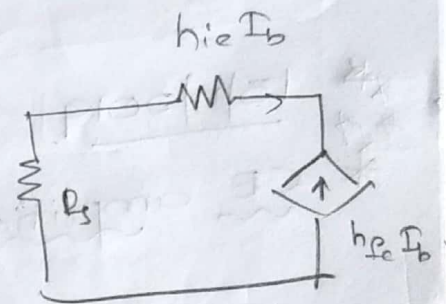


$$\begin{aligned}
 A_v &= \frac{V_o}{V_i} = \frac{+(1+h_{fe})R_L I_b}{h_{ie} I_b + (1+h_{fe})I_b R_L} \\
 &= \frac{(1+h_{fe})R_L I_b}{(h_{ie} + (1+h_{fe})R_L) I_b} \\
 &= \frac{(1+h_{fe})R_L}{h_{ie} + (1+h_{fe})R_L} \approx 1
 \end{aligned}$$

$$\begin{aligned}
 V_o &= I_b / V_o \quad / V_s = 0 \\
 &= \frac{I_b (1+h_{fe})}{(1+h_{fe})R_L I_b} \\
 &= \frac{(R_s + h_{ie}) I_b}{(1+h_{fe})R_L I_b}
 \end{aligned}$$

$$V_o = \frac{I_o}{V_o} = \frac{(1+h_{fe})I_b}{(R_s + h_{ie})I_b} = \frac{1+h_{fe}}{R_s + h_{ie}}$$



CC Approx

CC Exact

$$A_i = \frac{-h_{fc}}{1 + h_{oc}R_L}$$

$$Z_i = h_{ic} + A_i h_{rc} R_L$$

$$A_v = \frac{A_i}{Z_i} R_L$$

$$V_o = h_{oc} - \frac{h_{fc} h_{rc}}{R_s + h_{ic}}$$

$$A_i = -h_{fc} = 1 + h_{fe}$$

$$Z_i = h_{ie} + (1+h_{fe})R_L$$

$$A_v = \frac{(1+h_{fe})R_L}{h_{ie} + (1+h_{fe})R_L} \approx 1$$

$$V_o = \frac{1+h_{fe}}{R_s + h_{ie}} \leftarrow \text{bright}$$

$$V_o = \frac{1+h_{fe}}{R_s + h_{ie}} \leftarrow \text{faint}$$

CE - CC

$$h_{ic} = h_{ie}$$

$$h_{fc} = -(1 + h_{fe})$$

$$h_{oc} = h_{oe}$$

$$h_{rc} \approx 1$$

CE - CB

$$h_{ib} = \frac{h_{ie}}{1 + h_{fe}}$$

$$h_{fb} = \frac{-h_{fe}}{1 + h_{fe}}$$

$$h_{ob} = \frac{h_{oe}}{1 + h_{fe}}$$

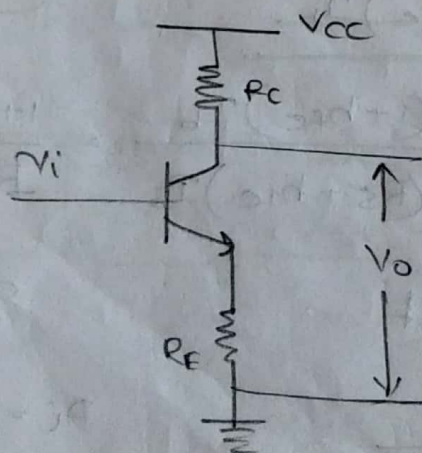
$$h_{rb} = \frac{h_{ie} h_{oe}}{1 + h_{fe}} - h_{re}$$

★  
★  
★  
★

13/11/2019

CE amplifier with  $R_E$ !

Wednesday

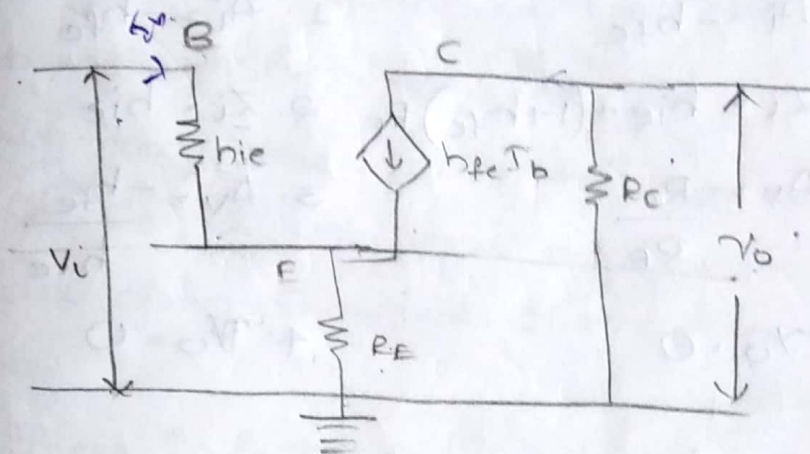


- Here  $R_E$  provides stability as w.k.t when a bypass capacitor is considered in ckt (across  $R_E$ ), the voltage gain depends on h-parameters.
- Hence, voltage gain is not stabilised.
- If CE is not present (only  $R_E$  is present) Voltage gain may be stabilized which is



independent of transistor parameters.

(c) Analysis!



$$A_i = \frac{I_o}{I_i} = \frac{-h_{fe} I_b}{I_b} = -h_{fe}$$

$$Z_i = \frac{V_i}{I_i} = \frac{h_{ie} I_b + (1+h_{fe}) I_b R_E}{I_b}$$

$$= h_{ie} + (1+h_{fe}) R_E$$

$$A_v = \frac{V_o}{V_i} = \frac{h_{fe} I_b + (1+h_{fe}) I_b R_E}{h_{ie} I_b + (1+h_{fe}) I_b R_E}$$

$$= \frac{-h_{fe} I_b \cdot R_c}{h_{ie} I_b + (1+h_{fe}) I_b R_E}$$

$$= \frac{-h_{fe} \cdot R_c}{h_{ie} + (1+h_{fe}) R_E}$$

$$= \frac{-h_{fe} \cdot R_c}{h_{ie} + (1+h_{fe}) R_E}$$

$$= \frac{-h_{fe} \cdot R_c}{h_{ie} + (1+h_{fe}) R_E}$$

Since  $h_{ie} \ll (1+h_{fe}) R_E$

Neglect  $h_{ie}$

$$= \frac{-h_{fe} R_c}{(1+h_{fe}) R_E} \approx \frac{-R_c}{R_E}$$

$$V_o = 0$$

### CE With $R_E$

1.  $A_i = -h_{fe}$
2.  $Z_i = h_{ie} + (1+h_{fe})R_E$
3.  $A_v = -\frac{R_c}{R_E}$
4.  $\gamma_o = 0$

### CE With bypass

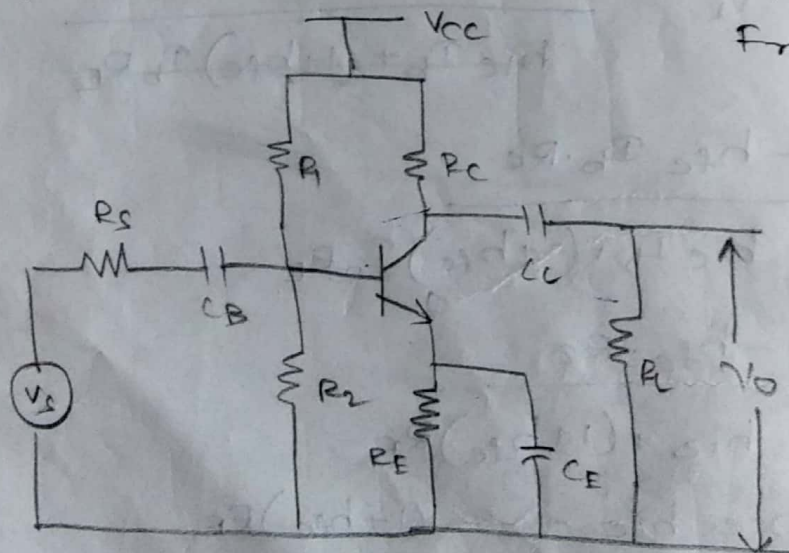
1.  $A_i = -h_{fe}$
2.  $Z_i = h_{ie}$
3.  $A_v = -\frac{h_{fe}}{h_{ie}} \times R_c$
4.  $\gamma_o = 0$

### (\*) Advantages:

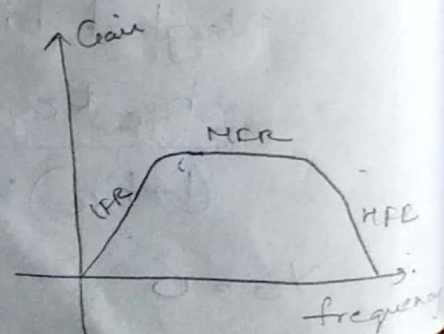
- Input impedance is high.
- Voltage gain is independent of  $h$  parameters. Hence, gain is stabilised.

### \* Low frequency response of BJT amplifiers:

15/11/2019  
Friday



	Low	Mid	High
Internal in Cap.	O.C	O.C	S.C
External Capacitors	O.C	S.C	S.C





### (i) Low frequency response:

- The range of frequencies for which gain decreases as the frequency  $\downarrow$ .
- At low frequencies, external capacitors ( $C_b, C_c, C_e$ ) & internal capacitors ( $C_{BE}, C_{BC}$ ) are open circuited. Hence, o/p voltage is zero.
- As the freq.  $\uparrow$ s, the external capacitances will allow the i/p signal. (As freq  $\uparrow$ s, reactance ( $X_c$ )  $\downarrow$ ). Hence, o/p voltage  $\uparrow$ s.
- At low frequencies, amplifier acts as high pass filter.

### (ii) Mid frequency response:

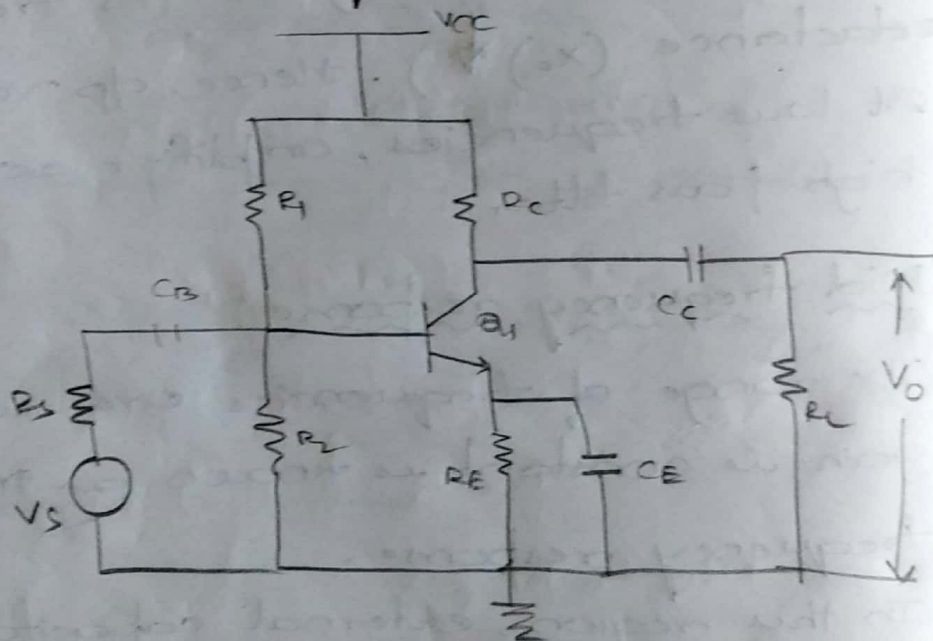
- The range of frequencies over which gain is constant is known as Mid frequency response.
- In this region, external capacitors acts like s.c & internal capacitors like o.c.
- Hence, the m/w acts like a resistor which is independent of frequency.
- Therefore, gain is constant.

### (iii) High frequency response:

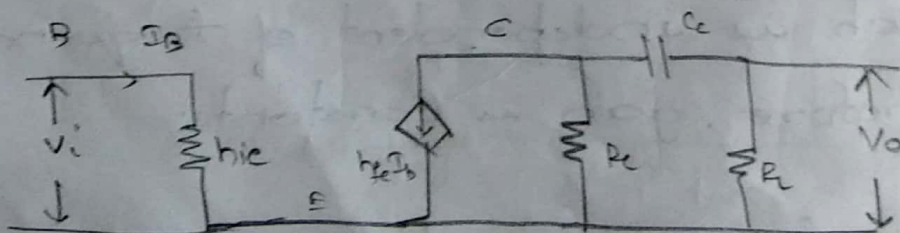
- The range of frequencies for which gain decreases as the frequency  $\uparrow$ s.

- At high frequencies, the internal & external capacitors act like a S.C.
- Due to the jn. capacitive effect, o/p voltage  $\downarrow$  as freq  $\uparrow$ s.
- In this region, amplifier acts like a low pass filter.

\* Effect of coupling / blocking capacitor at low frequency :

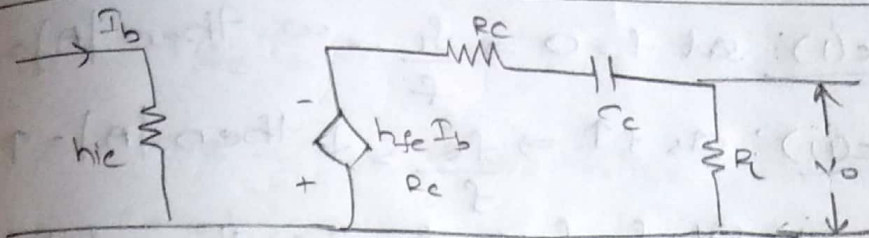


- While considering the effect of 1 capacitor other capacitors are S.C or neglected.



Converting current source to voltage source,





$$V_o = \frac{-h_{fe} I_B \cdot R_c \cdot R_L}{R_c + R_L + \frac{1}{j\omega C_c}}$$

$$V_i = +h_{ie} I_B$$

$$\frac{V_o}{V_i} = \frac{-h_{fe} R_c R_L}{\left(R_c + R_L + \frac{1}{j\omega C_c}\right) (+h_{ie})}$$

$$\frac{V_o}{V_i} = \frac{-h_{fe}}{\left(\left(\frac{1}{R_c} + \frac{1}{R_L}\right) + \frac{1}{j\omega C_c}\right) (+h_{ie})}$$

$$\frac{V_o}{V_i} = \frac{-h_{fe} (R_c \parallel R_L)}{h_{ie} \left[1 - \frac{j\omega_L}{\omega_c}\right]}$$

$$\frac{V_o}{V_i} = \frac{\frac{-h_{fe} \times R_L}{h_{ie}}}{1 - \frac{j\omega_L}{\omega}} = \frac{A_{vm}}{1 - j\frac{f_L}{f}}$$

$$\omega_L = \frac{1}{C_c (R_L + R_c)} \Rightarrow f_L = \frac{1}{2\pi C_c (R_L + R_c)}$$

$$|A| = \frac{A_{vm}}{\sqrt{1 + \left(\frac{f_L}{f}\right)^2}}$$

$$\angle A = 180^\circ + \tan^{-1}\left(\frac{f_L}{f}\right)$$

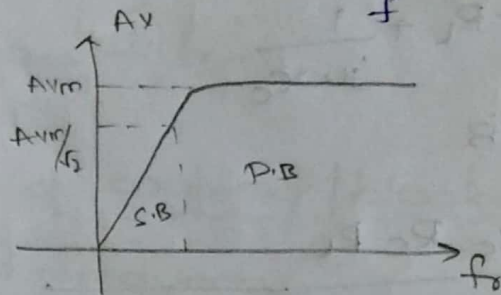
$$\text{At } f \gg f_L \Rightarrow \angle A = 225^\circ$$

→ Case (i): At  $f = 0 \Rightarrow \frac{f_L}{f} = \infty$  then  $|A| = 0$

Case (ii): As  $f \uparrow \Rightarrow \frac{f_L}{f} \downarrow$  then  $|A| \uparrow$

Case (iii): At  $f = f_L \Rightarrow \frac{f_L}{f} = 1$  then  $|A| = \frac{A_{vm}}{\sqrt{2}}$

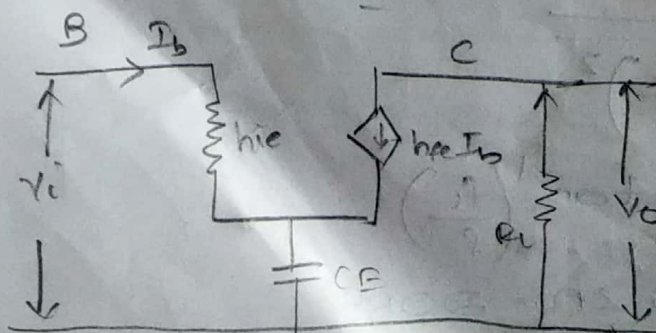
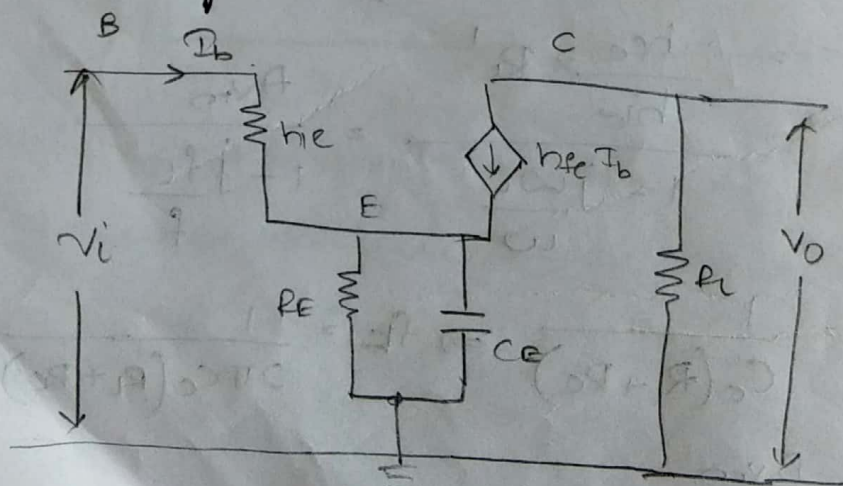
Case (iv): At  $f = \infty \Rightarrow \frac{f_L}{f} = 0$  then  $|A| = A_{vm}$



→ 11/y for  $C_B$ ,  $A = \frac{A_{vm}}{1 - j \frac{f_L}{f}}$

$$f_L = \frac{1}{2\pi C_B (R_s + R_i)}$$

\* Effect of bypass capacitor at low frequency:





$$V_o = -h_{fe} I_b R_L$$

$$V_i = h_{ie} I_b + (1+h_{fe}) I_b X_{CE}$$

$$\frac{V_o}{V_i} = \frac{-h_{fe} I_b R_L}{h_{ie} I_b + (1+h_{fe}) I_b X_{CE}}$$

$$\frac{V_o}{V_i} = \frac{-h_{fe} R_L}{h_{ie} + (1+h_{fe}) X_{CE}}$$

$$\frac{V_o}{V_i} = \frac{-h_{fe} R_L}{h_{ie} \left[ 1 + \left( \frac{1+h_{fe}}{h_{ie}} \right) X_{CE} \right]}$$

$$\frac{V_o}{V_i} = \frac{A_{vm}}{1 + \left( \frac{1+h_{fe}}{h_{ie}} \right) X_{CE}}$$

$$\Rightarrow \frac{V_o}{V_i} = \frac{A_{vm}}{1 + \frac{1+h_{fe}}{h_{ie}} \times \frac{1}{j\omega C_E}}$$

$$\frac{V_o}{V_i} = \frac{A_{vm}}{1 - j \frac{\omega_L}{\omega}}$$

$$\text{where } \omega_L = \frac{(1+h_{fe})}{h_{ie} C_E}$$

$$f_L = \frac{g_m}{2\pi C_E} \left[ \because \frac{h_{fe}}{h_{ie}} = \frac{\frac{I_C}{V_{be}}}{\frac{I_b}{V_{be}}} = g_m \right]$$

→ If 3 different lower frequencies are obtained then the overall lower cut off frequency is the highest among three.