N}{N^2-1} = \frac{N-1}{N+1}$$

$$N^2 - 3N + 1 = 0 \quad N = 2.618 \quad \text{or} \quad N = 0.3819.$$

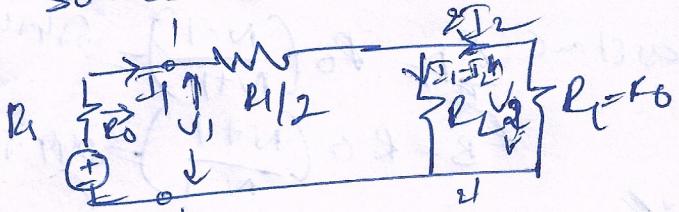
$$N \text{ in dB} = 20 \log_{10} 2.618 = 8.36 \text{dB}$$

$$① N \text{ in dB} = 20 \log_{10} 0.3819 = -8.36 \text{dB. Since attenuation cannot be negative}$$

$$N = 2.618 \text{ Nepm} = \frac{8.36 \text{ dB}}{\frac{2.618-1}{2.618+1}} \Rightarrow R_0 = 391.32\Omega$$

## L-TYPE ATTENUATOR:-

The attenuator is connected between a source with source resistance  $R_s = R_0$  and load resistance  $R_L = R_0$ .



$$V_2 = (I_1 - I_2) R_2 = I_2 R_L = I_2 R_0$$

$$I_1 R_2 = I_2 (R_2 + R_L)$$

$$\frac{I_1}{I_2} = \frac{R_2 + R_L}{R_2} = N$$

$$1 + \frac{R_L}{R_2} = N$$

$$R_2 = \frac{R_L}{N-1} = \frac{R_0}{N-1} \rightarrow ①$$

The resistance of the network as viewed from 1-D into the network is

$$R_0 = R_1 + \frac{R_2 R_0}{R_2 + R_0}$$

$$\frac{R_1}{2} = \frac{R_0^2}{R_2 + R_0}$$

Substituting the value of  $R_2$  from eqn ①.

$$\frac{R_1}{2} = \frac{R_0^2 / \frac{R_0}{N-1} + R_0}{\frac{R_0}{N-1} + R_0} = \frac{R_0^2 (N-1)}{R_0 + R_0(N-1)}$$

$$\frac{R_1}{2} = \frac{R_0^2 (N-1)}{R_0(1+N-1)} = \frac{R_0 (N-1)}{N} \rightarrow ②$$

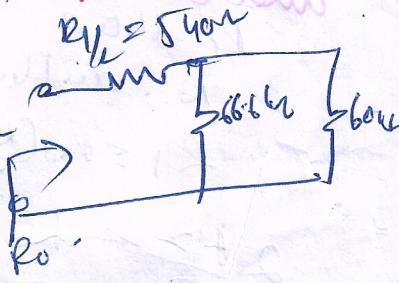
Attenuation  $N$  can be varied by varying the values of  $R_1$  &  $R_2$ .

1. Design L-type attenuator to operate into a load resistance of  $600 \Omega$  with attenuation of  $20 \text{ dB}$ .

$$N = \text{antilog } \frac{\text{dB}}{20} = \text{antilog } \frac{20}{20} = 10$$

$$\frac{R_1}{2} = R_0 \left( \frac{N-1}{N} \right) = 600 \left( \frac{10-1}{10} \right) = 540 \Omega$$

$$R_2 = R_0 / (N-1) = \frac{600}{10-1} = 66.66 \Omega$$

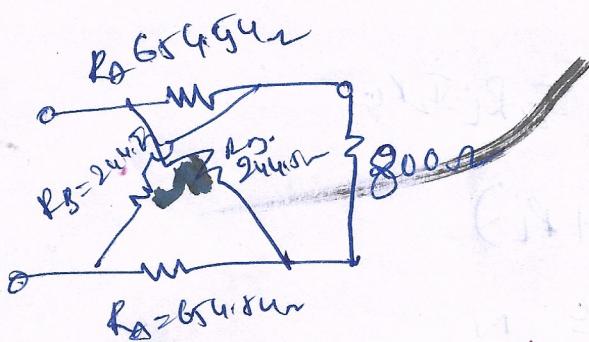


2. Design a lattice attenuator if the characteristic impedance of  $800\Omega$  and attenuation of  $20 \text{ dB}$

$$R_0 = 800\Omega \text{ & } D = 20 \text{ dB} \quad N = \text{antilog} \frac{D}{20} = \text{antilog} \frac{20}{20} = 10.$$

$$\text{series-arm resistance } R_A = R_0 \left( \frac{N-1}{N+1} \right) = 654.5\Omega$$

$$R_B = R_0 \left( \frac{N+1}{N-1} \right) = 244.5\Omega$$



3. A attenuator composed of symmetrical  $\Pi$ -section having series arm of  $275\Omega$  and each shunt arm of  $450\Omega$ . Find the characteristic impedance & attenuation in dB.

$$R_1 = 275\Omega \quad 2R_2 = 450\Omega \Rightarrow R_2 = 225\Omega$$

$$R_1 = R_0 \left( \frac{N^2 - 1}{2N} \right) = 275 \rightarrow B$$

$$R_2 = \frac{R_0}{2} \left( \frac{N+1}{N-1} \right) = 225$$

Divide eqn ② by ①

$$\frac{N^2/2N}{1/(N+1)(N-1)} = \frac{(N+1)(N-1)}{2N}$$

$$(N-1)^2 = 2N (0.1111) \quad N = 2.872 \text{ (or) } N = 0.348$$

$$N^2 - 3.222N + 1 = 0 \quad N = 2.872 \Rightarrow 9.11 \text{ dB}$$

$$\text{Nin dB} = 20 \log_{10} 2.872 = 9.16 \text{ dB. (it can't be negative)}$$

$$275 = R_0 \left( \frac{2.872^2 - 1}{2 \times 2.872} \right) \Rightarrow 212.92\Omega$$

3. Design a T-type attenuator to give attenuation of  $20 \text{ dB}$  and characteristic resistance of  $100\Omega$ .

$$R_0 = 100\Omega \quad D = 20 \text{ dB.}$$

$$N = \text{antilog} = \frac{D}{20} = 10$$

$$R_1 = R_0 \left( \frac{N^2 - 1}{2N} \right) = 49\Omega$$

$$2R_2 = R_0 \left( \frac{N+1}{N-1} \right) = 122.22\Omega$$

