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Applied Modelling and Computational Group, Department of Earth Science and Engineering

ICL-ICAM-BP

24th March 2021

Supervisors:

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Dynamic semi-structured meshes for fast numerical simulation of Multi-Phase Modelling in the energy industry



Starting date: 01 October 2020

Aim:

This project will develop and implement a semi-structured mesh within the Multi-Fluidity project to significantly improve its speed.

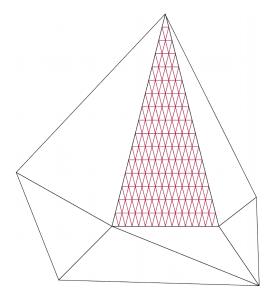


Figure 1. Semi-structured mesh.

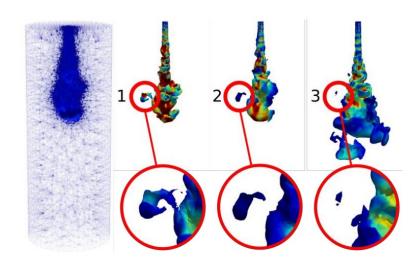


Figure 2. Creation and dispersion of a droplet.



Starting date: 01 October 2020

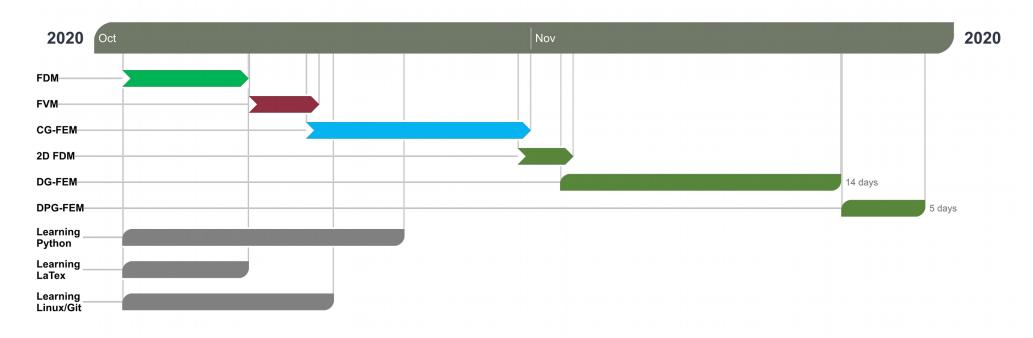


Figure 3. Work plan from October to mid-December 2020.

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- 1D-DG Petrov-Galerkin FEM: 2 documents

1- Report

8.1.1 Diffusion Form

$$\int_{\Omega}\phi_{i}rd\Omega+\int_{\Omega}\nu(\frac{\partial U}{\partial t},\frac{\partial U}{\partial x})^{T}d\Omega=0$$

where ν is the diffusion coefficient

$$\begin{split} \underbrace{\sum_{j=1}^{2} \frac{\partial U_{j}}{\partial t} \int_{\Omega} \phi_{i} \phi_{j} d_{\Omega} - \sum_{j=1}^{2} U_{j} \int_{\Omega} c \phi_{j} \frac{\partial \phi_{i}}{\partial x} d_{\Omega} + \sum_{j=1}^{2} U_{j} \oint_{\Gamma_{e}} \hat{n}.c \phi_{j} \phi_{i} d\Gamma_{e}}_{\textbf{Stabilisation part}} \\ + \underbrace{\sum_{j=1}^{2} \frac{\partial U_{j}}{\partial t} \int_{\Omega} \nu \phi_{j} d_{\Omega} + \sum_{j=1}^{2} U_{j} \int_{\Omega} c \nu \frac{\partial \phi_{j}}{\partial x} d_{\Omega}}_{\textbf{STABILISATION PART}} = 0 \end{split}$$

$$\begin{split} \sum_{j=1}^{2} \frac{\partial U_{j}}{\partial t} \left(\int_{\Omega} \phi_{i} \phi_{j} d_{\Omega} + \int_{\Omega} \nu \phi_{j} d_{\Omega} \right) + \sum_{j=1}^{2} U_{j} \left(\int_{\Omega} c \nu \frac{\partial \phi_{j}}{\partial x} d_{\Omega} - \int_{\Omega} c \phi_{j} \frac{\partial \phi_{i}}{\partial x} d_{\Omega} \right) \\ + \sum_{j=1}^{2} U_{j} \oint_{\Gamma_{e}} \hat{n}.c \phi_{j} \phi_{i} d\Gamma_{e} = 0 \end{split}$$

$$\begin{split} \nu &= \frac{r P^* r}{||\nabla_{xt} U||^2} \\ P^* &= \frac{1}{4} (||J_{xt}^{-1} c||_2)^{-1} = \frac{\Delta x}{8c} \end{split}$$

where J_{xt} is space-time Jacobian matrix:

1- Theory

 \mathbf{P}_{xt}^* is a function of \mathbf{A}_{xt}^* and the size and shape of the elements, for example:

$$\mathbf{P}_{xt}^* = \frac{1}{4} (|\mathbf{A}_{xt}^* \cdot \nabla_{xt} \mathbf{N}_{xti}|)^{-1},$$
 (37)

or using the 2 matrix norm and the space-time Jacobian matrix J_{xt} :

$$\mathbf{P}_{xt}^{*} = \frac{1}{4} (||\mathbf{J}_{xt}^{-1} \mathbf{A}_{xt}^{*}||_{2})^{-1}. \tag{38}$$

Since the matrices \mathbf{A}_{t}^{*} , \mathbf{A}_{x}^{*} , \mathbf{A}_{x}^{*} , \mathbf{A}_{z}^{*} that go to make up

$$\mathbf{A}_{xt}^{*} = (\mathbf{A}_{t}^{*T}, \mathbf{A}_{x}^{*T}, \mathbf{A}_{y}^{*T}, \mathbf{A}_{z}^{*T})^{T}$$
(39)

are diagonal the matrix \mathbf{P}_{xt}^* is also diagonal. In the traditional Petrov Galerkin method $\mathbf{A}_{xt}^* = \mathbf{A}_{xt}$ in the above and \mathbf{P}_{xt} replaces \mathbf{P}_{xt}^* . The finite element space-time Jacobian matrix for 3D time dependent problems is:

$$\mathbf{J}_{xt} = \begin{pmatrix} \mathbf{I} \frac{\partial t}{\partial t'} & \mathbf{I} \frac{\partial x}{\partial t'} & \mathbf{I} \frac{\partial y}{\partial t'} & \mathbf{I} \frac{\partial z}{\partial t'} \\ \mathbf{I} \frac{\partial t}{\partial x'} & \mathbf{I} \frac{\partial x}{\partial x'} & \mathbf{I} \frac{\partial y}{\partial x'} & \mathbf{I} \frac{\partial z}{\partial x'} \\ \mathbf{I} \frac{\partial t}{\partial y'} & \mathbf{I} \frac{\partial x}{\partial y'} & \mathbf{I} \frac{\partial y}{\partial y'} & \mathbf{I} \frac{\partial z}{\partial x'} \\ \mathbf{I} \frac{\partial t}{\partial t'} & \mathbf{I} \frac{\partial x}{\partial x'} & \mathbf{I} \frac{\partial y}{\partial y'} & \mathbf{I} \frac{\partial z}{\partial x'} \\ \mathbf{I} \frac{\partial t}{\partial x'} & \mathbf{I} \frac{\partial x}{\partial x'} & \mathbf{I} \frac{\partial y}{\partial x'} & \mathbf{I} \frac{\partial z}{\partial x'} \end{pmatrix}, \quad (40)$$

where the variables with \prime are the local variables and where **I** is the $\mathcal{M} \times \mathcal{M}$ identity matrix in which \mathcal{M} is the number solution variables at each DG node. For uniform space-time resolution with a time step size of Δt and an element size of Δx (in the x-direction), Δy (in the y-direction), Δz (in the z-direction), then:

$$\mathbf{J}_{xt} = \begin{pmatrix} \mathbf{I}_{2}^{1} \Delta t & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{I}_{2}^{1} \Delta x & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{I}_{2}^{1} \Delta y & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{I}_{2}^{1} \Delta z \end{pmatrix}. \tag{41}$$

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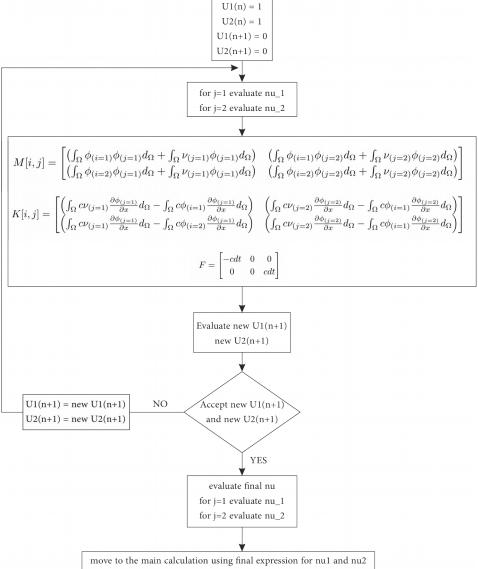


Figure 4. Flowchart for the DG Petrov-Galerkin diffusion method.



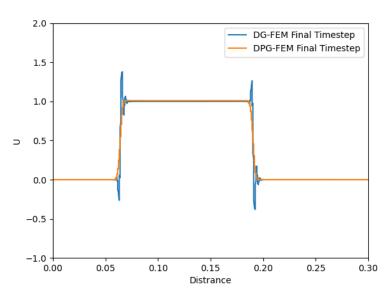


Figure 5. Illustration of the standard DG against DPG results for the same number of elements, 400.

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- 2D FDM

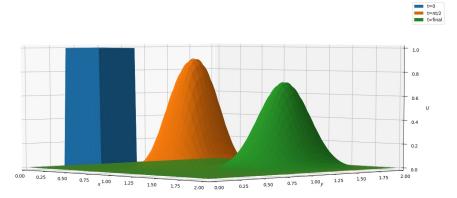


Figure 6. Travelling a square wave in 2D with 500 elements.

- 2D DG-FEM

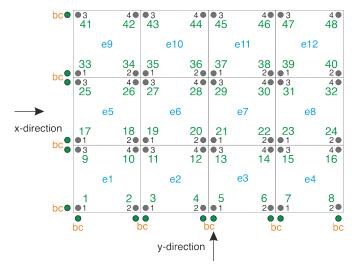


Figure 7. 2D domain with local & global node numbering.

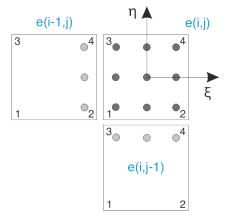


Figure 8. Volume integration using 3-point Gaussian quadrature method.



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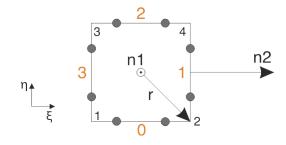


Figure 9. Surface integration using 2-point Gaussian quadrature method.



- Fortran Training - IC-FERST Workshop

- Training sessions: multi-phase time-loop in the IC-FERST, identified the key subroutines corresponding to momentum, magma, porous media equations and their variables.
- Training for connecting & working with workstations, downloading and compiling IC-FERST code.
- 2D test files e.g. flow pass in a cylinder & collapsing water column. changed the flow velocity, the shapes and the positions of the problem.

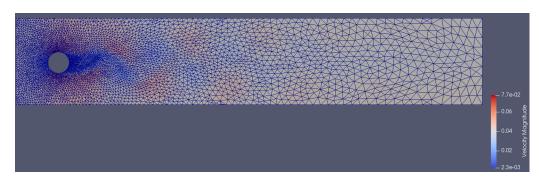


Figure 10. Flow pass a cylinder with the fixed mesh.

Simulation info:

Number of elements: 9444

Final time: 100 Time-step: 0.005

Reynolds number: 3900

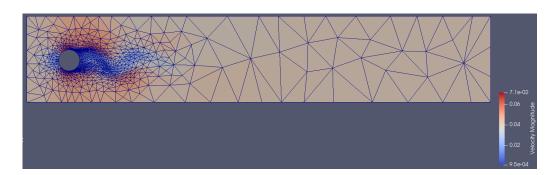


Figure 11. Flow pass a cylinder with the adaptive mesh.

Simulation info:

Initial number of elements: 168 Final number of elements: 2032

Final time: 100 Time-step: 0.005

Reynolds number: 3900

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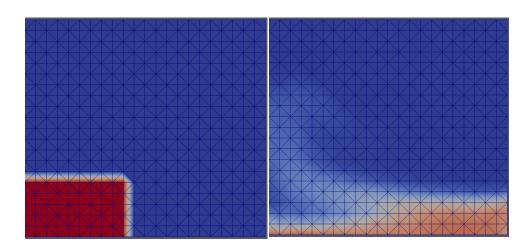


Figure 12. Collapsing water column under gravity with a fixed mesh.

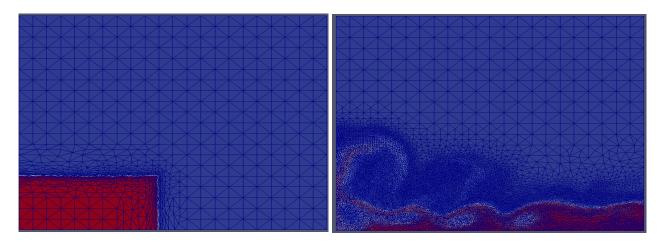


Figure 13. Collapsing water column under gravity with the adaptive mesh.

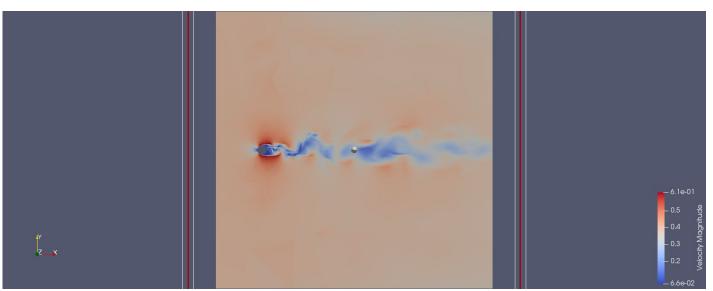


Figure 14. Flow pass in a cylinder in 3D with the adaptive mesh.

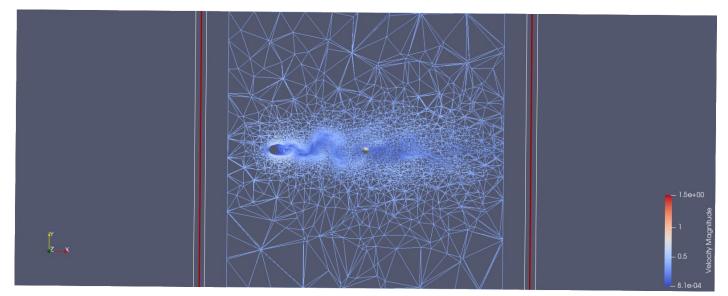


Figure 15.Sliced mesh view for the flow pass in a cylinder problem in 3D with the adaptive mesh.



Simulation info:

Initial number of elements: 8470 Final number of elements: 21480

Final time: 0.76 Time-step: 0.005

Reynolds number: 3900



Regular weekly meetings

- AMCG catch-up
- Porous media/Inertia
- BP catch-up

Theory

- Delaunay and barycenter triangulation (a few days)
- Voronoi diagram
- Structured mesh generation
- Unstructured mesh generation (~a month)
- Semi-structured mesh

Near-future work

- Will be working with Dr.
 Obeysekara on the mixing tank problem (end of March)
- 2D 1st order square wave DG-FEM (end of March)
- semi-structured 2D DG-FEM.
- Will be work with Prof. Pain and others on the Fortran code for semi-structured and with space-time within ICFERST/FLUIDITY.



END