

# **ECE 65: Components & Circuits Lab**

## **Lecture 17**

### **Transistor Amplifiers – Introduction**

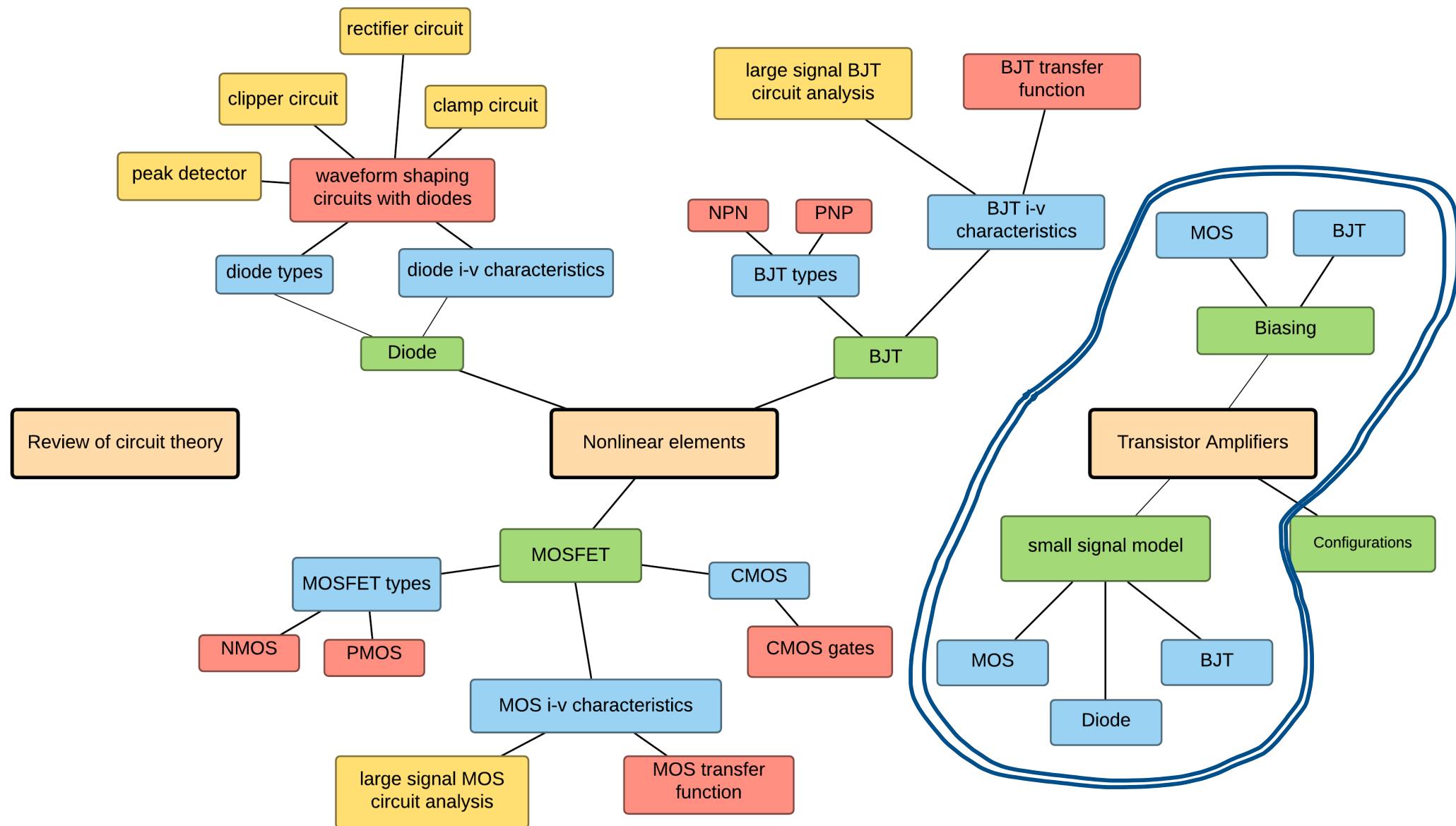
Reference notes: sections 5.1, 5.2

Sedra & Smith (7<sup>th</sup> Ed): sections 7.1

Saharnaz Baghdadchi

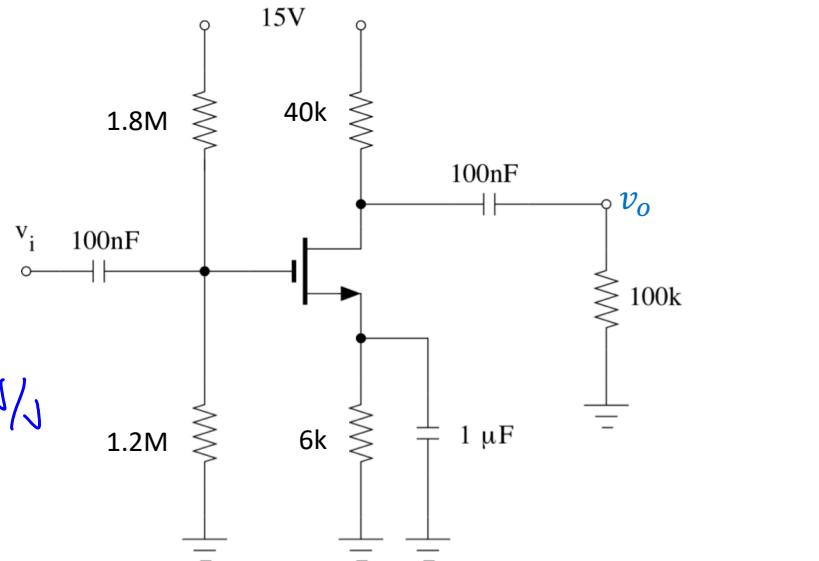
# Course map

## 5. Transistor Amplifiers – Bias and small signal

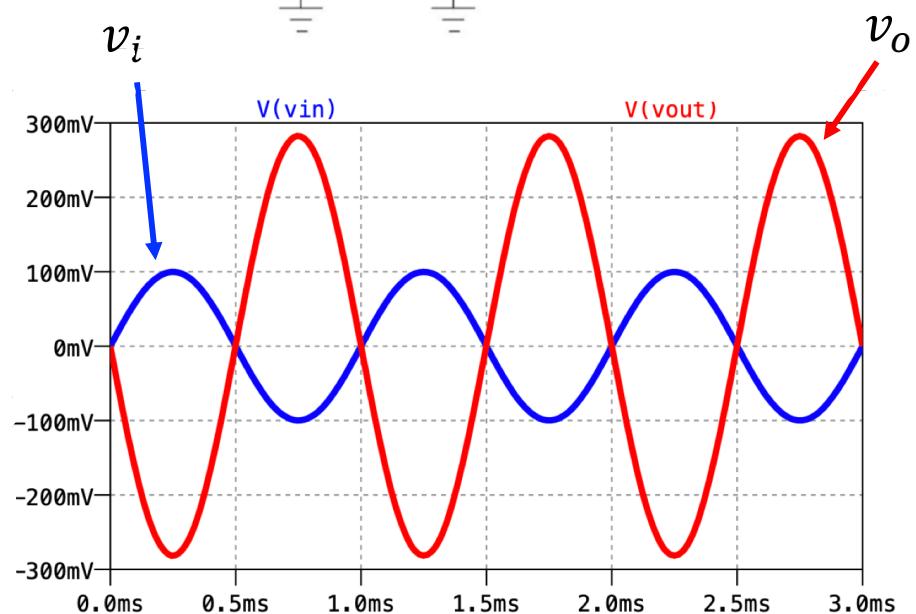
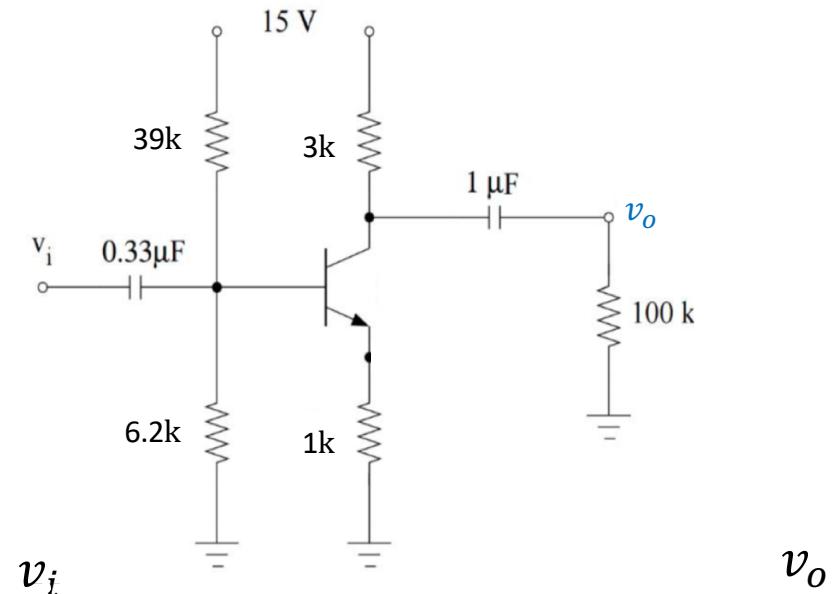


# Transistor Amplifiers

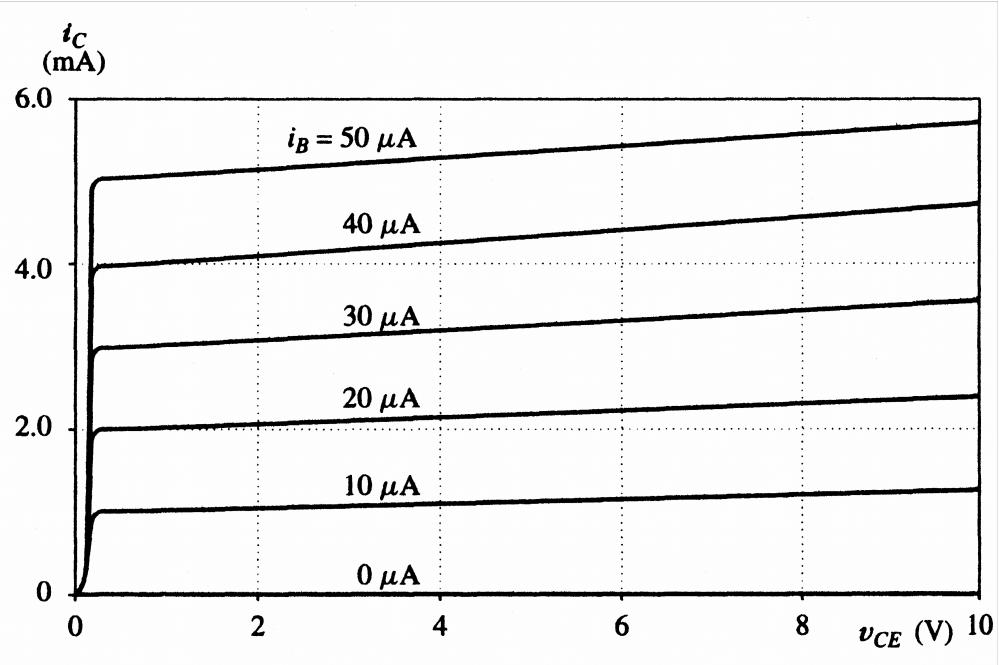
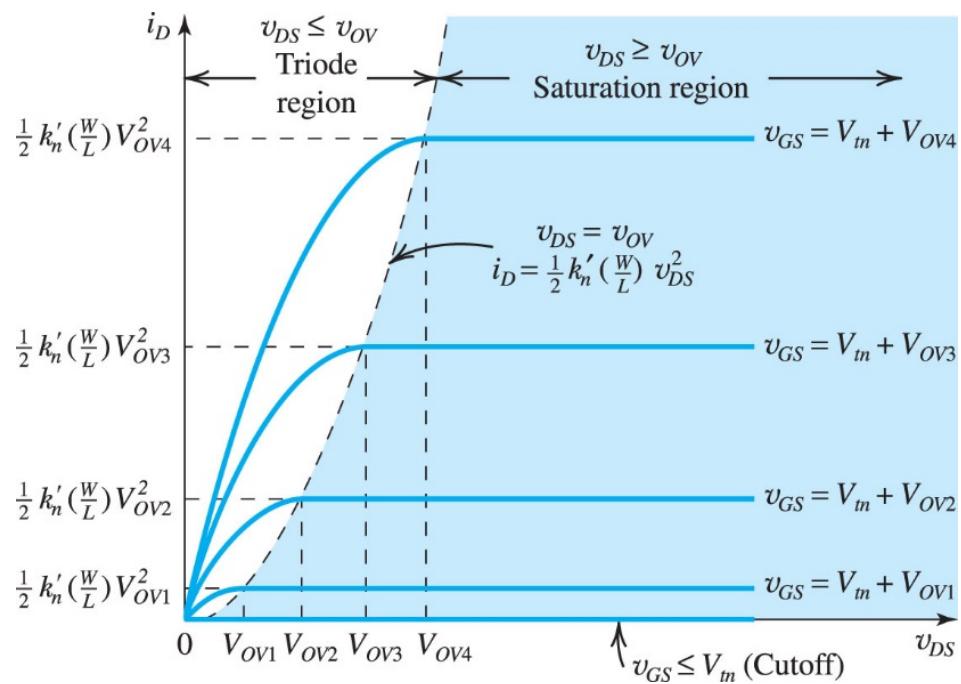
MOSFET as an amplifier



BJT as an amplifier

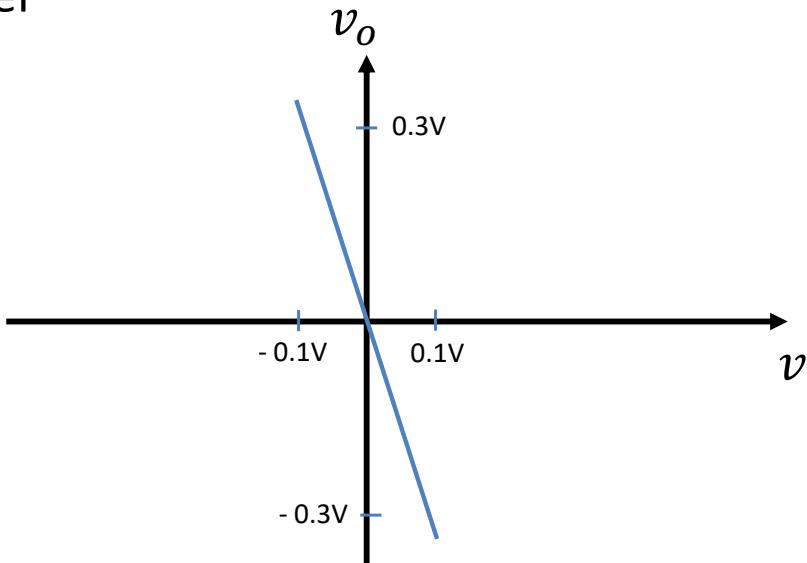


# In the active region, BJT and MOSFET operate as a voltage-controlled current source

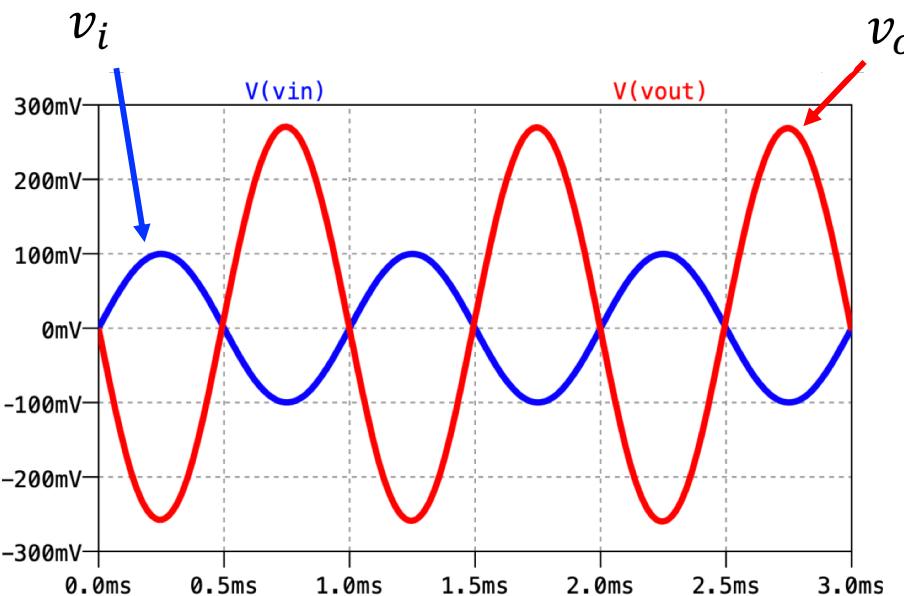
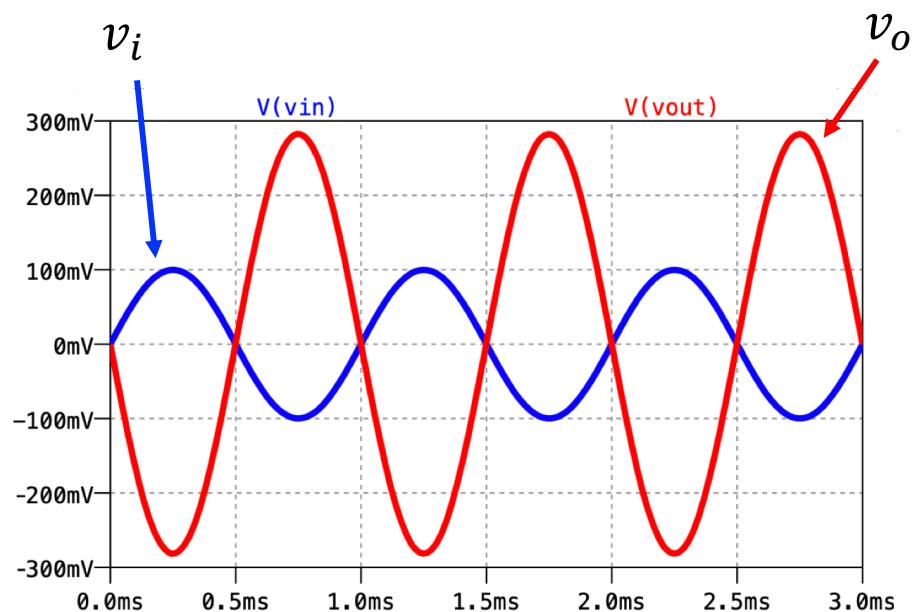


# Transistor Amplifiers

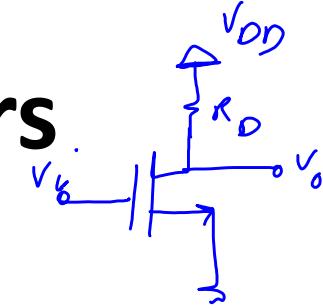
MOSFET as an amplifier



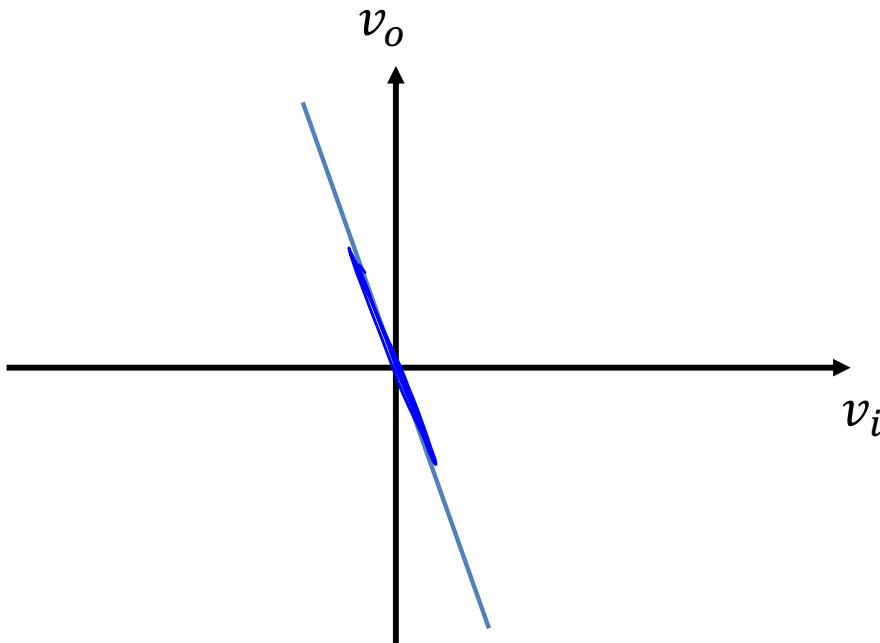
BJT as an amplifier



# Foundation of Transistor Amplifiers

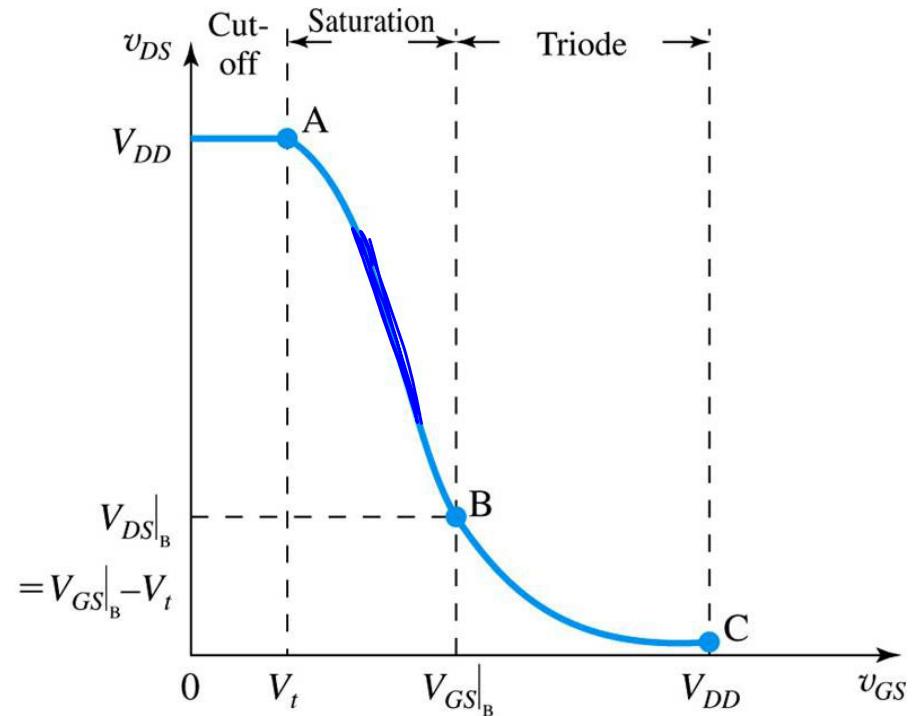


A voltage amplifier requires  
 $v_o/v_i = \text{const.}$



$v_o/v_i$  can be negative (minus sign represents a 180° phase shift)

MOS transfer function is NOT linear

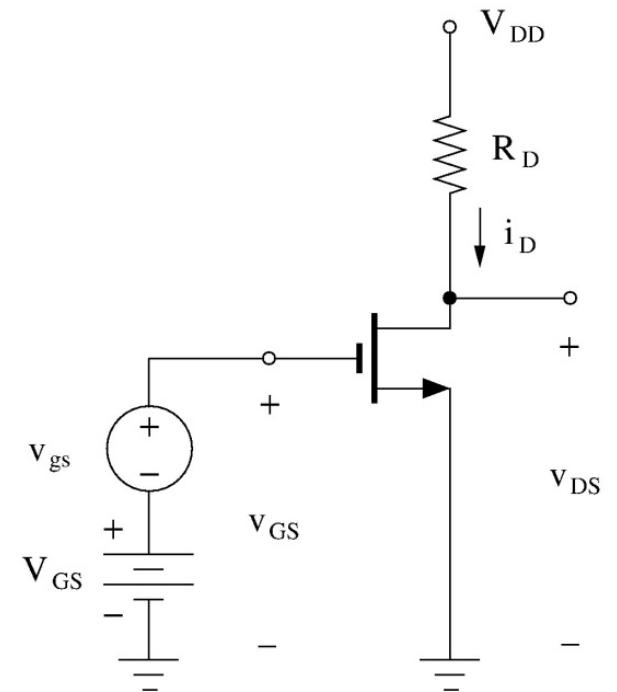
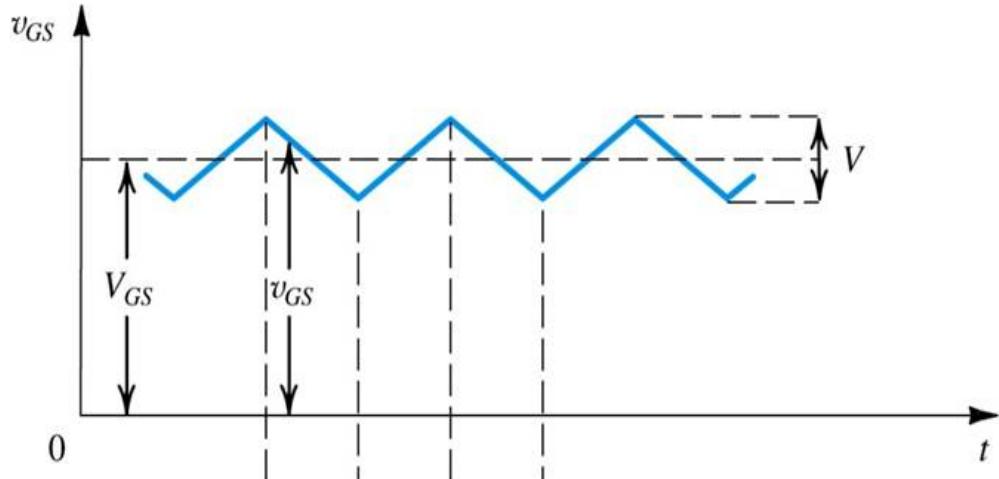


In saturation, however, transfer function looks linear (but shifted)

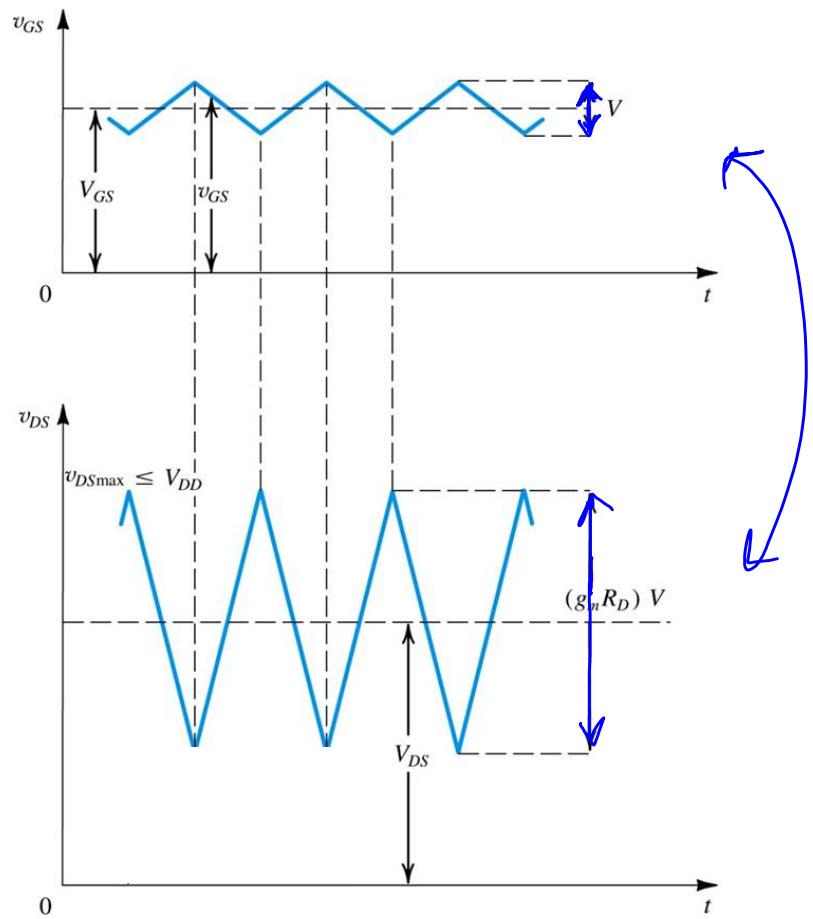
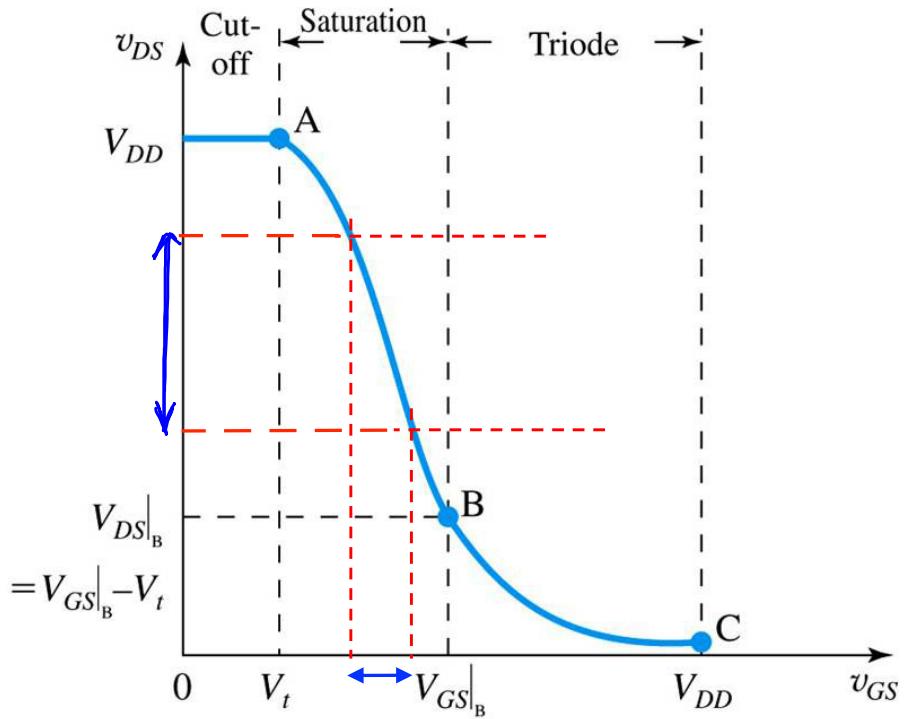
# Foundation of Transistor Amplifiers

Let us consider the response, if NMOS remains in saturation at all times and  $v_{GS}$  is a combination of a **constant value** ( $V_{GS}$ ) and a signal ( $v_{gs}$ ):

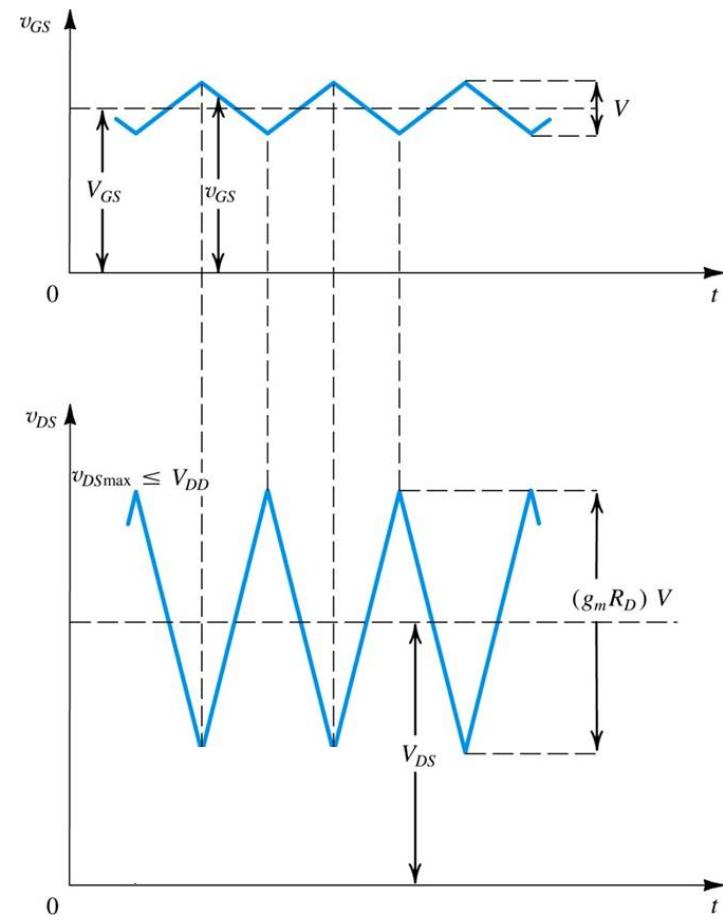
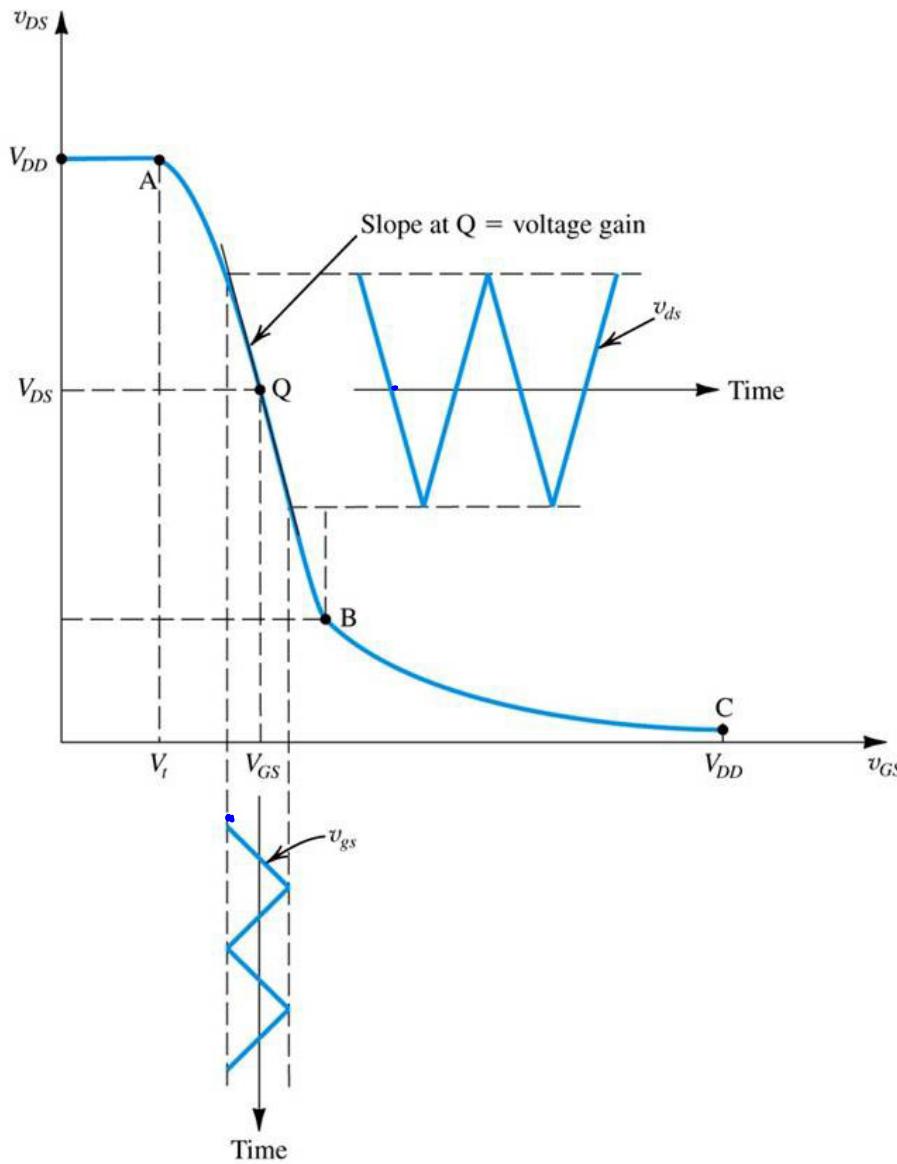
$$v_{GS} = V_{GS} + v_{gs}$$



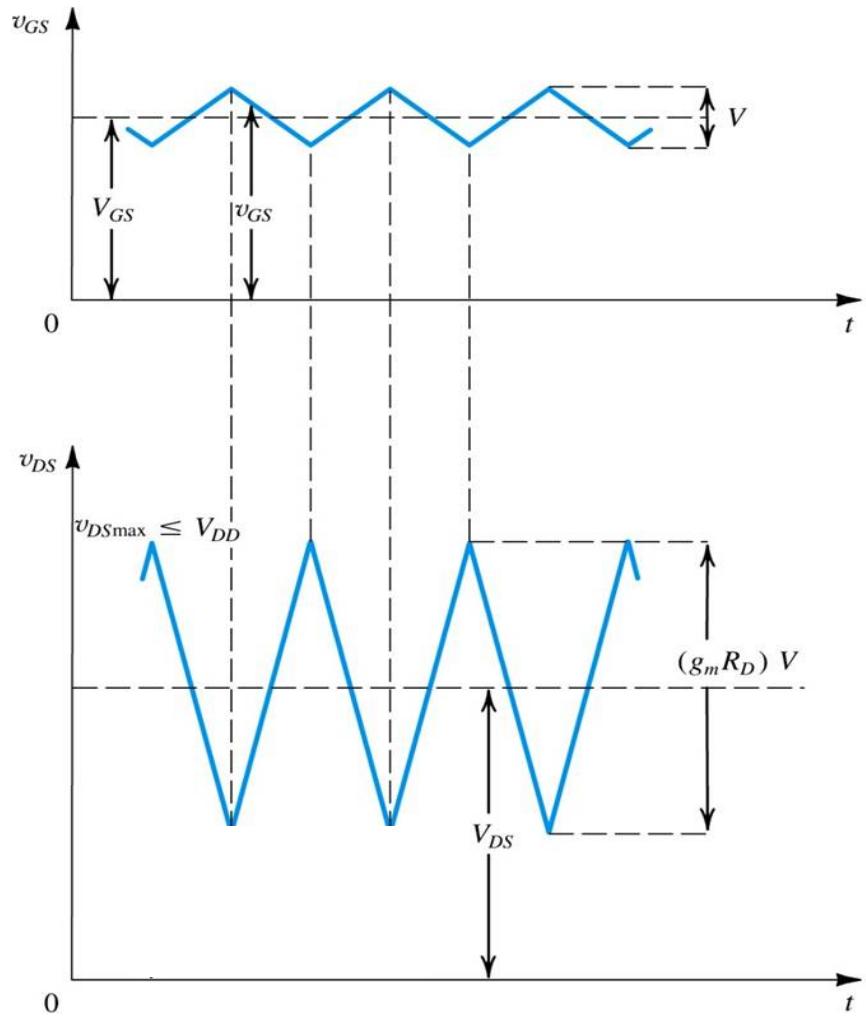
# The response to a combination of $v_{GS} = V_{GS} + v_{gs}$ can be found from the transfer function



# The response to a combination of $v_{GS} = V_{GS} + v_{gs}$ can be found from the transfer function



# Response to the signal appears to be linear



Response ( $v_o = v_{DS}$ ) is also made of a constant part ( $V_{DS}$ ) and a signal response part ( $\underline{v_{ds}}$ ).

Constant part of the response,  $V_{DS}$ , is ONLY related to  $V_{GS}$ , the constant part of the input (Q point on the transfer function of previous slide).

- i.e., if  $v_{gs}$  = 0, then  $v_{ds}$  = 0

The shape of the time varying portion of the response ( $\underline{v_{ds}}$ ) is similar to  $v_{gs}$ .

- i.e.,  $v_{ds}$  is proportional to the input signal,  $v_{gs}$

# Although the overall response is non-linear, the transfer function for the signal is linear!

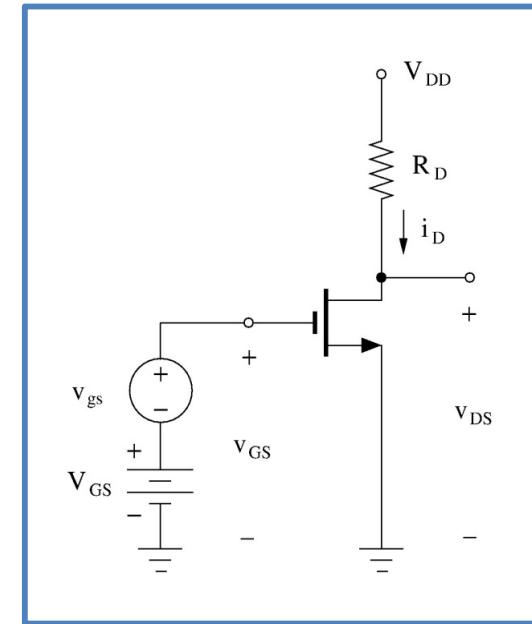
Constant:  
Bias      Signal and  
                response

$$\begin{aligned} v_{GS} &= V_{GS} + v_{gs} \\ v_{DS} &= V_{DS} + v_{ds} \\ i_D &= I_D + i_d \end{aligned}$$

↑      ↑

Under small  
signal  
approximation

$$\begin{aligned} v_{ds} &= - g_m R_D v_{gs} \\ i_d &= g_m v_{gs} \\ v_{ds} &= - i_d R_D \end{aligned}$$



NMOS ( $V_{OV} = v_{GS} - V_{tn}$ )

Cut - Off :  $V_{OV} < 0$

$$i_D = 0$$

Triode :  $V_{OV} \geq 0$  and  $v_{DS} \leq V_{OV}$

$$i_D = 0.5 \mu_n C_{ox} \frac{W}{L} [2V_{OV}v_{DS} - v_{DS}^2]$$

Saturation :  $V_{OV} \geq 0$  and  $v_{DS} \geq V_{OV}$

$$i_D = 0.5 \mu_n C_{ox} \frac{W}{L} V_{OV}^2 [1 + \lambda v_{DS}]$$

## Lecture 17 reading quiz

If in a MOSFET amplifier  $V_{DS} = 1\text{ V}$  and  $V_{OV} = 0.6\text{ V}$  where  $V_{GS} = 1\text{ V}$  and  $V_t = 0.4\text{ V}$

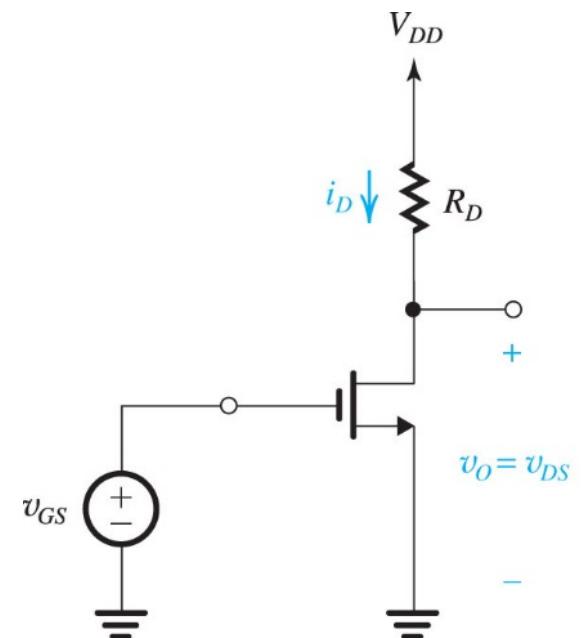
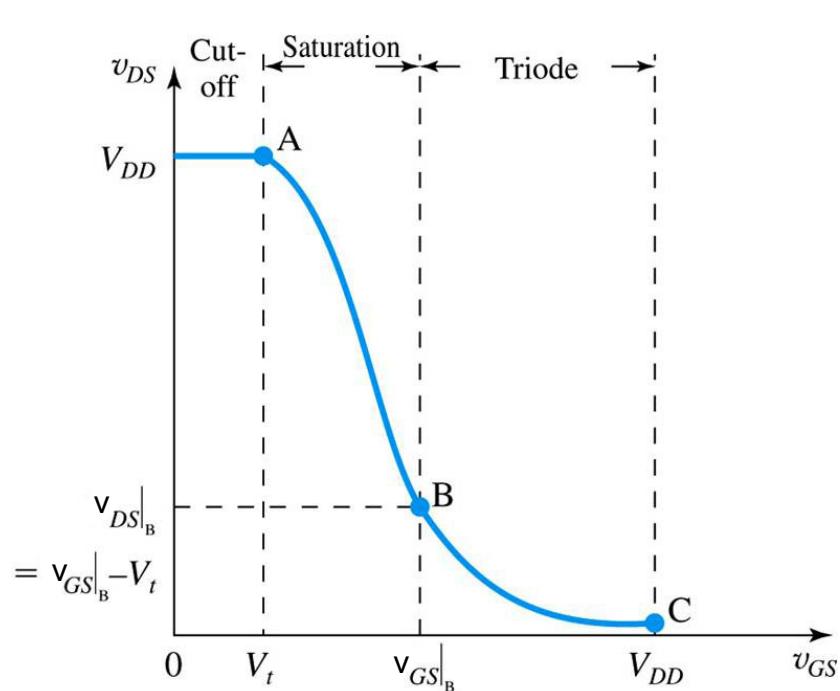
and the voltage gain of the amplifier ( $A_v = \frac{v_{ds}}{v_{gs}}$ ) is  $-10\text{ V/V}$ , Which one of the given input AC signals can be amplified without distortion?

## Discussion Question 1.

In the following circuit,

$$V_{DD} = 5 \text{ V}, R_D = 20 \text{ k}\Omega, V_t = 0.5 \text{ V}, k_n = 10 \text{ mA/V}^2 \text{ and } \lambda = 0.$$

Determine the coordinates of the saturation-region segment (AB) of the curve for the voltage transfer function.



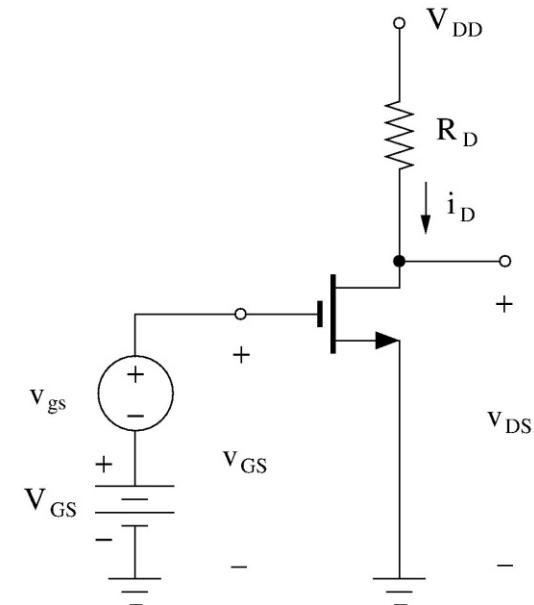
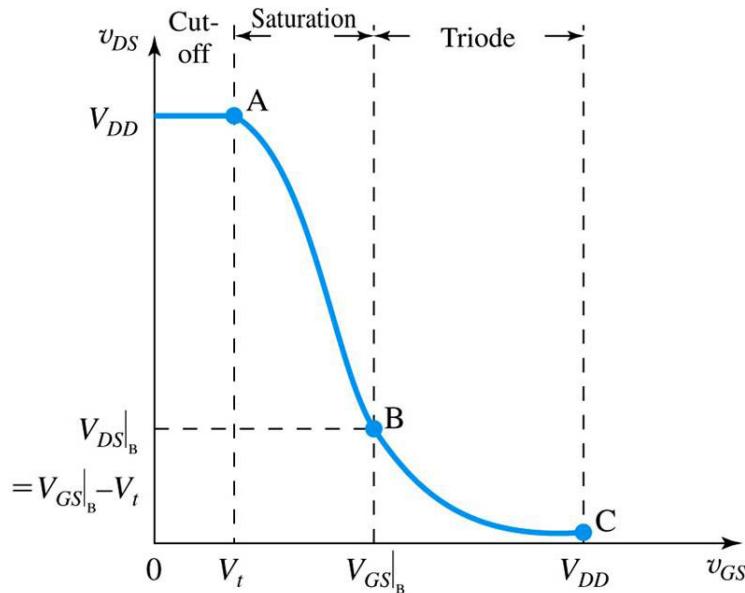
Hints:

## Discussion Question 1.

$$V_{DD} = 5 \text{ V}, R_D = 20 \text{ k}\Omega, V_t = 0.5 \text{ V}, k_n = 10 \text{ mA/V}^2 \text{ and } \lambda = 0.$$

- To find the  $V_{GS}$  and  $V_{DS}$  at point A, you can use the threshold of On/Cut-off in MOSFETs and the DS KVL (or the transfer characteristic graph).

- To find the  $V_{GS}$  and  $V_{DS}$  at point B, You can solve the MOSFET at the edge of saturation. This is when MOSFET is in saturation and  $V_{DS} = V_{GS} - V_t$ . By solving the characteristic drain current equation and the DS KVL, you can get the values of  $V_{GS}$  and  $V_{DS}$ .

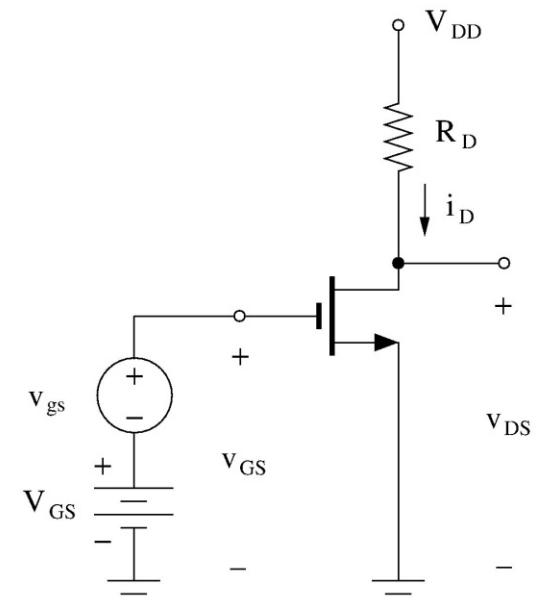
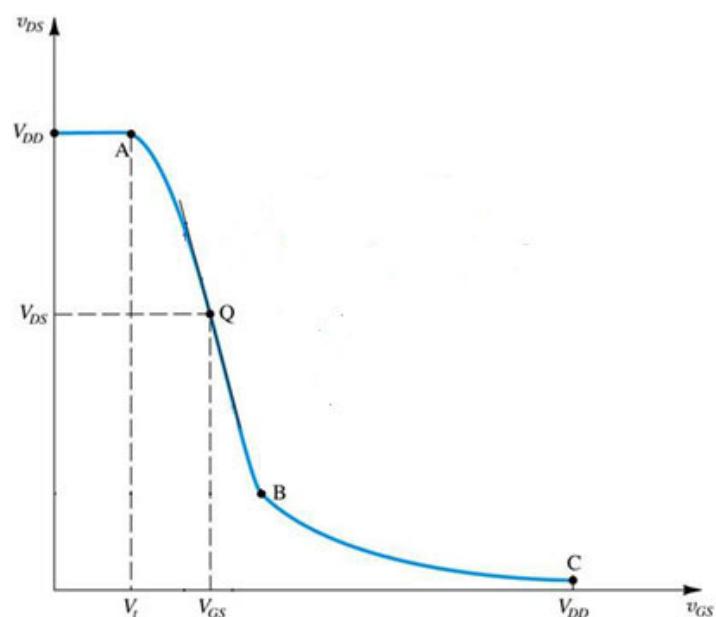


## Clicker Question 1.

In the following circuit,  $V_{GS} = 0.6 \text{ V}$ ,  $V_{DD} = 1.8 \text{ V}$ ,  $R_D = 17.5 \text{ k}\Omega$ ,  $V_t = 0.4 \text{ V}$ ,  $k_n = 4 \text{ mA/V}^2$  and  $\lambda = 0$ .

What is the maximum symmetrical signal swing allowed at the drain (what is the maximum allowable peak amplitude of  $v_{ds}$ )?

- A. 0.4 V
- B. 0.6 V
- C. 0.2 V



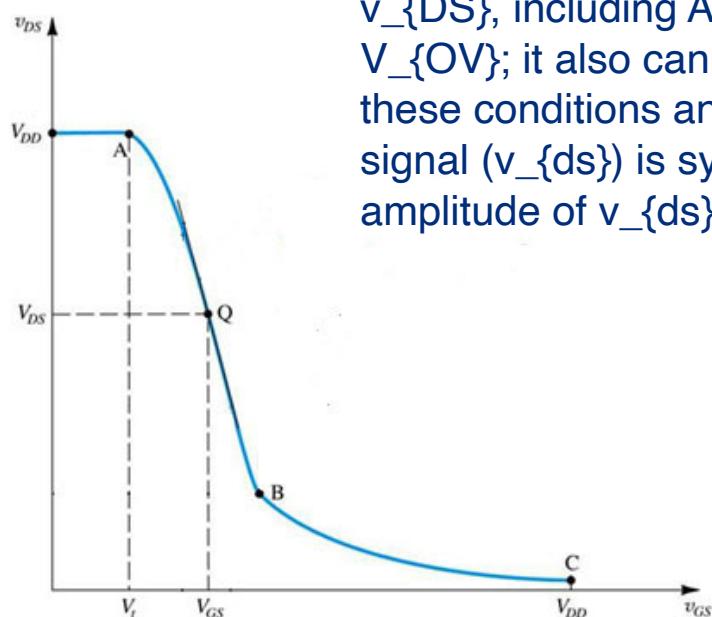
Hints:

## Clicker Question 1.

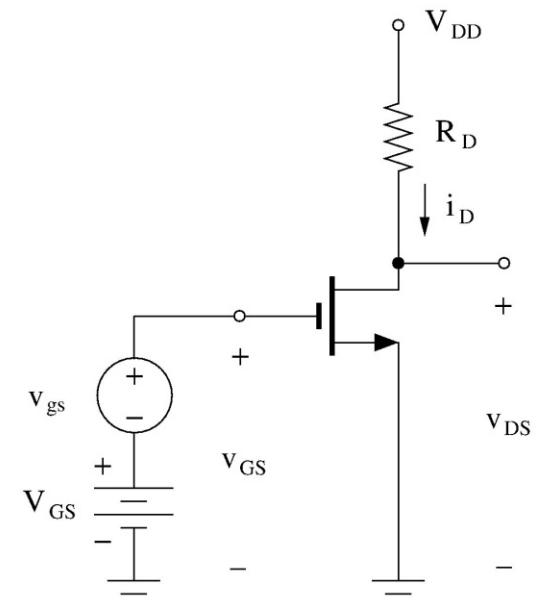
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What is the maximum symmetrical signal swing allowed at the drain (what is the maximum allowable peak amplitude of  $v_{ds}$ )?

- A. 0.4 V
- B. 0.6 V
- C. 0.2 V



- Find  $V_{OV}$  and  $V_{DS}$ .
- After adding an AC signal,  $v_{gs}$ , an AC signal  $v_{ds}$  will be superimposed on  $V_{DS}$ . The total  $v_{DS}$ , including AC and DC should not go below  $V_{OV}$ ; it also cannot exceed  $V_{DD}$ . Knowing these conditions and assuming that the AC output signal ( $v_{ds}$ ) is symmetric, how large the amplitude of  $v_{ds}$  can be?



# Simulation results for the Clicker Question 1

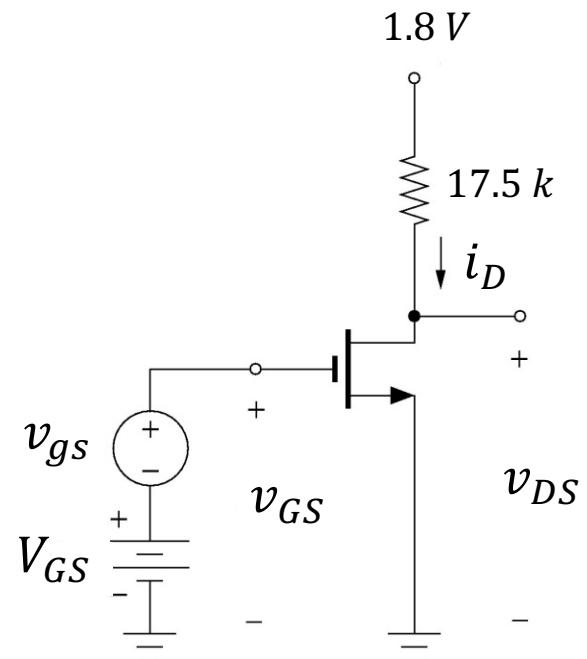
In the following circuit,  $V_{GS} = 0.6 \text{ V}$ ,  $V_t = 0.4 \text{ V}$ ,  $k_n = 4 \text{ mA/V}^2$  and  $\lambda = 0$ .

Draw the graph of  $v_{GS}$ ,  $v_{DS}$ , and  $I_D$  for

1.  $v_{gs} = 0.005 \sin(2\pi ft) \text{ (V)}$

2.  $v_{gs} = 0.010 \sin(2\pi ft) \text{ (V)}$

Use  $f = 1 \text{ kHz}$ .



# Simulation results for the Clicker Question 1

In the following circuit,  $V_{GS} = 0.6 \text{ V}$ ,  $V_t = 0.4 \text{ V}$ ,  $k_n = 4 \text{ mA/V}^2$  and  $\lambda = 0$ .

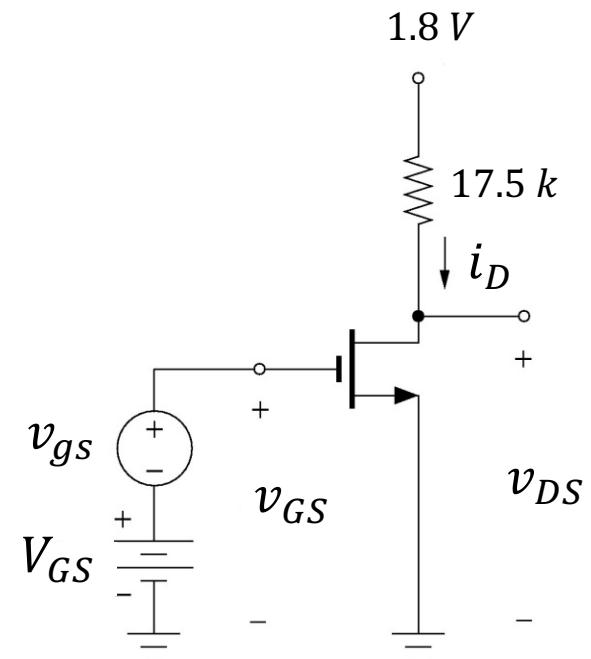
Draw the graph of  $v_{GS}$ ,  $v_{DS}$ , and  $I_D$  for

Bias point, or the operation point, or the Q point:

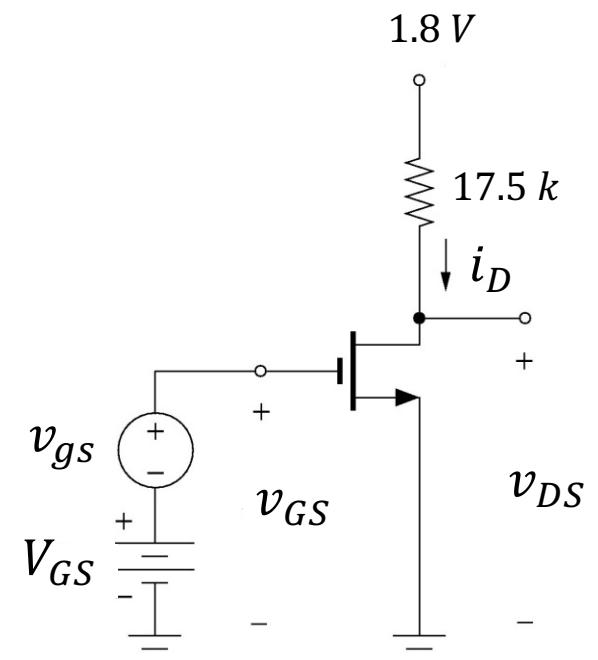
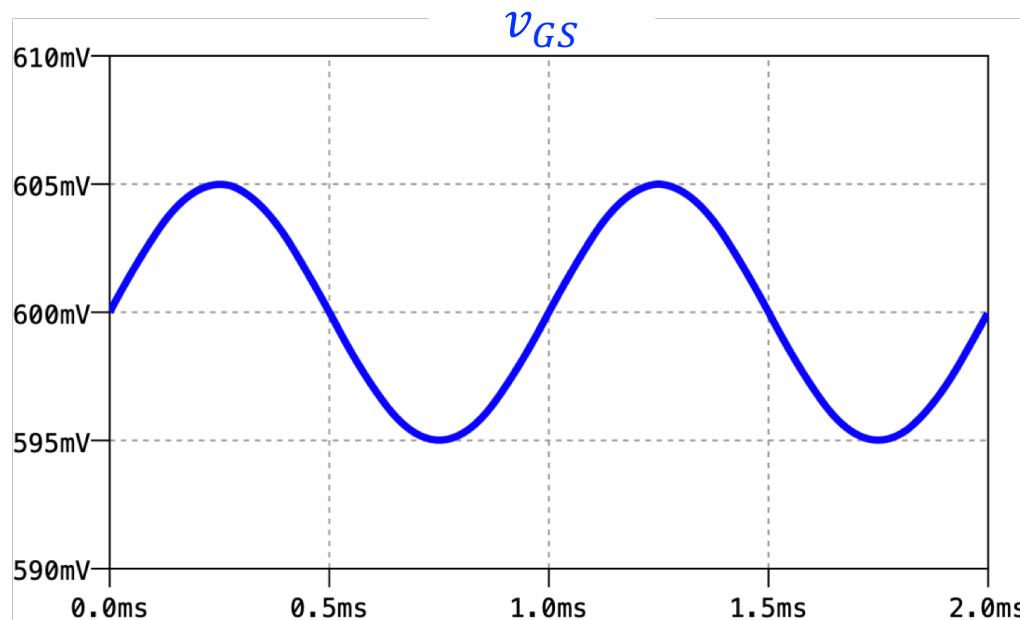
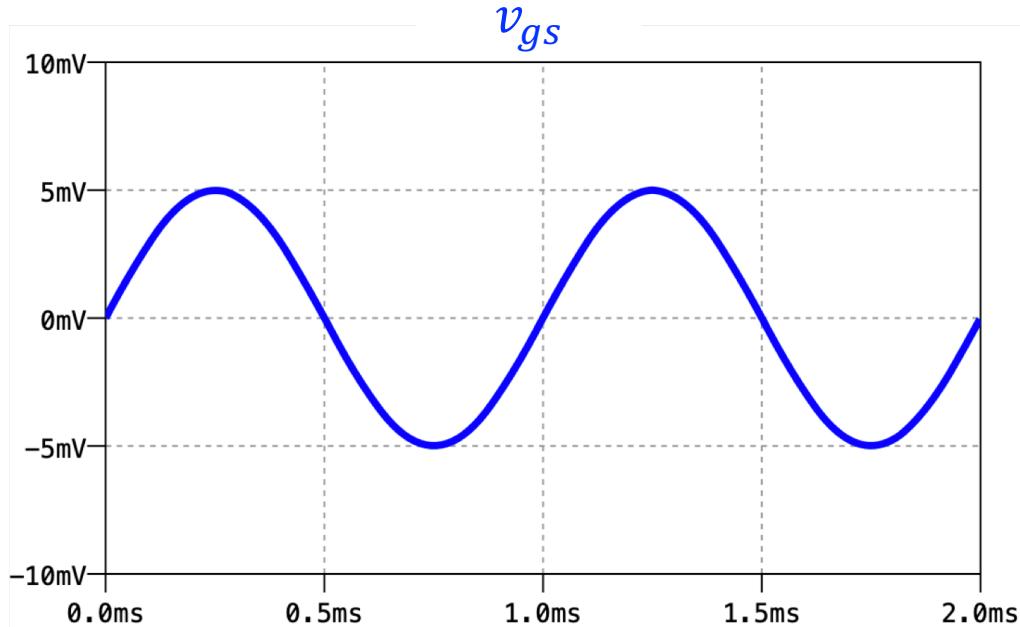
$$V_{GS} = 0.6 \text{ V}$$

$$V_{DS} = 0.4 \text{ V}$$

$$I_D = 0.08 \text{ mA}$$

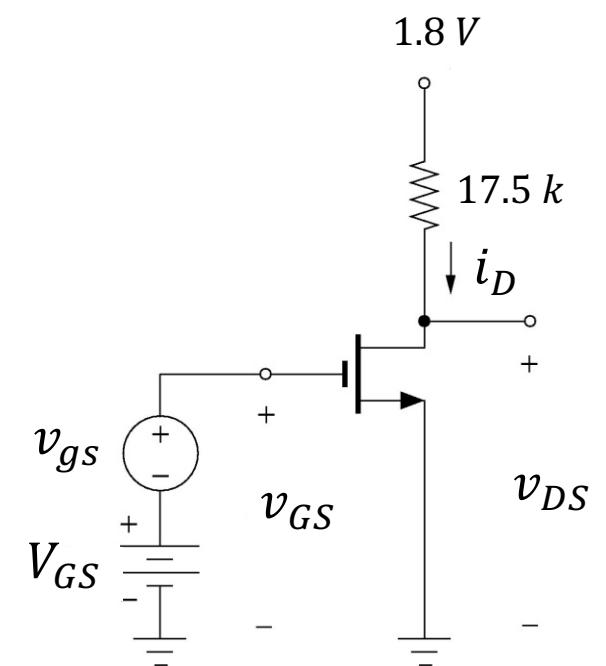
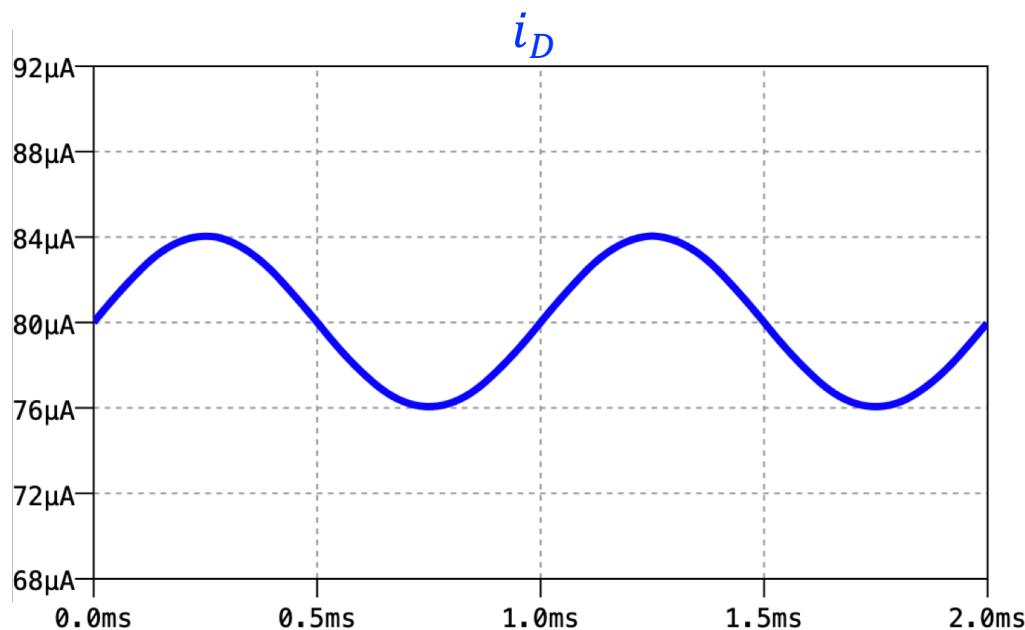
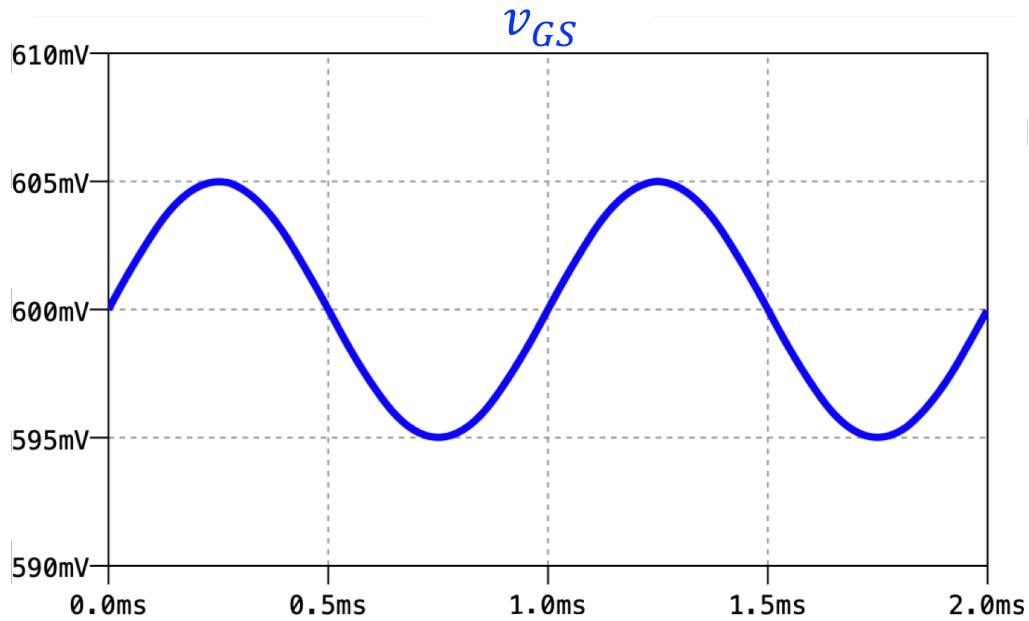


$$v_{gs} = 0.005 \sin(2\pi ft) (V)$$



@ Q:  $V_{GS} = 0.6 V$   
 $V_{DS} = 0.4 V$   
 $I_D = 0.08 mA$

$$v_{gs} = 0.005 \sin(2\pi ft) (V)$$



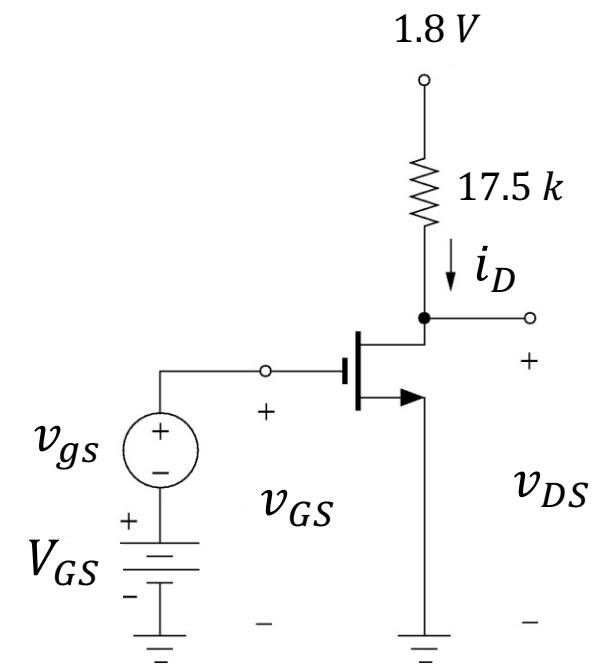
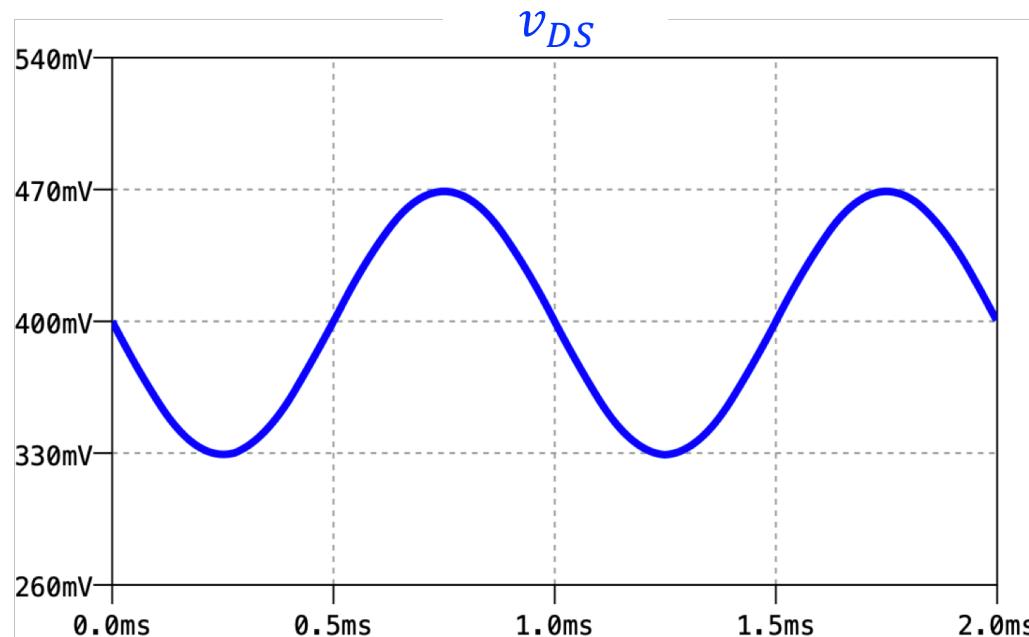
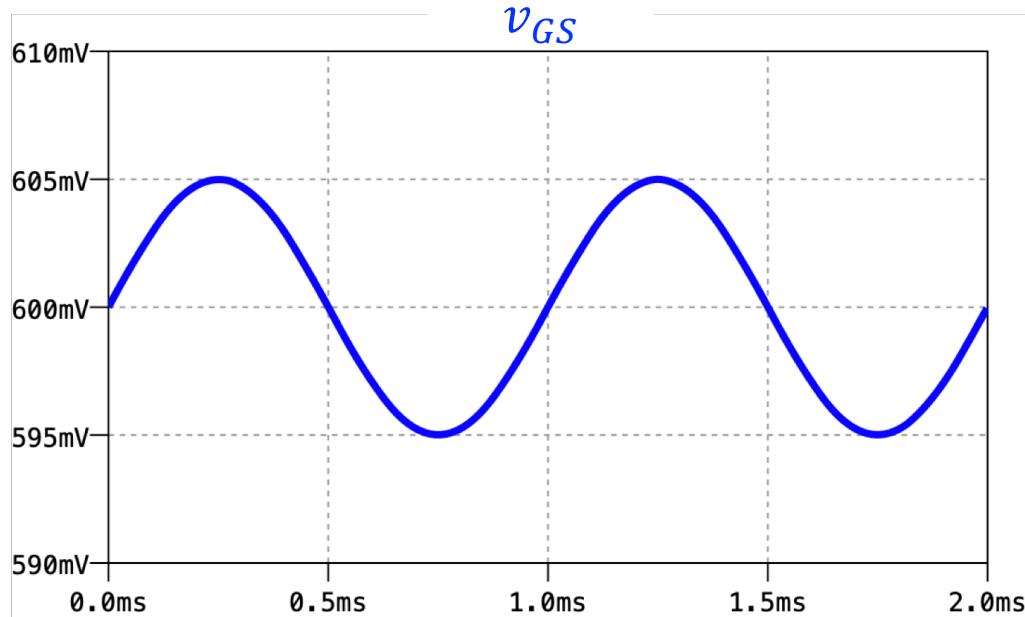
@ Q:  $V_{GS} = 0.6 V$

$V_{DS} = 0.4 V$

$I_D = 0.08 mA$

$$g_m = \frac{2 I_D}{V_{ov}}$$

$$v_{gs} = 0.005 \sin(2\pi ft) (V)$$



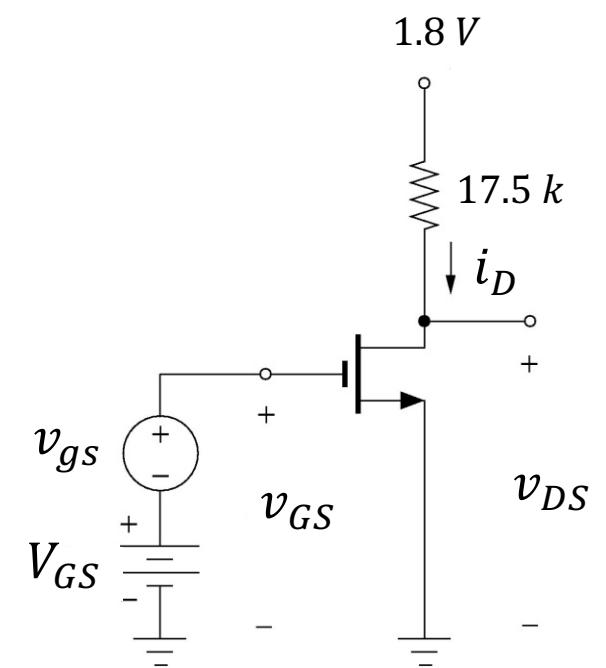
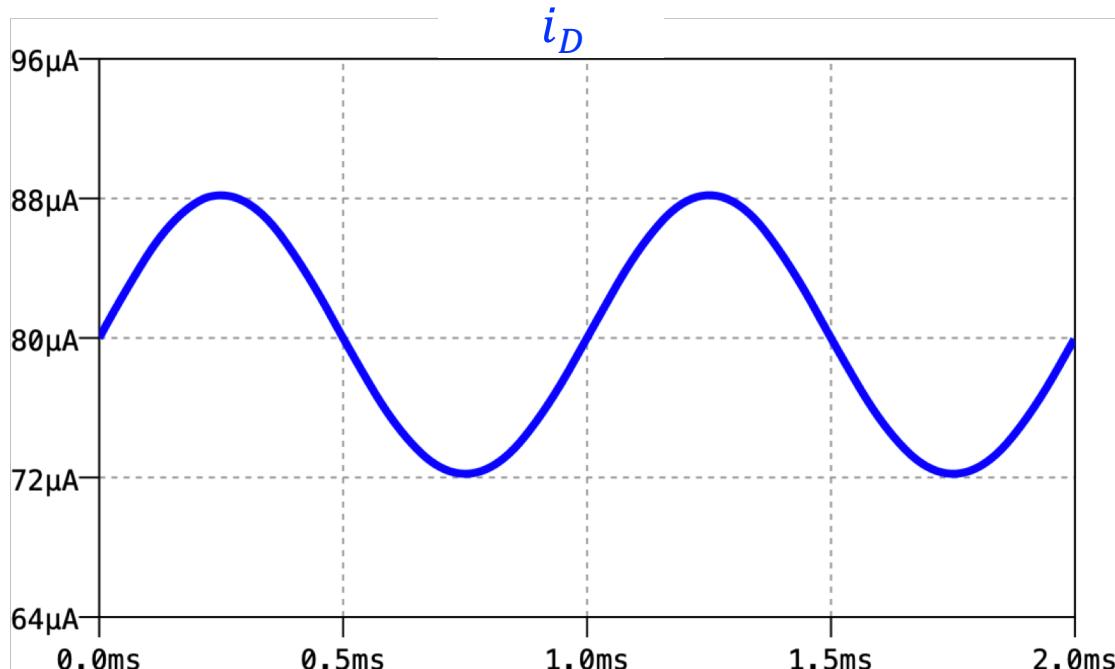
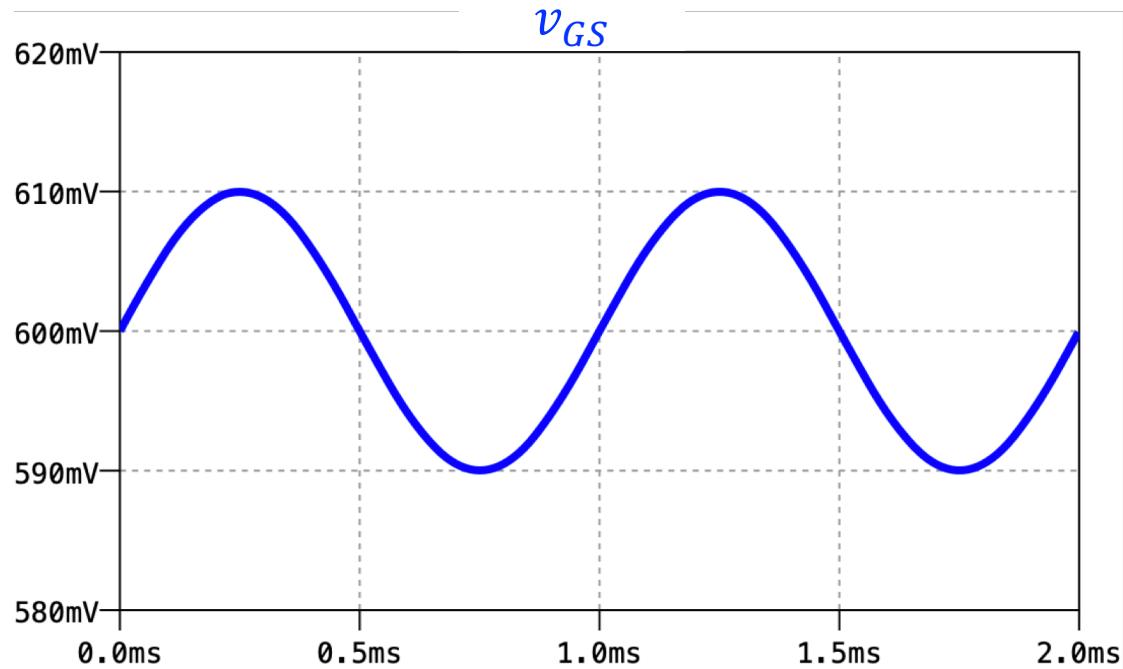
@ Q:  $V_{GS} = 0.6 V$

$V_{DS} = 0.4 V$

$I_D = 0.08 mA$

$A_v = \frac{v_{ds}}{v_{gs}} = -14 V/V$

$$v_{gs} = 0.01 \sin(2\pi ft) (V)$$



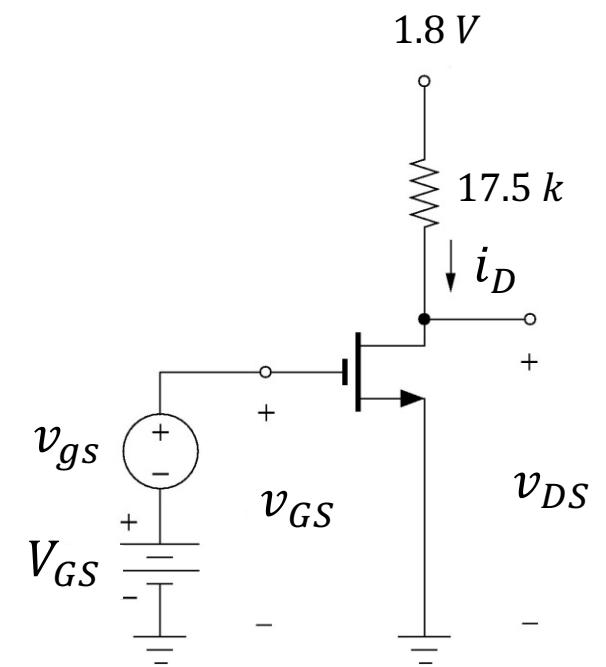
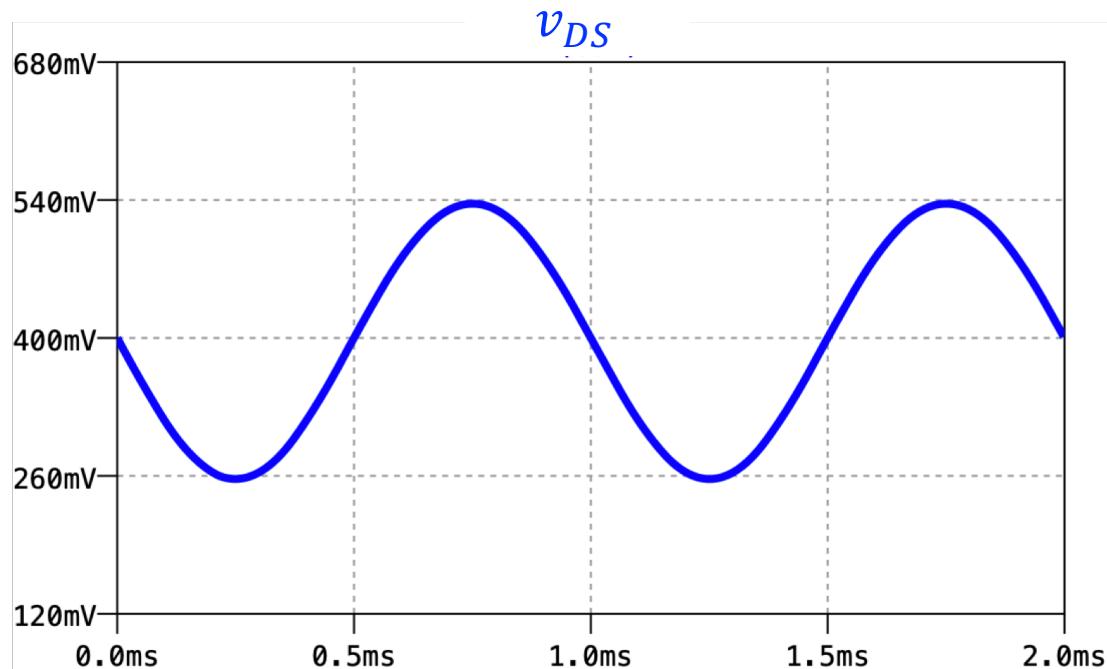
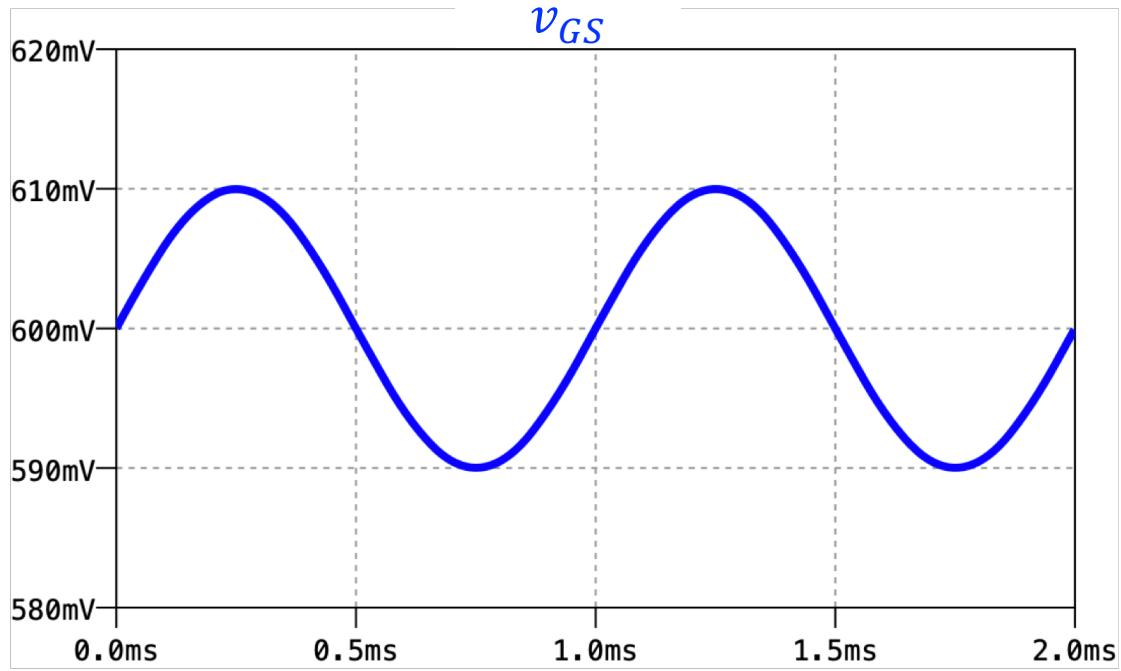
@ Q:  $V_{GS} = 0.6 V$

$V_{DS} = 0.4 V$

$I_D = 0.08 mA$

$g_m = \frac{i_d}{v_{gs}} = 0.08 \text{ mA/V}$

$$v_{GS} = 0.01 \sin(2\pi ft) (V)$$

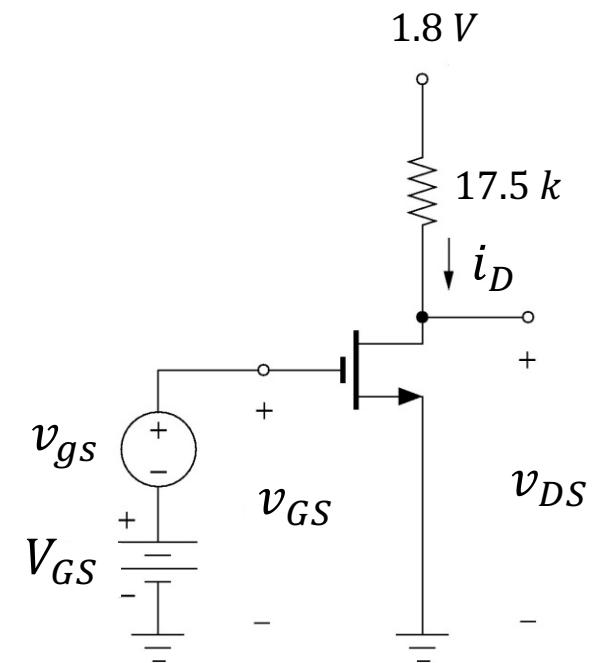
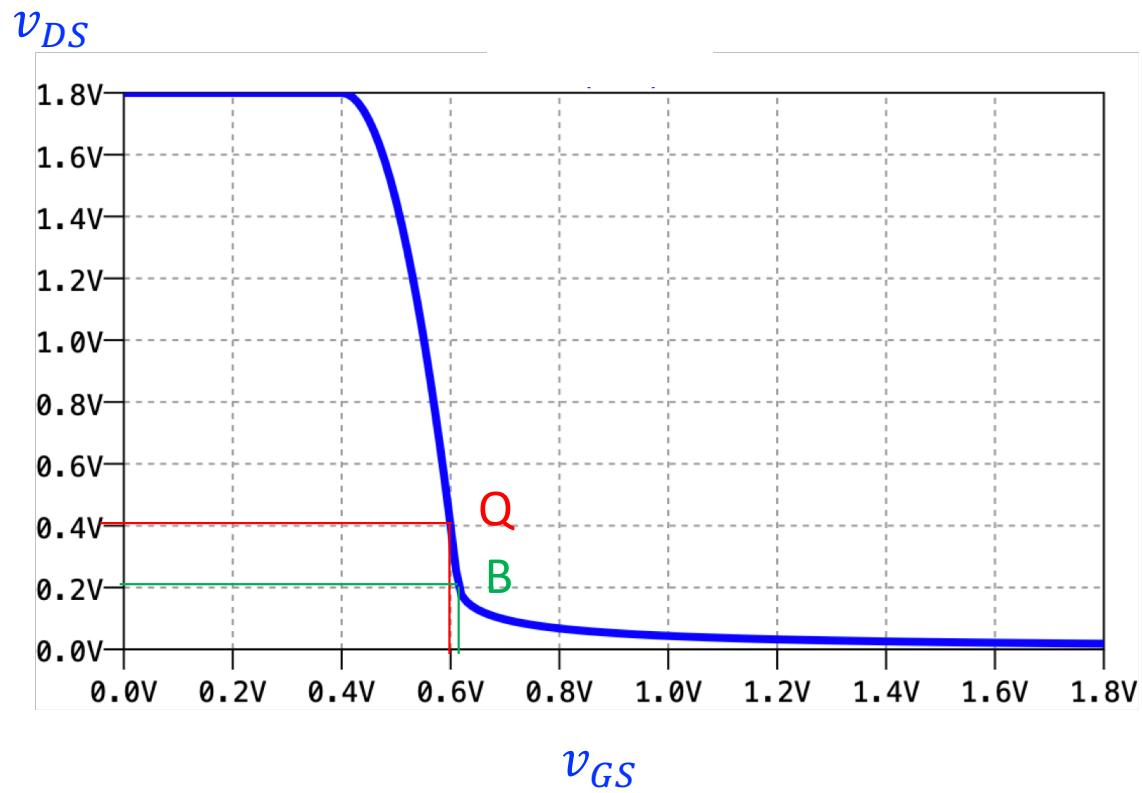


@ Q:  $V_{GS} = 0.6 V$

$V_{DS} = 0.4 V$

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$A_v = \frac{v_{ds}}{v_{gs}} = -14 V/V$



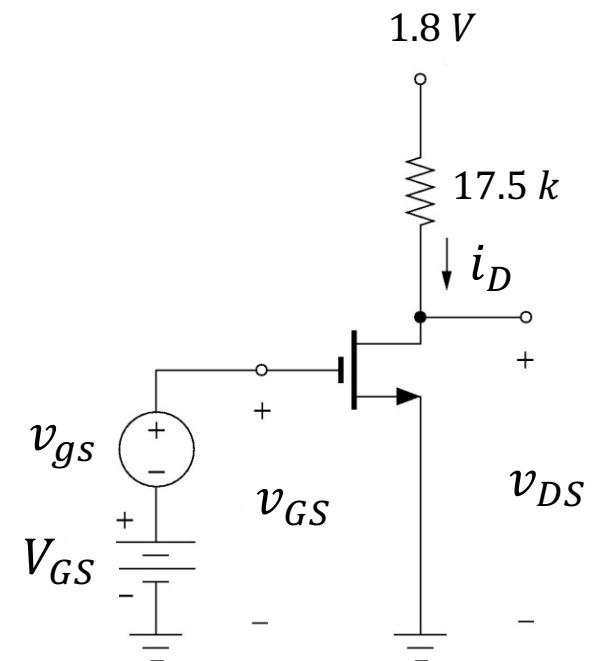
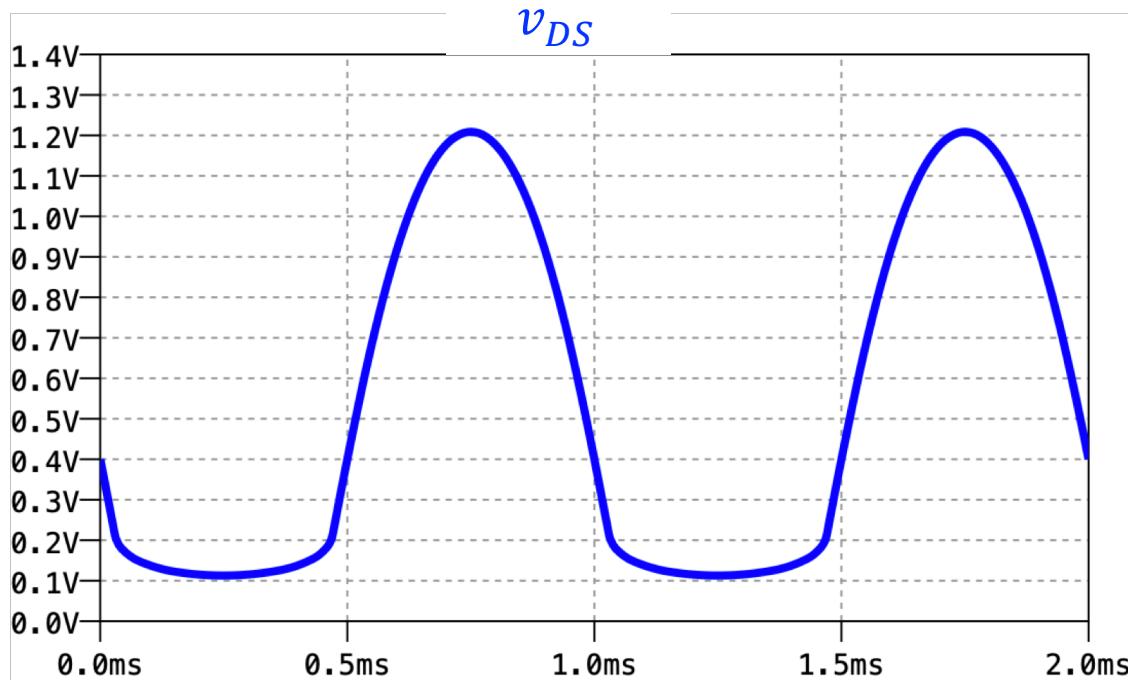
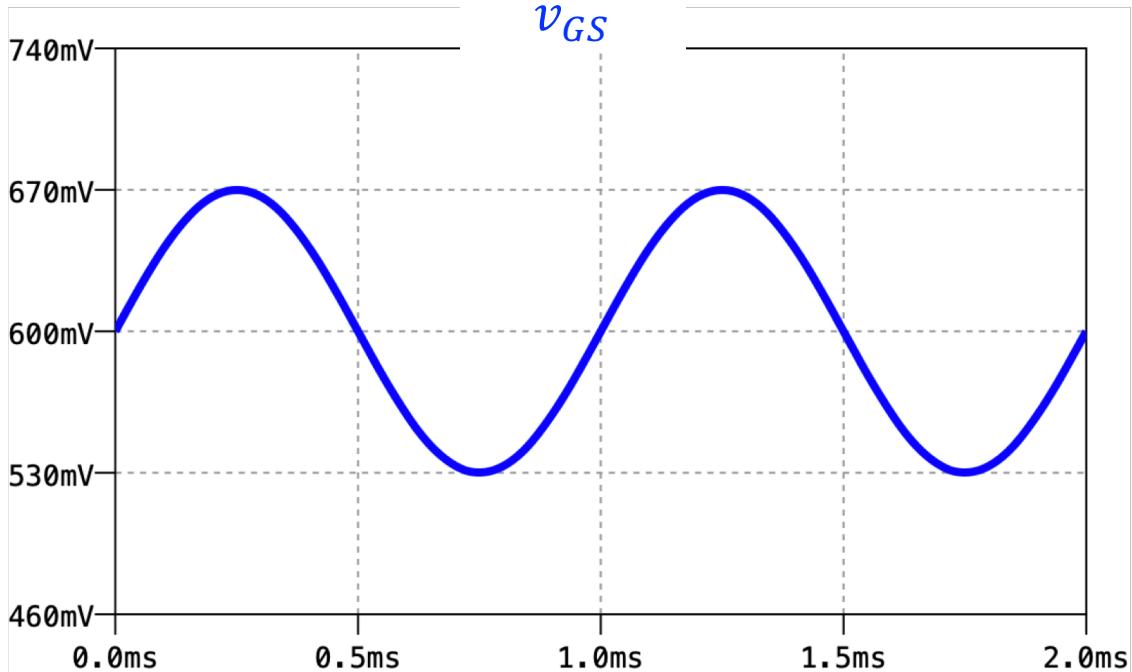
@ Q:  $V_{GS} = 0.6\text{ V}$

$V_{DS} = 0.4\text{ V}$

$I_D = 0.08\text{ mA}$

$V_{OV} = 0.2\text{ V}$

$$v_{GS} = 0.07 \sin(2\pi f_1 t) \text{ (V)}$$



@ Q:  $V_{GS} = 0.6 \text{ V}$   
 $V_{DS} = 0.4 \text{ V}$   
 $I_D = 0.08 \text{ mA}$   
 $V_{OV} = 0.2 \text{ V}$