

## GENG 8010–Part 1: Elements of Differential and Difference Equations

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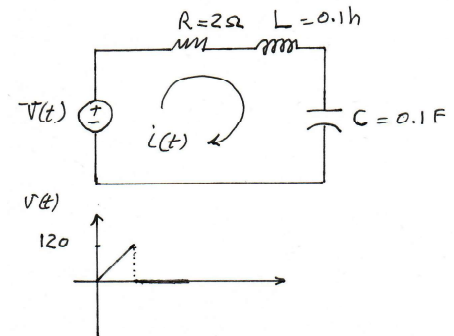
## Properties and further definitions XIII

**Integro–differential equations**– Let us illustrate this class of problems with the following simple RLC circuit

The circuit is described by

$$v(t) = Ri(t) + L \frac{di(t)}{dt} + \frac{1}{C} \int i(t) dt$$

The above is an integro-differential equation.



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## Properties and further definitions XIV

$$v(t) = 120t - 120tu(t-1)$$

Before taking Laplace Transform, we shall write  $v(t)$  as:

$$\begin{aligned} v(t) &= 120t - 120(t-1+1)u(t-1) \\ &= 120t - 120(t-1)u(t-1) - 120u(t-1) \end{aligned}$$

giving

$$V(s) = 120 \left( \frac{1}{s^2} - e^{-s} \left[ \frac{1}{s^2} + \frac{1}{s} \right] \right)$$

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## Properties and further definitions XV

Taking the Laplace transform of the integro-differential equation gives (with  $i(0) = 0$ )

$$2I(s) + 0.1sI(s) + 10 \frac{I(s)}{s} = 120 \left[ \frac{1}{s^2} - \left( \frac{e^{-s}}{s^2} + \frac{e^{-s}}{s} \right) \right]$$

$$\begin{aligned} I(s) &= 1200 \left[ \frac{0.01}{s} - \frac{0.01}{s+10} - \frac{0.1}{(s+10)^2} - \frac{0.01}{s} e^{-s} + \frac{0.01}{s+10} e^{-s} \right. \\ &\quad \left. + \frac{0.1}{(s+10)^2} e^{-s} - \frac{1}{(s+10)^2} e^{-s} \right] \end{aligned}$$

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## Properties and further definitions XVI

leading to

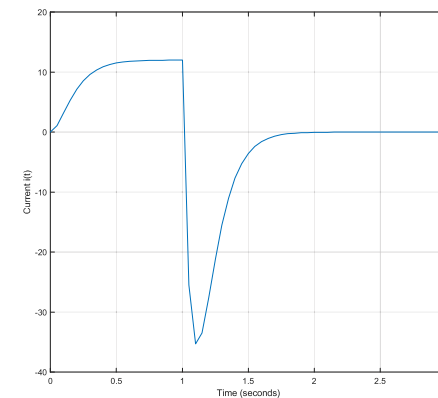
$$i(t) = 12[1 - u(t-1)] - 12[e^{-10t} - e^{-10(t-1)}u(t-1)] - 120te^{-10t} - 1080(t-1)e^{-10(t-1)}u(t-1)$$

$$i(t) = \begin{cases} 12 - 12e^{-10t} - 120te^{-10t}, & 0 \leq t < 1 \\ -12e^{-10t} + 12e^{-10(t-1)} - 120te^{-10t} - 1080(t-1)e^{-10(t-1)}, & t \geq 1 \end{cases}$$

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## Properties and further definitions XVII

The MATLAB response of the current in response to the applied voltage (solution of the differential equation for the given forcing function) is given below.



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## Properties and further definitions XVIII

## Theorem 8.2.7

**Transform of an integral**— Let  $f(t)$  be of exponential order and  $\mathcal{L}\{f(t)\} = F(s)$ , then

$$\mathcal{L}\left\{\int_0^t f(\tau)d\tau\right\} = \frac{F(s)}{s} \quad s > k$$

## Theorem 8.2.8

**Integral of a transform**— Let  $\frac{f(t)}{t}$  be of exponential order and  $\mathcal{L}\left\{\frac{f(t)}{t}\right\} = G(s)$ , for  $s > k$  and  $\mathcal{L}\{f(t)\} = F(s)$ , then

$$\mathcal{L}\left\{\frac{f(t)}{t}\right\} = \int_s^\infty F(x)dx$$

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## Properties and further definitions XIX

## Theorem 8.2.9

**Property of Dirac Delta Function**— Assuming  $f(t)$  is defined and integrable and is continuous in the vicinity of  $a$ , then

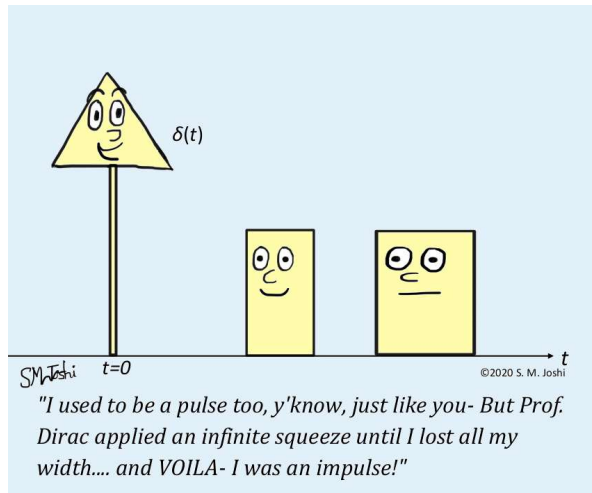
$$\begin{aligned} \int_0^\infty f(t)\delta(t-a)dt &= f(a) \\ \mathcal{L}\{\delta(t-a)\} &= e^{-as} \\ \mathcal{L}\{\delta(t)\} &= 1 \end{aligned}$$

## Summary: advantages of Laplace transform

1) Solution is routine and progresses systematically; 2) it gives the total solution; and 3) initial conditions are taken care of in the process.

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## Properties and further definitions XX



## Some system engineering concepts I

### Some defentions

**[ System]** A system is a collection of things which are related in such a way which make sense to think of them as whole.

**[ Single vs. multivariable]** A system is single variable iff  $\exists$  one input and one output. Otherwise, it is multivariable.

**[ Relaxedness]** A system is relaxed at time  $t_0$  iff the output  $y_{[t_0, \infty]}$  is solely and uniquely defined by input  $u_{[t_0, \infty]}$ .

**[ Memoryless]** A system is zero memory if  $y(t_1)$  depends only on  $u(t_1)$ .

**[Memory]** A system has "memory" if  $y(t_1)$  depends on  $u(t_1)$  as well as  $u(t)$ ,  $t < t_1$ .

## Some system engineering concepts II

### Remark

If a system has memory, it is impossible to determine  $y(t)$  without assuming the system has been relaxed or at rest. In that case,

$$y(t) = \mathcal{H} u(t)$$

where  $\mathcal{H}$  is some operator mapping the input space into output space.  $\mathcal{H} : \{u(t)\} \longrightarrow \{y(t)\}$ , or  $\mathcal{H}$  is the **mathematical model of the system**.

## Some system engineering concepts III

**[ Linearity]** A system is linear iff

$$\mathcal{H} [(a_1 u_1(t) + a_2 u_2(t))] = a_1 \mathcal{H} u_1(t) + a_2 \mathcal{H} u_2(t)$$

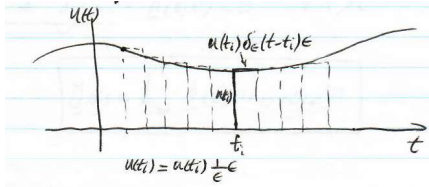
**[Causality]** A system is causal or non-anticipatory if the output of the system at time  $t$  does not depend on inputs applied after  $t$ .

**[Time invariance]** If the system's characteristic remains the same with time, then it is time invariant or stationary

$$\mathcal{H} \mathcal{S}_\tau u(t) = \mathcal{S}_\tau \mathcal{H} u(t)$$

where  $\mathcal{S}_\tau$  is the shifting operator, i.e.,  $\mathcal{S}_\tau u(t) = u(t + \tau)$ . Otherwise, the system is time varying.

## Some system engineering concepts IV



Consider the input  $u(t)$  as in the figure on the left. Every piecewise continuous function can be approximated by a series of pulse functions, and

$$u(t) \cong \sum_i u(t_i) \delta_\epsilon(t - t_i) \epsilon$$

$$y(t) = \mathcal{H} u(t) \cong \sum_i \mathcal{H} u(t_i) \delta_\epsilon(t - t_i) \epsilon$$

## Some system engineering concepts V

As  $\epsilon \rightarrow 0$ , the approximation will tend to exact equality and the summation will become an integration

$$y(t) = \int_{-\infty}^{\infty} \mathcal{H} \delta(t - \tau) u(\tau) d\tau$$

$$h(t, \tau) = \mathcal{H} \delta(t - \tau)$$

Response for time-varying non-causal single variable system

$$y(t) = \int_{-\infty}^{\infty} h(t, \tau) u(\tau) d\tau$$

for a causal system  $h(t, \tau) = 0 \quad \forall \tau > t$ , so

## Some system engineering concepts VI

Response for time-varying causal single variable system

$$y(t) = \int_{-\infty}^t h(t, \tau) u(\tau) d\tau$$

If the system is relaxed at  $t_0$  at which time the input is applied

Response for time-varying relaxed causal single variable system

$$y(t) = \int_{t_0}^t h(t, \tau) u(\tau) d\tau$$

## Some system engineering concepts VII

Theorem 8.3.1

**Relaxed system**— A system is relaxed at  $t_0$  iff  $u_{[t_0, \infty)} = 0$  implies  $y_{[t_0, \infty)} = 0$ .

For linear time invariant (LTI) systems  $h(t, \tau) = h(t - \tau)$ , so

Response for LTI relaxed causal single variable system

$$y(t) = \int_{t_0}^t h(t - \tau) u(\tau) d\tau$$

## Some system engineering concepts VIII

Assume  $t_0 = 0$ , also let  $t - \tau = \lambda \rightarrow -d\tau = d\lambda$  and at  $\tau = 0 \rightarrow t = \lambda$  and  $\tau = t \rightarrow \lambda = 0$  which gives.

$$y(t) = \int_{\lambda}^0 h(\lambda) u(t - \lambda) (-d\lambda) = \int_0^{\lambda} h(\lambda) u(t - \lambda) d\lambda$$

Response of LTI single variable system

$$y(t) = \int_0^t h(\tau) u(t - \tau) d\tau$$

Compare to previous discussion involving the Green Function

## Some system engineering concepts IX

Taking the Laplace transform of the above

I/O relation through transfer function

$$Y(s) = H(s)U(s)$$

and

$$H(s) = \frac{Y(s)}{U(s)} = \mathcal{L}\{h(t)\}$$

## First order response I

Consider the following first order system

$$\frac{dx(t)}{dt} + a_0 x(t) = b_0 r(t)$$

Taking Laplace transform

$$sX(s) - x(0) + a_0 X(s) = b_0 R(s) \Rightarrow (s + a_0)X(s) = b_0 R(s) + x(0)$$

Response of 1st order system

$$X(s) = \underbrace{\frac{b_0}{s + a_0} R(s)}_{\text{zero state response}} + \underbrace{\frac{x(0)}{s + a_0}}_{\text{zero input response}}$$

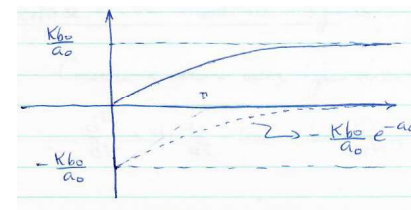
## First order response II

$$H(s) = \mathcal{L}\left\{\frac{\text{output}}{\text{input}}\right\} = \frac{X(s)}{R(s)} = \frac{b_0}{s + a_0}, \text{ with } x(0) = 0$$

$$\text{Considering } r(t) = Ku(t) \Rightarrow R(s) = \frac{K}{s}$$

$$\text{If } x(0) = 0$$

$$X(s) = \frac{Kb_0}{s(s + a_0)} = \frac{Kb_0/a_0}{s} + \frac{-Kb_0/a_0}{s + a_0}$$



$$x(t) = \frac{Kb_0}{a_0} (1 - e^{-a_0 t})$$

If  $a_0 > 0$  we say that the system is **stable** and  $-a_0$  is the **pole** of the system.

## First order response III



"Go West, young man!"

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## Second order response I

Consider a second order system described by

$$\frac{d^2x}{dt^2} + a_1 \frac{dx}{dt} + a_0x = b_1 \frac{dr}{dt} + b_0r$$

$$X(s) = \underbrace{\frac{b_1s + b_0}{s^2 + a_1s + a_0}}_{= H(s)} R(s) + \frac{\text{1st order polynomial involving IC}}{s^2 + a_1s + a_0}$$

The characteristic polynomial for this system is

$$\Delta(s) = s^2 + a_1s + a_0 = 0 \quad \text{with } s_{1,2} = \frac{-a_1 \pm \sqrt{a_1^2 - 4a_0}}{2}$$

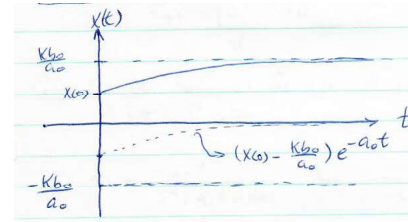
**Case 1**  $-a_1^2 > 4a_0 \implies$  distinct and real roots  $s_1, s_2$ , in which case,

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## First order response IV

If  $x(0) \neq 0$

$$X(s) = \frac{Kb_0}{s(s + a_0)} + \frac{x(0)}{s + a_0} = \frac{Kb_0}{a_0} \left( \frac{1}{s} \right) + \left( x(0) - \frac{Kb_0}{a_0} \right) \left( \frac{1}{s + a_0} \right)$$



$$x(t) = \frac{Kb_0}{a_0} + \left( x(0) - \frac{Kb_0}{a_0} \right) e^{-a_0t}$$

**Remark**— In both cases  $x_{ss} = \frac{Kb_0}{a_0}$ .

**Time Constant**—The value of time that makes the exponent of  $e$  equal to  $-1$  is called the time constant  $\tau$ , therefore  $\tau = \frac{1}{a_0}$  is the time interval over which the exponential decays by a factor of  $\frac{1}{e} = 0.368$ .

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## Second order response II

### Overdamped system response

$$x(t) = c_1 e^{s_1 t} + c_2 e^{s_2 t}$$

### Example—

$$H(s) = \frac{12}{s^2 + 4s + 3} \quad \text{with } R(s) = \frac{1}{s} \quad \text{and } I.C. = 0$$

$$x(t) = \mathcal{L}^{-1} \left\{ \frac{4}{s} + \frac{2}{s+3} - \frac{6}{s+1} \right\}$$

$$x(t) = 4 + 2e^{-3t} - 6e^{-t}$$

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## Second order response III

**Case 2**  $-a_1^2 = 4a_0 \implies$  repeated roots  $s_{1,2} = s_1$ , in which case,

$$X(s) = \frac{s+b}{(s-s_1)^2} = \frac{c_1}{s-s_1} + \frac{c_2}{(s-s_1)^2}$$

Critically damped system response

$$x(t) = c_1 e^{s_1 t} + c_2 t e^{s_1 t}$$

**Example–**

$$H(s) = \frac{9}{s^2 + 6s + 9} \quad \text{with } R(s) = \frac{1}{s} \quad \text{and } I.C. = 0$$

$$X(s) = \frac{1}{s} - \frac{1}{s+3} - \frac{3}{(s+3)^2}$$

## Second order response IV

$$x(t) = 1 - (1 + 3t)e^{-3t}$$

**Case 3**  $-a_1^2 < 4a_0 \implies$  complex conjugate pairs  $s_{1,2} = \sigma \pm j\omega$ , in which case,

$$X(s) = \frac{s+b}{(s+\sigma)^2 + \omega^2}$$

note that if

$$X(s) = \frac{N}{(s+\sigma-j\omega)(s+\sigma+j\omega)} = \frac{K_1}{s+\sigma-j\omega} + \frac{K_1^*}{s+\sigma+j\omega}$$

and if  $K_1 = Ae^{j\theta}$  then  $x(t) = 2Ae^{-\sigma t} \cos(\omega t + \theta)$

Underdamped system response

$$x(t) = 2Ae^{-\sigma t} \cos(\omega t + \theta)$$

## Second order response V

**Example–**

$$H(s) = \frac{-3s+17}{s^2+2s+17} \quad \text{with } R(s) = \frac{1}{s} \quad \text{and } I.C. = 0$$

$$X(s) = \frac{-3s+17}{s(s^2+2s+17)} = \frac{1}{s} - \frac{s+5}{(s+1)^2 + (4)^2}$$

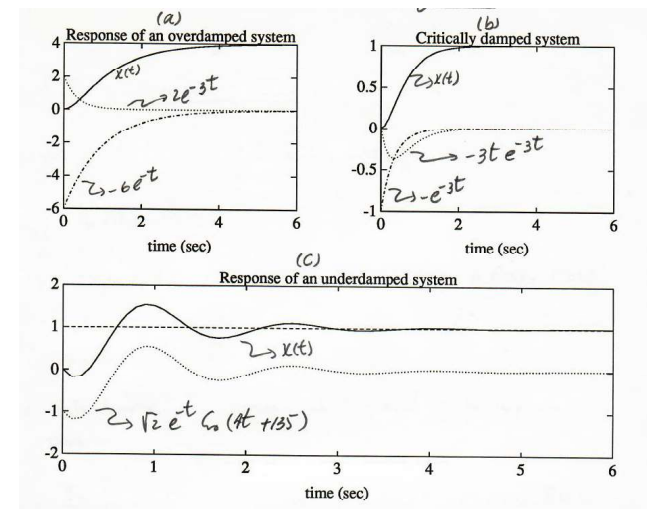
$$= \frac{1}{s} - \left( \frac{K_1}{s+1-j4} + \frac{K_1^*}{s+1+j4} \right)$$

This gives  $K_1 = \sqrt{\frac{1}{2}}/45^\circ$

$$x(t) = 1 + \sqrt{2}e^{-t} \cos(4t + 135^\circ)$$

The response of the three example cases are plotted below

## Second order response VI



## Second order response VII

