ARAMIG KELKELYA MAE 476: Midtenn I 1) Data Head of Disk Dr. Teagle MAE 476-Sec 03 Due: 11/9/2022 a) Find type of system (0,1,2) based on value of K (for which system is stable) # of poles at origin from transfer function = system type $G_1(s) = G_1(s) \cdot G_2(s) = \frac{K(s+a)}{S(s+1)(s+2)(s+3)}$ $\frac{T_{CR} = \frac{K(6+\alpha)}{S(5+1)(6+2)(5+3)}}{1 - \left(-\frac{K(5+\alpha)}{S(5+1)(5+2)(5+3)}\right)} = \frac{K(5+\alpha)}{S(6+1)(5+2)(5+3) + K(5+\alpha)} = \frac{K(5+\alpha)}{(6^2+5)(6^2+55+6) + K5 + K\alpha}$ $Tcl = \frac{K(s+a)}{s^{4} + 6s^{3} + 6s^{2} + 5^{3} + 5s^{2} + 6s + Ks + Ka} = \frac{K(s+a)}{s^{4} + 6s^{3} + 11s^{2} + (6nk)s + Ka}$ $K = \frac{K(s+a)}{s^{4} + 6s^{3} + 6s^{2} + 5^{3} + 5s^{2} + 6s + Ks + Ka} = \frac{K(s+a)}{s^{4} + 6s^{3} + 11s^{2} + (6nk)s + Ka}$ Check Stability: (coeff. are > 0 & all elements in 1st column are > 0) $b_1 = -\frac{1}{\alpha_1} \frac{\alpha_2}{\alpha_3} = -\frac{1}{6} \frac{11}{6+K-66} = \frac{60-K}{6} > 0 = 7K < 60$ 54: 1 11 Ka 53: 6 6+K 0 $b_2 = \frac{1}{a_1} \frac{a_4}{a_5} = \frac{1}{6} \frac{ka}{0} = \frac{6ka}{6} = ka > 0 = > k > 0$ or a < 052: 60-K Ku 0 S': C, O - (too large see variables $C_{1} = \frac{\begin{vmatrix} \alpha_{1} & \alpha_{3} \\ b_{1} & b_{2} \end{vmatrix}}{\begin{vmatrix} \beta_{1} & \alpha_{3} \\ b_{1} & b_{2} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{1} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{2} \\ \beta_{3} & b_{2} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{2} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{2} \\ \beta_{3} & b_{3} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{2} \\ \beta_{3} & b_{3} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{2} \\ \beta_{3} & b_{3} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{2} \\ \beta_{3} & b_{3} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{2} \\ \beta_{3} & b_{3} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{2} \\ \beta_{3} & b_{3} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{2} \\ \beta_{3} & b_{3} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{3} & b_{3} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{3} & b_{3} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{3} & b_{3} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{3} & b_{3} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}} = \frac{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\begin{vmatrix} \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}} = \frac{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}} = \frac{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}} = \frac{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}} = \frac{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}} = \frac{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}} = \frac{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}} = \frac{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}} = \frac{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}} = \frac{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}} = \frac{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}} = \frac{\langle \beta_{2} & \beta_{1} \\ \beta_{2} & b_{3} \end{vmatrix}}{\langle$ Let K=305& a=0.5 Poles: 0=51 - Type 0 -0.8455±1.730=53,4 K2+(36a-54)K-360>0 ess= lim sn+Kv sk solve by quad. (Kis dependent on a formula (Ex: if a = 1 -> K, x-12, (K2>30) Ky= Rim (s. GDCR(S)) $d_1 = \frac{\begin{vmatrix} GO - K & K\alpha \\ G & O \end{vmatrix}}{\begin{vmatrix} C_1 & O \end{vmatrix}} = \frac{C_1 K\alpha}{C_1} = \frac{C_1 K$ Kp=lin (1-30(s+a5) Kp= 15=1 K<60 & K>6 apply extrema K=-6 (60)2-(36a-54).60-360>0 (-6)2+(36a-54)-(=6)-360>0 1. For K=30 4 a=0.5, From testing in MATLAR 3240-(36a-54).60 >0 (36a-64):(-6) > 324 the pystem is stable I have determined that ((36a-54)60>-3240 36a-64 <-- 64 1 and the positioning a is able to reach 36a-54 > -9 (a < 0) emor Kp=1 36a > 45 => (a > 4) .. Range of a can be between these all value if k is selected correctly

3)
$$V_{C_{1}} = \frac{30^{\circ}}{5} = \frac{17}{6} \text{ ad/s}$$
, Assume $K_{+} = 1$, $V = r = 1$ $\left(\frac{k_{8}}{5 \tau_{g+1}} = 1\right)$

$$V_{c} \longrightarrow \frac{K_{c}}{|S_{c}|} + \frac{K_{c}}{|S_{c}|} \longrightarrow \frac{K_{c}}{|S_{c}|$$

$$T_{r} = \mathcal{T}(s) = \frac{K_{\alpha} \left(\frac{K_{m}}{s \tau_{m+1}}\right) | \mathcal{X}_{t}}{1 - \left(-K_{\alpha} \left(\frac{K_{m}}{s \tau_{m+1}}\right) | \mathcal{K}_{t}\right)} = \frac{K_{\alpha} K_{m} K_{t}}{s \tau_{m} + 1 + K_{\alpha} K_{m}}$$

$$\mathcal{T}(s) = \frac{V_{b}(s)}{s \tau_{m} + 1 + K_{b} K_{m}}$$

$$\frac{E}{R} = \frac{1}{1 + GD_{CG}} \implies \frac{E(S)}{V_{C}(S)} = \frac{1}{1 + \frac{Ka Km}{5 Cm^{\frac{1}{2}}}} \implies E(S) = \frac{S C_{m} + 1}{5 C_{m} + 1 + Ka Km} \cdot V_{C}(S)$$

Determine necessary loop gain Kakmkt for step input

$$\frac{1}{180} = \frac{\text{lim}}{5 = 0} \left(\frac{\text{ST}_{m+1}}{\text{ST}_{m+1} + \text{KaKmKt}}, \frac{17}{6} \right)$$

$$\frac{6}{180} = \frac{1}{1 + KaKmKt}$$

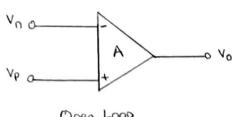
$$\frac{1}{30} = \frac{1}{1 + KaKmKt}$$

necessary loop gain

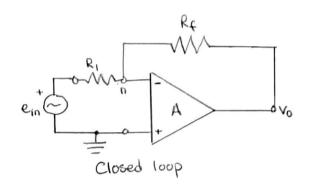
$$\Im(s) = \frac{KaKm}{0.5 \cdot 6 + 1 + KaKm} = \frac{Vb(s)}{Vc(s)}$$

Assume Vo(s) is max at 30%





Open Loop



Node n: Lin=Lout

Current eqn:
$$\frac{ein-v_n}{R_1} + \frac{v_0-v_n}{R_f} = 0$$
, $v_n = \frac{v_0}{G_1}$ (G = op-amp gain)

$$V_0 = \frac{G_1 \left(\frac{R_f}{R_1} \right) e_{in}}{\frac{R_f}{R_1} - G_1}$$

Let K= Ri

Open Loop Sensitivity = Unity = 1 (5 G = 1)

$$S_{G}^{T,cl} = \frac{G}{T} \cdot \frac{dT}{dG} = \frac{G}{T} \cdot \frac{d}{dG} \left(\frac{G}{1 - GK} \right)$$

 $\frac{d}{dG}\left(\frac{G}{1-GK}\right) = \frac{1 \cdot (1-GK) - G(-K)}{(1-GK)^2} = \frac{1}{(1-GK)^2}$

$$K = \frac{R_1}{R_f}$$

$$T.F = \mathcal{Y}(s) = T = \frac{V_0}{e_{in}} = \frac{G_1}{1 - G_i K}$$

$$Cop Sensitivity = Unity = 1$$

$$Cd = \frac{G_1}{1 - G_i K} = \frac{G_1}{1 - G_i K}$$

$$Cd = \frac{G_1}{1 - G_i K} = \frac{1}{1 - G_i K}$$

.. Closed loop sensitivity is much smaller than that of the open leop.

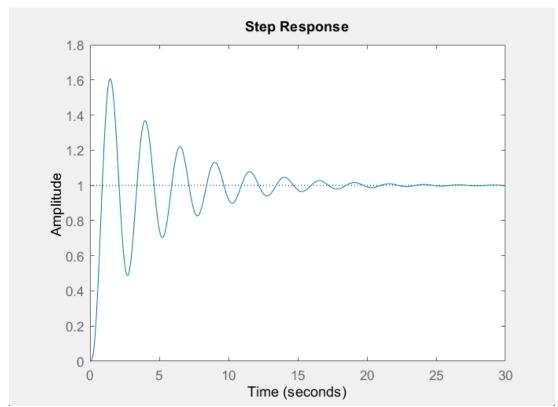
Find sensitivity due to changes in R, , ST. Comment on Sensitivity, especially when GIK>>1.

$$S_{G}^{Tcc} = \frac{1}{1 - G_{1}\left(\frac{R_{1}}{R_{c}}\right)} = \frac{1}{1 - \frac{V_{0}\left(\frac{R_{1}}{R_{c}}\right)}{V_{0}\left(\frac{R_{1}}{R_{c}}\right)}}$$

$$G_{1} = \frac{V_{0}}{V_{0}}$$

 $S_{G}^{TCL} = \frac{1}{1 - G_{G}(\frac{R_{1}}{R_{F}})} = \frac{1}{1 - \frac{V_{O}(R_{1})}{V_{N}(R_{F})}} = \frac{1}{V_{N}(\frac{R_{1}}{R_{F}})} = \frac{1}{V_{N}(\frac{R_{1}}{R_{1}})} =$

```
MidtermP1.m * MidtermP2.m
                              × +
 1
 2
 3
 4
 5
 6
 7
          clear;clc;
 8
 9
          K = 30;
10
          a = 0.5;
11
12
          num = [K K*a];
13
          den = [1 \ 6 \ 11 \ 6+K \ K*a];
14
          sys = tf(num,den);
15
          poles_are=pole(sys);
16
          roots_char_eqn = roots(den);
17
          disp(roots_char_eqn);
18
19
          step(sys);
20
21
22
```



```
1
          % Aramis Kelkelyan
 2
          % MAE 476: Midterm
 3
          % Problem 2
 4
          % Date: 11/8/2022
 5
 6
          clear;clc;
 7
 8
 9
          kp = 7;
10
          sys = tf([kp],[1 5+kp]);
11
          clp = feedback(sys,1);
12
          figure(1);
13
          step(clp);
14
15
          % part g)
16
          kI = 0; kp2 = 7;
17
          sys = tf(12, [1 12]);
18
          clp = feedback(sys,2);
19
          figure(2);
20
          step(clp);
21
22
```

Graphs on the next page

