



**Politecnico
di Torino**

A.Y. 2024/25

Electronic Systems for Sensor Acquisition

Prof. Marco Vacca

LAB 01

Analog Temperature Sensor

Components of the working group :

Moussa Swaidan : s334402

Niyousha ebrahimi balsini : s328088

Ammar hussein : s329829

1,1 - Exercise : Active Current Bridge

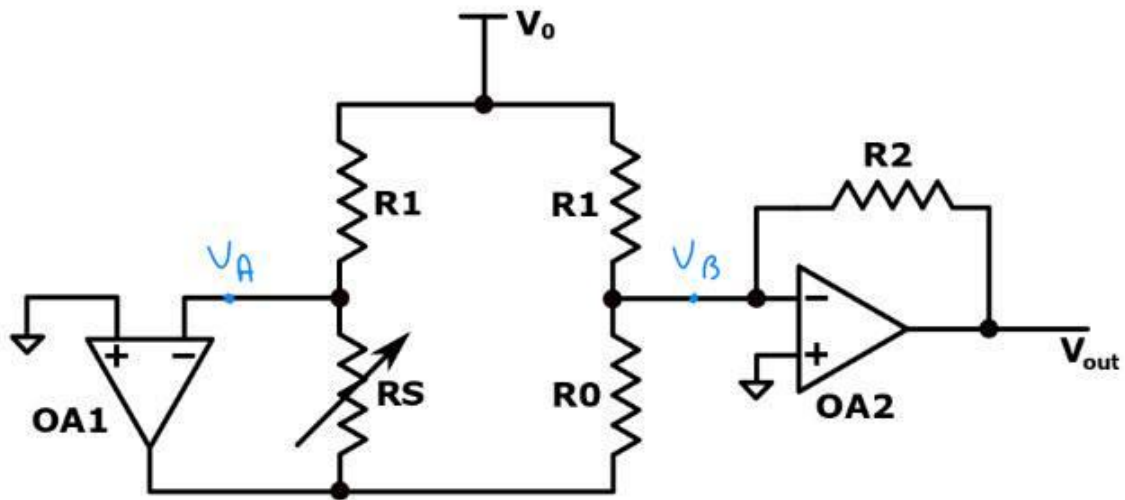


Figure 1 : Active Current Bridge

The specifications of the circuit are the following:

- Sensor type: Pt 1000 temperature sensor
- $R_s = R_0 (1 + \alpha t)$, where $R_0 = R@T_{min}$ (so that the output voltage is always positive) and the average value of $\alpha = 0,00385 \text{ } ^\circ\text{C}^{-1}$
- Current flowing through the sensor must be lower than 1mA to avoid self-heating (much less if you can).
- $V_0 = 10\text{V}$ (obtained from external power supply)
- Temperature range: $T_{min} = 0 \text{ } ^\circ\text{C}$, $T_{max} = 100 \text{ } ^\circ\text{C}$
- $V_{out@T_{min}} = 0\text{V}$
- $V_{out@T_{max}} = 10\text{V}$

From the figure of the specification of the Temperature Sensor PT1000 , We can get the value of the Resistance at $T_{min} = 0 \text{ } ^\circ\text{C}$ We get that :

- $R_0 = 100 \text{ ohms}$
- $R_{s, MIN} = 100 \text{ ohms}$
- $R_{s, MAX} = 138,5 \text{ ohms}$

Node Voltage at Point A (connected to OA1):

The voltage at Point A (let's call it V_A) is the result of a voltage divider between R_1 and R_S :

$$V_A = V_0 \cdot \frac{R_S}{R_1 + R_S}$$

Node Voltage at Point B (connected to OA2):

The voltage at Point B (let's call it V_B) is the result of a voltage divider between R_1 and R_0 :

$$V_B = V_0 \cdot \frac{R_0}{R_1 + R_0}$$

The differential voltage between points A and B is:

$$V_{diff} = V_A - V_B$$

Substituting the values of V_A and V_B :

$$V_{diff} = V_0 \cdot \frac{R_S}{R_1 + R_S} - V_0 \cdot \frac{R_0}{R_1 + R_0}$$

The differential voltage V_{diff} is fed into OA2, which is configured as a non-inverting amplifier with a feedback resistor R_2 . Then , We get the formula of the Output Voltage :

$$V_{out} = -V_{diff} \times \frac{R_2}{R_1}$$

By substituting the value of V_{diff} We get the equation of V_{out} :

$$V_{out} = - \left\{ V_0 \cdot \frac{R_S}{R_1 + R_S} - V_0 \cdot \frac{R_0}{R_1 + R_0} \right\} \cdot \frac{R_2}{R_1}$$

Following the calculation of the Resistances in order to get V_{out} between a minimum value = 0 V and a maximum value = 10 V , And choosing $R_1 = 120 \text{ Kohm}$. We get that $R_2 = 620 \text{ ohm}$

At the end , We have the following values of the resistances of the Resistors :

- $R_0 = 100 \text{ ohm}$, $R_1 = 120 \text{ Kohm}$, $R_2 = 620 \text{ ohm}$, $R_S = \begin{matrix} \text{Min} = 100 \text{ ohm} \\ \text{Max} = 138,5 \text{ ohm} \end{matrix}$

1,2 - Exercise : Voltage Reference

Design a simple voltage reference to be used together with your measurement bridge .

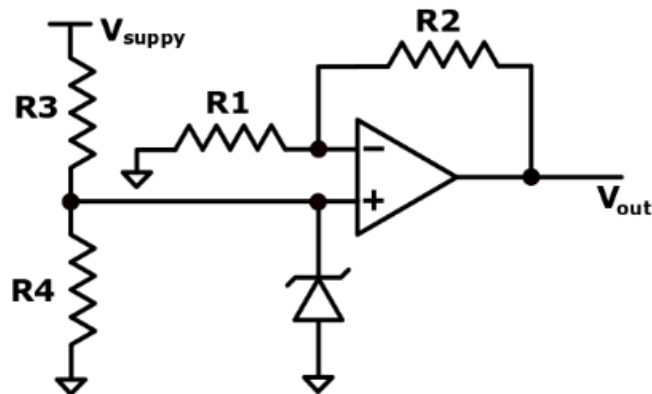


Figure 2 : Simple Voltage Reference

The Specification of this Circuit are the followings :

- V_{out} = 10 V
- Considering that the Zener Diode present in the laboratory is of V_Z = 5 V

Following this consideration We need to force the Voltage that will be limited by the Zener Voltage to be higher than 5V in order for the voltage entering the Operational Amplifier in the positive terminal to be a constant voltage equal to 5V

Voltage Divider (R3 and R4):

- R3 and R4 create a voltage divider from the supply voltage V_{supply} .
- The voltage at the non-inverting input of the op-amp (V₊)

$$V_+ = V_{supply} \cdot \frac{R_4}{R_3 + R_4}$$

The Voltage generator we can set it as $V_{\text{supply}} = 15 \text{ V}$

A possible choice to get V_+ bigger than 5 V , We can choice that $V_+ = 10 \text{ V}$ by choissing $R_3 = 10 \text{ Kohm}$ & $R_4 = 20 \text{ Kohm}$

Considering that We want to get that $V_{\text{out}} = 10 \text{ V}$ as a DC voltage and not alternating for this reason the presence of the Zener Diode in order to limit the voltage entering the positive terminal of the Operational Amplifier :

$$V_+ \approx V_Z$$

Having an Operational Amplifier is working as non-Inverting Amplifier , We get the equation of V_{out} :

$$V_{\text{out}} = V_+ \cdot \left(1 + \frac{R_2}{R_1} \right)$$

Considering that V_+ is set approximately equal to V_Z :

$$V_{\text{out}} = V_Z \cdot \left(1 + \frac{R_2}{R_1} \right)$$

Following that $V_Z = 5 \text{ V}$ & $V_{\text{out}} = 10 \text{ V}$.

Then , Any choice of R_1 & R_2 is accepted with the only constraint of having R_1 and R_2 of equal values

Finally , The chosen values of Resistances of the Resistors in order to respect the specifications of this Design Process :

- $R_1 = 10 \text{ Kohm}$; $R_2 = 10 \text{ Kohm}$; $R_3 = 10 \text{ Kohm}$; $R_4 = 20 \text{ Kohm}$

1.3 – EXERCISE: Analog to Digital Converter

Complete your design by including a simple PWM Analog To Digital Converter as seen during the course. You can use a simple comparator and a sawtooth signal generated by the waveform generator available in the laboratory. The schematic is reported in Figure 3. Remember that this circuit works with positive voltage values.

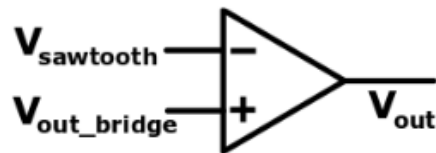


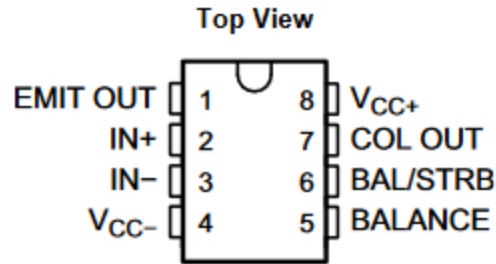
Figure 3 : Comparator

The specifications of the circuit are the following:

- Frequency = 100Hz
- At 100 °C the maximum value of Duty Cycle should be $D_{max} = 100\%$.

Sawtooth Waveform Parameters:

- Frequency: The waveform frequency is given as 100 Hz.
- Period: Since frequency $f=100$ Hz Then We get the period $T= 1/f = 0.01s$ or 10 ms.
- Rise Time and Fall Time: In a sawtooth waveform, the rise time is the duration over which the voltage increases from 0 to the peak, and the fall time is the period of time in which the voltage is zero
- Peak to Peak Voltage: is the voltage between the two extremes of voltage between the maximum and minimum voltage
- Offset: Adjust the offset as needed to align the waveform with the input requirements of the comparator.



- Voltage from Collector output Vcc- = 40 V
- Operating free-air temperature range = [0,70] Celsius

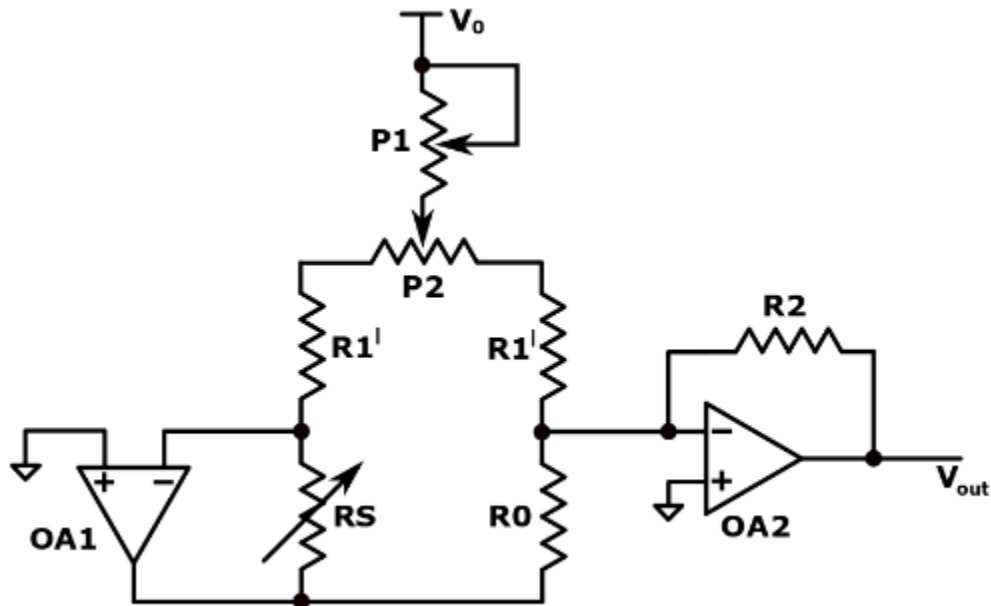
PARAMETER		TEST CONDITIONS		T _A ⁽¹⁾	LM111 LM211 LM211Q			LM311			UNIT
					MIN	TYP ⁽²⁾	MAX	MIN	TYP ⁽²⁾	MAX	
V _{IO}	Input offset voltage	See ⁽³⁾	25°C	0.7		3	2		7.5	mV	
			Full range			4	10				
I _{IO}	Input offset current	See ⁽³⁾	25°C	4		10	6		50	nA	
			Full range			20	70				
I _{IB}	Input bias current	1 V ≤ V _O ≤ 14 V	25°C	75		100	100		250	nA	
			Full range			150	300				
I _{IL(S)}	Low-level strobe current ⁽⁴⁾	V _{I(strobe)} = 0.3 V, V _{ID} ≤ -10 mV	25°C	-3			-3			mA	
V _{ICR}	Common-mode input-voltage range ⁽³⁾	Lower range	Full range	-14.7		-14.5	-14.7		-14.5	V	
		Upper range		13	13.8	13	13.8				
A _{VD}	Large-signal differential-voltage amplification	5 V ≤ V _O ≤ 35 V, R _L = 1 kΩ	25°C	40	200		40	200		V/mV	
I _{OH}	High-level (collector) output leakage current	I _{I(strobe)} = -3 mA, V _{ID} = 5 mV	25°C	0.2		10					nA
			Full range			0.5					μA
		V _{ID} = 5 mV, V _{OH} = 35 V	25°C				0.2		50	nA	
V _{OL}	Low-level (collector-to-emitter) output voltage	I _{OL} = 50 mA	V _{ID} = -5 mV	25°C	0.75		1.5				V
			V _{ID} = -10 mV	25°C				0.75	1.5		
		V _{CC+} = 4.5 V, V _{CC-} = 0 V, I _{OL} = 8 mA	V _{ID} = -8 mV	Full range	0.23		0.4				
			V _{ID} = -10 mV	Full range				0.23	0.4		
I _{CC+}	Supply current from V _{CC+} output low	V _{ID} = -10 mV,	No load	25°C	5.1		6	5.1		7.5	mA
I _{CC-}	Supply current from V _{CC-} output high	V _{ID} = 10 mV,	No load	25°C	-4.1		-5	-4.1		-5	mA

A possible choice for this design exercise could be :

- Rise Time = Fall Time = Half the duration of the Period = 5 ms
- Peak – to – Peak Voltage = An appropriate choice is 10 V

Exercise 1,4 – Error Correction :

For this exercise on **Error Correction using a Bridge Circuit**, you are required to compensate for errors in a bridge configuration. The circuit in Figure 4 aims to address the errors that can arise in sensor systems using discrete components.



Breakdown of the Exercise:

1. Bridge Circuit Overview:

- The bridge consists of resistors R1 & R0, and potentiometers P1 & P2
- The operational amplifier OA2 is used in a differential configuration to output V_{out}, which is sensitive to the balance of the bridge.
- Errors like offset voltage, bias current, sensor mismatches, and component tolerances can affect the accuracy of the bridge output.

2. Compensation Mechanism:

- The potentiometer P1 adjusts the gain of the circuit.
- P2 compensates for errors that unbalance the bridge.
- When the potentiometers are centered, the equivalent resistance of R1 becomes:

$$R_1 = R1' + P2/2 + P1$$

- This configuration provides flexibility in tuning the bridge to minimize errors.

3. Task Requirements:

• Selection of Potentiometers:

- Choose values for P1 and P2 that result in an equivalent resistance close to the original R1 of the bridge.
- If matching R1 precisely isn't possible due to limited potentiometer options, consider adjusting R2 as an alternative.

Detailed Design Steps

1. Bridge Balance and Selection of Potentiometer Values

- The bridge is balanced when the voltage at the midpoints of both branches (across OA1) is the same.
- When potentiometers P1 and P2 are centered, the new effective resistance for R1 becomes:

$$R_1 = R1' + P2/2 + P1$$

- Let's assume the following component values to balance the bridge:
 - $R1' = 1 \text{ Kohm}$
 - $P1 = 500 \text{ Kohm}$
 - $P2 = 1 \text{ Kohm}$

In the middle position, the combined resistance R1 would then be:

$$R_1 = 1 \text{ k}\Omega + \frac{1 \text{ k}\Omega}{2} + 500 \Omega = 2 \text{ k}\Omega$$

By adjusting P1 and P2, you can make small adjustments to R1 to balance the bridge if the measured parameter (like resistance RSR_SRS) shifts due to environmental changes.

2. Gain Adjustment Using OA2

- **Choosing R2 :** The gain of the second operational amplifier OA2 can be set to amplify the differential voltage from OA1.
- For a moderate gain, let's choose $R2=10 \text{ Kohm}$

- The gain can be adjusted based on the desired output voltage range. If needed, add a feedback resistor across OA2 to further control the gain.

3. Compensating for Errors

Errors can arise from:

- **Temperature changes** affecting resistor values.
- **Offset voltages** in the operational amplifiers.
- **Component tolerances** causing mismatches in R_0 , R_1 , or R_S .

The potentiometers P1 and P2 allow for fine-tuning to address these mismatches and bring the bridge back into balance, minimizing the differential voltage across the input of OA1 when the bridge is balanced. This effectively compensates for drift or tolerance variations in R_0 and R_S .

4. Testing and Final Adjustment

- Adjust P1 and P2 experimentally until the output voltage at OA2 is minimized when the bridge is balanced (i.e., when there's no error).
- If the available potentiometer values do not perfectly balance the bridge, you may need to adjust R_0 slightly to achieve a close approximation.

Summary of Component Values

- **R1'**: 1 Kohm (fixed resistor)
- **R0**: 1 Kohm
- **P1**: 500 ohm potentiometer for fine adjustments
- **P2**: 1 Kohm potentiometer for further adjustment
- **R2**: 10 Kohm (gain control for OA2)