

# **ECE 65: Components & Circuits Lab**

## **Lecture 19**

### **BJT Amplifier small signal model**

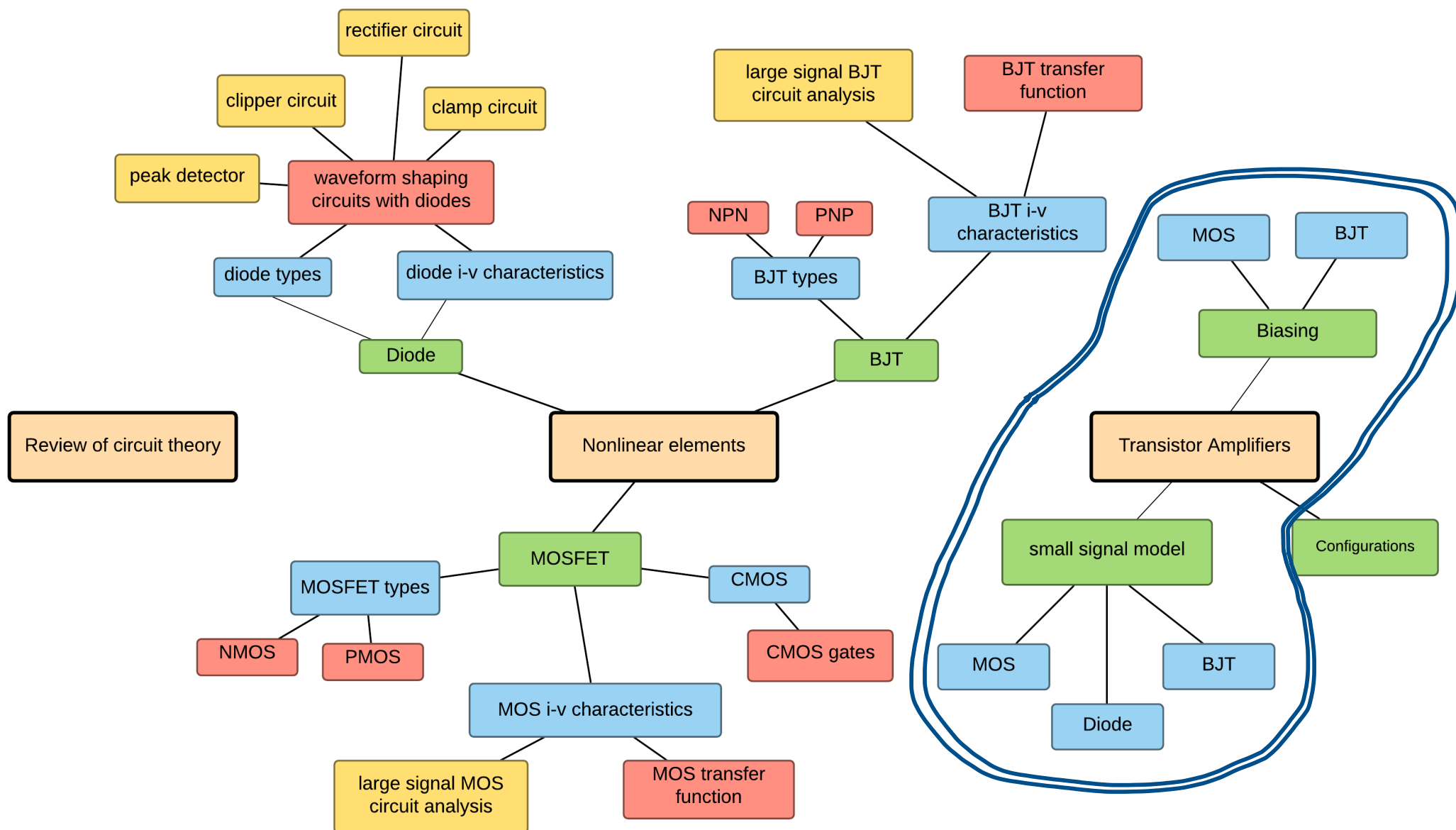
Reference notes: sections 5.1, 5.2

Sedra & Smith (7<sup>th</sup> Ed): sections 7.1

Saharnaz Baghdadchi

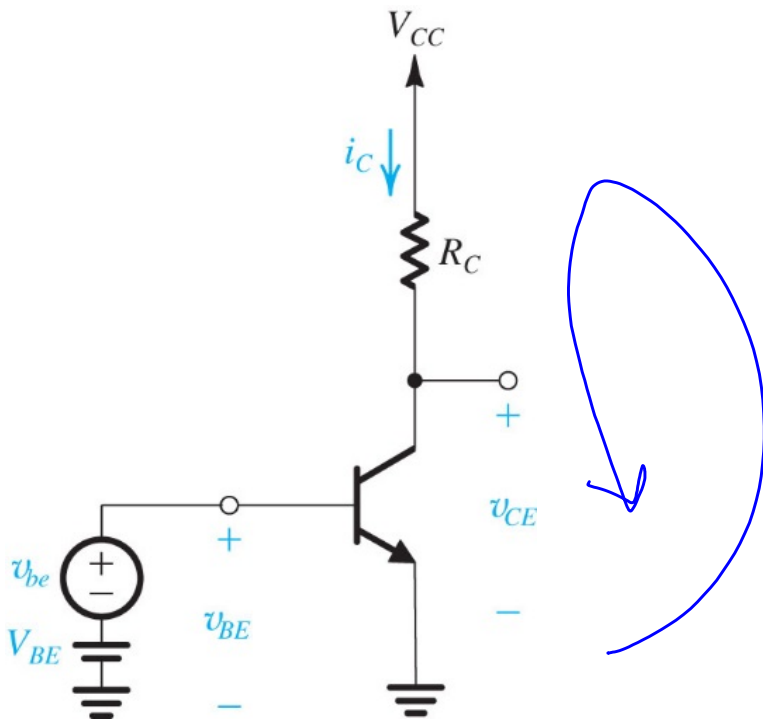
# Course map

## 5. Transistor Amplifiers – Bias and small signal



# Derivation of BJT small signal model

The DC Bias point:  $v_{be} = 0$



$$I_C = I_S e^{V_{BE}/V_T}$$

[The early effect is neglected here ( $\lambda = 0$ ) ]

$$I_B = I_C / \beta$$

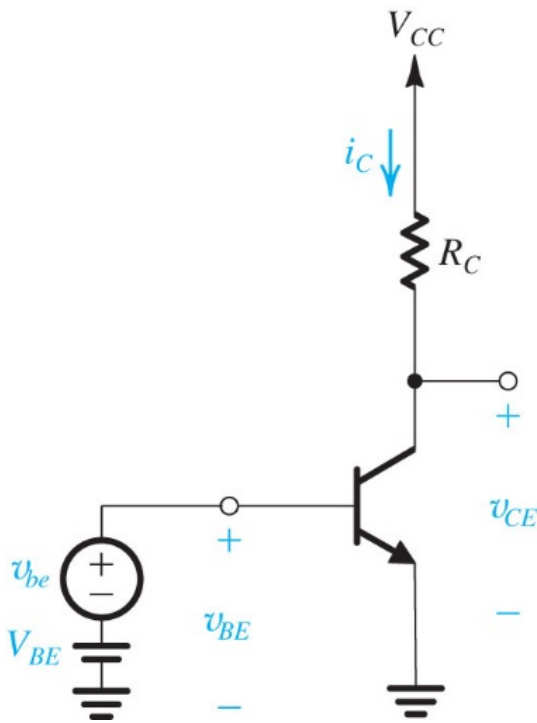
$$I_E = \frac{\beta + 1}{\beta} I_C$$

$$V_{CE} = V_{CC} - R_C I_C$$

# Derivation of BJT small signal model

When  $v_{be}$  is applied:

The total instantaneous base-emitter voltage is:  $v_{BE} = V_{BE} + v_{be}$



$$i_C = I_S e^{v_{BE}/V_T} = I_S e^{(V_{BE}+v_{be})/V_T}$$

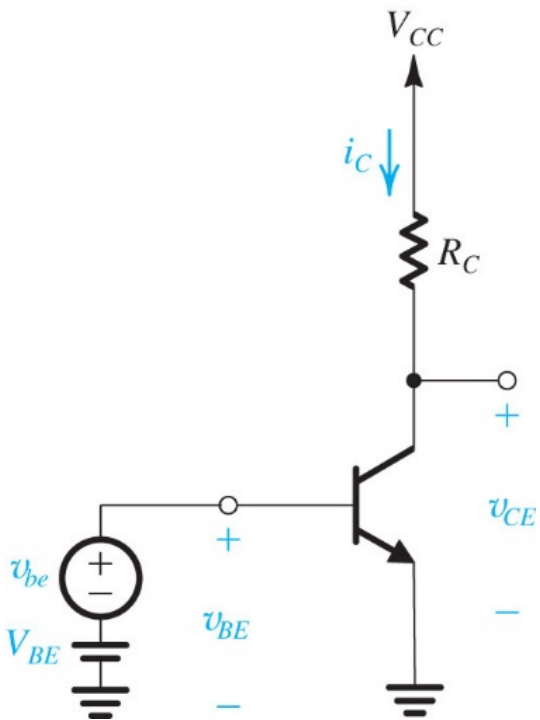
$$i_C = I_S e^{V_{BE}/V_T} e^{v_{be}/V_T}$$

Since  $I_C = I_S e^{V_{BE}/V_T}$ ,

$$i_C = I_C e^{v_{be}/V_T}$$

# Derivation of BJT small signal model

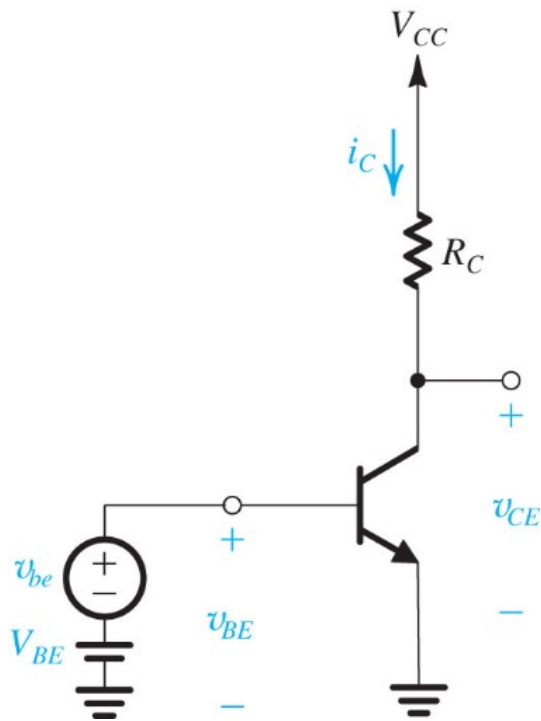
$$i_C = I_C e^{v_{be}/V_T}$$



If  $v_{be} \ll V_T$  , using Taylor series expansion and neglecting the higher order terms in the exponential series expansion,

$$i_C \simeq I_C \left( 1 + \frac{v_{be}}{V_T} \right)$$

# Derivation of BJT small signal model



$$i_c \simeq I_C \left( 1 + \frac{v_{be}}{V_T} \right)$$

Under small signal approximation for BJT (  $\underline{v_{be}} \ll V_T$  ),

$$i_c = I_C + \frac{I_C}{V_T} v_{be}$$

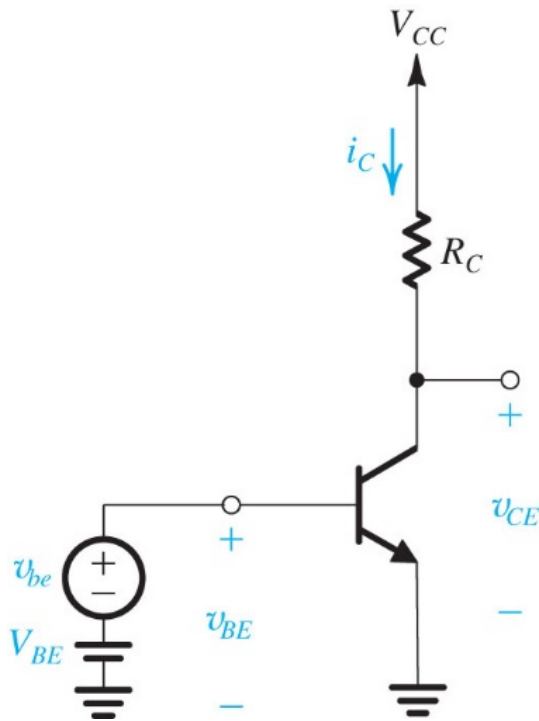
$$i_c = \frac{I_C}{V_T} v_{be}$$

The BJT transconductance  $\textcolor{red}{g_m}$  is defined as  $g_m \equiv \frac{i_c}{v_{be}}$

$$g_m = \frac{I_C}{V_T}$$

$$i_c = g_m v_{be}$$

# Derivation of BJT small signal model



$$i_C = I_C + \frac{I_C}{V_T} v_{be}$$

$$i_B = \frac{i_C}{\beta} = \frac{I_C}{\beta} + \frac{1}{\beta} \frac{I_C}{V_T} v_{be}$$

$$i_B = I_B + i_b$$

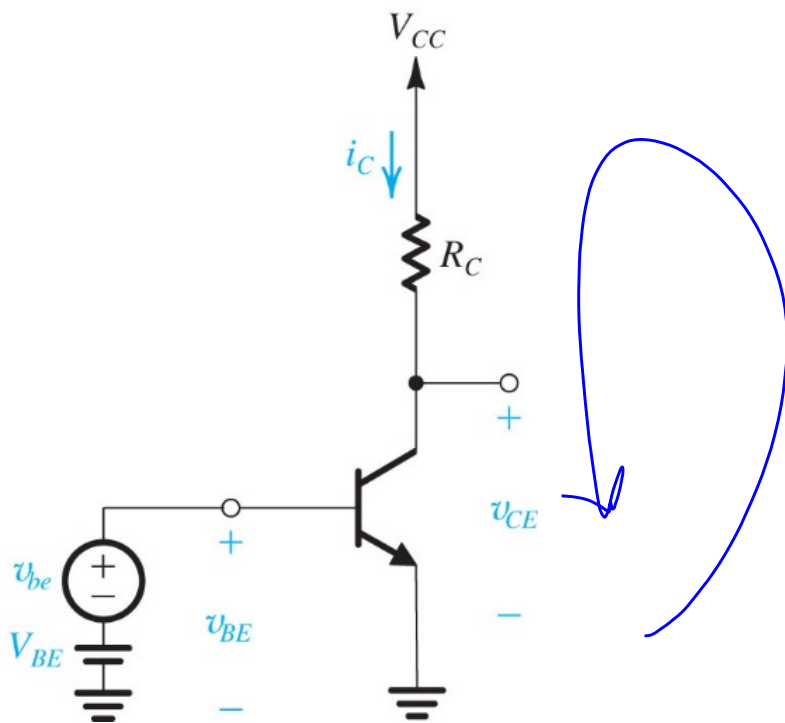
$$i_b = \frac{1}{\beta} \frac{I_C}{V_T} v_{be} = \frac{g_m}{\beta} v_{be}$$

The small signal input resistance between base and emitter is denoted by  $r_{\pi}$

$$r_{\pi} \equiv \frac{v_{be}}{i_b} \rightarrow r_{\pi} = \frac{\beta}{g_m} = \frac{V_T}{I_B}$$

# Derivation of BJT small signal model

The voltage gain in this amplifier configuration:



$$v_{CE} = V_{CC} - i_c R_C$$

$$= V_{CC} - (i_c + I_C) R_C$$

$$= (V_{CC} - I_C R_C) - i_c R_C$$

$$= V_{CE} - i_c R_C$$

$$v_{ce} = -i_c R_C = -g_m v_{be} R_C$$

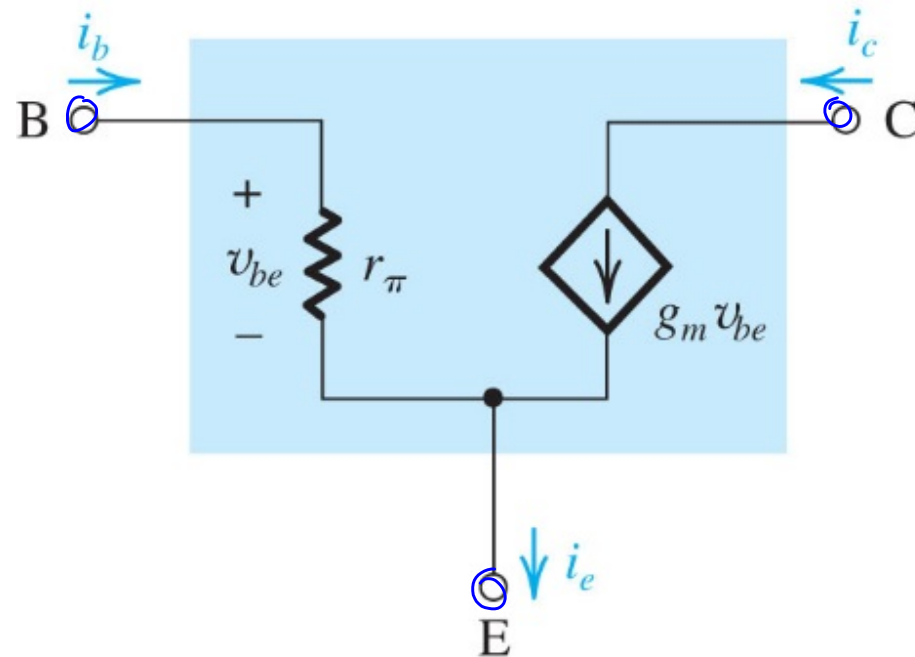
$$A_v \equiv \frac{v_{ce}}{v_{be}} = -g_m R_C$$



# BJT small signal model

$$i_b = \frac{v_{be}}{r_\pi}$$

$$i_c = g_m v_{be}$$

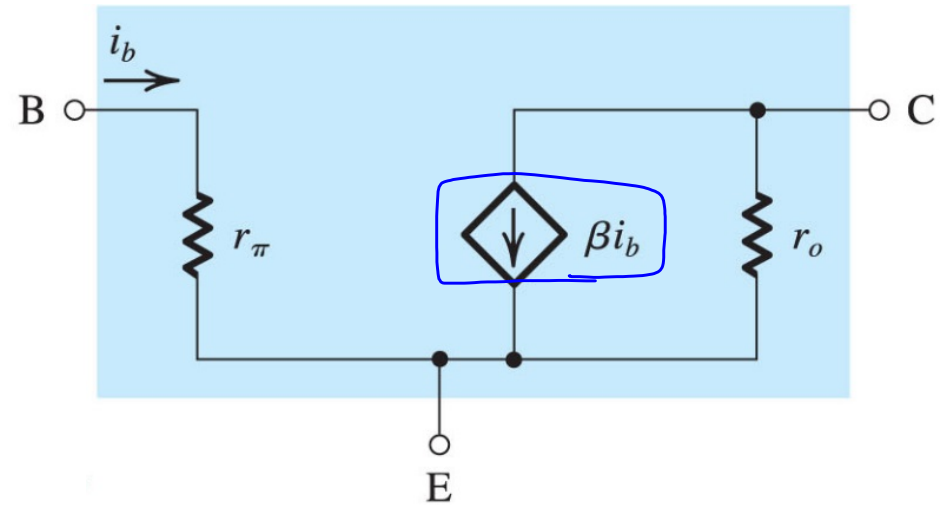
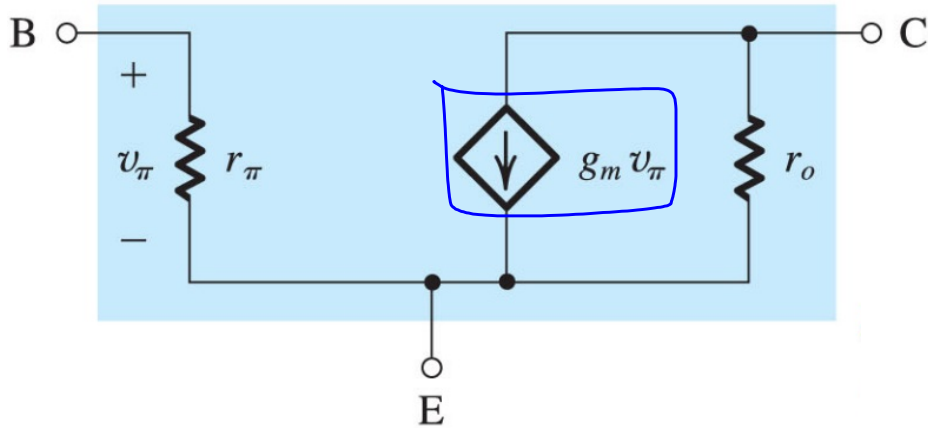


# BJT small signal model

$$v_{\pi} = v_{be}$$

$$i_b = \frac{v_{be}}{r_{\pi}}$$

$$i_c = g_m v_{be} + \frac{v_{ce}}{r_o}$$



$$V_A = \frac{1}{\lambda}$$

$$g_m = \frac{I_C}{V_T}$$

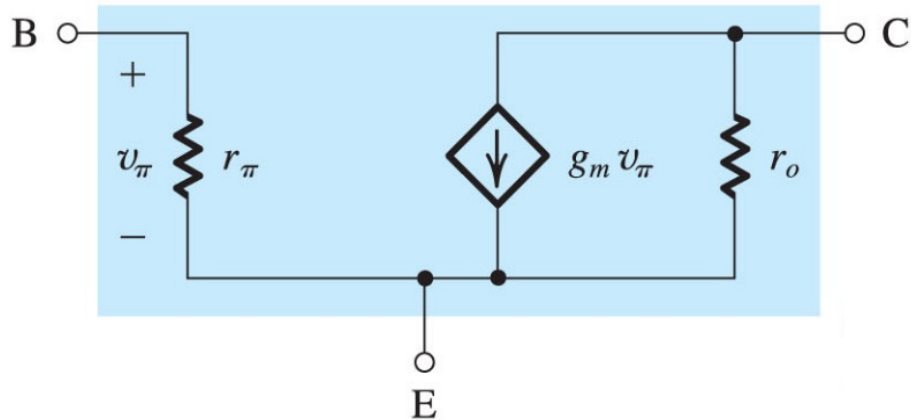
$$r_o \approx \frac{V_A}{I_C}$$

$$r_{\pi} = \frac{\beta}{g_m} = \frac{V_T}{I_B}$$

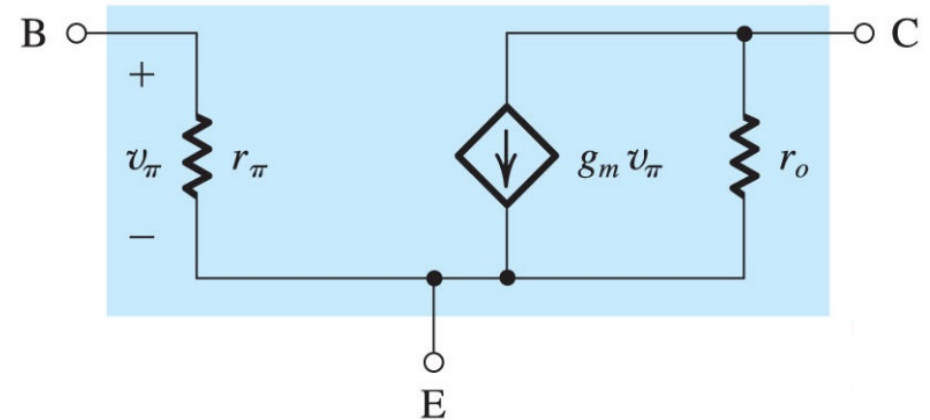
$$g_m v_{be} = g_m (i_b r_{\pi}) = (g_m r_{\pi}) i_b = \beta i_b$$

# PNP small signal model is identical to NPN

PNP



NPN

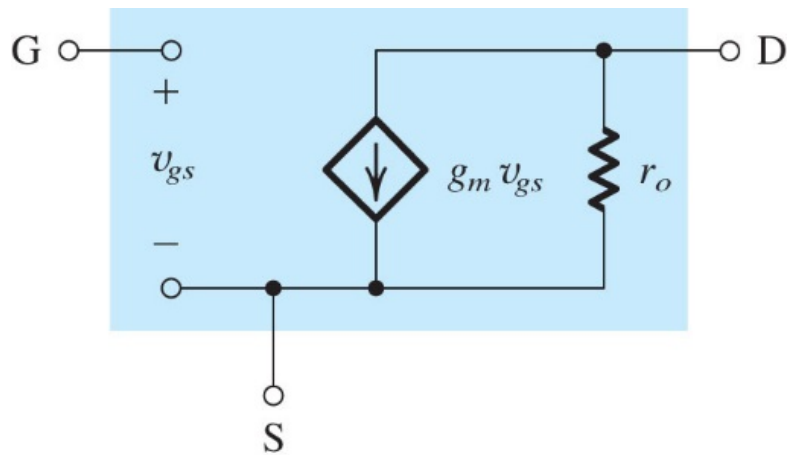


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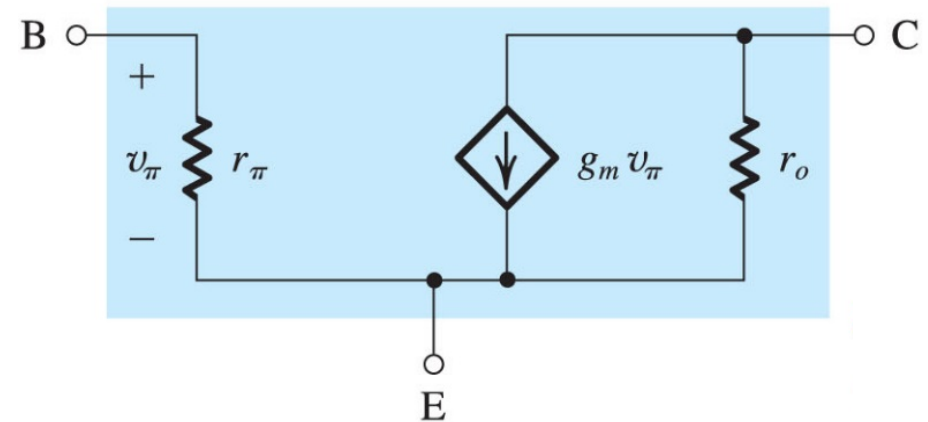
PNP small-signal circuit model is identical to NPN

# Summary of transistor small signal models

NMOS/PMOS



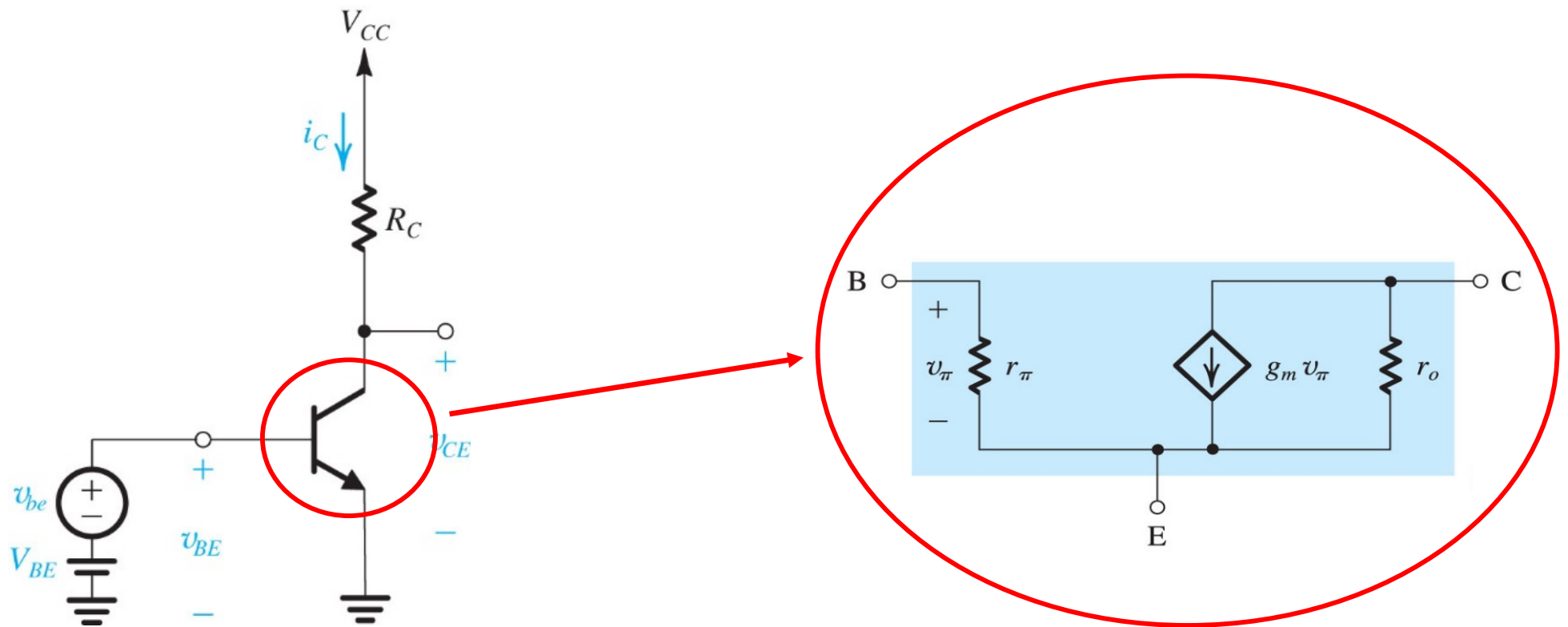
NPN/PNP BJT



## Comparison of MOS and BJT small-signal circuit models:

1. MOS has an infinite resistor in the input ( $v_{gs}$ ) while BJT has a finite resistor,  $r_\pi$  (typically several  $k\Omega$ ).
2. BJT  $g_m$  is substantially larger than that of a MOS (BJT has a much higher gain).
3.  $r_o$  values are typically similar (10s of  $k\Omega$ ).

# BJT Small Signal Model



# Review of amplifier circuit analysis

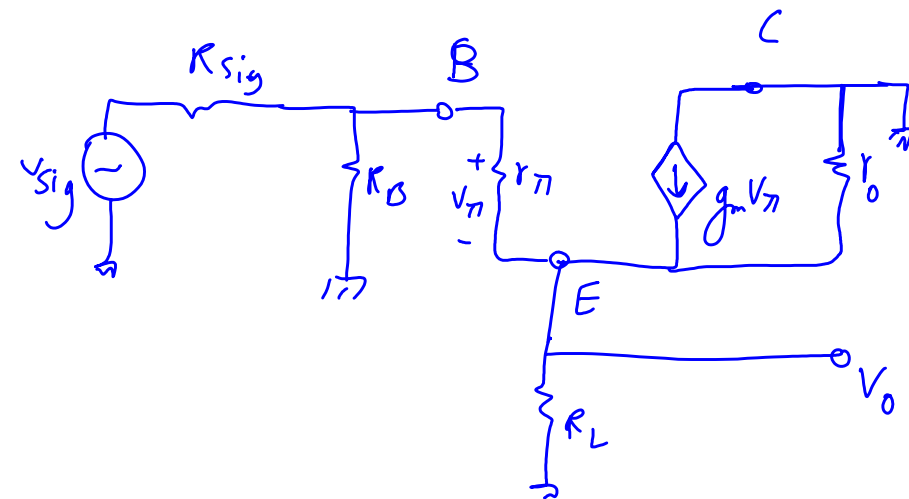
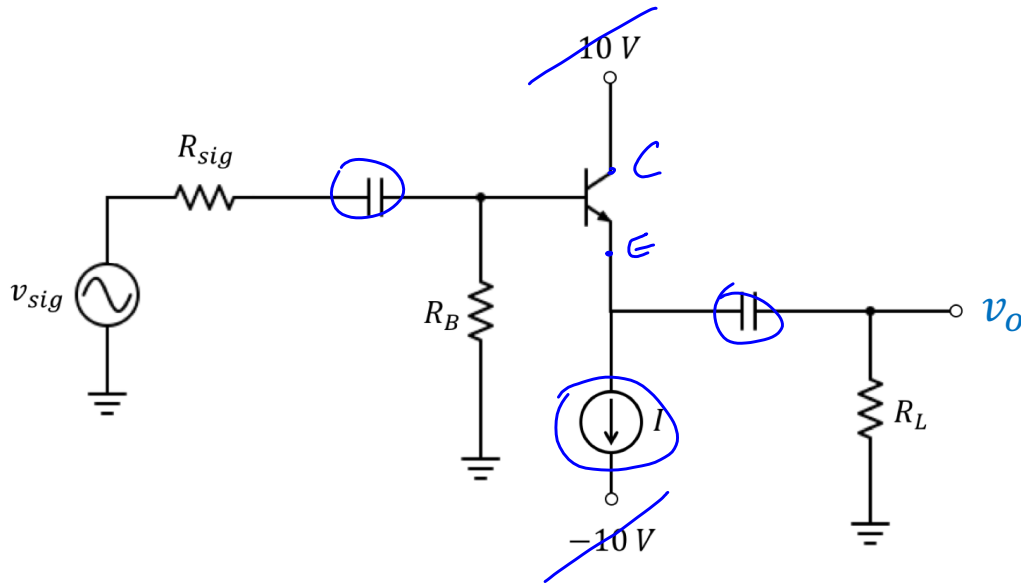
- Under small signal approximation, we can analyze the **Signal** and **Bias** circuits separately for a given amplifier circuit.
- The **Signal** and **Bias** circuits are different.
- **Bias** is the state of the system when there is no signal. In drawing and analyzing the **Bias** circuit, the capacitors are open and signal sources are set to zero.
- **Signal** circuit  $\equiv$  signal equivalent circuit  
 $\equiv$  small signal equivalent circuit

# Review of amplifier analysis

- In drawing the **Signal** circuit you should
  - replace the transistors with their small signal models without changing anything in the model
  - keep the resistors – find the node they are connected to in the original circuit and connect them to the right node in the signal circuit.
  - short the capacitors
  - set the independent DC current and voltage sources to zero.

## Example:

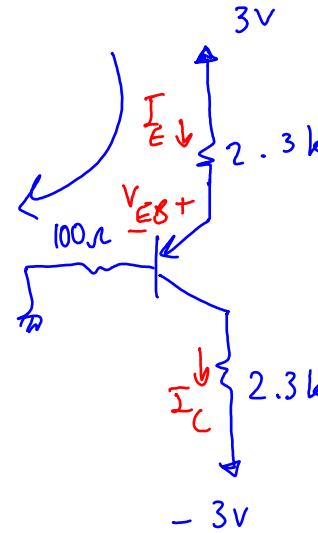
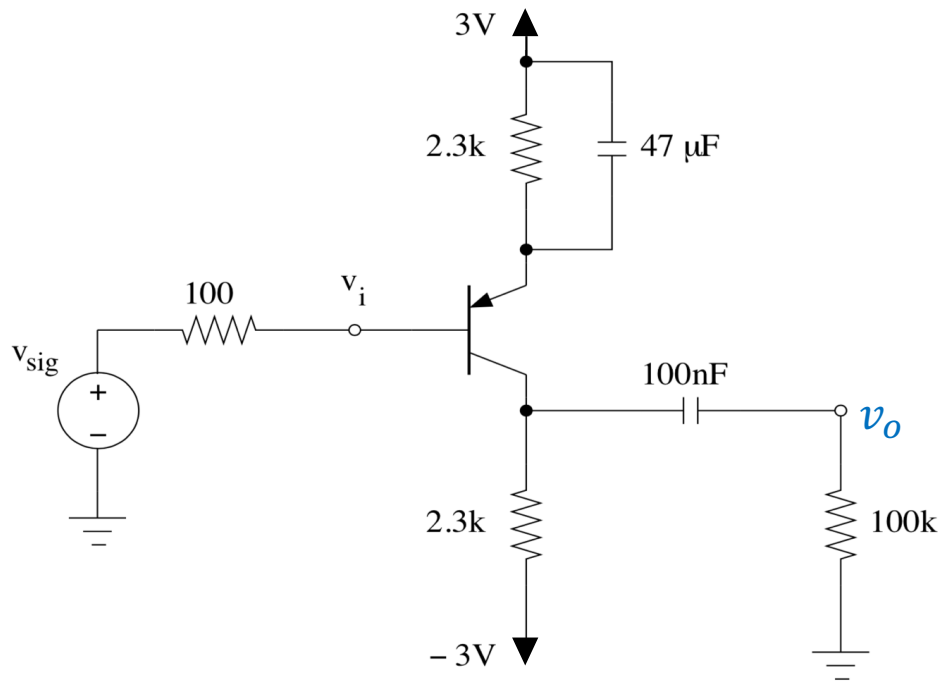
Draw the signal circuit (assume capacitors are short for signal).





## Lecture 19 reading quiz:

Find the transconductance,  $g_m$ , in this circuit ( $V_{D0} = 0.7 \text{ V}$ ,  $V_T = 26 \text{ mV}$ ,  $V_A = 150 \text{ V}$ ).



$$EB \text{ KVL: } 3V = 2.3k \times I_E + V_{BE} + 0.7kI_B$$

$$BJT \text{ is in active: } I_B = \frac{I_E}{1 + \beta} = \frac{I_E}{201}$$

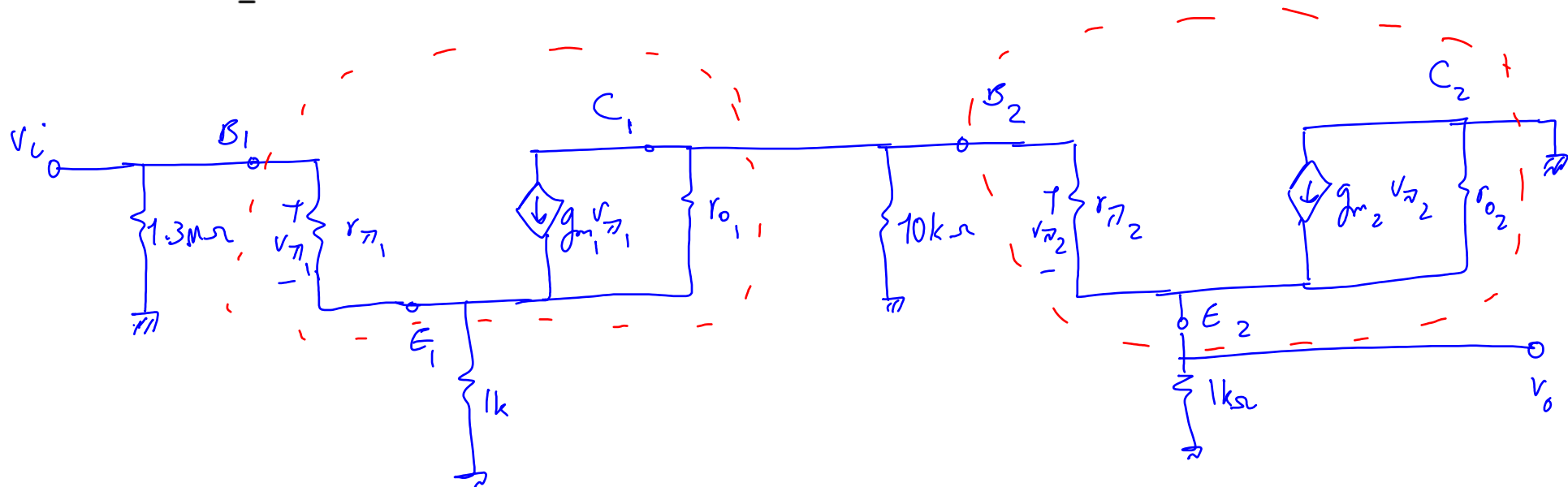
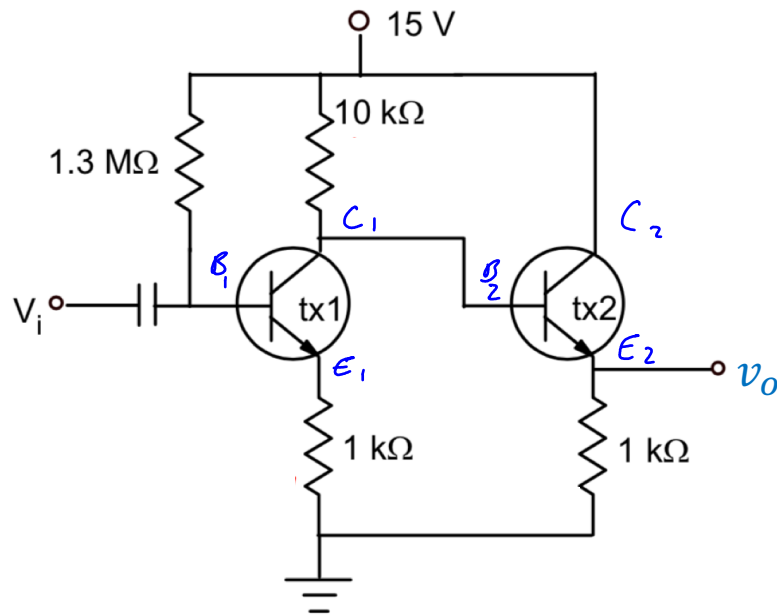
$$EB \text{ KVL: } 3V \approx 2.3k \times I_E + 0.7V \rightarrow I_E \approx 1mA \text{ and } I_C \approx I_E$$

$$EC \text{ KVL: } 3V = 2.3k \times I_E + V_{EC} + 2.3k \times I_C - 3V \rightarrow V_{EC} = 1.3V > 0.7V$$

$$g_m = \frac{I_C}{V_T} = \frac{1 \times 10^{-3} \text{ A}}{26 \times 10^{-3} \text{ V}} = 38.5 \text{ mA/V}$$

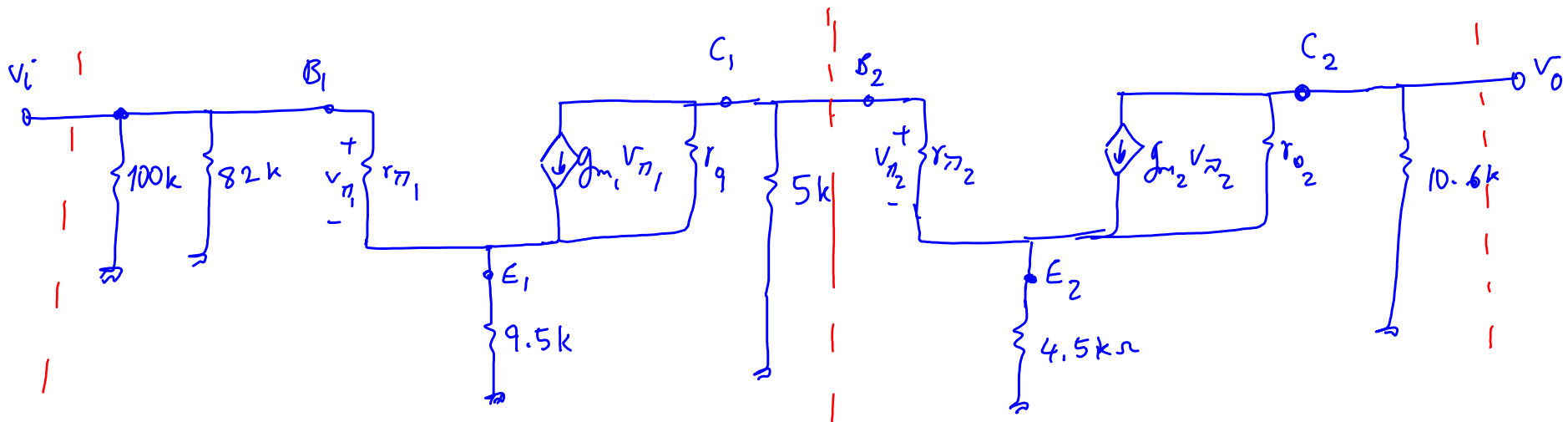
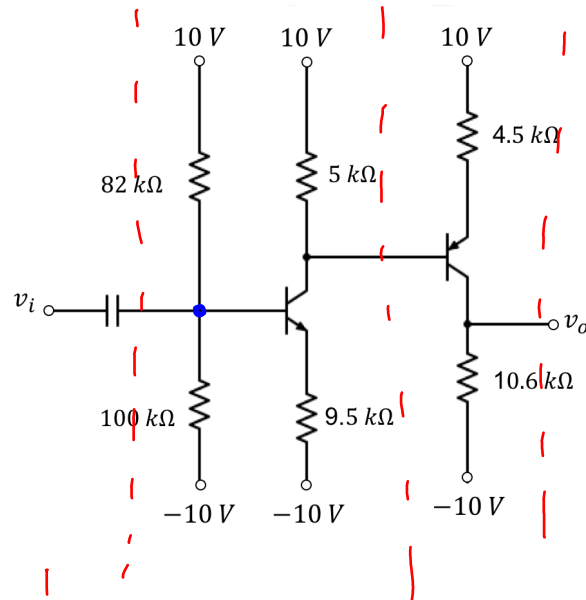
## Discussion question 1.

Draw the signal circuit (assume capacitors are short for signal).



## Discussion question 2.

Draw the signal circuit (assume capacitors are short for signal).

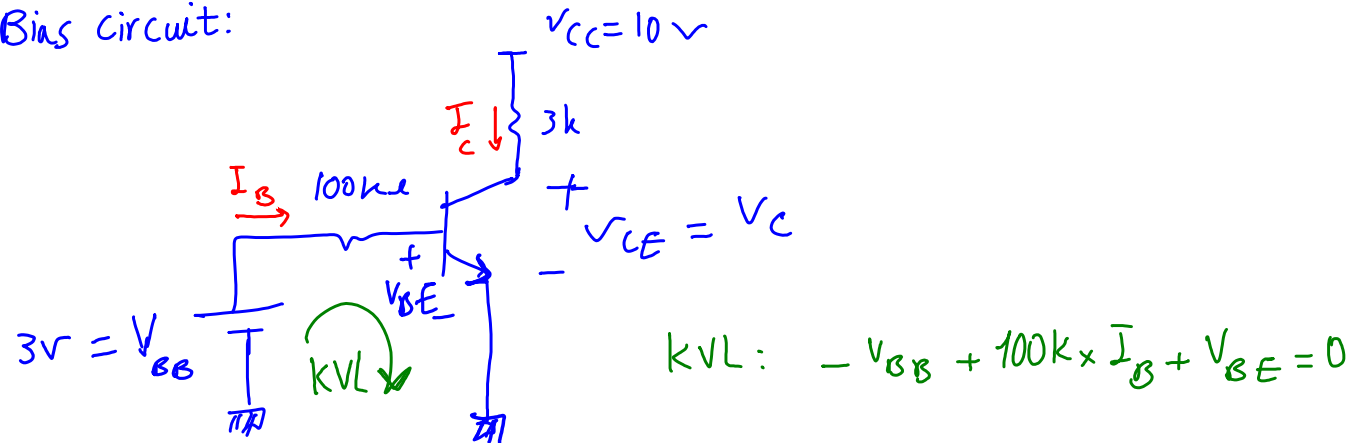
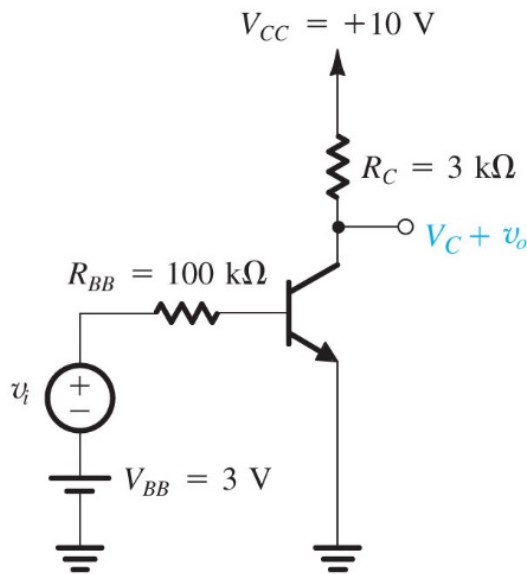


## Discussion question 3

For this amplifier circuit, find the small signal parameters, draw the signal circuit (assume capacitors are short for signal) and find  $v_o/v_i$ .

Assume  $\beta = 100$ ,  $V_T = 25 \text{ mV}$  and neglect the early effect.

Bias circuit:



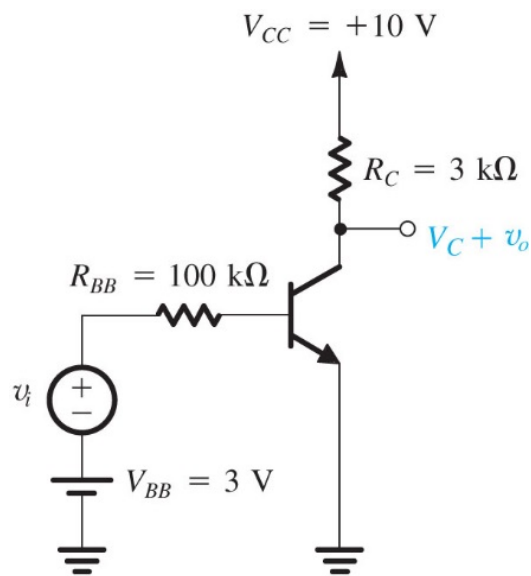
$$I_B = \frac{3 - 0.7}{100 \text{ k}\Omega} = 0.023 \text{ mA}$$

$$I_C = \beta I_B = 100 \times 0.023 \text{ mA} = 2.3 \text{ mA}$$

## Discussion question 3

For this amplifier circuit, find the small signal parameters, draw the signal circuit (assume capacitors are short for signal) and find  $v_o/v_i$ .

Assume  $\beta = 100$ ,  $V_T = 25 \text{ mV}$  and neglect the early effect.



small signal parameters:

$$g_m = \frac{I_C}{V_T} = \frac{2.3 \text{ mA}}{25 \text{ mV}} = 0.092 \text{ A/V}$$

$$r_\pi = \frac{\beta}{g_m} = \frac{100}{0.092} \approx 1.09 \text{ k}\Omega$$

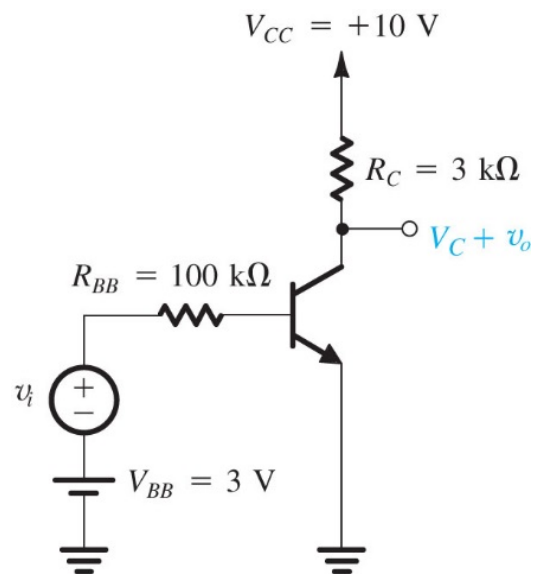
neglect the early effect:  $\lambda = 0$  or  $V_A = \infty$

$$r_o = \infty$$

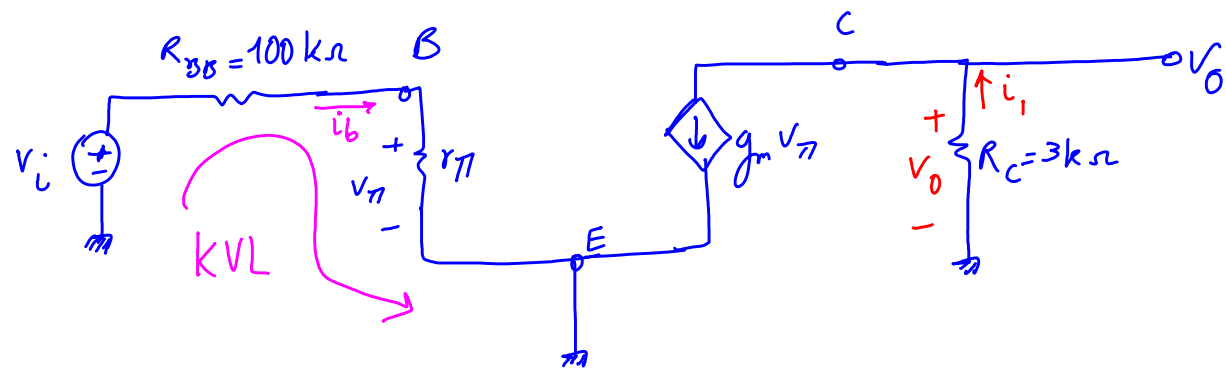
## Discussion question 3

For this amplifier circuit, find the small signal parameters, draw the signal circuit (assume capacitors are short for signal) and find  $v_o/v_i$ .

Assume  $\beta = 100$ ,  $V_T = 25 \text{ mV}$  and neglect the early effect.  $v_{\pi} = v_{be}$



signal circuit:



KCL @ node (C) :  $i_1 = g_m v_{\pi} \rightarrow v_o = -3\text{k}\Omega \times i_1$

$$v_o = -3\text{k}\Omega \times g_m v_{\pi}$$

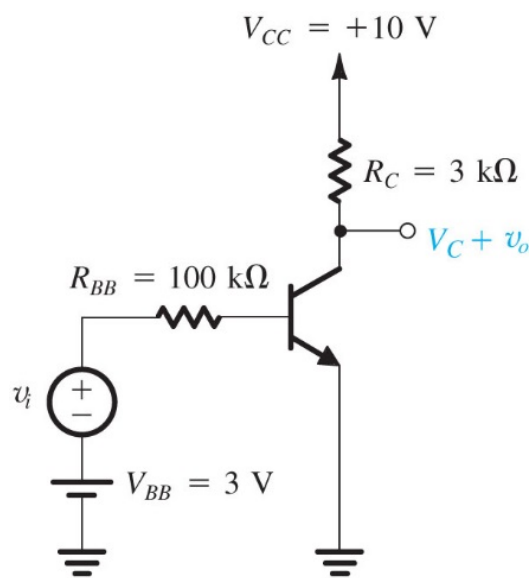
KVL:  $v_i = R_{BB} i_b + r_{\pi} i_b \rightarrow i_b = \frac{v_i}{R_{BB} + r_{\pi}}$   
and  $v_{\pi} = r_{\pi} \times i_b$

$$v_{\pi} = \frac{r_{\pi}}{r_{\pi} + R_{BB}} \times v_i$$

## Discussion question 3

For this amplifier circuit, find the small signal parameters, draw the signal circuit (assume capacitors are short for signal) and find  $v_o/v_i$ .

Assume  $\beta = 100$ ,  $V_T = 25 \text{ mV}$  and neglect the early effect.



$$V_o = -3 \text{ k} g_m v_{\pi} = -276 v_{\pi} \Rightarrow \boxed{v_o = -276 v_{\pi}}$$

$$v_{\pi} = \frac{1.09 \text{ k}\Omega}{1.09 \text{ k}\Omega + 100 \text{ k}\Omega} v_i \Rightarrow \boxed{v_{\pi} = 0.011 v_i}$$

$$\Rightarrow \boxed{A_v = \frac{V_o}{V_i} = -3.04 \text{ V/V}}$$