$$\nabla x \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} \rightarrow \vec{D} \qquad \vec{D} = \vec{E} \vec{E}$$

$$\nabla x \vec{E} = -\frac{\partial \vec{B}}{\partial t} \rightarrow \vec{D} \qquad \vec{J} = \sigma \vec{E}$$

$$\nabla \cdot \vec{D} = \vec{C} \vec{U}$$

$$\nabla \cdot \vec{B} = \vec{O}$$

Homogeneous Medium: is one for which the quantities &, M, and or we constant throughout the medium.

Isotropic Medius The medium is instropic if E is a realise Constant, so that D and E have energishere the same direction.

* The Maewell's equations (D& D) one for eource-free
regions, that is, regions in which there are no impressed
rollages or currents (no generators).

* Sunstituting D, B, and J in Marnell's equ

$$\nabla x H = \sigma E + e \frac{\partial E}{\partial t}$$
 differential composition $\nabla x E = -\mu \frac{\partial B}{\partial t}$

| Differential | form |
|--------------|------|
| | |

Law

Gaus's Law

Moneintanes of isolated

Faraday's law

$$\nabla \times \overline{H} = J + \frac{\partial \overline{D}}{\partial t}$$

$$\oint \overline{H} - d\overline{a} = \int \left(J + \frac{\partial \overline{D}}{\partial k} \right) d\overline{a}$$

where the statement was a first at the statement of the s

Amperi's crent

- a time-helmonie field is one that varies periodically of simulately with time.

$$z=x+iy=xL\emptyset=xe^{i\emptyset}$$

 $A=\sqrt{x^2+y^2}$ $\emptyset=ten^{4}(\sqrt[3]x)$

$$\varphi = \text{wt} + \theta$$
 $j(\text{wt} + \theta)$
 $z = 91 e$
 $z = 91$

$$\bar{A} = \text{Re } \{ \text{As e}^{\text{jot}} \}$$
 $\bar{A}_s = \text{Re }^{\text{jo}}$

- Maxwell's equations

$$\nabla x H = J + \frac{\partial \overline{D}}{\partial t}$$
 $\nabla \cdot \overline{D} = P_0$

$$\nabla x \bar{E} = -\frac{\partial \bar{B}}{\partial t}$$

$$\nabla . \bar{B} = 0$$

Let $\overline{H} = \overline{H}_{e}^{e}$ $\overline{E} = \overline{E}_{s}^{e}$ $\overline{E} = \overline{E}_{s}^{e}$

$$7 \times H_s e^{j\omega t} = \sigma E + e \frac{\partial E}{\partial t}$$

$$= \sigma E_s e^{j\omega t} + E \frac{\partial}{\partial t} (E_s e^{j\omega t})$$

$$= \sigma E_s e^{j\omega t} + j\omega e E_s e^{j\omega t}$$

and
$$\nabla \times \vec{E}_s e^{i\omega t} = -\mu \frac{\partial}{\partial t} \left(\vec{H}_s e^{i\omega t} \right)$$

$$\nabla \times (\nabla \times \overline{A}) = \nabla (\nabla \cdot \overline{A}) - \nabla \overline{A}$$

$$\Rightarrow \nabla \times (\nabla \times \overline{H}_S) = \nabla (\nabla \cdot \overline{H}_S) - \nabla \overline{H}_S = \nabla \times [\sigma + \tilde{J} \omega \in) \tilde{E}_S$$

$$\Rightarrow$$
 $-\nabla^2 \vec{H}_s = [\sigma + j\omega \epsilon] (-j\omega M \vec{H}_s)$ $\begin{cases} :: een (4) \end{cases}$

Ily for
$$\nabla \times (\nabla \times \vec{E_s}) = \nabla (\nabla /\vec{E_s}) - \nabla \vec{E_s} = \nabla \times \left(-\text{jneates} \right)$$

where is the propagation constant of the medium. and $\nabla \bar{E}_{5} - 7\bar{E}_{5} = 0$ and $\nabla \bar{E}_{5} - 8\bar{E}_{6} = 0$ are the homogeneous nector Helmholtz's equations or Simply マニ マナリカ $x^2 = x^2 \beta^2 + 2j\alpha\beta$ and $|z^2| = \alpha^2 + \beta^2$ Re{2} = 2-β2 → € $3 = jwn(\sigma + jwt)$ $= j\sigma wn - wnt$ 12 = WM Jo2+1622 Re{22} = -10 ME -> (8) from P & D ~ 2 = - WME equating (1) 49 x+p= wer Jo7+w72 -> (1) 20 = - WAE + WM J 07 + WEZ X = -WME + WME + or ELWZ $\alpha^2 = \frac{\omega^2 \pi t}{\alpha} \left[1 + \frac{\sigma^2}{e^2 \omega^2} - 1 \right]$ $= \left[\begin{array}{c|c} X = 10 \end{array} \right] \frac{ME}{2} \left[\sqrt{1 + \frac{\sigma^2}{4^2 E^2}} - 1 \right]$

and
$$-\partial \beta = -\omega^2 \mu \epsilon - \omega \mu \int \sigma^2 + \omega^2 \epsilon^2$$

$$\beta^2 = \frac{\omega^2 \mu \epsilon}{\partial \epsilon} \left[\int \frac{1 + \sigma^2}{\omega^2 \epsilon^2} + 1 \right]$$

- long dielectric: is a medium in which an EM Wane, our it propagator, borring power owing to imprefect disletter in this case, a and B were raine as given in 10 10 4 13.

_ borders d'elabrie: in bossers dielabries, o-22 NOE

i.e., oro, E= Eota, M=MOMZ

Substituting in 1 4 13.

X = 0, B = NO / NE [VI+0/41] = 20 JME

- free space: $\sigma = 0$, $f = \xi_0$, and $M = M_0$ d = 0 $\theta = W / M_{\xi_0}$

Good conductors:

A perfect of a good conductor is one, in which

anow

Ily
$$\beta = 29 \left[\frac{NL}{2} \left[\frac{\sigma}{\epsilon w} + 1 \right] \right] = \sqrt{\frac{10^7 \text{NLH} \sigma}{2 \text{ WW}}} = \sqrt{\frac{10^7 \text{NLH} \sigma}{2}}$$

$$\lambda = \beta = \sqrt{\frac{1000}{2}}$$
 in a good conductor.

Let
$$\overline{E}_s = E_{ns}(z) \overline{q}_n$$

from
$$\nabla = -7 = 0$$

$$\Rightarrow \nabla E_{xs}(z) - \vartheta E_{xs}(z) = 0$$

$$\Rightarrow \left(\nabla^2 - \eta^2\right) E_{xs}(z) = 0$$

$$\nabla V = \frac{\partial V}{\partial x^2} + \frac{\partial V}{\partial y^2} + \frac{\partial V}{\partial x^2}$$

here
$$V = E_{3s}(2)$$

then
$$\frac{\partial^2 E_1(z)}{\partial z^2} + \frac{\partial^2 E_2(z)}{\partial z^2} = \frac{\partial^2 E_2(z)}{\partial z^2} = 0$$

$$\frac{\partial}{\partial z^2} E_{xs}(z) - \chi E_{xs}(z) = 0$$

the solur
$$E_{x}(z) = E_{0}e^{-3z} + E_{0}e^{3z}$$
 homogeneous DE.

E., E. are constants

the turn
$$E_s = e^{(-7)(-2)}$$
 denotes a want transling along $-\overline{a}_z$, where ar we assume want propagation along \overline{a}_z , hence,

In E field with an a-component traveling is the + Z - direction.

$$\Rightarrow$$
 $E_{xs}(z) = E_0 e^{-i z}$

Substitute Enerz) in the abone

$$E(z,t) = Re \left\{ E_s e^{-\frac{3}{2}z} \int_{a}^{b} \int$$

$$E(z,t) = E_0 e^{-\alpha z} \cos(\omega t - \beta z) \overline{\alpha_n} \rightarrow \overline{(4)}$$

My we can define H(z,t) as below,

where
$$H_0 = \frac{E_0}{\eta}$$

nele n: characteristie de interince impedance of the medium.

$$\eta = \int \frac{\text{jou}}{\sigma + \text{jwe}} = |\eta| e^{\text{jon}}$$

$$|\gamma| = \frac{\sqrt{M/\epsilon}}{\left(1 + \left(\frac{\sigma}{W\epsilon}\right)^2\right)^{4/4}}$$
, $\left[\tan 2\sigma_{\eta} = \frac{\sigma}{W\epsilon}\right] \rightarrow \frac{1}{16}$

$$\overline{H(z,t)} = \operatorname{Re} \left\{ \frac{E_0}{|\eta|} e^{i\alpha\eta} e^{-i\alpha z} e^{-i(\omega t - \beta z)} \overline{a_y} \right\}$$

$$\overline{H(z,t)} = \frac{E_0}{|\eta|} e^{-i\alpha z} \cos(\omega t - \beta z - O_0) \overline{a_y} \rightarrow \overline{D_0}$$

If we observe eens (y) & (B), the magnitude $\frac{1}{2}$ wares $\frac{1}{2}$ decreases with $\frac{1}{2}$ ($\frac{1}{2}$ >1), as the ware propagates along the z-axis $(\frac{1}{2})$.

Hence, & is known as the attenuation constant of attenuations

It is a measure of the spatial state of decay of the wane in the medium, measured in NP/m and can be expected in decibels/m (do/m).

the bignial value, whereas, an increase of 1Np indicates an increase by a factor of e.

1 Np = 20 loge = 8.686 dB.

if $\sigma=0$, which is the case of a border of the space, $\alpha=0$ and the mane doesn't get attenuated as it propagates

the quantity B is a measure of the phase wift per unit length in sad/m. Hunce, B is called a phase constant and phase mumber.

 $u = \frac{N}{\beta}$, $\lambda = \frac{2\pi}{\beta}$

=> Eans (4) & (5) show that, E and H are

out of phase by on at any instant of time due to

the complex intrincic impedance of the medium.

at any time E hads H (or H legs E) by On.

The conduction current density

 $J = \sigma E$ and the displacement current density $J_d = \frac{\partial D}{\partial t}$ = E & [Ese]

= jwfEs ent

the statio of $\overline{f}/\overline{f} = \frac{\overline{\sigma}}{\overline{j} + \overline{k}} = \frac{\overline{\sigma}}{\overline{j} + \overline{k}} = \frac{\overline{\sigma}}{\overline{j} + \overline{k}}$

1 f/s = tano. → 17

tario: is the long tangent, O: loss angle of the medium.

to determine how long a medium is.

> occur -> tours >0, the medium

is said to be lossen or perfect delectrice.

> 0>> Net → teno >00, the medium is a good conductor.

> the characterister behavior of a medium depends worker not only on the constitutione parameters or, E, and re but also on the frequency of operation.

> A medium that is sugarded as a good conductor at low flequencies, may be a good dielectrice at higher frequencies.

From eens
$$60 \le 19$$
 $ton 200_{1} = \overline{w}e$
 $ton 200_{2} = \overline{w}e$
 $ton 200_{3} = \overline{w}e$
 $ton 200_{4} = \overline{w}e$

and we know $\nabla x H_s = (\sigma + j w + f) E_s$ $= jw + \left[1 - \frac{j\sigma}{w} + \frac{j}{E_s}\right] E_s$

Where
$$\left[\epsilon_{c} = \epsilon \left[1 - \frac{j\sigma}{\omega t} \right] \rightarrow \overline{(18)} \right]$$

$$= \epsilon' - j \epsilon''$$
 where $\epsilon' = \epsilon'$ and $\epsilon'' = 7/\omega$

E: is the complex premittinity of the medium

the section of
$$e'$$
 and e'' =) $e'_{e''} = \frac{\partial e}{\partial x} = \frac{\partial e}{\partial x}$

which is the loss tangent of the mediums.

Uniform Plane waves:

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial T}$$

$$\nabla x = \left(\frac{\partial Az}{\partial y} - \frac{\partial A\eta}{\partial z}\right) \overline{a}_{x}$$

$$+ \left(\frac{\partial Ax}{\partial z} - \frac{\partial Az}{\partial x}\right) \overline{a}_{y} + \left(\frac{\partial A\eta}{\partial x} - \frac{\partial A\eta}{\partial y}\right) \overline{a}_{z}$$

$$+ \left(\frac{\partial Ax}{\partial z} - \frac{\partial Az}{\partial x}\right) \overline{a}_{y} + \left(\frac{\partial A\eta}{\partial x} - \frac{\partial Ax}{\partial y}\right) \overline{a}_{z}$$

$$\frac{\partial}{\partial t} \left[\nabla x \vec{H} \right] = \left[\frac{\partial}{\partial y} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Ay}{\partial t} \right) \right] \vec{\sigma}_{x} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Ax}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{y} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Ay}{\partial r} \right) - \frac{\partial}{\partial y} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Ay}{\partial r} \right) - \frac{\partial}{\partial y} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Ay}{\partial r} \right) - \frac{\partial}{\partial y} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial y} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial y} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial Az}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{\partial}{\partial z} \right) \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial}{\partial z} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial}{\partial z} \right) \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial}{\partial z} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial}{\partial z} \right) \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial}{\partial z} \right) \right] \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial}{\partial z} \right) \vec{\sigma}_{z} + \left[\frac{\partial}{\partial z} \left(\frac{\partial}{\partial z$$

$$\nabla \cdot \vec{E} = 0 \Rightarrow \quad \nabla \vec{E} = M \cdot \frac{\partial \vec{E}}{\partial t}$$

$$\lim_{n \to \infty} \nabla \vec{H} = M \cdot \frac{\partial \vec{H}}{\partial t}$$

wane cenations. (in

I uniform plane wave has the same magnitude of electrice and magnetice fields in the direction of the were

In other words, E & H are considered to be independent of their sterputial dimensions.

Then $abla E = \frac{\partial E}{\partial x^2} \longrightarrow
abla$ Then $abla E = \frac{\partial E}{\partial x^2} \longrightarrow
abla E = \frac{\partial E}{$

and the eyes
$$\nabla^2 E = ME \frac{\partial^2 E}{\partial t^2} \rightarrow \Omega$$

$$\frac{\partial^2 E}{\partial x^2} = Mt \frac{\partial^2 E}{\partial t^2}$$

since the direction of ware propagation.
is is and E hay of (8) & components.

then
$$\frac{\partial^2 E_y}{\partial x^2} = \mu \epsilon \frac{\partial^2 E_y}{\partial t^2}$$
 \longrightarrow (21)

they is a loond-order PDE. This is the PDE for voltage (b) ownent along a when teaminion medium. The general form of colution is E= f,(x-20t)+f,(x+20t)

where
$$v_o = / I M \in$$

$$= \int_{1}^{\infty} (x - v_o t)$$

func, to becomes zero, Rince the direction of want

24- 11 E スー " H

 $\nabla v = \frac{\partial v}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial v}{\partial x}$

- VXXXA

= VAx ax + V Ay ay

+ \$\overline{A_2 a_2}

VA= V(V.A)

Wares (14)

$$\frac{\partial \vec{E}_x}{\partial x^2} = Mf \frac{\partial \vec{E}_x}{\partial t^2}, \quad \frac{\partial \vec{E}_y}{\partial x^2} = Mf \frac{\partial \vec{E}_y}{\partial t^2}, \quad \frac{\partial \vec{E}_z}{\partial x^2} = Mf \frac{\partial \vec{E}_z}{\partial t^2}$$

in a charge free sugion
$$\rho_{e} = 0 = 0$$
. $\overline{E} = 0$.

$$\frac{\partial E_x}{\partial a} + \frac{\partial E_y}{\partial y} + \frac{\partial E_z}{\partial z} = 0 \longrightarrow 22$$

Since the direction of wome propagation is it and according to the definition of when uniform planewane, E is independent

$$\frac{\partial E_y}{\partial y} = \frac{\partial E_z}{\partial z} = 0$$

now een (22) becomes
$$\frac{\partial E_{x}}{\partial x} = 0$$

$$\Rightarrow$$
 from $\frac{\partial E_x}{\partial x^2} = \mu E \frac{\partial E_x}{\partial E_x}$ and $\frac{\partial E_x}{\partial x} = 0$

$$\Rightarrow \frac{\partial^2 E_{\chi}}{\partial t^{\chi}} = 0$$

Ez: 15 either zero, constant in time, or investingther uniformly with time.

=> of similar analysis would show that there is no wanters
2-component of H.

Finally, we can conclude that uniform plane electromagnetic wares are terenewire and have components
of E and H only in directions perpendicular to the
directions of propagation.

$$\nabla x = \frac{-\partial E_2}{\partial x} \bar{a}_y + \frac{\partial E_y}{\partial x} \bar{a}_z$$

$$\nabla x \bar{H} = \frac{-\partial \bar{H}_2}{\partial x} \bar{\alpha}_y + \frac{\partial \bar{H}_y}{\partial x} \bar{\alpha}_z$$

we know in the space $\nabla xH = \frac{\partial D}{\partial t} = \epsilon_0 \frac{\partial E}{\partial t}$

$$\frac{-\partial H_2}{\partial x} \bar{\alpha}_y + \frac{\partial H_y}{\partial x} \bar{\alpha}_z = \mathcal{E}_{\partial} \left[\frac{\partial E_2}{\partial x} \bar{\alpha}_y + \frac{\partial E_y}{\partial x} \bar{\alpha}_z \right]$$

$$\frac{\partial E_2}{\partial x} = \frac{\partial E_3}{\partial x} = -\mu_0 \left[\frac{\partial H_3}{\partial t} = \frac{\partial H_2}{\partial t} = \frac{\partial H_2}{\partial t} = \frac{\partial H_3}{\partial t} = \frac{\partial$$

enating dy 4 dz terms

$$-\frac{\partial H_2}{\partial x} = t, \frac{\partial E_y}{\partial t} \rightarrow \frac{23(a)}{\partial t} + \frac{\partial E_2}{\partial x} = \mu_0 \frac{\partial H_y}{\partial t} \rightarrow \frac{23(b)}{\partial t}$$

$$\frac{\partial Hy}{\partial x} = \epsilon_0 \frac{\partial E_2}{\partial t} \qquad \frac{\partial E_3}{\partial x} = -\mu_0 \frac{\partial H_2}{\partial t} \longrightarrow 23 \text{ }$$

now. $\bar{E} = f_i(x-v_0t)$

No = Justo & Just

it f (x-vot)

Oti = ti

and if
$$E_y = f_1(x-v_0t)$$
, thus

$$\frac{\partial E_y}{\partial t} = f_1'(x-v_0t)(-v_0) \longrightarrow \text{Substitute thus}$$

neglected and their hence

and there hence

$$H_2 = \sqrt{\frac{E_0}{\mu_0}} = \sqrt{\frac{E_0}{E_0}} (8_1) \sqrt{\frac{\mu_0}{E_0}}$$

$$H_2 = \sqrt{\frac{E_0}{\mu_0}} = \sqrt{\frac{\mu_0}{E_0}} (8_1) \sqrt{\frac{\mu_0}{E_0}}$$

$$H_2 = \sqrt{\frac{\mu_0}{\mu_0}} = \sqrt{\frac{\mu_0}{E_0}} (8_1) \sqrt{\frac{\mu_0}{E_0}}$$

$$H_2 = \sqrt{\frac{\mu_0}{\mu_0}} = \sqrt{\frac{\mu_0}{E_0}} (8_1) \sqrt{\frac{\mu_0}{E_0}}$$

$$H_3 = \sqrt{\frac{\mu_0}{\mu_0}} = \sqrt{\frac{\mu_0}{E_0}} (8_1) \sqrt{\frac{\mu_0}{E_0}}$$

$$H_4 = \sqrt{\frac{\mu_0}{\mu_0}} = \sqrt{\frac{\mu_0}{E_0}} (8_1) \sqrt{\frac{\mu_0}{E_0}}$$

wanes (F)

JM is said to be characteristic impedance (dr)
intrincic impedance. If a non-conductine,
medium

for free- space

$$E = E_0$$
 / $M = MO$

$$U = \frac{10}{\beta} = \sqrt{\frac{210}{40}} = \frac{217}{\beta}$$

which the wone amplitude is alternated by the factor
$$e^{4z}$$
 ($\alpha z=1$)

which the wane amplitude is alternated by the factors
$$e^{42}$$
 ($42=1$)

= e^{-1} ($=37$ % of max value) is called stein depths.

$$\alpha = \sqrt{\frac{9}{2}} =)$$
 $\delta = \sqrt{\frac{9}{1000}} = \sqrt{\frac{1}{11400}}$

we know the de resistance

We know the de steinlame!

Rule =
$$\frac{d}{ds}$$

For a good conductor, when sintance is $Re \{ \gamma \}$,

 $\delta = \frac{1}{\sqrt{11} f N \sigma}$, $\gamma = \sqrt{\frac{3 k M}{\sigma}}$, $\alpha = \sqrt{\frac{11}{11} f N \sigma}$

$$9 = \sqrt{\frac{1000}{5}} = \sqrt{\frac{211}{5}} = \sqrt{\frac{211}{5}} = \sqrt{\frac{2}{5}} = \sqrt{\frac{2$$

$$\eta = \frac{\sqrt{2}}{6\delta} \left(\frac{1+j}{\sqrt{2}} \right) = \frac{1+j}{6\delta}$$

since the ac sientance / sein sientance is seal point of in.

$$Re\{n\} = Re\{\frac{1+j}{\sigma\delta}\} = \frac{1}{\sigma\delta}$$

$$Re\{n\} = \frac{1}{\sigma\delta} = \sqrt{\frac{\pi + \mu}{\sigma}}$$

The absorme eer is the significance of a unit width and unit length of the conductor. It is equivalent of the de significance for a unit length of the conductor having curs- sectional area 1×5.

> Thus, for a given width w, and length I, the ac

$$R_{ac} = \frac{1}{\sqrt{5}ke} = \frac{R_{c}l}{ke}$$

$$R_{ac} = \frac{1}{\sqrt{5}ke} = \frac{R_{c}l}{ke}$$

$$\Rightarrow$$
 Let $s=5$ he and $w=2\pi a$

tion
$$R_d = \frac{d}{\sigma(a \pi a^2)}$$
 and $R_{ac} = \frac{d}{\sigma \delta(a \pi a^2)}$

$$\frac{R_{ac}}{R_{dc}} = \frac{x}{45(2\pi \alpha)} \times \frac{5(2\pi \alpha^{2})}{x} = \frac{\alpha}{25} = \frac{\alpha}{2} \sqrt{11} + 118$$

$$\frac{R_{ac}}{R_{ac}} = \frac{\alpha}{2} \sqrt{11} + 118$$

Power and the Poynting Unitor:

$$\overline{E}$$
. $(\nabla x \overline{\mu}) = \sigma E^2 + \overline{E} \cdot \epsilon \frac{\partial \overline{E}}{\partial F} \longrightarrow \overline{D}$

$$\nabla \cdot (\bar{A} \times \bar{B}) = \bar{B} \cdot (\nabla \times \bar{A}) - \bar{A} \cdot (\nabla \times \bar{B})$$

$$\nabla \cdot (\overline{H} \times \overline{E}) = \overline{E} \cdot (\nabla \times \overline{H}) - \overline{H} \cdot (\nabla \times \overline{E})$$

$$\Rightarrow$$
 $E \cdot (\nabla x \hat{H}) = \nabla \cdot (\hat{H} \times \hat{E}) + \hat{H} \cdot (\nabla x \hat{E}) \rightarrow \bigcirc$

$$\nabla \cdot (\overrightarrow{H} \times \overrightarrow{E}) + \overrightarrow{H} (\nabla \times \overrightarrow{E}) = \sigma \overrightarrow{E} + \overrightarrow{E} \cdot \overrightarrow{E} \xrightarrow{\partial \overrightarrow{E}}$$

$$= \sigma \overrightarrow{E} + \overrightarrow{E} \cdot \overrightarrow{E} \xrightarrow{\partial \overrightarrow{E}}$$

$$= \sigma \overrightarrow{E} + \overrightarrow{E} \cdot \overrightarrow{E} \xrightarrow{\partial \overrightarrow{E}}$$

$$= \sigma \overrightarrow{E} + \overrightarrow{E} \cdot \overrightarrow{E} \xrightarrow{\partial \overrightarrow{E}}$$

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$$\Rightarrow \nabla \cdot (\vec{E} \times \vec{H}) = -\frac{\partial}{\partial t} \left[\frac{1}{2} \vec{D} \cdot \vec{E} + \frac{1}{2} \vec{B} \cdot \vec{H} \right] - \sigma \vec{E}^2$$

$$\Rightarrow \int \nabla \cdot (E \times H) du = -\frac{\partial}{\partial t} \left[\int_{V} (\frac{1}{2} D \cdot E + \frac{1}{2} B \cdot H) dx \right] - o \int_{V} E^{2} du$$

Ambiging sinergence theseem to the left-hand eide

$$\Rightarrow \oint (\bar{E} \times \bar{H}) \cdot d\bar{s} = -\frac{\partial}{\partial t} \left[\int_{V} \pm (\bar{B} \cdot \bar{E}) + \frac{1}{2} (\bar{B} \cdot \bar{H}) \right] - \int_{V} e^{z} du.$$

the wolume

rate of devicace in energy total power learning sided in E and H fuldy.

Ohmic pomes divipated.

Poynting's thedem: state that the net power flowing out of a given volume is it equal to the time state of decrease in the energy stoled within it mines the ohmic lovely.

$$\overline{h}(z,t) = \frac{E_0}{|\eta|} e^{z} \cos(wt-\beta z-\alpha_0) \overline{\alpha_y}$$

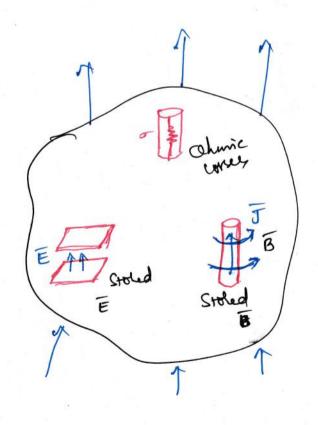
$$\overline{p}(z,t) = \frac{E_0^2}{|\eta|} e^{2\alpha z} \cos(\omega t - \beta z) \cos(\omega t - \beta z - 0\eta) \overline{a}_z$$

$$= \frac{E_0^2 - 2\alpha z}{2|\eta|} \left[\cos \alpha_{\eta} + \cos \left(2\omega t - 2\beta z - \alpha_{\eta} \right) \right] \bar{\alpha}_z$$

the onerage payorting rector

$$P_{\text{avg}}(z) = \frac{E_o^2}{2|\eta|} = \frac{2\lambda z}{2|\eta|} \cos \alpha_z$$

The total ang power covering a given surface 'S'.



Reflection of a plane wane:

At normal incidence.

$$\begin{aligned}
& = \frac{-37}{10} = \frac{-37}{10} = \frac{-37}{10} \\
& = \frac{-37}{10} = \frac{-37$$

$$(\sigma_1, \epsilon_1, M_1)$$

$$\uparrow \epsilon_i$$

$$\downarrow \epsilon_i$$

$$\downarrow$$

$$\begin{split}
E_{RS}(z) &= E_{SIO} e^{-\frac{1}{2}(-z)} \\
&= E_{SIO} e^{-\frac{1}{2}z} \\
&= E_{SIO} e^{-\frac{1}{2}z} \\
&= -\frac{1}{2}(-z) \\
&=$$

$$E_{ts}(z) = E_{to} e^{-\frac{3}{2}z} \bar{a}_{x}$$

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$$E_{to} -\frac{3}{2}z \bar{a}_{y}$$

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$$\Rightarrow \text{ The total piedel in medium 1 is}$$

$$\bar{E}_1 = \bar{E}_1 + \bar{E}_2$$

$$\bar{H}_2 = \bar{H}_1 + \bar{H}_2$$

$$\bar{H}_3 = \bar{H}_1 + \bar{H}_2$$

Fewers the boundary conditions defined, the langential components of E&H over continuous at the boundary

:
$$E_i(0) + E_n(0) = E_t(0)$$

$$H_{i}(0) + H_{a}(0) = H_{t}(0) \Rightarrow H_{io} - H_{ao} = H_{to}$$

$$\Rightarrow$$
 $2E_{10} = \left(1 + \frac{m_1}{m_2}\right) E_{to}$

$$\Rightarrow$$
 $E_{to} = \left(\frac{2\eta_{\lambda}}{\eta_1 + \eta_{\lambda}}\right) E_{io}$

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→<u>(1)</u>

$$2E_{svo} = \left(1 - \frac{m_1}{m_2}\right) E_{to}$$

$$E_{340} = \frac{2(\frac{\eta_2 - \eta_1}{\gamma_1})(\frac{2\eta_2}{\eta_1 + \eta_2})^{\frac{2}{10}}}{(\frac{2\eta_2}{\eta_1 + \eta_2})^{\frac{2}{10}}}$$

$$=\left(\frac{\eta_2-\eta_1}{\eta_1+\eta_2}\right) E_{io}$$

The suffection coefficient

$$T = \frac{E_{sio}}{E_{io}} = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$$

The transmission coefficient

$$T = \frac{E_{to}}{E_{10}} = \frac{2\eta_2}{\eta_1 + \eta_2}$$

 \Rightarrow a) 1+T=T

1) T, T are diminonless and may be complex.

Cale(i): Medium 1 is a perfect dielectric $(\sigma_1 = 0, \Lambda_1, \epsilon_1)$

and Medium 2 is a purpost conductor ($\sigma_2 \simeq 0$, M_2 , ε_2).

for a preject conductor $\eta = \sqrt{\frac{10M_2}{\sigma_2}}$

Substituting 8 02 =0 > n2 -70.

 $T = \frac{\eta_2 - \eta_1}{\eta_3 + \eta_1} = -\frac{\eta_1}{\eta_1} = -1$

 $T = \frac{2\eta_2}{\eta_1 + \eta_2} = 0$

>> This shows the wane is totally sufferted. This is due to the fields in a perfect conductor warrhed so there can be and transmitted ware. (Ez=0)

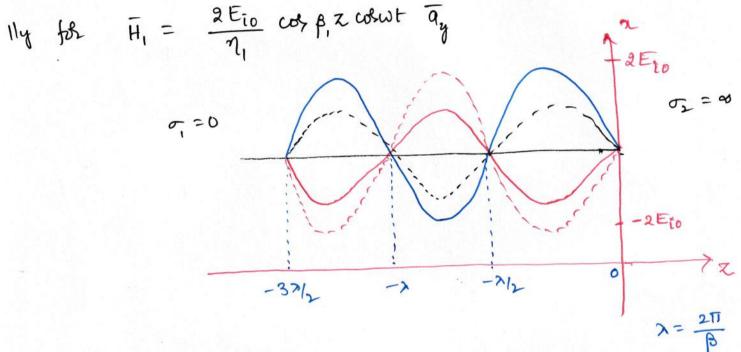
> The totally reflected wome combines with the Hundring wane. A standing wome doesn't more travel, it commits of two waves (Ei and Ex) of send amphibits but opposite directions.

 $\overline{E}_{1s} = \overline{E}_{is} + \overline{E}_{ks} = (\overline{E}_{io} \overline{e}^{3/2} + \overline{E}_{no} \overline{e}^{3/2}) \overline{a}_{x}$ My His = His - Has = (Hio e - Horo e) Tay

T=-1, $\sigma_1=0$, $\alpha_1=0$, β_1 , $\Rightarrow \beta=j\beta$,

$$\begin{aligned}
E_{1S} &= -E_{i0} \left(e^{i} - e^{-j\beta_{i} Z} \right) \overline{a}_{x} \\
&= -2j E_{i0} \sin \beta_{i} Z \overline{a}_{x} \\
\overline{E} &= R_{0} \int_{0}^{\infty} E_{i} \int_{0}^{\infty} e^{-j\beta_{i} Z} \overline{a}_{x}
\end{aligned}$$

$$\begin{split} & = \mathbb{R} \left\{ -2 \right\} = \mathbb{R} \left$$



$$E_1 = 2E_{10} \sin \beta z \sin \omega t \ \overline{a}_{x}$$

 $t = 0, 7/8, 7/4, 37/8, 7/2, --- T = \frac{25}{4}$

$$t=0 \Rightarrow E_{1}=0$$

$$t=T_{8} \Rightarrow \frac{2\pi}{810} \Rightarrow \bar{E}_{1}=2E_{10} \sin \beta_{1} Z \sin \left[\frac{1}{10}Z_{10}\right] = \sqrt{2}E_{10} \sin \beta_{1} Z$$

$$t=T_{4} \Rightarrow \frac{2\pi}{410} \Rightarrow \bar{E}_{1}=2E_{10} \sin \beta_{1} Z \sin \left[\frac{1}{10}Z_{10}\right] = 2E_{10} \sin \beta_{1} Z$$

$$t = 3\sqrt{g} \Rightarrow \frac{6\sqrt{1}}{8\sqrt{9}} \Rightarrow \frac{6\sqrt{1}}{8\sqrt{9}} \Rightarrow \frac{1}{8\sqrt{9}} = -\sqrt{2} \times \frac{1}{9\sqrt{9}} = -\sqrt$$

(a) if $n_2 > n$, $n_1 > 0$ $\sigma_1 = 0 = \sigma_2$.

also a transmitted wave in medium 2.

=> However, the insident and sufferted wance have amplitudes
that are not exact in magnitude.

$$T = \frac{E_{500}}{E_{i0}} = \frac{n_2 - n_1}{n_2 + n_1} \implies E_{500} = TE_{i0}$$

$$T = \frac{E_{40}}{E_{i0}} = \frac{2n_2}{n_2 + n_1} \implies E_{40} = TE_{i0}$$

Eis = Eis + Ens < total field in medium 1.

here
$$\sigma_1 = 0 = \sigma_2$$
, $\alpha_1 = 0 = \alpha_2$

$$\beta_1 = j\beta_1 \text{ and } \beta_2 = j\beta_2$$

$$E_{1S} = \left(E_{2S} + E_{2S} +$$

$$= \left(E_{io} e^{-j\beta z} + T E_{io} e^{j\beta z} \right) \overline{a_x}$$

$$\begin{split} & = \mathbb{R}_{e} \left\{ E_{io} \stackrel{\text{Swt}}{\in} \frac{1}{2} \underbrace{\sum_{i=1}^{j \text{wt}} \sum_{j \text{wt}} \sum_{i=1}^{j \text{wt}} \sum_{i$$

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and the minimum values of IE, Occurs at

$$Z_{min} = -\frac{(2n+1)\pi}{2\beta_1} = -\frac{(2n+1)\pi}{4}$$
, $m = 0, 1, 2, ---$

Care (26): if
$$\eta_2 < \eta_1$$
, $T < 0$

$$Z_{\text{max}} = \frac{-(2n+1)\pi}{2\beta} = \frac{-(2n+1)\lambda_1}{4}, n=0,1,2-$$

locations of minimum value of [E]

Note:

- 1. |Hi| minimum occurry wherever there is |E, maximum and vice-versa
- 2. The transmitted ware in medium 2 is purely a travelling ware, and consequently there are no maxima or minima in this vagion.
- is called the standing were ratio.

$$S = \frac{|E_1|_{\text{max}}}{|E_1|_{\text{min}}} = \frac{|H_1|_{\text{max}}}{|H_1|_{\text{min}}} = \frac{|H_1|_{\text{T}}}{|I-|T|}$$

Since 0 5 [T] 51, 155 0.

- SWR is dimensionless and expressed in decibely (dB).

