

# **Report 1.0.1**

## **Simulation of Humanoid using MATLAB Teach Toolbox**

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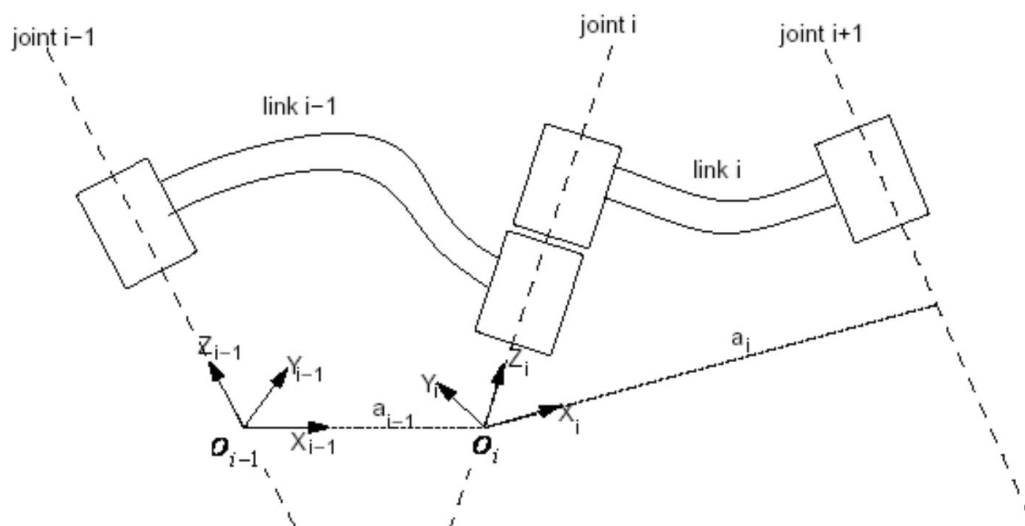
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# Introduction

## DH Parameters

Denavit-Hartenberg (DH) comes in variety of modified and standard. The link and joint parameters in the modified convention as shown in figure below are as follows:

- Twist angle,  $\alpha_{i-1}$  is the angle between  $z_{i-1}$  to  $z_i$  measured about  $x_{i-1}$
- Link length,  $a_{i-1}$  is the distance from  $z_{i-1}$  to  $z_i$  measured along  $x_{i-1}$
- Offset length,  $d_i$  is the distance from  $x_{i-1}$  to  $x_i$  measured along  $z_i$
- Joint angle,  $\theta_i$  is the angle between  $x_{i-1}$  to  $x_i$  measured about  $z_i$



The D-H parameters are determined as per table below.

Link, $i$	$\alpha_{i-1}$	$a_{i-1}$	$d_i$	$\theta_i$
1				
2				

The frame transformation  ${}^{i-1}T_i$  describing the finite motion from link  $i-1$  to link  $i$  may then be expressed as the following sequence of elementary transformations, starting from link  $(i-1)$ :

1. A rotation  $\alpha_{i-1}$  about  $x_{i-1}$ .
2. A translation  $a_{i-1}$  along the  $x_{i-1}$  axis
3. A rotation  $\theta_i$  about  $z_i$ ;
4. A translation  $d_i$  along the same axis  $z_i$ ;

The homogeneous transformation  ${}^{i-1}T_i$  is represented as a product of four basic transformations as follows:

$$\begin{aligned}
{}^{i-1}T_i &= R(x_{i-1}, \alpha_{i-1}) T(x_{i-1}, a_{i-1}) R(z_i, \theta_i) T(z_i, d_i) \\
&= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & C\alpha_{i-1} & -S\alpha_{i-1} & 0 \\ 0 & S\alpha_{i-1} & C\alpha_{i-1} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & a_{i-1} \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} C\theta_i & -S\theta_i & 0 & 0 \\ S\theta_i & C\theta_i & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \\
&= \begin{bmatrix} C\theta_i & -S\theta_i & 0 & a_{i-1} \\ S\theta_i C\alpha_{i-1} & C\theta_i C\alpha_{i-1} & -S\alpha_{i-1} & -d_i S\alpha_{i-1} \\ S\theta_i S\alpha_{i-1} & C\theta_i S\alpha_{i-1} & C\alpha_{i-1} & d_i C\alpha_{i-1} \\ 0 & 0 & 0 & 1 \end{bmatrix}
\end{aligned}$$

An alternative representation of  ${}^{base}T_{end-effector}$  can be written as

$${}^{base}T_{end-effector} = {}^b T_e = \begin{bmatrix} r_{11} & r_{12} & r_{13} & p_x \\ r_{21} & r_{22} & r_{23} & p_y \\ r_{31} & r_{32} & r_{33} & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

where  $r_{kj}$ 's represent the rotational elements of transformation matrix ( $k$  and  $j = 1, 2$  and  $3$ ).  $p_x$ ,  $p_y$  and  $p_z$  denote the elements of the position vector. For a six jointed manipulator, the position and orientation of the end-effector with respect to the base is given by

$${}^0T_6 = {}^0T_1(q_1) {}^1T_2(q_2) {}^2T_3(q_3) {}^3T_4(q_4) {}^4T_5(q_5) {}^5T_6(q_6)$$

where  $q_i$  is the joint variable (revolute or prismatic joint) for joint  $i$ , ( $i = 1, 2, \dots, 6$ ).

D-H parameter	Classical convention	Modified convention
Joint axis	$z_{i-1}$ is for joint $i$	$z_i$ is for joint $i$
Link length ( $a_i$ )	The distance from $o_i$ to the intersection of the $z_{i-1}$ and $x_i$ axes along the $x_i$ axis	The distance from $z_i$ to $z_{i+1}$ measured along $x_i$
Twist angle( $\alpha_i$ )	The angle from the $z_{i-1}$ axis to the $z_i$ axis about the $x_i$ axis	The angle between $z_i$ to $z_{i+1}$ measured about $x_i$
Offset length ( $d_i$ )	The distance from the origin of the $(i-1)$ frame to the intersection of the $z_{i-1}$ axis with the $x_i$ axis along the $z_{i-1}$ axis	The distance from $x_{i-1}$ to $x_i$ measured along $z_i$
Joint angle ( $\theta_i$ )	The angle between the $x_{i-1}$ and $x_i$ axes about the $z_{i-1}$ axis	The angle between $x_{i-1}$ to $x_i$ measured about $z_i$

## Algorithm for modified D-H Convention:

**Step - 1:** Assigning of base frame: the base frame  $\{0\}$  is assigned to link 0. The base frame  $\{0\}$  is arbitrary. For simplicity chose  $z_0$  along  $z_1$  axis when the first joint variable is zero. Using this convention, we have  $a_0 = 0$  and  $\alpha_0 = 0$ . This also ensures that  $d_1 = 0$  if the joint is revolute and  $\theta_1 = 0$  if the joint is prismatic.

**Step - 2:** Identify links. The link frames are named by number according to the link to which they are attached (i.e. frame  $\{i\}$  is attached rigidly to link  $i$ ). For example, the frame  $\{2\}$  is attached to link 2.

Identify joints. The z-axis of frame  $\{i\}$ , called  $z_i$ , is coincident with the joint axis  $i$ . The link  $i$  has two joint axes,  $z_i$  and  $z_{i+1}$ . The  $z_i$  axis is assigned to joint  $i$  and  $z_{i+1}$  is assigned to joint  $(i+1)$ .

For  $i = 1, \dots, n$  perform steps 3 to 6.

**Step - 3:** Identify the common normal between  $z_i$  and  $z_{i+1}$  axes, or point of intersection. The origin of frame  $\{i\}$  is located where the common normal ( $a_i$ ) meets the  $z_i$  axis.

**Step - 4:** Assign the  $z_i$  axis pointing along the  $i$ th joint axis.

**Step - 5:** Assign  $x_i$  axis pointing along the common normal ( $a_i$ ) in the direction from  $z_i$  axis to  $z_{i+1}$  axis. In the case of  $a_i = 0$ ,  $x_i$  is normal to the plane of  $z_i$  and  $z_{i+1}$  axes.

- As seen from figure 3.7, the joints may not necessarily be parallel or intersecting. As a result, the z-axes are skew lines. There is always one line mutually perpendicular to any two skew lines, called the common normal, which has the shortest

distance between them. We always assign the x-axis of the local reference frames in the direction of the common normal. Thus, if  $a_i$  represents the common normal between  $z_i$  and  $z_{i+1}$ , the direction  $x_i$  is along  $a_i$ .

- If two joint z-axes are parallel, there are an infinite number of common normals present. We will pick the common normal that is collinear with the common normal of the previous joint.
- If the z-axes of two successive joints are intersecting, there is no common normal between them (or it has zero length). We will assign the x-axis along a line perpendicular to the plane formed by the two axes.

**Step - 6:** The  $y_i$  axis is selected to complete right-hand coordinate system.

**Step – 7:** Assigning of end-effector frame: If the joint  $n$  is revolute, the direction of  $x_n$  is chosen along the direction of  $x_{n-1}$  when  $\theta_n = 0$  and the origin of frame  $\{n\}$  is chosen so that  $d_n = 0$ . If the joint  $n$  is prismatic, the direction of  $x_n$  is chosen so that  $\theta_n = 0$  and the origin of frame  $\{n\}$  is chosen at the intersection of  $x_{n-1}$  with  $z_n$  so that  $d_n = 0$ .

**Step – 8:** The link parameters are determined as mentioned in table 4.

Link, $i$	$a_{i-1}$	$\alpha_{i-1}$	$d_i$	$\theta_i$
1				
2				

- $a_{i-1}$  = the distance from  $z_{i-1}$  to  $z_i$  measured along  $x_{i-1}$
- $\alpha_{i-1}$  = the angle between  $z_{i-1}$  to  $z_i$  measured about  $x_{i-1}$
- $d_i$  is the distance from  $x_{i-1}$  to  $x_i$  measured along  $z_i$
- $\theta_i$  is the angle between  $x_{i-1}$  to  $x_i$  measured about  $z_i$

**Step - 9:** Form  ${}^0T_n = {}^0T_1 {}^1T_2 {}^2T_3 \dots {}^{n-1}T_n$ . This gives the position and orientation of the end-effector frame expressed in the base coordinates.

Two additional parameters are Sigma and Offset.

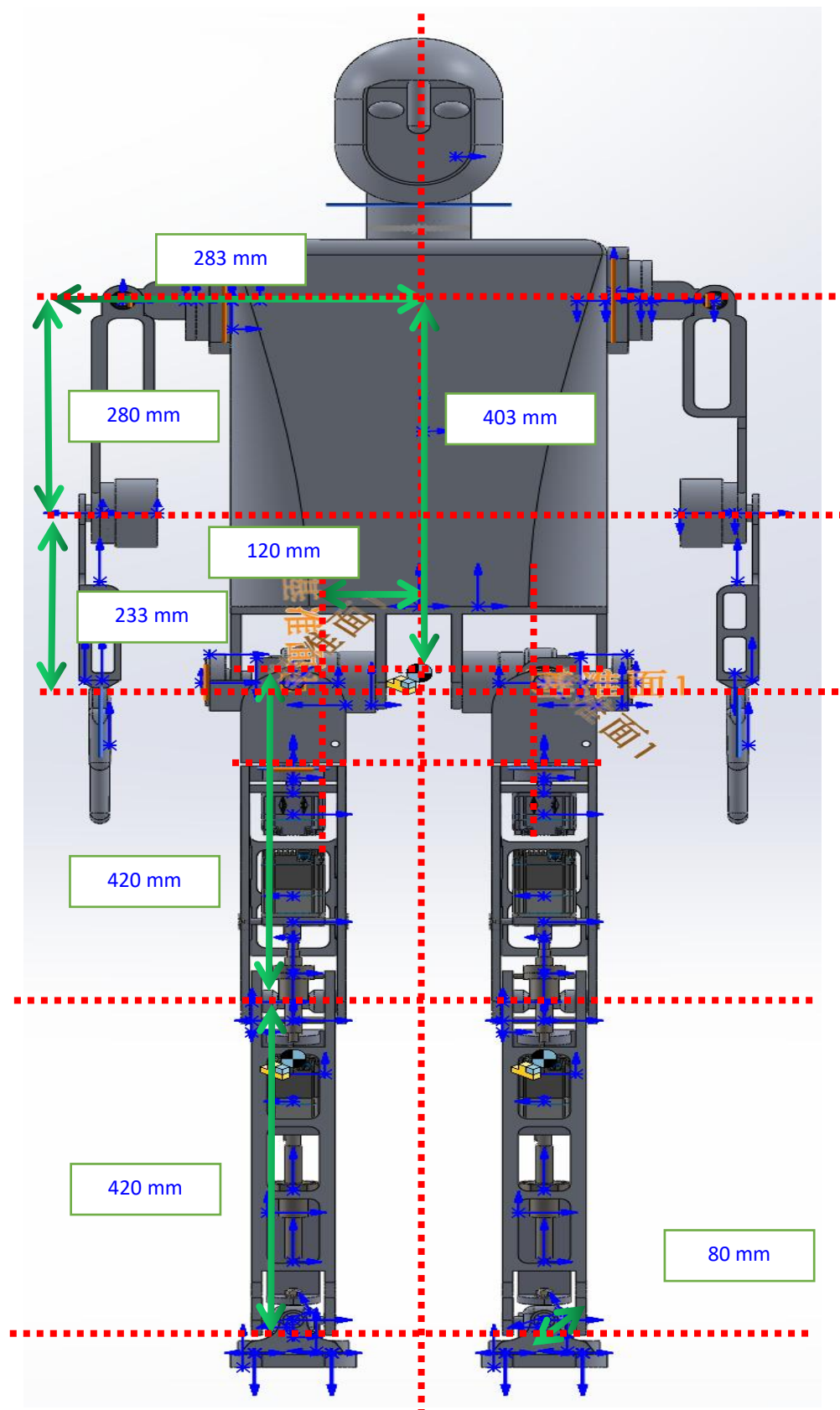
Link [THETA, D ,A ,ALPHA ,SIGMA ,OFFSET]

OFFSET is a constant displacement between the user joint angle vector and the true kinematic solution. SIGMA=0 for a revolute and 1 for a prismatic joint.

# Structure

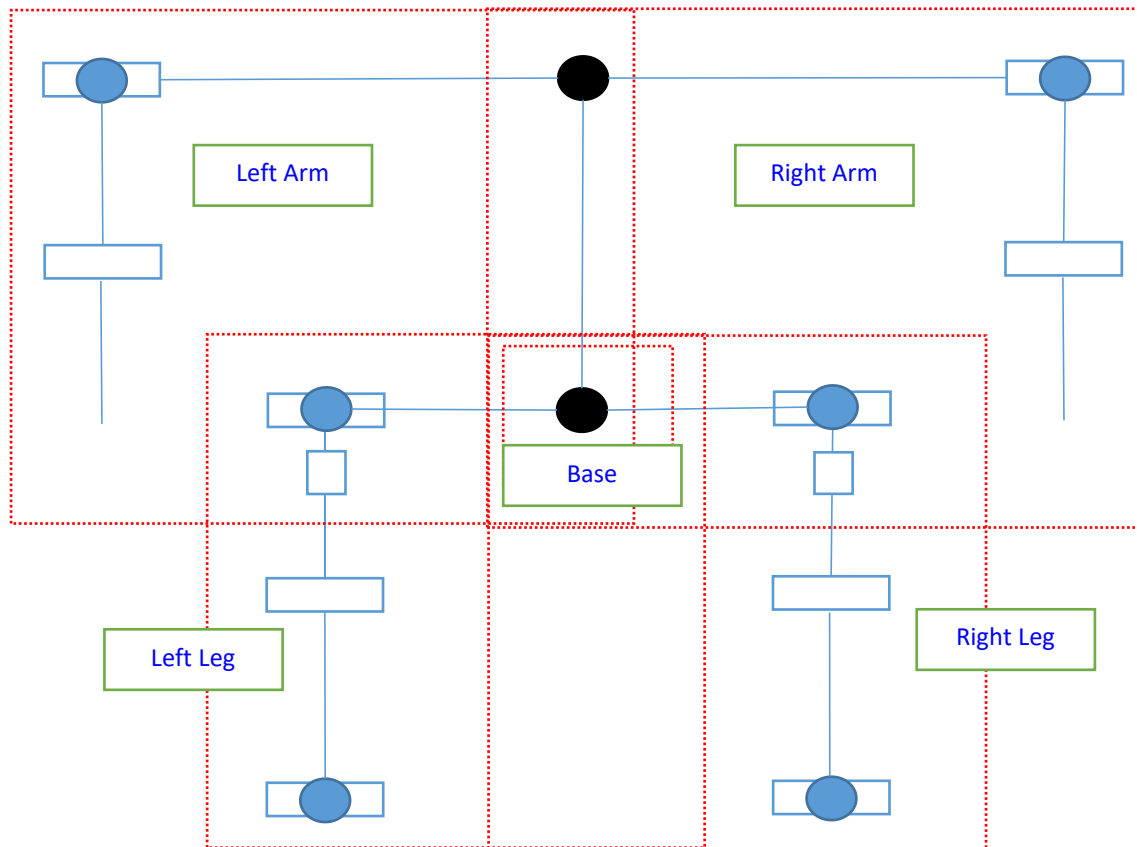


## Solid Works Model



## Free-Body Diagram

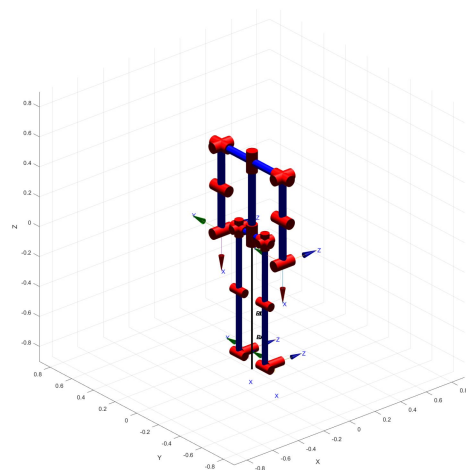
Complete free-body diagram of the humanoid looks like below.



However, we cannot get the DH parameters for the whole robot at once. Therefore, we split it to 5 parts: Left Arm, Right Arm, Base, Left Leg, and Right Leg. Then we can start from the base and apply the DH convention to get the DH parameters for each part.

# Results

# Final Model in MATLAB Teach Toolbox



## Denavit-Hartenberg Parameters

### Platform

platform:: 1 axis, R, modDH, slowRNE

j	theta	d	a	alpha	offset
1	q1	0	0	0	0

### Left Arm

LA:: 6 axis, RRRRRR, modDH, slowRNE

j	theta	d	a	alpha	offset
1	q1	0	0	0	0
2	q2	0.49077	0	0	0
3	q3	-0.283	0	1.57	-1.57
4	q4	0	0	1.57	0
5	q5	0	0.287	1.57	0
6	q6	0	0.287	1.57	0

## Right Arm

RA:: 6 axis, RRRRRR, modDH, slowRNE

j	theta	d	a	alpha	offset
1	q1	0	0	0	0
2	q2	0.49077	0	0	0
3	q3	0.283	0	1.57	-1.57
4	q4	0	0	1.57	0
5	q5	0	0.287	1.57	0
6	q6	0	0.287	1.57	0

## Left Leg

LL:: 8 axis, RRRRRRRR, modDH, slowRNE

j	theta	d	a	alpha	offset
1	q1	0	0	0	0
2	q2	-0.12	0	1.57	0
3	q3	0	0	1.57	-1.57
4	q4	0	0	-1.57	-1.57
5	q5	0	0.42	1.57	0
6	q6	0	0.42	0	0
7	q7	0.0772	0	-1.57	0
8	q8	0	0	0	0

## Right Leg

RL:: 8 axis, RRRRRRRR, modDH, slowRNE

j	theta	d	a	alpha	offset
1	q1	0	0	0	0
2	q2	0.12	0	1.57	0
3	q3	0	0	1.57	-1.57
4	q4	0	0	-1.57	-1.57
5	q5	0	0.42	1.57	0
6	q6	0	0.42	0	0
7	q7	0.0772	0	-1.57	0
8	q8	0	0	0	0

## Jacobian Matrices

### Left Arm

Jacob\_LA =

-0.0002	-0.0002	0	0	0	0
0.0011	0.0011	-0.0014	-0.5740	0.0002	0
-0.2825	-0.2825	0.5740	-0.0009	-0.2870	0
-1.0000	-1.0000	0	0	0	0
-0.0008	-0.0008	-1.0000	0.0016	1.0000	0
0.0008	0.0008	-0.0024	-1.0000	0.0008	1.0000

### Right Arm

Jacob\_RA =

0.0002	0.0002	0	0	0	0
-0.0002	-0.0002	-0.0014	-0.5740	0.0002	0
0.2835	0.2835	0.5740	-0.0009	-0.2870	0
-1.0000	-1.0000	0	0	0	0
-0.0008	-0.0008	-1.0000	0.0016	1.0000	0
0.0008	0.0008	-0.0024	-1.0000	0.0008	1.0000

### Left Leg

Jacob\_LL =

0.0000	-0.0772	-0.0001	0.0000	-0.0772	-0.0772	0	0
0.0764	0.0007	-0.0765	0.8400	0.0003	0	0	0
-0.1193	0.8400	0.0007	0	0.4200	0	0	0
-1.0000	-0.0000	1.0000	0	0	0	0	0
-0.0008	-1.0000	-0.0008	0	-1.0000	-1.0000	0	0
-0.0008	0.0008	0.0008	1.0000	0.0008	0.0008	1.0000	1.0000

### Right Leg

Jacob\_RL =

-0.0002	-0.0772	-0.0001	0.0000	-0.0772	-0.0772	0	0
0.0766	0.0007	-0.0765	0.8400	0.0003	0	0	0
0.1207	0.8400	0.0007	0	0.4200	0	0	0
-1.0000	-0.0000	1.0000	0	0	0	0	0
-0.0008	-1.0000	-0.0008	0	-1.0000	-1.0000	0	0
-0.0008	0.0008	0.0008	1.0000	0.0008	0.0008	1.0000	1.0000