

Resistive Load Inverter

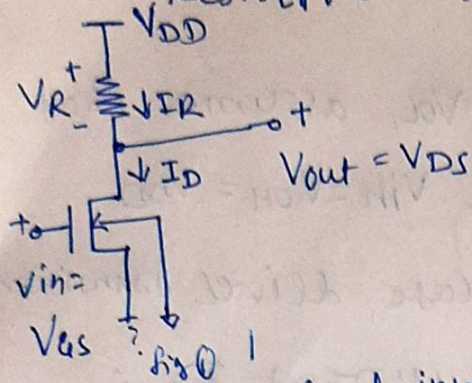


Fig: Resistive load inverter.

$$I_{Dsat} = \frac{k_n}{2} (V_{gs} - V_t)^2 \quad \text{--- (A)}$$

$$I_{Dlin} = \frac{k_n}{2} \left[2(V_{gs} - V_t) \cdot \frac{V_{ds} - V_{dsat}}{V_{dsat}} \right] \quad \text{--- (B)}$$

$$= \frac{k_n}{2} [2(V_{in} - V_t) \cdot (V_{out} - V_{out,sat})] \quad \text{--- (C)}$$

Calculation of V_{OH}

o/p voltage V_{out} is given by

$$V_{out} = V_{DD} - R_L I_D$$

When the i/p voltage V_{in} is low than the threshold voltage of the driver MOSFET the driver transistor is cut off. Since the drain current of the driver transistor is equal to the load current $I_R = I_D = 0$

Put I_D in eqn (1), eqn (1) & (2)

$\therefore V_{out} = V_{OH} = V_{DD}$

operating Regions of the driver transistor in the resistive-load inverter.

i/p voltage range

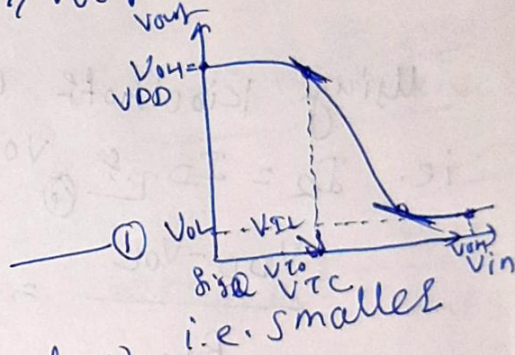
Region
cut-off

$$V_{in} < V_{TO}$$

$$V_{TO} \leq V_{in} < V_{out} + V_{TO}$$

Saturation
Linear

$$V_{in} \geq V_{out} + V_{TO}$$



Calculation of V_{OL}

To calculate the o/p low voltage V_{OL} , assume that the i/p voltage is equal to V_{OH} . i.e. $V_{in} = V_{OH} = V_{DD}$.

Since $V_{in} - V_{TO} > V_{out}$ in this case driver transistor operates in the linear region. current I_R is

$$I_R = \frac{V_{DD} - V_{out}}{R_L} \quad \text{--- (3)}$$

Using Kirchhoff's current law (KCL) for the o/p node, i.e. $I_R = I_D$ if $V_{out} = V_{OL}$ (4)

$$\frac{V_{DD} - V_{OL}}{R_L} = \frac{k_n}{2} [2(V_{DD} - V_{TO}) \cdot V_{OL} - V_{OL}^2] \quad \text{--- (5)}$$

$$\therefore \cancel{\frac{k_n}{2}} \left(\frac{V_{DD} - V_{OL}}{R_L} \right) \frac{2}{k_n} = 2(V_{DD} - V_{TO}) \cdot V_{OL} - V_{OL}^2 \quad \text{--- (6)}$$

$$\therefore V_{OL}^2 - 2(V_{DD} - V_{TO})V_{OL} + \frac{2}{k_n R_L} (V_{DD} - V_{OL}) = 0 \quad \text{--- (7)}$$

$$V_{OL}^2 - \left[2(V_{DD} - V_{TO}) + \frac{2}{k_n R_L} \right] V_{OL} + \frac{2}{k_n R_L} V_{DD} = 0 \quad (8)$$

in eqn (8)

$$a=1, \quad b = - \left[2(V_{DD} - V_{TO}) + \frac{2}{k_n R_L} \right], \quad c = \frac{2 V_{DD}}{k_n R_L}$$

$$\text{Roots} = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a} \quad (9)$$

$$= \frac{-b \pm \sqrt{4 \left\{ (V_{DD} - V_{TO}) + \frac{1}{k_n R_L} \right\}^2 - 4(1) \left(\frac{2 V_{DD}}{k_n R_L} \right)}}{2}$$

$$= \frac{2 \left[(V_{DD} - V_{TO}) + \frac{1}{k_n R_L} \right] \pm 2 \sqrt{\left\{ (V_{DD} - V_{TO}) + \frac{1}{k_n R_L} \right\}^2 - \frac{2 V_{DD}}{k_n R_L}}}{2}$$

$$V_{OL} = V_{DD} - V_{TO} + \frac{1}{k_n R_L} - \sqrt{\left\{ (V_{DD} - V_{TO}) + \frac{1}{k_n R_L} \right\}^2 - \frac{2 V_{DD}}{k_n R_L}} \quad (10)$$

Calculation of V_{IL} :

V_{IL} is the smaller of the two i/p voltage values at which the slope of the VTC becomes equal

(-1) i.e. $\frac{dV_{out}}{dV_{in}} = -1$ from fig (1) When $V_{in} = V_{IL}$,

V_{out} is $< V_{OH}$, $V_{out} > V_{in} - V_{TO}$, driver transistor operate in saturation.

By Applying KCL at o/p node

$$I_R = I_D$$

$$\frac{V_{DD} - V_{out}}{R_L} = \frac{k_n}{2} (V_{gs} - V_{to})^2 \quad \text{--- (11)}$$

$V_{gs} = V_{in}$

$$\frac{V_{DD} - V_{out}}{R_L} = \frac{k_n}{2} (V_{in} - V_{to})^2 \quad \text{--- (12)}$$

differentiate both sides of eqn (12) w.r.t. V_{in} ,

$$\frac{d}{dV_{in}} \left(\frac{V_{DD} - V_{out}}{R_L} \right) = \frac{d}{dV_{in}} \left[\frac{k_n}{2} (V_{in} - V_{to})^2 \right] \quad \text{--- (13)}$$

$$-\frac{1}{R_L} \frac{dV_{out}}{dV_{in}} = \frac{k_n}{2} \left[2(V_{in} - V_{to}) \cdot (1) \right]$$

at $V_{in} = V_{IL}$ & $\frac{dV_{out}}{dV_{in}}$ eqn (13) \Rightarrow

$$-\frac{1}{R_L} (-1) = \frac{k_n}{2} [2(V_{IL} - V_{to})]$$

$$+\frac{1}{k_n R_L} + V_{to} = V_{IL}$$

$$\therefore V_{IL} = V_{to} + \frac{1}{k_n R_L} \quad \text{--- (14)}$$

by substituting eqn (14) in eqn (11) : eqn (11)

$$V_{out} = V_{DD} - \frac{k_n R_L}{2} \left(V_{to} + \frac{1}{k_n R_L} - V_{to} \right)^2$$

$$V_{out}|_{V_{in}=V_{IL}} = V_{DD} - \frac{1}{2k_n R_L}$$