The primary position variables are (x, y, s), where x and y are the displacements along the normal and binormal vectors
Let $\boldsymbol{t}$ denote the tangential vector along s, then $\boldsymbol{n}$, $\boldsymbol{b}$, $\boldsymbol{t}$ consist a right-handed system.
The action in t is expressed by

$$S = \int L_t c dt ,$$
$$L_t = -\frac{mc}{p_0}\sqrt{1 - \dot{x}^2 + \dot{y}^2 + (1 + x/\rho)^2 \dot{s}^2} + a_x\dot{x} + a_y\dot{y} + (1 + x/\rho)a_s\dot{s} ,$$

where p_0 and $(a_x, a_y, a_z) = e(A_x, A_y, A_z)/p_0$ are the design momentum and the normalized vector potentials, respectiv
derivative by ct. SAD's coordinate only has the radius of curvature ρ in the local x-s plane. Note that ρ is the curvature of
not that of the orbit. The transverse vector potentials (a_x, a_y) are non-zero only in the solenoid region, where $1/\rho$ is zero.
Currently SAD does not handle the electrostatic potential.
As SAD uses s for the independent variable instead of t, the Lagrangean L for s is written as

$$\begin{aligned} L =& L_t\frac{dct}{ds} , \\ =& -\frac{mc}{p_0}\sqrt{c^2t'^2 - x'^2 + y'^2 + (1 + x/\rho)^2} + a_x x' + a_y y' + (1 + x/\rho)a_s , \end{aligned}$$

where $'$ is the derivative by s.