Reactor Core Physics Design and Operating Data for Cycles and 2 of TMI Unit 1 Power Plant Volume 1

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MASTER

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Reactor Core Physics Design and Operating Data for Cycles 1 and 2 of TMI Unit 1 PWR Power Plant Volume 1

NP-1410, Volume 1 Research Project 519-4

Final Report, August 1980 Work Completed, August 1979

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Prepared by The Babcock & Wilcox Company Lynchburg, Virginia

EPRI PERSPECTIVE

PROJECT DESCRIPTION

This report is one of several recently published documents intended to provide reference information on power reactor design and operating data. It is contained in two volumes. Volume 1 is being given the same breadth of distribution as was given to the Quad Cities 1, EPRI NP-240; Peach Bottom 2, EPRI NP-563; and Zion 2, EPRI NP-1232, reports. Volume 2, however, which contains only operating state-point data, is available only upon request to the Research Reports Center.*

Samples of these state-point data are given in Appendices A and B of Volume 1.

PROJECT OBJECTIVE

The purpose of RP519 has been to provide reference information on power reactor design and operating data for prototypical BWR and PWR designs. The project was begun because there was a lack of information in the open literature which was sufficiently complete to allow the testing of nuclear fuel management computer codes.

PROJECT RESULTS

This report contains information from a prototypical Babcock & Wilcox Co. reactor design. The following can be considered as companion reports:

- EPRI Topical Report NP-240 (Quad Cities 1)
- EPRI Final Report NP-472 (Monticello)
- EPRI Topical Report NP-563 (Peach Bottom 2)
- EPRI Final Report NP-827 (Turkey Point 3)
- EPRI Final Report NP-79-2-LD (Surry 1)
- EPRI Final Report NP-79-4-LD (Millstone 1)
- EPRI Final Report NP-1232 (Zion 2)

^{*}Research Reports Center P. O. Box 50490 Palo Alto, CA 94303 (415) 965-4081

Similar information from a CE reactor (ANO-2) will be published later this year as an account of work performed under RP1385.

This report will likely be most useful to nuclear fuel engineers who wish to exercise fuel management calculational methods; others, however, may have need for its fuel bundle design details, etc.

R. N. Whitesel, Project Manager Fuels, Waste and Environment Program Nuclear Safety and Analysis Department Nuclear Power Division

ABSTRACT

This report contains design and operating data for the first two fuel cycles at Three Mile Island Unit 1. These data are provided for use in benchmark testing of the Advanced Recycle Methodology Package and qualification of other reactor analysis and fuel management codes.

The design data include descriptions of the fuel pins, guide tubes, control elements, spacer grids, instrumentation, and core loading plans. The operating data supplied contain the plant primary and secondary side flows and temperatures, the operating rod pattern, and an incore detector signal map for each statepoint measurement. In addition, representative startup test results are provided for both cycles.

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ACKNOWLEDGMENT

The collection of the data presented in this volume was made possible by the cooperation and assistance of Metropolitan Edison Company (the operator of Three Mile Island Unit 1) and the Babcock & Wilcox Company (the reactor supplier).

The Project Manager for the Electric Power Research Institute was Dr. Robert N. Whitesel, who contributed many helpful suggestions as the work progressed. Dr. Y. S. Kim of NUS Corporation has participated in the technical and general editing of the final report.

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1. INTRODUCTION

This report provides design and operational data for the first two cycles of operation at Three Mile Island Unit 1 (TMI-1). The design data have been gathered primarily from B&W drawings and contract design documents; references to data available in public documents are provided where possible. The operating data provided were obtained from the on-line computer Performance Data Outputs (PDO) taken during plant operation.

2. TMI-1 FUEL ASSEMBLY AND CORE DESIGN DATA

Three Mile Island Unit 1 (TMI-1) is a pressurized water reactor operating at a design power level of 2535 Mwt. The reactor coolant (RC) system comprises two loops with one hot leg and two cold legs per loop. The reactor core contains 177 fuel assemblies each consisting of 208 fuel rods, 16 control rod guide tubes, and one incore instrument guide tube. Reactivity is controlled by 61 full-length Ag-In-Cd control rod assemblies and soluble boron shim. Eight partial-length Ag-In-Cd control rods are used to control the axial power distribution. In cycle 1 only, 68 burnable poison rod assemblies were inserted in the core. These assemblies were used mainly to ensure a negative moderator temperature coefficient of reactivity. The pertinent reactor design data and core loadings for the first two cycles of operation at TMI-1 are presented below.

2.1. Fuel Assembly Design Data

2.1.1. Fuel Assembly Configuration

The Mark B fuel assembly design consisting of a 15×15 array of rods is used at TMI-1. An assembly cross section is shown in Figure 2-1; general design information and dimensions are given in Table 2-1. Figure 2-2 shows the axial position of the active elements for a fuel rod, burnable poison rod, and control rod relative to the lower end fitting of an assembly.

2.1.2. Fuel Pin Description

B&W fuel pins consist of low-enriched UO₂ pellets clad in Zircaloy-4. Table 2-2 describes the design data for the fuel pellet and cladding used at TMI-1. Figure 2-3 shows a typical fuel pin.

2.1.3. Instrument Tube Description

The central cell in each fuel assembly consists of an instrument tube sized to accept an incore instrument string. A spacer sleeve prevents unacceptable grid movement and is located around the instrument tube between grid positions.

Table 2-3 provides the spacer sleeve and instrument tube dimensions. Figure 2-7, which shows the complete incore instrument, also shows the spacer sleeve and instrument tube.

2.1.4. Guide Tube Description

Each 15 by 15 fuel assembly contains 16 control rod guide tube locations as shown in Figure 2-1. These guide tubes may be empty or may contain a control rod assembly, orifice rod assembly, or burnable poison rod assembly. The guide tube design information is provided in Table 2-4.

2.1.5. Spacer Grid Description

Three different assembly designations were used in TMI-1. The Mark B-2, B-3 and B-4 assemblies are neutronically identical and have the same intermediate spacer grid spacing. The Mark B-2 assemblies, however, contain longer end spacer grids, as shown in Figure 2-4. The grid masses and dimensions are provided in Table 2-5.

2.1.6. Control Rod Assembly Description

Sixty-nine assemblies in the core contain movable Ag-In-Cd control rod assemblies in the guide tube locations. Figures 2-5 and 2-6 are drawings of the full and partial-length control rod assemblies. Details on the cladding, poison material, and dimensions are provided in Table 2-6. Section 2.3.2 describes the locations of the control rod assemblies.

2.1.7. Burnable Poison Rod Assembly Description

During the first cycle of operation at TMI-1 burnable poison rod assemblies (BPRAs) were inserted in selected fuel assemblies (see section 2.3.3) to shape the core radial power distribution and to provide a more negative moderator temperature coefficient. These BPRAs consisted of $16 \text{ Al}_2\text{O}_3\text{-B}_4\text{C}$ poison rods which fit into the assembly guide tubes. The BPRA is very similar to the full-length control rod assembly shown in Figure 2-5. The BPRA remains fully inserted during cycle operation. Design information is provided in Table 2-7, and $B_4\text{C}$ enrichments are given in Figure 2-9.

2.1.8. Orifice Rod Assembly Description

To prevent excess bypass flow, orifice rod assemblies (ORAs) are employed in selected fuel assemblies for cycles 1 and 2 at TMI-1. These rods did not protrude into the active core region at any time during operation. Design data are given in Table 2-8. The placement of the ORAs for cycles 1 and 2 is given in Figures 2-18, 2-19, and 2-20.

2.1.9. Fuel Assembly Loadings

The fuel assembly loading information for cycles 1 and 2 of TMI-1 is presented in Table 2-9. The placement of the various assemblies from each batch is shown in Figures 2-9 and 2-10 and described in section 2.3.1.

2.2. Instrumentation Design Data

2.2.1. Incore Detectors

There are 364 incore detectors at TMI which are grouped into 52 strings, each containing seven equally spaced rhodium detectors. Figures 2-7 and 2-8 are detector string drawings, and design data are provided in Table 2-10.

2.2.2. Excore Detectors

The excore instrumentation system has four neutron detector channels divided into three ranges of sensitivity: source, intermediate, and power range. The three ranges combine to give a continuous measurement of reactor power from below source level to over 125% of full power.

The source range instrumentation consists of two redundant, high-sensitivity ${\rm BF}_3$ proportional counters on opposite sides of the core. The intermediate range instrumentation consists of two electrically gamma-compensated ion chambers on opposite sides of the core. Both sets of instrumentation are positioned axially near the core midplane.

The power range instrumentation has four linear level channels originating in four detector assemblies, each of which contains two uncompensated ion chambers. The ion chambers are positioned to represent the top and bottom halves of the core. The individual currents from the chambers are fed to individual linear amplifiers.

2.3. Core Fuel and Poison Loading

2.3.1. Core Fuel Loading

The core loading diagrams for cycles 1 and 2 of operation at TMI-1 are presented in Figures 2-9 and 2-10, respectively. Fuel assembly locations by assembly identification number for cycle 1 and 2 are given in Figures 2-11 and 2-12. Figure 2-13 shows the cycle 2 core loading on the basis of the location of each assembly in cycle 1. Detailed core design data, including thermal-hydraulic information, is given in Table 2-11. Reactor coolant temperature versus power level is shown in Figure 2-14. Reflector and baffle volume fractions are given in Figure 2-15. The reactor vessel and internals are shown in Figures 2-16 and 2-17.

2.3.2. Control Rod Assembly Core Locations

Figures 2-18 through 2-20 show the CRA locations by operating group for the first two cycles of TMI-1 operation. Two distinct control rod operating group configurations were used during cycle 1, while only one configuration was used for the second cycle.

2.3.3. Burnable Poison Rod Assembly Core Locations

The core locations of the BPRAs used in cycle 1 of TMI-1 are given in Figure 2-9. At the end of cycle 1 the BPRAs were removed from all fuel assemblies, and cycle 2 was operated without BPRAs.

2.3.4. Nuclear Instrumentation Locations

Figure 2-21 shows the incore and excore locations of the nuclear instrumentation used at TMI-1 for both cycles of operation.

Table 2-1. Fuel Assembly Configuration

Item	Value	Source	Comments
Assembly pitch, in.	8.587	Physics Test Manual, TMI-1, Cy-1 p 1.1-1	Hereafter referred to as PTM
Assembly axial length, in.	165.625	TMI-1 Final Safety Hereafter reference Analysis Report, to as FSAR Vol 1A, p 3-97; No. 50-289	
Fuel pins per assembly	208	PTM, p 1.1-4	·
Fuel pin pitch, in.	0.568	FSAR Vol 1, p 1-64	
Guide tubes per assembly	16	FSAR Vol 1, p 1-65	
Instrument cells per assembly	1	PTM, p 1.1-1	

Table 2-2. Fuel Pin Description

Item	Value	Source	Comments
Fuel cladding material	Zirc-4	FSAR Vol 1, p 1-64	Cold-worked
Fuel cladding density, $1b/in.$ ³	0.238	Internal B&W document	Hereafter referred to as IBWD
Fuel cladding OD, in.	0.430	FSAR Vol 1, p 1-64	
Fuel cladding ID, in.	0.377	FSAR Vol 1, p 1-64	
Fuel pin axial length, in.	153.125	FSAR Vol lA, p 3-97	
Fuel pin active fuel length, in.	Table 2-9	IBWD	
Pellet-cladding diam. gap, in.	0.007	FSAR Vol 1, p 1-64	
Fuel pellet length, in.	0.700	FSAR Vol 1, p 1-64	
Fuel pellet OD, in.	0.370	FSAR Vol 1, p 1-64	
Fuel pellet dish factor ^(a)	0.9822	IBWD	
Fuel pellet density	Table 2-9	IBWD	

⁽a) The solid volume reduction factor from the volume of a solid cylinder without dishing.

Table 2-3. Instrument Tube Description

Item	<u>Value</u>	Source					
Instrument Tube							
Material	Zirc-4	FSAR Vol 1A, p 3-97					
Density, $lb/in.^3$	0.238	IBWD					
OD, in.	0.493	FSAR Vol 1A, p 3-97					
ID, in.	0.441	FSAR Vol 1A, p 3-97					
Spacer Sleeve							
Material	Zirc-4	FSAR Vol 1A, p 3-97					
Density, lb/in. ³	0.238	IBWD					
OD, in.	0.554	IBWD					
ID, in.	0.502	IBWD					

Table 2-4. Guide Tube Description

Item	<u>Value</u>	Source
Material	Zirc-4	IBWD
Density, $lb/in.^3$	0.238	IBWD
OD, in.	0.530	IBWD
ID, in.	0.498	IBWD

Table 2-5. Spacer Grid Description

Item	Value	Source
No. per assembly Intermed grids End grids	6 2	FSAR Vol 1, p 1-64
Material	Inconel 718	FSAR Vol 1A, p 3-97
Density, lb/in. ³	0.297	IBWD
Intermed grid ht, in.	1.50	IBWD
Mass, lb Intermed grid Mark B-2 end grid Mark B-3, B-4 end grid	1.6 4.6 3.0	

Table 2-6. Control Rod Assembly Description

Item	Value	Source	Comments
Pins per assembly	16	FSAR Vol 1, p 1-65	
CR driver rate, in./min	3/30		Jog rate/Run rate
CR stroke, in.	139		
Full-length control pins			
Absorber cladding material	304 SS	FSAR Vol 1, p 1-65	Cold-worked
Absorber cladding density, lb/in. ³	0.29	IBWD	
Absorber cladding OD, in.	0.440	FSAR Vol 1, p 1-65	
Absorber cladding ID, in.	0.398	FSAR Vol 1, p 1-65	
Absorber material	Ag-In-Cd	FSAR Vol 1, p 1-65	80% Ag, 15% In, 5% Cd
Absorber density, lb/in. ³	0.367	IBWD	
Absorber OD, in.	0.392	IBWD	
Absorber length, in.	134	FSAR Vol 1, p 1-65	
Partial-length control pins (APSRs)			
Absorber cladding material	304 SS	FSAR Vol 1, p 1-65	Cold-worked
Absorber cladding density, $1b/in.^2$	0.29	IBWD	
Absorber cladding OD, in.	0.440	FSAR Vol 1, p 1-65	
Absorber cladding ID, in.	0.398	FSAR Vol 1, p 1-65	
Absorber material	Ag-In-Cd	FSAR Vol 1, p 1-65	80% Ag, 15% In, 5% Cd
Absorber density, lb/in. ³	0.367	NMM	
Absorber OD, in.	0.375	IBWD	
Absorber length, in.	36	FSAR Vol 1, p 1-65	
Follower tube material	304 SS	IBWD	
Follower tube density, lb/in. ³	0.29	IBWD	
Follower tube OD, in.	0.440	IBWD	
Follower tube ID, in.	0.398	IBWD	

Table 2-7. Burnable Poison Rod Assembly Description

Item	Value	Source	Comments
BPRs per assembly	16	FSAR Vol 1, p 1-65	
BPR cladding material	Zirc-4	FSAR Vol 1, p 1-65	Cold-worked
BPR cladding density, lb/in. ³	0.238	IBWD	
BPR cladding OD, in.	0.430	IBWD	
BPR cladding ID, in.	0.360	IBWD	
BPR Pellets			
Material	Al ₂ O ₃ -B ₄ C	FSAR Vol 1, p 1-65	$\left\{ \begin{smallmatrix} 1 & 0 \\ B \end{smallmatrix} \right.$ in $B_4 C$ is the major absorber
Density, lb/in. ³	0.119	IBWD	
OD, in.	0.340	IBWD	
Length, in. (a)	126	FSAR Vol 1, p 1-65	
B ₄ C enrichment	Figure 2-9		

⁽a) Total of all pellets.

Table 2-8. Orifice Rod Assembly Description

Item	Value	Source	Comments
ORs per assembly	16	FSAR Vol 1, p 1-65	
OR material	304 SS	FSAR Vol 1, p 1-65	Annealed
OR material density, lb/in. ³	0.29	IBWD	
OR OD, in.	0.480	IBWD	
OR length, in.			The ORs do not reside in the active core.

Table 2-9. Fuel Assembly Loadings, Cycles 1 and 2

Item	Value	Source	Comments		
Batch 1					
Assembly design	Mark B-2	IBWD			
Fuel enrich., wt % 235U	2.06	IBWD			
Fuel pellet density, g/cm3	10.138	IBWD	92.5% TD/assembly		
²³⁸ U loaded, g/assy	454,723	IBWD			
²³⁵ U loaded, g/assy	9,551	IBWD			
Active length, in.	144.0	PTM, p 1.1-2	Before densif'n		
Batch 2					
Assembly design	Mark B-3	IBWD			
Fuel enrich., wt $% 235$ U	2.75	IBWD			
Fuel pellet density, g/cm3	10.138	IBWD	92.5% TD/assembly		
²³⁸ U loaded, g/assy	451,118	IBWD			
²³⁵ U loaded, g/assy	12,742	IBWD			
Active length, in.	144.0	PTM, p 1.1-2	Before densif'n		
Batch 3					
Assembly design	Mark B-3	IBWD			
Fuel enrich., wt % $^{235}\mathrm{U}$	3.05	IBWD			
Fuel density, g/cm^3	10.138	IBWD	92.5% TD		
²³⁸ U loaded, g/assy	449,992	IBWD			
²³⁵ U loaded, g/assy	14,149	IBWD			
Active length, in.	144.0	PTM, p 1.1-2	Before densif'n		
Batch 4					
Assembly design	Mark B-4	IBWD			
Fuel enrich., wt % $^{235}\mathrm{U}$	2.64	IBWD			
Fuel density, g/cm^3	10.25	IBWD	93.5% TD		
²³⁸ U loaded, g/assy	451,942	IBWD			
²³⁵ U loaded, g/assy	12,248	IBWD			
Active length, in.	142.5	IBWD	Before densif'n		

Table 2-10. Incore Instrument Description (a)

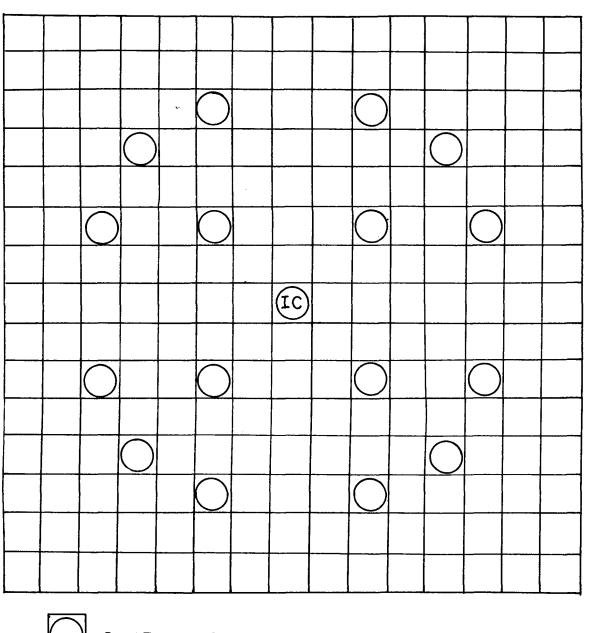
Item	Value	Comments
Instr. cladding material	Inconel 600	
Cladding OD, in.	0.062	
Detector material	Rhodium	
Detector mat. density, lb/in. ³	0.449	
OD, in.	0.018	
Nominal length, in.	4.75	
Detector leadwire material	Inconel 600	
OD, in.	0.009	
Backgrd detector material	Inconel 600	
OD, in.	0.009	
Insulation material	MgO	
Insulation density,	∿90% TD	
OD, in.	0.042	
Fillerwire material	Inconel 600	
OD, in.	0.062	
Detector axial spacing, in.	20.417	Equally spaced over active fuel length

⁽a) All values in this table were obtained from internal Babcock & Wilcox documents.

Table 2-11. Core Design Data

Item	Value	Source	Comments
Core rated power, MWt	2535	PTM p 1.1-1	
No. of FAs	177	PTM p 1.1-1	
Core equiv. diam., in.	128.9	FSAR Vol 1A, p 3-81	
Core active height	Table 2-9	•	
Reflector thickness, in.			
Top/bottom/side	12/12/18	FSAR Vol 1, p 1-66	All water + steel
Reflector volume fractions	Figure 2-15		
Core inlet coolant temp, F	554.0	FSAR Vol 1, p 1-68	100% FP
Core avg coolant temp, F	579.7	FSAR Vol 1, P 1-68	>15% FP
Core avg fuel temp, F	1280.0	FSAR Vol 1A, p 3-79	100% FP
Cycle 1			
Cycle exposure, EFPD	466.4	BAW-1443	14,406 MWd/mtU (core avg fuel BU)
No. of batch 1 assys	56	PTM pp 22-38	
No. of batch 2 assys	61	PTM pp 22-38	
No. of batch 3 assys	60	PTM pp 22-38	
No. of batch 4 assys	0	PTM pp 22-38	
No. of CRAs	69	PTM p 1.1-3	
No. of BPRAs	68	PTM p 1.1-3	
Cycle 2			
Cycle exposure, EFPD	256.2	IBWD	17,547 MWd/mtU (cycle 2 core avg BU)
No. of batch 1 assys	0	IBWD	
No. of batch 2 assys	61	IBWD	
No. of batch 3 assys	60	IBWD	
No. of batch 4 assys	56	IBWD	
No. of CRAs	69	IBWD	
No. of BPRAs	0	IBWD	

Figure 2-1. Mark B Assembly Pin Layout



	GUIDE TUBE	
	FUEL PIN CELL	
IC	INSTRUMENT CHANNEL	CELL

TYPICAL FUEL ROD POISON LOWER END POISON LOWER END 13.13 BURNABLE POSION ROD FUEL LOWER END 9.80 CONTROL ROD 10.80 APSR FULLY INSERTED LOWER END (MK-B 2, 3, & 4) FITTING **-** 0.030 MAX 4-1/4 (MK-B3 & MK-B4) 4-5/8 (MK-B2)

Figure 2-2. Relative Axial Positions of Active Elements of Assembly Components

NOTE: ALL DIMENSIONS IN INCHES.

Figure 2-3. Typical Mark B Fuel Pin

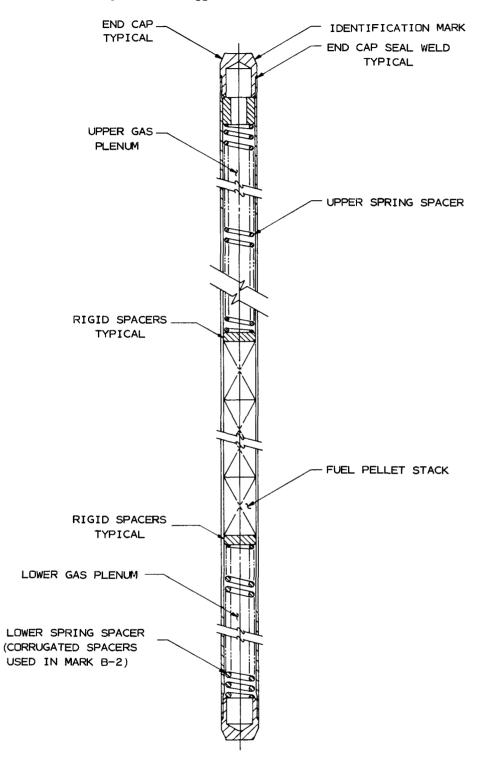
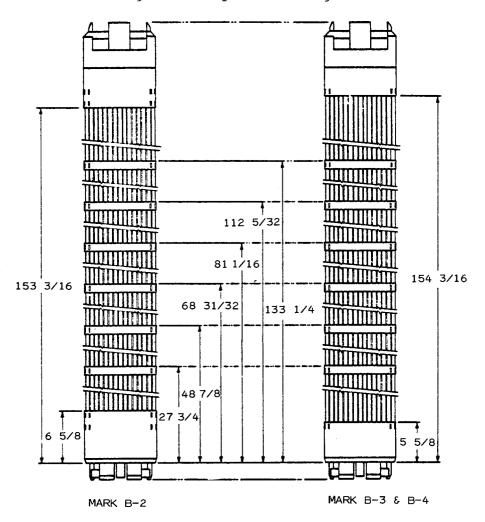
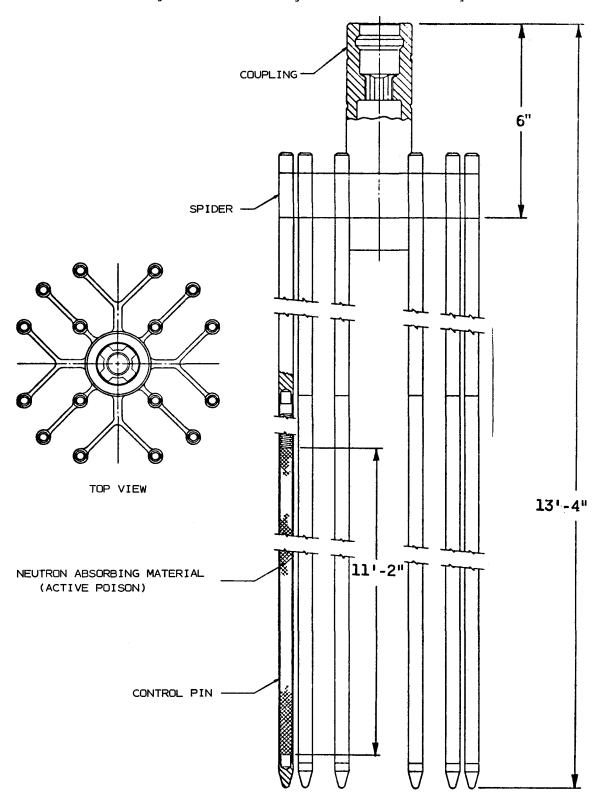


Figure 2-4. Spacer Grid Diagram



NOTE: DIMENSIONS IN INCHES.

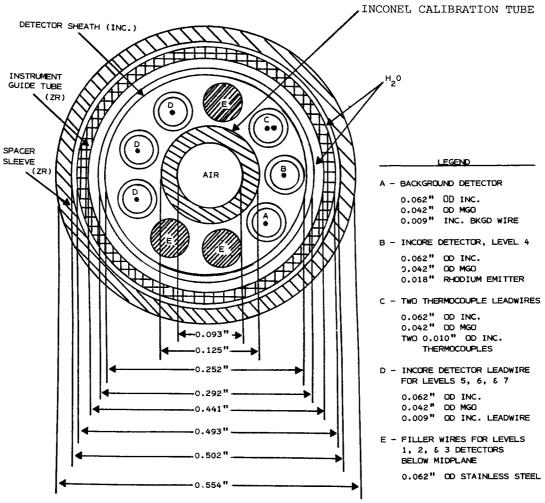
Figure 2-5. Full-Length Control Rod Assembly



COUPLING . SPIDER 13'-4" TOP VIEW FOLLOWER MATERIAL-NEUTRON ABSORBING MATERIAL (ACTIVE POISON) PART-LENGTH CONTROL ROD

Figure 2-6. Partial-Length Control Rod Assembly

Figure 2-7. B&W Rhodium Emitter, Self-Powered Neutron
Detector Assembly at Core Midplane
INCONEL CALIBRE



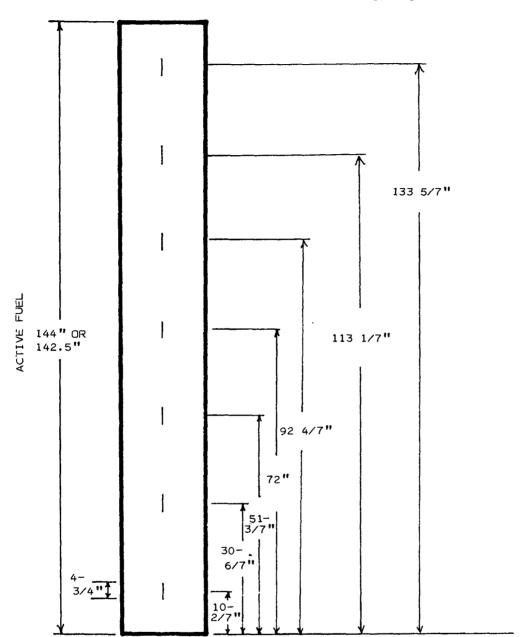


Figure 2-8. Incore Detector Axial Spacing

Figure 2-9. Cycle 1 Enrichment and BPRA Configuration

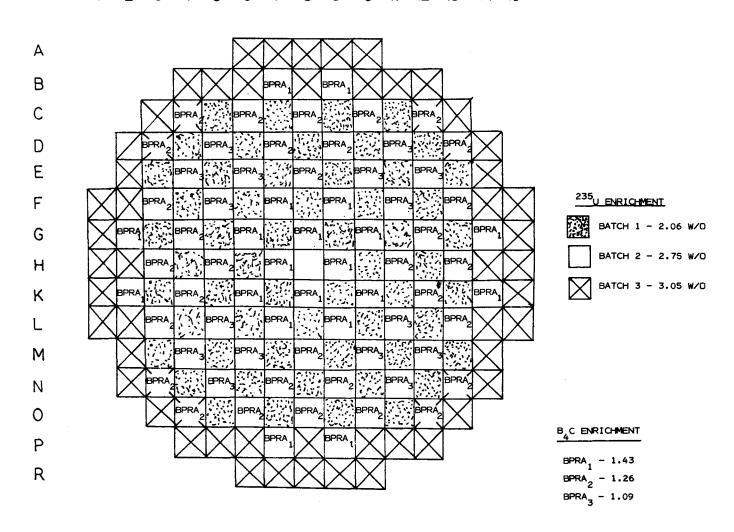


Figure 2-10. TMI-1 Cycle 2 Enrichment Configuration

23456789101112131415

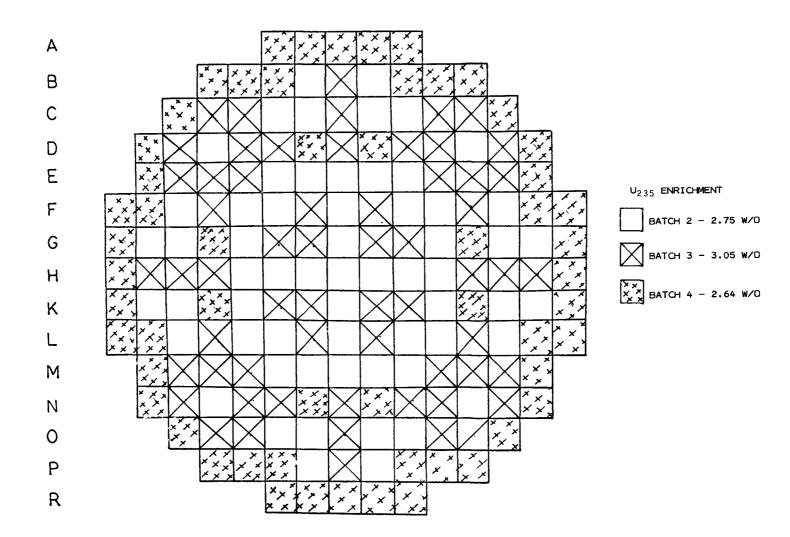


Figure 2-11. TMI-1 Cycle 1 Fuel Assembly ID Loading Diagram

Α						CI	cz	сз	CH	C5	ì					
В				C6	c٦	СВ	BI	c٩	BR	C 10	CII	CIZ				
С			C13	C14	AI	В3	AZ	B4	-A3	B5	A4	C15	C16			
D	1	сıч	CIB	A 5	B6	AG	B 7	PT	88	AB	B 9	A9	CI9	c20		
E		CZI	AIO	B10	AII	311	A12	BIZ	АІЗ	B 13	AI4	B14	A15	CZZ		
F	C23	C24	B15	A16	B16	AIT	BI7	AIB	B18	AIQ	B 19	A20	B2 0	c 2 5	C26	INITIAL ENRICHMENT_
G	CZ7	BZI	A21	B22	A22	B23	A23	B24	A24	B25	A25	BZG	A26	вгт	C28	A - BATCH 1, 2.06 W/D
Н	C29	C30	B28	A27	B29	A28	B30	B31	ВЗ2	A29	B33	A30	B34	C31	c32	B - BATCH 2, 2.75 W/D C - BATCH 3, 3.05 W/D
K	C33	B35	A31	અદ છ	АЗг	837	A33	B38	A34	B39	A35	B40	A36	BAI	C34	
L	C35	C36	B42	PST	B43	ค38	1344	A39	1345	A40	B46	A41	1347	C37	C38	
М		C39	A42	B48	A43	B49	ษาป	ß50	A45	B51	A46	852	A47	C40		•
N		C41	C42	BPB	B 53	A49	B54	A60	B55	A51	B56	A52	C43	C44		
0			C45	C46	A53	B57	A54	858	A55	B59	A56	C47	c48			-
Р				C49	C50	C51	BGO	C52	861	C53	C54	৫55				XNN FUEL ASSEMBLY ID
R						056	৫১৭	C58	୯୪୨	C60			-			

Figure 2-12. TMI-1 Cycle 2 Fuel Assembly ID Loading Diagram

Α						DI	DS	DЗ	ÞФ	<i>D</i> 5						
В				06	דס	80	BIT	сз	ВІВ	D9	D10	DII				
С			DIZ	C6	CI	В3	В6	c9	B 9	85	C 5	CIZ	DB			
D	•	DIA	CIT	BIZ	C2	сч	DI5	C14	DIG	CII	CH	B33	CZO	DIJ		
Ε		D18	C23	C27	CI3	Вп	Bi	B22	Вг	ВІЗ	CIG	C28	CSP	DIO		
F	DSO	DZI	B15	CZI	B16	BT	89	Вч	CIO	826	B19	C22	B20	DZZ	D23	
G	D24	B23	BIO	D25	B21	C24	CIB	B24	CIS	C25	вал	DSP	B14	B25	D27	INITIAL ENRICHMENT B - BATCH 2, 2.75 W/O
н	DSB	029	C 3 0	C42	B 54	B28	B30	B31	B32	B34	BØ	CIA	C31	C32	DSd	C - BATCH 3, 3.05 W/D D - BATCH 4, 2.64 W/D
K	D30	B37	B48	D31	B 35	୦୫୦	C46	B38	C43	ር3ፕ	ઉના	D32	ß52	P&A	D33	
L	D34	D35	B42	୯୫୨	B43	B36	হে	<u>გ</u> 58	C53	855	846	C40	B47	D36	TEC	
М		D38	૯૩5	C33	C45	B49	৪৫০	B40	B61	351	C48	C34	C36	PEŒ		
N		D40	СЧІ	B 29	c57	C50	D41	C47	D42	C54	c59	1350	ट बर्ग	D43		
0			D44	C49	C56	B 57	853	C52	656	B 59	C59	c55	D45			
Р				D46	D47	D48	1344	୯୭୫	B 45	D49	D 50	D51				XNN FUEL ASSEMBLY ID
R						D52	D53	D54	D 55	D56						

Figure 2-13. TMI-1, Cycle 1-Cycle 2 Full Shuffle Pattern

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
A						4	4	4	4	4					
В				4	4	4	2 F-7	3 A-8	2 F-9	4	4	4			
С			4	3 B-4	3 A-6	2 C-6	2 D-5	3 B-8	2 D-11	2 C-10	3 A-10	3 B-12	4		
D		4	3 D-2	2 E-8	3 A-7	3 B−5	4	3 C-4	4	3 9-11	3 A-9	2 H-11	3 D-14	4	
E		4	3 F-1	3 G-1	3 C-3	2 E-6	2 B-7	2 G-4	2 B-9	2 E-10	3 C-13	3 G-15	3 F-15	4	
F	4	4	2 F-3	3 E-2	2 F-5	2 D-7	3 B-6	2 C-8	3 B-10	2 G-12	2 F-11	3 E-14	2 F-13	4	4
G	4.	2 G-6	2 E-4	4	2 G-2	3 F2	3 D-3	2 G-8	3 C-12	3 F-14	2 G-14	4	2 E-12	2 G-10	4
н	4	3 H-1	3 H−2	3 N-3	2 N-7	2 H-3	2 - 7	2 H-8	2 H-9	2 H-13	2 D-9	3 D-13	3 H-14	3 ⊢-15	4
к	4	2 K-6	2 M –4	4	2 K-2	3 L-2	3 0-4	2 K-8	3 N-13	3 L-14	2 K-14	4	2 M-12	2 K-10	4
L	4.	4	2 L-3	3 M-2	2 L-5	2 K-4	3 P-6	2 0-8	3 P-10	2 N–9	2 L-11	3 M-14	2 L-13	4	4
М		4	3 ∟–1	3 K-1	3 D-3	2 M-6	2 P-7	2 K-12	2 P-9	2 M-10	3 0-13	3 K-15	3 ∟–15	4	
N		4	3 N-2	2 H-5	3 R-7	3 P-5	4	3 0–12	4	3 P−11	3 R-9	2 M-8	3 N-14	4	
0			4	3 P-4	3 R-6	2 0-6	2 N-5	3 P-8	2 N-11	2 0-10	3 R-10	3 P-12	4		
Р				4	4	4	2 L-7	3 R-8	2 L-9	4	4	4		•	
R						4	4	4	4	4			•		

BATCH
Y PREVIOUS CORE LOCATION
IN CYCLE 1

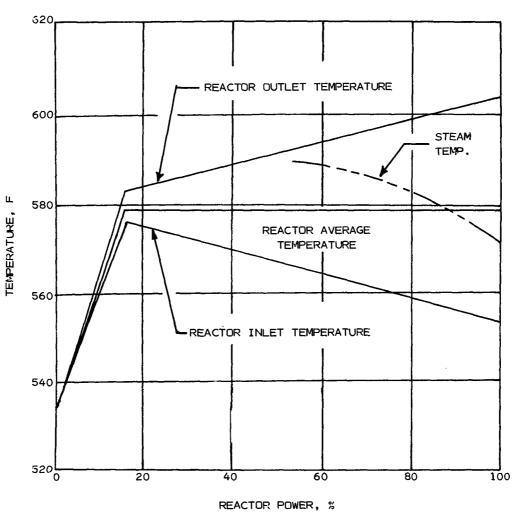
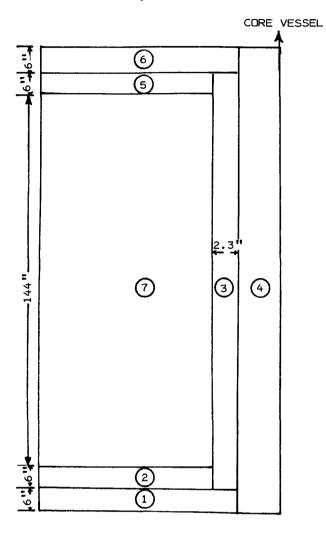


Figure 2-14. Reactor Temperature Vs Power Level

Figure 2-15. Reflector and Baffle Volume Fractions



LEGEND

- 1. LOWER REFLECTOR STEEL REGION
- 2. LOWER REFLECTOR REGION
- 3. BAFFLE REGION
- 4. OUTER REFLECTOR REGION
- 5. UPPER REFLECTOR REGION
- 6. UPPER REFLECTOR STEEL REGION
- 7. FUEL REGION

REGION	<u>VOID</u>	ZR CLADDING	_SS	MODERATOR
1		-	0.426	0.574
2	0.315	0.102		0.583
3			0.330	0.670
4			0.198	0.802
5	0.315	0.102		0.583
6			0.196	0.803

- STUDS - INTERNALS VENT VALVE PLENUM ASSEMBLY -- CONTROL ROD GUIDE TUBE CORE SUPPORT INLET MOZZLE OUTLET MOZZLE -- FUEL ASSEMBLY CORE BARREL -REACTOR VESSEL SURVEILLANCE SPECIMEN -THERMAL SHIELD LOWER GRID -GUIDE LUGS FLOW DISTRIBUTOR INCORE INSTRUMENT

Figure 2-16. Reactor Vessel View Diagram

CORE BAFFLE
REGION

21.550
TYP REF

55.898
TYP
REF

47.311
TYP
REF

21.550
TYP
REF

Figure 2-17. Reactor Vessel Internals

NOTE: ALL DIMENSIONS IN INCHES.

Figure 2-18. TMI-1 Cycle 1 Control Rod Configuration, 0-250 EFPD

Α										!							
В			*		٦		4		٦		*						
С				5		3		3		5							
D			4		8		ی		8		I						
E		5		ی		\		1		ی		5					
F	٦		8		2		2		2		8		7			CR GROUP	PURPOSE
G		3		١		5		5		١		3				1-4 5 6	SAFETY DOPPLER DOPPLER
Н	7		ی		2		٦		2		ی		7			7 8	TRANSIENT APSR
ĸ		3		١		5		5		Ý		3					
L	٦		8		2		2		2		8		٦				
M		5		6		١		١		6		5					
N			4		8		6		8		4						
0				5		3		3		5)	K	ORIFICE ROD	ASSEMBLY
Р			*		٦		4		٦		*						
R												•					

Figure 2-19. TMI-1 Cycle 1 Control Rod Configuration, 250-466 EFPD

Α																
В			*		4		7		4		*					
С				5		3		3		5						
D			٦		8		6		8		٦					
Ε		5		ی		1		- 1		9		5				
F	4		8		2		2		2		8		4		CR GROUP	ASSIGNMENT
<u>:</u> G		Ś		1	3	5		5		١		3			1–4 5	SAFETY DOPPLER
Н	٦		ی		ય		٦		2		ی		٦		6 7 8	DOPPLER TRANSIENT APSR
K		3		١		5		5		1		3				
L	4		8		2		2		2		8		4			
М		5		6		i		1		6		5				
N			7		8		6		8		7					
0				5		3		3		5				*	ORIFICE ROD A	SSEMBLY
Р			*		7		7		4		*		•			
R											·					
										•						

Figure 2-20. TMI-1 Cycle 2 Control Rod Configuration, 0-256.2 EFPD

											_						
A																	
В				*		4		5		4							
С				*	2	*	٦	*	7	*	2	*					
D	1		*	6	*	8	*	3	*	8	*	6	*				
Ε			2	*	ტ	*	1	*	1	*	3	*	2				
F		4	*	8	*	5	*	6	*	5	*	8	*	4		CR GROUP	PURPOSE
G			٦	*	١	*	3	*	3	*	١	*	7			1-4 5-7	SAFETY CONTROL
Н		5	*	3	*	6	*	4	*	6	*	3	*	5		8	APSR
K			7	*	1	*	3	*	3	*	1	*	7				
L		4	*	8	*	5	*	6	*	5	*	8	*	4			
M			2	*	3	*	١	*	ı	*	3	*	2				
N			*	6	*	8	*	3	*	8	*	6	*		 	ORIFICE ROD	ACCEMOL V
0				*	ಒ	*	7	*	٦	*	2	*				LOCATIONS	ASSEMBL Y
Р						4		5		4		*		•			
R													•				
											•						

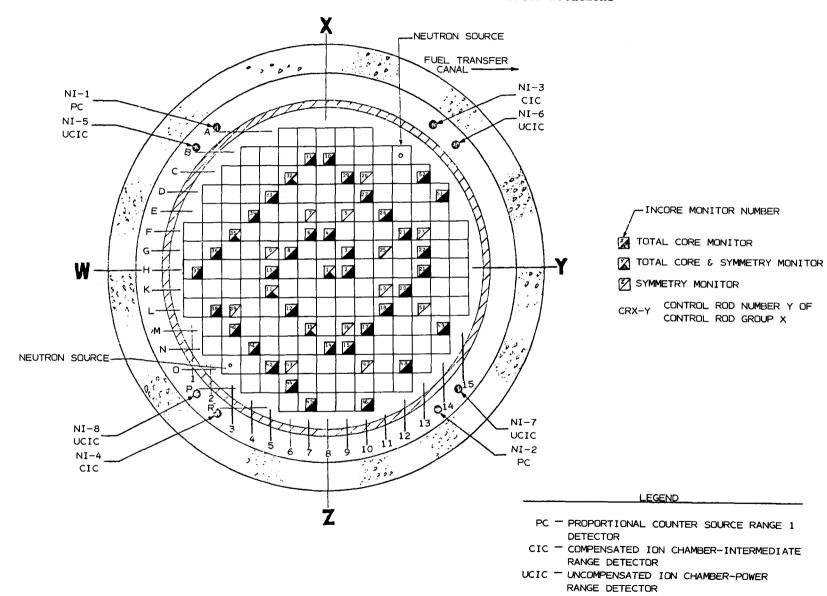


Figure 2-21. Nuclear Instrumentation Detector Locations

3. STARTUP TEST RESULTS

Startup tests were conducted both at hot zero power (HZP) and during power escalation for the first two cycles of operation at TMI-1. A brief description of the tests and the measurement results are given below.

3.1. All-Rods-Out Critical Boron Concentration and Differential Boron Worth

The all-rods-out critical boron concentration (AROCBC) test was conducted at HZP by borating the reactor coolant system so that control rod groups 1-6 and 8 were fully withdrawn and group 7 was positioned to maintain criticality (approximately 80% withdrawn). Once steady-state conditions were established, control rod group 7 was withdrawn to 100% (full out), and the resultant reactivity change was measured with a reactimeter.* The reactivity addition from the group 7 rod worth was then converted to an equivalent change in boron concentration and added to the equilibrium critical boron concentration to yield the measured results. The AROCBC test results for cycles 1 and 2 are presented in Table 3-1.

Measurements of the differential boron worths at HZP were performed in conjunction with the control rod worth measurements. The control rod worths were measured by the boron swap technique in which a boration/deboration rate was established and the control rods were withdrawn/inserted to compensate for the changing core reactivity. The reactimeter was used to provide a continuous reactivity calculation throughout the measurement. The differential boron worth was then determined by summing the incremental reactivity values measured with the reactimeter during the rod worth measurements over a known boron concentration range. The average differential boron worth is the measured change in reactivity divided by the change in boron concentration. Table 3-1 gives the differential boron worth measured for cycles 1 and 2.

^{*}Reactimeter" is the name given to the Babcock & Wilcox reactivity meter, which solves the monoenergetic, point reactor kinetics equations with six delayed neutron groups for core net reactivity based on periodic samples of neutron flux.

3.2. Control Rod Group Worths

Control rod group reactivity worth was measured at HZP using the rod drop and boron/rod swap methods. The boron/rod swap method was used to determine differential and integral rod worths for control rod groups 5 through 8 from 100 to 0% withdrawn, and for group 4 from 100 to 50% withdrawn. The rod drop method was used to obtain the total worth of groups 1 through 4 (group 4 from 50 to 0% withdrawn). The HZP rod group worths are given in Table 3-2 for TMI-1 cycles 1 and 2. Figures 3-1 through 3-3 provide integral rod worth curves for cycle 1.

For cycle 1, rod worths were determined at three different power levels using an insert/withdrawal technique to measure differential rod worths. Using the reactimeter, the differential worth was obtained by dividing the known change in core reactivity by the change in rod position. Results are summarized in Table 3-3.

3.3. Reactivity Coefficients

The four measured coefficients of reactivity presented in this report are defined as follows:

- The temperature coefficient of reactivity is the fractional change in core net reactivity per unit change in fuel and moderator temperature.
- The moderator temperature coefficient of reactivity is the fractional change in core net reactivity per unit change in moderator temperature.
- The power Doppler coefficient of reactivity is the fractional change in core net reactivity per unit change in core power.
- The Doppler coefficient of reactivity is fractional change in core net reactivity per unit change in fuel temperature.

The technique used to measure the isothermal temperature coefficient at zero power was to first establish steady-state conditions and then initiate a positive heatup by closing the turbine bypass valves. After the core average temperature increased by about 10F, core temperature and neutron flux were stabilized and the process was reversed by decreasing the core average temperature to the initial value by opening the turbine bypass valves. This procedure was repeated two times at each chosen boron concentration to establish the reproducibility of measured value. The temperature coefficient from the measured data was then calculated by dividing the change in core reactivity by the corresponding change in core temperature. The measured HZP temperature coefficients for cycles 1 and 2 are summarized in Table 3-4.

The temperature coefficients at power were measured by increasing the reactor coolant average temperature by 5F. The actual temperature change, rod movement,

reactivity additions, and any power changes were monitored. The individual reactivity effects were summed and then divided by the change in core average temperature to obtain the temperature coefficient.

The power Doppler coefficient of reactivity was measured in a similar manner. After the prerequisite conditions were established, reactor power was decreased by 5% while the data were recorded. The reactivity effects of the power change were summed and then divided by the change in power to obtain the power Doppler coefficient. The measurement was repeated by increasing core power by 5% to the initial level.

The moderator, temperature, and Doppler coefficients* of reactivity were calculated from the measured temperature and power Doppler coefficients.

Table 3-5 contains the various reactivity coefficients at power measured for the first two cycles of operation at TMI-1.

3.4. Dropped Control Rod Test

The dropped control rod test for cycle 1 was conducted at 40% full power by measuring the worth of the control rod in location H-4 as it was inserted in the core and by measuring the resultant maximum quadrant power tilt with the dropped rod at 86, 49, and 0% withdrawn. In cycle 2 the maximum quadrant power tilt was measured with the control rod in location E-11 at 0% withdrawn. The results of these measurements are provided in Table 3-6.

3.5. Pseudo-Ejected Rod Worth Test

The Pseudo-ejected rod test was conducted during cycle 1 startup at 40% FP with equilibrium xenon established in the core. Control rod groups 1 through 5 were positioned at 100% withdrawn, group 6 at 75%, group 7 at 0%, and group 8 at 13% withdrawn to maintain core axial imbalance $^{\#}$ at 0 \pm 2%.

Control rod H-8 was withdrawn to 100% (in small increments) by performing a rod swap with control rod group 6. Differential reactivity worth was measured on group 6 using the fast insert/withdrawal technique with control rod H-8 positioned at 0% withdrawn and again at every 20% withdrawal interval. The total reactivity

The Doppler coefficient is determined from the power Doppler coefficient and the calculated relationship between power and fuel temperature.

^{*}Axial imbalance = [(% power in top half of core) - (% power in bottom half of core)](fraction of total core power).

worth of rod H-8 from 0 to 100% withdrawn was then obtained by integrating the differential worth data measured on group 6. Core power distribution measurements were taken with control rod H-8 positioned at 100% withdrawn. The test results are summarized in Table 3-7.

Table 3-1. Critical Boron Concentration and Boron Worth — Hot Zero Power

Item	<u>Value</u>	Source	Comments
AROCBC, ppmB			
Cycle 1	1617	TMI-1 Initial Startup Report No. 50-289	At 532F mod temp.
Cycle 2	1384	IBWD	At 532F mod temp.
Differential B worth, % \(\Delta k \/ 100 \) ppmB			
Cycle 1	1.06 1.05 1.06	TMI-Initial Startup Report No. 50-289	At ∿1320 ppmB At ∿1520 ppmB At ∿1590 ppmB
Cycle 2	0.97	IBWD	At ∿1257 ppmB

Table 3-2. Control Rod Worths at Hot Zero Power

Item	<u>Value</u>	Source	Comments
CR group integral worths, % $\Delta k/k$			
Cycle 1	(1.)		
Group 1 (8 rods, 0-100% (a) 2 (8, 0-100) 3 (8, 0-100) 4 (8, 0-49)	4.33 ^(b)	TMI-Initial Startup Report, No. 50-289	Corrected measured worth is 5.85 based on previous plant comparisons
5 (12 rods)	1.03		to calculation
6 (8)	1.25		
7 (9)	1.10		
8 (8)	0.39		
Cycle 2			
Group 1-4 (37 rods)	7.444	IBWD	
5 (8)	0.68		
6 (8)	1.06		
7 (8)	0.772		
Total 1-7 (61 rods)	9.956		

⁽a) 0-100% withdrawn interval.

Table 3-3. TMI-1, Cycle 1 - Measured Differential Rod Worths at Power

Power level,	Boron conc,	Rod gr	oup pos	sition,	% wd	Δ rod worth,
% FP	ppmB	1-5	_6_		8	10^{-3} % $\Delta k/k/\%$ wd
40	1192	100	72.2	0	33	9.44
40	1188	100	65.5	0	13	11.39
76	1120	100	85.5	15.0	20	15.03
100	1092	100	86.0	11.0	0	11.55

⁽b) Uncorrected.

Table 3-4. TMI-1 Temperature Coefficient Measurements at Hot Zero Power Conditions

Boron conc, ppmB	Control : positie (% wd	on	Temp coeff, $10^{-\frac{1}{4}} \ \Delta k/k/^{\circ}F$
Cycle 1			
1601		(100) (78) (100)	+0.449
1461	7	(100) (78) (0) (27)	+0.304
1269		(100) (95) (0) (27)	-0.527
1245	5-7	(100) (50) (0) (27)	-0.604
Cycle 2			
1375	Groups 1-7	(100) (0)	+0.094
1154	Groups 4 5-8	(100) (0)	-0.530

Table 3-5. TMI-1 Reactivity Coefficients at Power

Core	Boron conc,	Coe	eff of reactivity	γ, 10 ⁻⁴ Δk	:/k
% FP	ppmB	Temp	Power Doppler	Moder.	Doppler
Cycle 1					
100	1090	-0.329	-1.14	-0.222	-0.107
Cycle 2					
100	820	-1.26	-1.17	-1.1	

Table 3-6. TMI-1 Dropped Rod Test

CR position,	Max quadrant power tilt, % (incore det's)		
Cycle 1, H-4 (a)			
86	+0.26 XY,	-0.71 ZW	
49	+5.69 XY,	-6.01 ZW	
0	+13.98 YZ,	-14.07 ZW	

Measured reactivity worth of CR in location H-4 = 0.094% $\Delta k/k$.

- (a) Banks 1-5 100% wd, bank 6 88%, bank 7 15%, and bank 8 35%.
- (b) Quadrant tilt % =

Quadrant axes shown in Figure 2-21.

Table 3-7. TMI-1, Cycle 1 — Core Tilt and Rod
Worth During Pseudo-Rod Ejection

Rod position,	Incore imbalance,	Quadrant tilt, %			Fuel assembly	
% wd % wd	_WX	<u> XY</u>	_WZ	<u>YZ</u>	location	
0	-1.90	-0.28	+0.26	-0.21	+0.22	K-10
100	-8.37	-0.28	+0.01	-0.15	+0.42	н-8

The measured worth of CR in location H-8 was 0.278% $\Delta k/k$.

Figure 3-1. TMI-1 Cycle 1 — Control Rod Group Integral Worth at Zero Power, 532F, 0 EFPD

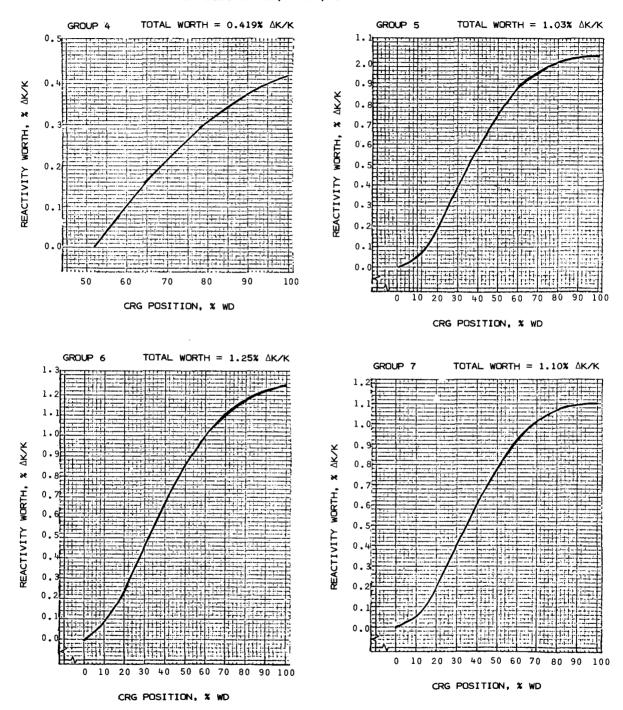


Figure 3-2. TMI-1 Cycle 1 — Control Rod Group 8 Integral Worth at Zero Power, 532F, 0 EFPD

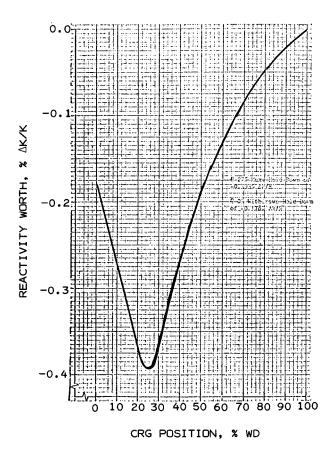
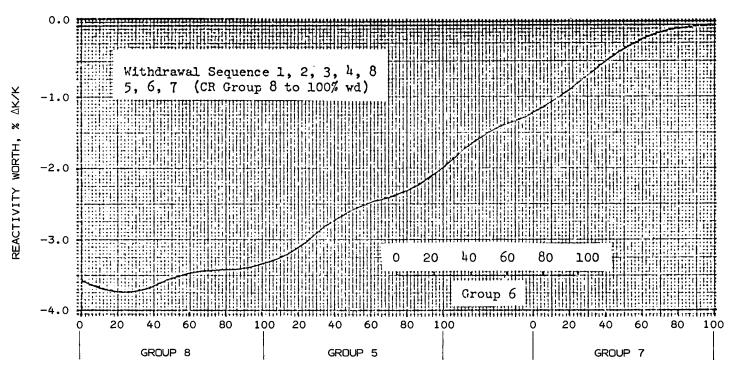


Figure 3-3. TMI-1 Cycle 1 — Total Reactivity Worth Vs Rod Withdrawal at Zero Power, 532F, 0 EFPD



CONTROL ROD POSITION, % WD

4. TMI-1 OPERATING DATA

The operating data for the first two cycles at TMI-1 have been obtained from core performance data computer outputs taken during plant operation.

4.1. Operational Histograms

Figures 4-1 through 4-4 show the core power, critical boron concentration, and rod position histories in 500-MWd/mtU increments for cycles 1 and 2.

4.2. Core Performance

4.2.1. Operating Data

Core performance data for the first two cycles of operation at TMI-1 are provided in Appendixes A and B. The following definitions have been used in preparing the tables:

- Core Power Core power in megawatts thermal (MWt) is based on a reactor heat balance.
- Core Boron Concentration This figure is based on samples taken periodically by the plant staff.
- Core Outlet Pressure The core outlet pressure is measured outside the core by a pressure tap. The plant computer corrects the pressure reading back to the core elevation by applying the Bernoulli equation. The correction (about 50 psi) is added to the reading and printed by the computer.

Reactor Coolant Total Flow - Total primary side system flow.

Feedwater Flow - Secondary side flow for the designated loop.

- RODW The rod withdrawal in percent as measured by magnetic reed switches, having 2-inch spacing and which start at the fully inserted position.
- SPND-UNC The uncorrected incore detector signal in nanoamps for each detector in the core. One SPND-UNC map is included in the first case for each cycle. Each block represents a detector string with the first value being that for the level 1 detector in the string located nearest the bottom of the active fuel length.

BKCAL — The calibrated background signal (in nanoamps) measured for each detector string.

SPNDBC - The corrected incore detector signal (in nanoamps).

4.2.2. Incore Detector Signal Processing

The SPNDBC signals in Appendixes A and B represent the measured signal that would be expected if all the incore detectors were undepleted and of nominal sensitivity and there were no signal losses during measurement. This consistent set of instrument-independent signals is obtained from the raw detector signals, SPND-UNC, by applying several corrections.

A correction (CALFI) is applied to the detector signal to correct for current losses in the cables connecting the incore detectors to the multiplexer. This correction factor is based on leakage measurements taken at the plant and is usually small.

The leakage-corrected signals are adjusted by a factor (SCF) to account for asbuilt variations in detectors. These slight variations in length and lateral surface area cause small differences in the initial sensitivity. Based on tests conducted by B&W, a correlation between detector length and sensitivity was developed and is applied to each detector to yield a leakage- and sensitivity-corrected signal.

Signals generated by each detector are also affected by the amount of rhodium depletion that has occurred in the detector. To adjust for the depletion effects, a correction factor is calculated based on the following equation:

$$DCF = \frac{Q_{\infty}}{Q_{\infty} - Q_{t}}$$

where

DCF = depletion correction factor (inverse of fraction depleted),

Q = total output charge available from detector,

 \mathbf{Q}_{+} = total output charge generated to date by the detector.

The value of Q_{∞} is determined for each detector based on a B&W correlation, while Q_{+} is constantly updated by the on-line computer system.

A final correction is required to account for background losses caused primarily by gamma interaction with the detector sheath and leadwire. The background signal is measured for each string at level 7 and is corrected for current leakage to obtain a calibrated value, BKCAL. A background signal (BKG) for each level is obtained by proportioning the level 7 background signal over the axial length of the assembly based on the measured power shape.

The instrument-independent signal is then calculated as follows:

where

SPNDBC = instrument-independent Rh signal, n-amps,

SPND-UNC = raw measured Rh signal, n-amps,

CALFI = detector leakage correction,

DCF = detector depletion correction factor,

SCF = detector sensitivity correction factor,

BKG = background signal correction.

For further information on signal processing and the conversion from detector signals to assembly powers, see "Nuclear Applications Software Package," <u>BAW-10123</u>, Babcock & Wilcox, February 1978.

4.2.3. Heat Balance Calculations

The core power calculated for each data case is determined by weighing the plant primary and secondary side heat balances. The core power above 50% of full power is given by

$$Q = *QSEC + (1 - \alpha)QPRIM$$

where

Q = core power Btu/h,

QSEC = core power from secondary side heat balance, Btu/h,

QPRIM = core power from primary side heat balance, Btu/h,

 α = weighing factor.

The weighing factor used above is

$$\frac{\text{PWR} - 15.0}{85.0}$$
 for 15.0 < PWR < 100.0

where PWR is the percent of full power using QSEC above 50% and QPRIM below 50%. Heat balance calculations are made on approximately 6-minute intervals.

The primary side heat balance for TMI-1 is calculated as follows:

$$QPRIM_{A} = W_{A}[H(T_{OUT,A},P) - H(T_{IN,A},P)] - WLET \times H(T_{IN,LET},P) + QPRO - QPUMP$$

where

WLET = letdown flow rate, lb/h,
 QPRO = primary side surface heat loss, Btu/h
QPUMP = heat addition from two pumps, Btu/h.

The inlet temperature $T_{\text{IN,A}}$ is obtained by flow weighing the measured inlet temperatures for each inlet leg of the loop. The primary side heat balance QPRIM is the sum of the heat balances performed for the two primary loops.

The secondary side heat balance is calculated as follows:

QSEC =
$$FF_A(H_A - H_{IN,A}) - H_{MKUP} \times MKUP - QPUMP + QPRO + FF_B(H_B - H_{IN,B})$$

+ $H_{IN,B} \times WLET - QPUMP + QPRO$

where

QSEC = secondary side power, Btu/h,

FFA = feedwater flow rate for loop A, lb/h,

FFB = feedwater flow rate for loop B, lb/h,

MKUP = makeup flow rate, lb/h (equals WLET),

HMKUP = makeup coolant enthalpy, Btu/lb

HA, HB = outlet steam enthalpy, loop A or B, Btu/lb,

HIN,A, HIN,B = enthalpy of inlet coolant, loop A or B, Btu/lb.

Following is a sample heat balance calculation for TMI-1 using Case 1 from cycle 2.

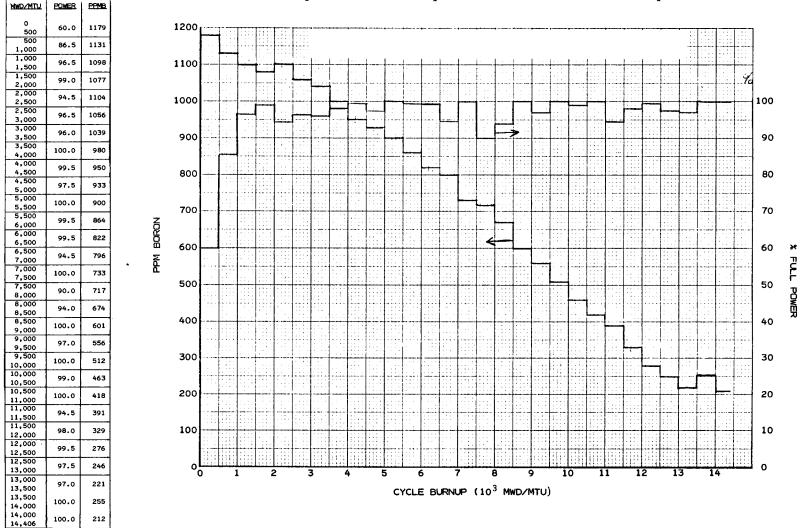
Primary heat balance	Flow rate, 10 ⁶ 1b/h	Temperature, F
Loop A inlet	68.99	571.32, 569.58 = 570.45
Loop B inlet	69.436	570.35, 570.08 = 570.22
Letdown	0.0246	∿570.3
Loop A outlet	68.99	589.23
Loop B outlet	69.436	589.00
Core pressure = 2178.3		
H(570,2178) = 572.34		
H(589,2178) = 597.82		
QPRIMA = 68.99 × 10 ⁶ (597.82		$02466 \times 10^{6} (572.34)$ $(34.812 \times 10^{6}) = 1.71 \times 10^{9} \text{ Btu/h}$
QPRIMB = 69.436 × 10 ⁶ (597.8		0.02466 × 10^6 (572.34) - (34.812 × 10^6) = 1.72 × 10^9 Btu/h
QRPIM = 3.43×10^9 Btu/h =	1005.3 MWt.	

```
Flow
          Secondary side heat balance
                                               10^6 lb/h
                                                             Temp, F
                                               1.9887
                                                             374.18
          Feedwater loop A
          Feedwater loop B
                                                             374.18
                                               2.0246
          Steam loop A
                                               1.9887
                                                             590.73
          Steam loop B
                                               2.0246
                                                             587.71
          Core pressure = 908.7
          H(590.7, 908.7) = 1250.20
                                            H(374.18, 908.7) = 348.57
          H(587.7, 908.7) = 1248.78
                                            H(makeup)
                                                                = 93.58
QSEC = 1.9887 \times 10^6 (1250.20 - 348.57) - (93.58 \times 0.02466 \times 10^6) - 34.812 \times 10^6
      +0.93 \times 10^{6} + 2.0246 \times 10^{6} (1248.78 - 348.57) + (348.57 \times 0.02466 \times 10^{6})
                      -34.812 \times 10^6 + 0.93 \times 10^6 = 3.55 \times 10^9 Btu/h
     = 3.55 \times 10^9 Btu/h = 1041.4 MWt
   \alpha = 0.29
Core power = 1041.4 (0.29) + (1 - 0.29)(1005.3) = 1015.77
```

The difference between the on-line computer (OLC) core power and this number is caused by the use of handbook-interpolated enthalpy values instead of the OLC-calculated values.

CORE AVERAGE

Figure 4-1. TMI-1 Cycle 1 - Power and Boron History



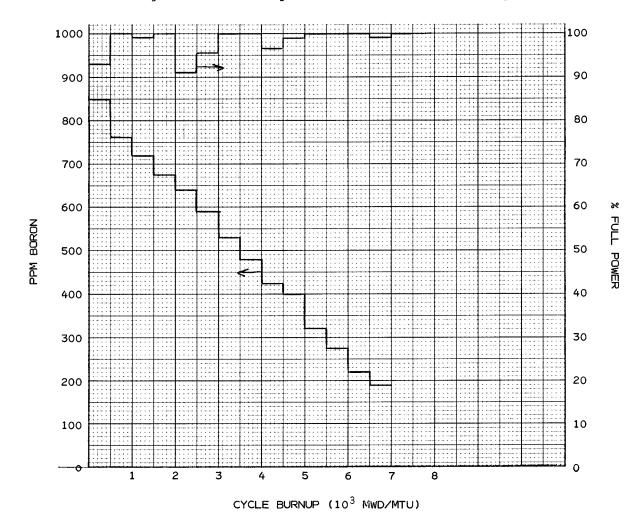
AVERAGE % WD

MWD/MTU GP6 GP7 GP8 1,000 1,000 1,500 1,500 2,000 2,500 2,500 3,000 3,000 13 10 3,500 4,000 4,000 4,500 5,000 5,000 5,500 6,000 % ROD WITHDRAWN 6,000 6,500 6,500 7,000 7,000 13 10 7,500 7,500 8,000 8,000 8,500 9,500 9,000 9,500 10,000 10,000 10,500 11,000 11,500 12,000 20H 12,000 12,500 12,500 13,000 13,500 14,000 14,000 14,406 CYCLE BURNUP (103 MWD/MTU)

Figure 4-2. TMI-1 Cycle 1 - Rod Position History

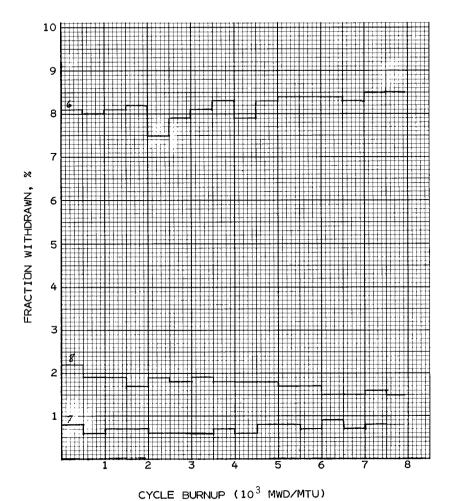
CORE AVERAGE				
MWD/MTU	POWER	PPMB		
0 500	93.0	850		
500 1,000	100.0	763		
1,000 1,500	99.0	720		
1,500 2,000	100.0	674		
2,000 2,500	91.0	640		
2,500 3,000	95.5	590		
3,000 3,500	100.0	532		
3,500 4,000	100.0	478		
4,000 4,500	96.5	434		
4,500 5,000	99.0	400		
5,000 5,500	100.0	321		
5,500 6,000	100.0	276		
6,000 6,500	100.0	232		
6,500 7,000	99.0	189		
7,000 7,500	100.0			
7,500 7,940	100.0			

Figure 4-3. TMI-1 Cycle 2 - Power and Boron History



AVERAGE % WD*					
MWD/MTU	GP6	GP7	GP8		
0 500	81	8	22		
500 1,000	80	6	19		
1,000	81	7	19		
1,500	82	7	17		
2,000 2,500	75	6	19		
2,500 3,000	7 9	6	18		
3,000 3,500	81	6	19		
3,500 4,000	83	7	18		
4,000 4,500	79	6	18		
4,500 5,000	83	8	18		
5,000 5,500	84	8	17		
5,500 6,000	84	7	17		
6,000 6,500	84	9	15		
6,500 7,000	83	7	15		
7,000 7,500	85	8	16		
7,500 7,940	85	8	15		

Figure 4-4. TMI-1 Cycle 2 - Rod Position History



APPENDIX A Operating Data, Cycle 1

Table A-1. Operating Data, Cycle 1

Case _	ore burnup, MWd/mtU	Core power, MWt	Core boron conc,
1	655.0	2512 1	1101 0
1	986.0	2513.1	1101.0
2	1756.0	2559.5	1095.0
3		2506.5	1083.0
4	2001.0	2516.2	1083.0
5	2248.0	2538.7	1073.0
6	2520.3	2500.3	1069.0
7	2763.0	2481.4	1057.0
8 -	3223.0	2500.8	1039.0
9	3409.0	2526.1	1008.0
10	3652.0	2495.0	1001.0
11	3836.0	2518.2	997.0
12	4055.0	2515.1	983.0
13	5082.0	2540.9	910.0
14	5296.0	2521.4	896.0
15	5727.0	2495.3	888.0
16	5939.0	2532.0	858.0
17	6154.0	2515.7	824.0
18	6549.0	2509.9	801.0
19	6759.0	2523.7	785.0
20	6968.0	2534.7	753.0
21	7199.0	2526.2	743.0
22	7711.0	2528.2	706.0
23	8459.0	2540.2	633.0
24	9133.0	2511.1	576.0
25	9326.0	2539.9	548.0
26	10187.0	2512.3	462.0
27	10400.0	2524.5	456.0
28	10600.0	2495.6	440.0
29	10814.0	2515.1	408.0
30	11808.0	2538.5	310.0
31	12850.0	2505.2	227.0
32	13745.0	2529.0	258.0

TMI-1 CY-1

YEAR 74 MONTH 08 DAY 09 HOUR 08 MINUTE 34 REF EST +

CORE POWER (MWT)		CORE AVG BURNUP (MWD/MTU)		CORE BORON CONC (PPMB)
2513.1		655.00		1101.0
COOLANT FLOWS (LB/HR * E-6)		PRESSURE (PSIA)		COOLANT TEMPERATURES DEGREES F
RC FLOW LOOP A	70.085	CORE OUTLET	2179.5	LOOP A INLET TEMP(1) 556.43
RC FLOW LOOP B	69.469	SECONDARY LOOP A	893.70	LOOP A INLET TEMP(2) 554.93
RC TOTAL FLOW	139.72	SECONDARY LOOP B	893.70	LOOP 8 INLET TEMP(1) 555.54
FEEDWATER FLOW LOOP A	5.2800			LOOP B INLET TEMP(2) 555.45
FEEDWATER FLOW LOOP B	5.4085			FEEDWATER (LOOP A) 461.09
LETDOWN FLOW	•51508E-01			FEEDWATER (LOOP B) 461.09
				REACTOR OUTLET (LOOP A) 601.06
				REACTOR OUTLET (LOOP B) 600.84
				STEAM TEMP (LOOP A) 591.15
				STEAM TEMP (LOOP 8) 591.56

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
						******	*******			*******	:				
Δ															
8						19.60		99.70		19.70					
С			*******	******	*******	*******	******	*******	******			*****	*******	: :	
v		******	* :	, , , , , , , , , , , , , , , , , , , ,	100.00	· .	· * * * * * * * * * * * * * * * * * * *	, , ,*******	, , , , , , , , , , , , , , , , , , ,	•	******	*******	*******	*******	•
0		* .	,	99.70		10.00		92.30		7.89		99.90			•
E		*	99.80		93.20		98.70		98.70		92.30		99.80		•
F	*	* 18.60		6.66		99.80		99.80		99.70		13.20		19.60	
G	*	*	99.71		99.70		99.70		101.00		98.70		98.70		
н	*	99.80		92.30	,	99.80*		19.70		99.80	*	92.20*		99.80*	*
к	* * *	* :	99.90		99.70		99.70		101.00	,	98.60*		99.70		
L	*	* 19.60°	, , , ,	5.85	, ,	99.90		99.70		99.70	*	5.70		19.6û*	*
н		• •	101.00		91.30		98.80		99.90		92.30		99.70	******	• •
N		* ; * ;	, , , , , ,	99.80	·	5.73		93.30		7.92	* * * * * * * * * * * * * * * * * * *	99.70*	*	******	i i i
0		•			99.70		99.00		99.50		99.70* *******	*	*		
P				****		19.90	****	85.10		19.60*	******	******			
R					•	*									
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15

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TMI-1 CY-1
YEAR 74 MONTH 09 DAY 05 HOUR 16 MINUTE 12 REF EST

CORE POWER (MWT)		CORE AVG BURNUP (NHD/MTU)		CORE BORON CONC (PPMB)
2559•5		986.00		1095.0
CCOLANT FLOWS (LB/HR * E-6)		PRESSURE (PSIA)		COOLANT TEMPERATURES DEGREES F
RC FLCW LOOP A	70.203	CORE OUTLET	2178.8	LOOP A INLET TEMP(1) 555.93
RC FLCW LOOP B	69.276	SECONDARY LOOP A	892.30	LOOP A INLET TEMP(2) 554.45
RC TOTAL FLCW	139.53	SECONDARY LOOP 8	892.30	LOOP B INLET TEMP(1) 555.09
FEEDWATER FLOW LOOP A	5.3278			LOOP B INLET TEMP(2) 555.26
FEEDWATER FLOW LOOP B	5.4804			FEEDWATER (LOOP A) 463.09
LETDONN FLOW	.34974E-01			FEEDWATER (LOOP B) 463.09
				REACTOR OUTLET (LOOP A) 600.81
				REACTOR OUTLET (LOOP B) 600.58
				STEAM TEMP (LOOP A) 590.80
				STEAM TEMP (LOOP B) 591.28

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В				• •	• :	16.50		99.70		16.58					
С			* * * * * * * * * * * * * * * * * * *	* * * * * * * * * * * * * * * * * * *	100.00		98.80	* * * * * * * * * * * * * * * * * * *	98.80	· · · · · · · · · · · · · · · · · · ·	101.00		*	•	
פ				99.70		11.10	, , , , , , , , , , , , , , , , , , ,	89.10		11.00		99.90	, ,	, ,	•
ε	********		99.70		90.10		99.70		98.70		89.00		99.70		, , ,
F	* :	16.50	, ,	10.90		99.70		99.80		99.70		11.10		16.40	
G	* :		99.60		39.70		99.70		99.80		101.00		98.70		
н	* :	99.80	, , , ,	90.20	, ,	99.80		16.50		99.86		89.00		99.70	
ĸ	* *	,	100.03		99.70		99.70		101.00		99.70		99.70		
L	+ + +	16.40		14.30	,	99.90		99.70		99.70		11.00		15.40	
*	4		99.80		90.30		99.70		99.90		90.10*		99.70		
N				99.80		10.90		89.00		12.20	-	98.60			
0		4		, ,	99.70		98.93		99.50		99.70*				
o		•				16.70		99.70		16.40*	*	4		-	
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APPENDIX B
Operating Data, Cycle 2

Table B-1. Operating Data, Cycle 2

Case	Core burnup, MWd/mtU	Core power,	Core boron conc,
7	9654.0	1013.4	1075.0
1 2	9657.0	1003.2	1075.0
3	9694.0	1879.3	923.0
4	9702.0	1834.5	896.0
5	9702.0	1859.5	894.0
6	9796.0	2517.5	838.0
7	10038.0	2524.5	799.0
		2526.4	778.0
8	10254.0		769.0
9	10446.0	2517.1	
10	10799.0	2507.3	731.0
11	10890.0	2497.4	731.0
12	11103.0	2531.5	699.0
13	11290.0	2502.7	699.0
14	11477.0	2541.6	660.0
15	11710.0	1168.5	660.0
16	11855.0	2540.6	660.0
17	12040.0	2525.4	595.0
18	12239.0	2531.6	589.0
19	12379.0	2508.4	556.0
20	12629.0	2517.5	550.0
21	12839.0	2524.0	520.0
22	13051.0	1279.6	629.0
23	13298.0	2518.3	489.0
24	13482.0	2533.7	470.0
25	13697.0	2513.6	442.0
26	13888.0	2522.9	434.0
27	14094.0	2522.6	409.0
28	14315.0	2530.5	394.0
29	14508.0	2518.7	440.0
30	14727.0	2519.0	330.0
31	14935.0	2524.3	328.0
32	15152.0	2525.2	300.0
33	15372.0	2523.2	274.0
34	15578.0	2515.2	268.0
35	15793.0	2529.6	241.0
36	16046.0	2513.9	206.0
37	16224.0	2498.4	206.0
38	16422.0	2541.5	182.0
39	16642.0	2527.1	182.0
40	16857.0	2524.1	149.0
41	17075.0	2504.8	123.0
42	17229.0	2515.9	115.0
43	17261.0	2515.8	115.0
44	17473.0	2512.9	115.0
4 5	17545.0	2520.0	115.0

TMI-1 CY-2

YEAR 76 MONTH 05 DAY 28 HOUR 21 MINUTE 07 REF EST

CORE POWER (MWT)		CORE AVG BURNUP (MWD/MTU)		CORE BORON CONC (PPMB)
1013.4		9654.0		1075.0
COOLANT FLOWS (LB/HR * E-6)		PRESSURE (PSIA)		COOLANT TEMPERATURES DEGREES F
RC FLOW LOOP A	68.990	CORE OUTLET	2178.3	LOOP A INLET TEMP(1) 571.32
RC FLOW LOOP B	69.436	SECONDARY LOOP A	908.70	LOOP A INLET TEMP(2) 569.58
RC TOTAL FLOW	138.30	SECONDARY LOOP B	908.70	LOOP B INLET TEMP(1) 570.35
FEEDWATER FLCW LOOP A	1.9887			LOOP B INLET TEMP(2) 570.08
FEEDWATER FLOW LOOP 8	2.0246			FEEDWATER (LOOP A) 374.18
LETDOWN FLOW	.24 663E-01			FEEDWATER (LOOP B) 374.18
				REACTOR OUTLET (LOOP A) 589.23
				REACTOR OUTLET (LOOP B) 589.00
				STEAM TEMP(LOOP A) 590.73
				STEAM TEMP (LOOP B) 587.71

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8						99.69		99.81		100.00			*			
u				•		77.03		33.01		. 100.60.			•			
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C			•	•	99.78		8.85		8.91		99.84	•	*	•		
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G	* ;		6.88	•	99.72		99.75		99.69		98.73		* 8.91			
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	*	,		•									•		,	
K	* :	•	8.88		99.69		99.81		100.00		98.70		* 8.91			,
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L	*	99.78		* 36.72	. 4	. 99.904		81.57*		99.864		36.66	•	99.72	, ,	
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N				81.81		36.75		99.60		36.78		81.60	•			
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140.90* * 226.30 * * 218.70 * * 181.40 * * 189.10 * * 198.10 * * 152.10 * * 272.60* 250.00* 188.90* 199.40* 229.10* 163.00* * 161.70* 153.40* * 161.70* 153.40* * 219.0:* 201.80* * 225.90* 204.60* * 199.50* 184.90* * 197.7* 179.50* * 201.50* 170.80* * 136.40* 60.30* * 209.90* 176.20* * 209.90* 176.20* * 285.40* 231.90* * 253.30* 215.70* * 154.50* 172.60* * 219.70* 195.60* * 148.30* 130.90* 176.10* 176.10* 227.30* 217.20* 162.40* 156.10* 180.30* * 1+7.10* * 2+6.50* * 210.90* * 193.10* * 195.50* * 185.70* * 131.10* * * * * * * 178.20* 160.90* * 169.80* 124.10* 152.50* 148.20* 127.80* 125.20* 122.90* 100.40* 151.50* * 178.20* 160.90* * 236.30* 219.60* * 223.60* 225.90* * 185.40* 203.00* * 184.80* 193.20* * 208.80* 210.50* * 158.00* 135.40* * 221.90* * 213.40* * 178.40* * 183.40* * 202.00* * 138.40* 114.10* 106.70* 79.70* 82.90* 88.50* 64.20* * 132.40* 138.30* 208.90* 106.90* 106.90* 120.70* 210.50* 207.70* 216.00* 168.20* 211.20* 168.00* 168.20* 201.50* 161.50* 133.30* 110.40* # 168.90* 141.50* 99.60* 168.90+ 218.90+ 221.80+ 188.70+ 180.00+ 201.70+ 110.40+ 141.50* 161.9.* 152.40* 132.70* 131.00* 148.30* 122.80* 134.60* 136.0(* 120.30* 115.50* 114.10* 61.80* * 173.90* 231.10* 234.00* 300.40* 224.20* 276.40* 144.50* 255.10* 186.70* 230.30* 207.00* 249.40* 163.50* 177.10* 174.40* 174.40+ 239.40+ 231.10+ 189.60+ 194.30+ 227.30+ 168.80+ 167.60* 1/7.70* 242.80* 225.30* 235.60* 220.30* 188.90* 154.00* 187.50* 168.90* 185.60* 183.10* 108.00* 116.80* 187.70* 170.10* 176.30* 170.10* 221.50* 214.90* 175.40* 174.30* 183.90* 132.30* 247.40* 234.70* 171.40* 175.80* 214.60* 235.70 * * 235.70* * 221.20* * 171.30* * 174.20* * 199.00* * 143.20* L * 182.60* 184.90* * 182.50* 250.00* * 223.30* 250.00* * 184.10* 177.30* * 190.00* 180.10* * 200.40* 207.50* * 172.40* 143.80* * * 171.30* * 193.00* * 287.00* * 267.50* * 218.00* 171.30* 244.80* 233.20* 181.10* 180.40* * 232.40* * 223.90* * 199.60* * 187.90* М 208.40* 216.40* 180.30 130.40* 90.00* * 153.60* * * * * * 158.00* 238.60* 240.10* 307.50* 228.50* 281.91* 192.00* 210.30* 190.00* 219.30* 188.60* 260.40* 250.90* 202.60* 198.10* 200.20* 239.20* 157.90* 157.90* 208.20* 202.20* 184.30* 274.80* 228.80* 259.90* 219.90* 264.66* 161.66* 198.70* 161.70* 197.70* 179.50* 121.30* 123.30* * 245.00* * 247.20* * 223.90* * 240.10* * 230.20* * 174.70* * 175.90* * 208.00* * 191.50* *-200.60* * 236.70* * 234.70* * 199.20* * 205.10* * 204.00* * 119.90* * * 130.13* * 139.50* * 135.00* * 119.80* * 127.20* * 122.40* * 77.10* 87.36* 126.80* 128.10* 114.00* 110.60* 102.70* 77.10* 56.50* ***********************

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YEAR 76 MONTH 05 DAY 29 HOUR 02 MINUTE 44 REF EST

CORE POWER (MHT)		CORE AVG BURNUP (MWD/MTU)		CORE BORON CONC (PPMB) 1075.0					
1003.2		965 7.0							
COOLANT FLOWS (LB/HR * E-6)		PRESSURE (PSIA)	COOLANT TEMPERATURES Degrees F						
RC FLOW LOOP A	68.702	CORE OUTLET	2176.2	LOOP A INLET TEMP(1) 569.04					
RC FLOW LOOP 8	69.044	SECONDARY LOOP A	907.40	LOOP A INLET TEMP(2) 567.36					
RC TOTAL FLOW	138.29	SECONDARY LOOP B	907.40	LOOP B INLET TEMP(1) 571.20					
FEEDWATER FLOW LOOP A	1.8915			LOOP B INLET TEMP(2) 570.89					
FEEDMATER FLOW LOOP 8	2.0961			FEEDWATER (LOOP A) 373.90					
LETDOWN FLOW	.24599E-01			FEEDWATER (LOOP B) 373.90					
				REACTOR OUTLET (LOOP A) 587.67					
				REACTOR OUTLET (LOOP B) 590.11					
				STEAM TEMP(LOOP A) 587.78					
				STEAM TEMP (LOOP B) 589.01					

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е				********	******* * •	******** * * 99.69	********	99.75	• • • • • • • • • • • • • • • • • • •	* 100.00°	* * * * * * * * * * * * * * * * * * *	* * * * * * * * * * *	* * *	
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