# A Comparison on Fuel Economy and Emissions for Conventional Hybrid Electric Vehicles and the UTS Plug-in Hybrid Electric Vehicle

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Abstract—This paper covers a comparative study on fuel economy and emissions of a conventional hybrid electric vehicle (HEV) and the UTS plug-in HEV (PHEV). The interaction between the components such as energy storage system, electric machine, power control unit and internal combustion engine of the UTS PHEV are complex in order to optimize the fuel economy and emissions brought by the vehicle. In this work, the model of the UTS PHEV is derived and implemented numerically in the MATLAB/SIMULINK environment to study its operational performance in various drive cycles measured under life conditions. The simulation results in terms of fuel economy and emissions of the series and parallel HEV from the Advanced Vehicle Simulator and UTS PHEV are compared and the pros and cons discussed.

Keywords- hybrid electric vehicle; plug-in hybrid electric vehicle; powertrain; energy management strategy; fuel economy; emissions

## I. INTRODUCTION

Figures 1-3 show the block diagrams for a series hybrid electric vehicle (HEV), parallel HEV and the proposed UTS plug-in HEV (PHEV). These block diagrams consist of an energy storage system (ESS), a power control unit (PCU), one or two electric machines (EMs) and an internal combustion engine (ICE) [1,2]. The series HEV model contains two separate EMs, which are used as the motor and generator, respectively, and an ESS with no ultracapacitor bank. The proposed UTS PHEV, however, has only one EM which functions as either a motor or generator at a time and in the ESS there is an ultracapacitor bank for fast charging and discharging during the regenerative braking and fast acceleration. The full size of ICE in a parallel HEV is required because when the state of charge (SOC) of the ESS

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is low, the ICE will move the vehicle alone. The ICE in UTS PHEV can move the vehicle while charging the ESS until the ESS SOC reaches a high level and the EM will take over to move the vehicle. A special energy management strategy (EMS) for the UTS PHEV is needed in order to save the weight, space and cost while improving the fuel economy and emissions.

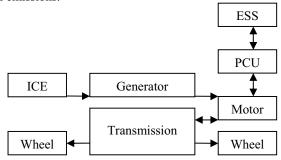


Figure 1. Block diagram of the series HEV configuration

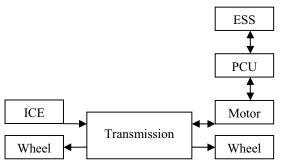


Figure 2. Block diagram of the parallel HEV configuration

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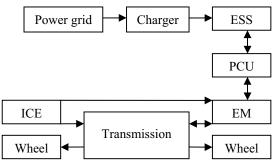


Figure 3. Block diagram of the UTS PHEV configuration

## II. ADVISOR VEHICLE MODEL

The Advanced Vehicle Simulator (ADVISOR) is a software package based on the MATLAB/SIMULINK, originally developed by the U.S. Department of Energy (DOE) and the National Renewable Energy Laboratory (NREL), to simulate and analyze light and heavy vehicles, including hybrid and fuel cell vehicles [3]. It allows the user to perform rapid analysis of the performance, emissions and fuel economy of conventional, electric and hybrid vehicles [4].

The ADVISOR model has been validated and used as a benchmark of reference model. The ADVISOR model vehicle contains two separate Ems, which are used as the motor and generator, respectively, and an ESS with no ultracapacitor bank. The UTS PHEV, however, has only one EM which functions as either a motor or generator at a time, specified by the special EMS, and there is an ultracapacitor bank in the ESS.

To simulate the UTS PHEV, we have derived a model, and verified the model by comparing the simulation results with those of the ADVISOR HEV.

Another difference between the ADVISOR and the UTS PHEV model is that ADVISOR utilizes backward looking vehicle simulation architecture, while the UTS PHEV model performs a forward vehicle simulation.

## III. UTS PHEV VEHICLE MODEL

The vehicle type selected is an average 5-passenger sedan, which is the majority of vehicles on road. Table 1 lists the parameters of a typical of this type. In the simulation, the air drag density is chosen as  $1.2 \text{ kg/m}^3$ , and the gravitational acceleration  $9.81 \text{ m/s}^2$  [5].

TABLE I. PARAMETERS OF AN AVERAGE 5-PASSENGER SEDAN

Name	Value	Units

Aerodynamic drag coefficient	0.335	-
Coefficient of rolling resistance	0.009	-
Frontal area	2.00	m <sup>2</sup>
Wheel radius	0.282	m
Vehicle mass	1379	kg

The development of vehicle model begins with the calculations of vehicle energy and power requirements for typical driving conditions based on the parameters and target specifications of the vehicle. The size and capacity of each vehicle component are then determined through a power flow analysis accordingly to meet the requirements. Combining the constitutive equations of all components, we obtain a mathematical model of the vehicle. The vehicle performance for a given EMS and driving cycle is simulated in the MATLAB/SIMULINK environment. Figure 4 shows the UTS PHEV model in the MATLAB/SIMULINK environment [6-8].

#### IV. EMS FOR THE UTS PHEV

The EMS is responsible for deciding in which mode that the vehicle is operating. Figure 5 shows various operating modes of the proposed EMS to control the distribution of power amongst the components, including the mechanical braking, regenerative braking, EM only, ICE recharge, ICE and EM assist and ICE only mode according to the vehicle power demand in cruising or braking and the SOC level of ESS [9-11].

#### V. MODEL VERIFICATION

For a comparative study, the UTS PHEV code is modified to incorporate the conventional HEV model and energy management scheme.

# A. Drive Cycles

Two standard U.S. Environmental Protection Agency (EPA) drive cycles: the high way fuel economy test (HWFET) and urban dynamometer driving schedule (UDDS) for highway and city driving are simulated to determine the fuel economy and emissions brought by the vehicles. Figures 6 and 7 illustrate the time history of the HWFET and UDDS drive cycles. The HWFET drive cycle ends at 765 seconds and the UDDS at 1369 seconds.

# B. Vehicle Performance

Figures 6 and 7 illustrate the simulation results for two standard U.S. EPA drive cycles in terms of the vehicle speed and force, ESS current, voltage, power and SOC, EM speed, torque and power, wheel speed and torque and the acquired and required speeds.

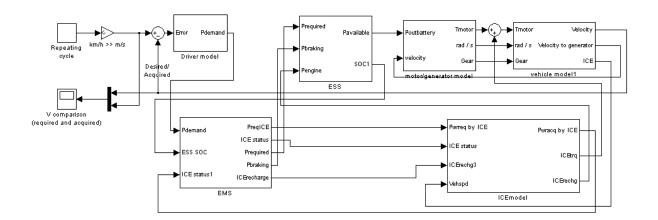


Figure 4. The UTS PHEV model in MATLAB/SIMULINK

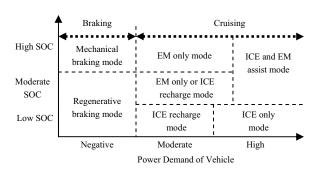


Figure 5. EMS for the UTS PHEV

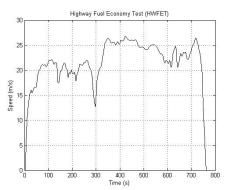


Figure 6. The HWFET drive cycle

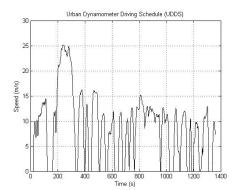


Figure 7. The UDDS drive cycle

As shown in Figures 8 and 9, the actual vehicle speed and force of the HWFET and UDDS drive cycles simulated by the ADVISOR (red lines) and the UTS PHEV model (blue lines) agree well with each other, as expected.

# C. Energy Storage System

From the ESS current, voltage and output power in Figures 8 and 9, one can deduce that the peak currents are due to the high power demand to achieve fast vehicle accelerations during the respective periods. The negative values on the graph represent the regenerative braking events during the hard braking periods in the cycle. In the ESS voltage graph, the voltage increases during recharging from regenerative braking and decreases during high current discharge when the power demand from EM is at peak.

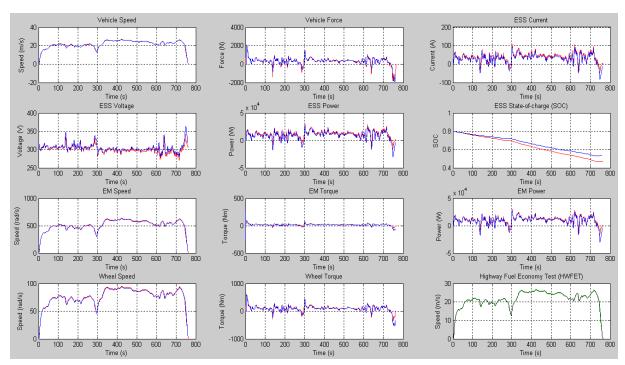


Figure 8. Simulation results of the HWFET drive cycle (Red line: ADVISOR, Blue line: UTS PHEV, Green line: acquired speed, and Black line: required speed)

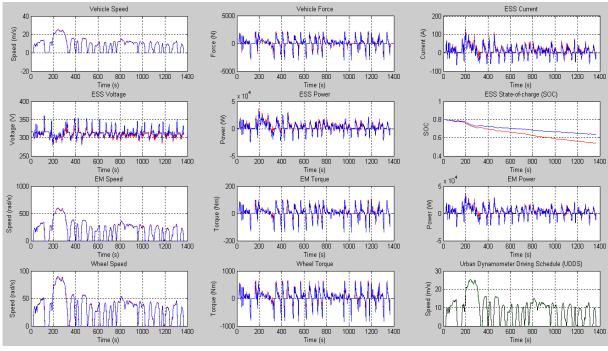


Figure 9. Simulation results of the UDDS drive cycle (Red line: ADVISOR, Blue line: UTS PHEV, Green line: acquired speed, and Black line: required speed)

The SOC of the battery system of the two vehicle configurations during the HWFET and the UDDS drive cycles are shown in Figures 8 and 9. The overall trend of the energy consumption and generation of the two models

matches reasonably well. However, there is some discrepancy between the battery SOC results of the UTS PHEV and conventional HEV in the HWFET drive cycle.

This is because the UTS PHEV code has a better EMS and can capture more regenerative braking energy.

#### D. Electric Machine

The EM speed, torque and power of the ADVISOR and UTS PHEV code for the HWFET and UDDS drive cycles are included in Figures 8 and 9. As shown in the simulation results, when the vehicle accelerates, the required EM torque increases quickly, and when the vehicle reaches the relatively stable highway velocity level, a much smaller torque is required to overcome the resistance and air drag to the vehicle. The speed, torque and power results from the two codes match reasonably well.

## E. Wheels

Figure 8 depicts the wheel speed and torque requirement for the HWFET drive cycle of the two codes. The maximum wheel torque, 600Nm, occurs when the vehicle is accelerating from standstill to the highway speed. The required torque then reduces since the HWFET drive cycle only consists of mild accelerations and decelerations. The overall results and trends match very closely. Figure 9 shows the wheel and torque required during the UDDS drive cycle and the results from both ADVISOR and UTS PHEV codes match very well.

#### F. Remarks

From Figures 8 and 9, it can be seen that the acquired and required speeds agree reasonably well. The UTS PHEV code followed the desired drive cycle speed very well for both standard drive cycles. In combination with the previous discussion, it can be concluded that the results of the UTS PHEV code are correct and the components of the vehicle subsystems are correctly sized as the vehicle is capable of achieving performance to a target velocity.

## VI. A COMPARISON ON FUEL ECONOMY AND EMISSIONS

This study compares the fuel economy and emissions, such as hydro-carbon (HC), carbon-monoxide (CO) and nitrogen-dioxide (NO $_{\rm x}$ ) for the conventional HEV and the UTS PHEV, for the HWFET, UDDS and a cobination of UDDS and HWFET drive cycles. The combined drive cycle is determined by weighting the city at 55% and the highway at 45% as the following

$$FE_{combined} = \frac{1}{\frac{0.55}{FE_{city}} + \frac{0.45}{FE_{highway}}} \tag{1}$$

Note that the SOC values are part of the EMS parameters. Although not related to component sizing, they have a direct impact on the fuel economy and emissions of the UTS PHEV design. The EMS for each configuration is different. The UTS PHEV is simulated using a specially developed EMS. The fuel economy and emissions for different drive cycles are given in Tables 2-4.

TABLE II. FUEL ECONOMY AND EMISSIONS COMPARISON FOR THE HWFET DRIVE CYCLES

Configuration	Fuel economy (mpg)	HC (g/mile)	CO (g/mile)	NO <sub>x</sub> (g/mile)
Series	50	0.241	0.359	0.192
Parallel	66	0.240	0.277	0.120
UTS PHEV	68	0.212	0.314	0.114

TABLE III. FUEL ECONOMY AND EMISSIONS COMPARISON FOR THE UDDS DRIVE CYCLES

Configuration	Fuel economy (mpg)	HC (g/mile)	CO (g/mile)	NO <sub>x</sub> (g/mile)
Series	55	0.266	0.468	0.232
Parallel	54	0.330	0.372	0.130
UTS PHEV	90	0.254	0.238	0.055

TABLE IV. FUEL ECONOMY AND EMISSIONS COMPARISON FOR THE COMPOSITE DRIVE CYCLES

Configuration	Fuel economy (mpg)	HC (g/mile)	CO (g/mile)	NO <sub>x</sub> (g/mile)
Series	53	0.254	0.412	0.212
Parallel	59	0.282	0.322	0.125
UTS PHEV	79	0.233	0.267	0.072

A significant improvement in the fuel economy and emissions were achieved by the UTS PHEV model. Based on the analysis results, the following observations can be made. The fuel economy of the UTS PHEV is about 26% higher than that of the series HEV, 3% higher than the parallel HEV for the UDDS drive cycle, while for the HWFET drive cycle, it is 39% higher than that of the series HEV and 40% higher than the parallel HEV. The improvement for fuel economy for the combined drive cycle is 33% higher than the series HEV and 25% higher than the parallel HEV.

The ultracapacitor bank played a helpful role in the improvement of fuel economy and emissions. The series and parallel HEV has only the battery in the ESS system while the UTS PHEV has both the battery and ultracapacitor bank in the ESS system.

## VII. CONCLUSION

The results of the vehicle subsystems in terms of ESS current, voltage, output power and SOC, EM speed and torque, vehicle speed and force and wheels speed and torque are within reasonable and expected range of actual typical behavior of these subsystems. The components of the vehicle subsystems are correctly sized as the vehicle is capable of achieving performance to a target velocity. In combination with previous discussion, it can be concluded that results of the UTS PHEV code are correct.

The fuel economy and emissions for the UDDS, HWFET and combined drive cycles are improved significantly.

#### ACKNOWLEDGMENT

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