

**University of Glasgow**

**James Watt School of Engineering**

**Simulation of Engineering Systems 3**

## **Assignment: Instrument Landing System Lateral Beam Guidance System**

### **Part 1: Modelling, Simulation & Validation**

#### **Aim**

Part 1 of this Simulation of Engineering Systems 3 Assignment involves the modelling, simulation, and validation of an Instrument Landing System (ILS) Lateral Beam Guidance System. This part of the assignment involves developing a mathematical model of the lateral dynamics of an aircraft approaching using ILS for guidance. This model will be implemented in MATLAB code and as a Simulink block diagram. The responses from the Simulink block diagram will be used to analyse and validate the MATLAB model and its associated simulation. This document provides background information about this system, followed by the problem specification for the mathematical model of the system and its simulation. Also, the Assignment Specifications are provided as a step-by-step guide for this part of the assignment.

#### **Introduction**

Most major airports have an ILS which can be used for automated or assisted landing of aircraft. Basically, this is a short range navigational aid which provides azimuth (horizontal) and vertical position information. This assignment involves the development of a simulation of this system for lateral beam guidance as outlined in this document.

#### **Background**

The ground-based elements of ILS comprise of a *localiser transmitter*, a *glideslope transmitter* and *marker beacons*. These provide the azimuth, vertical and distance signals respectively (see Figure 1).

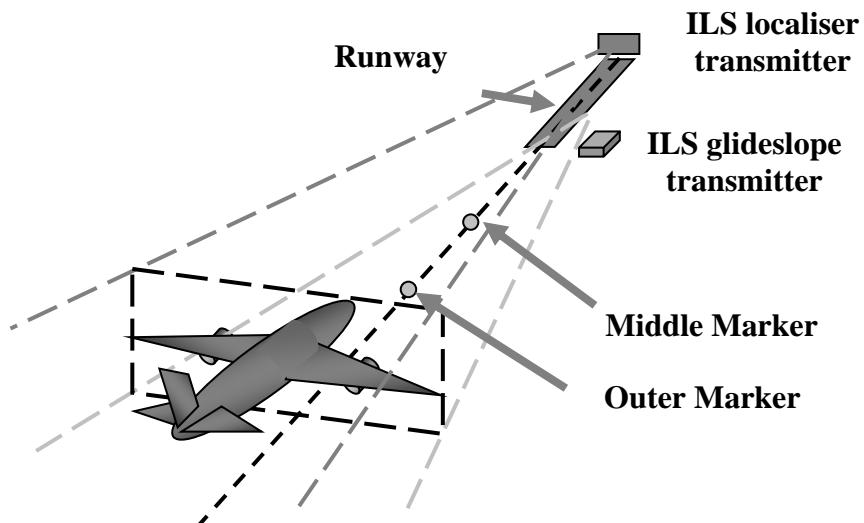


Figure 1: ILS Diagram

On the aircraft there is a *localiser antenna*, a *glideslope antenna*, an *ILS receiver unit* and a *marker beacon antenna and receiver*. The position of the aircraft relative to the localiser and glideslope is displayed on an indicator in the cockpit and is used to land safely.

### *The Localiser System*

The localiser transmitter is positioned at the far end of the runway which the aircraft is approaching. It transmits on a given frequency in the band 108 MHz to 112MHz. The signals radiate to the left and right of the centre line of the runway as shown in Figure 2. The signal to the left is modulated by a

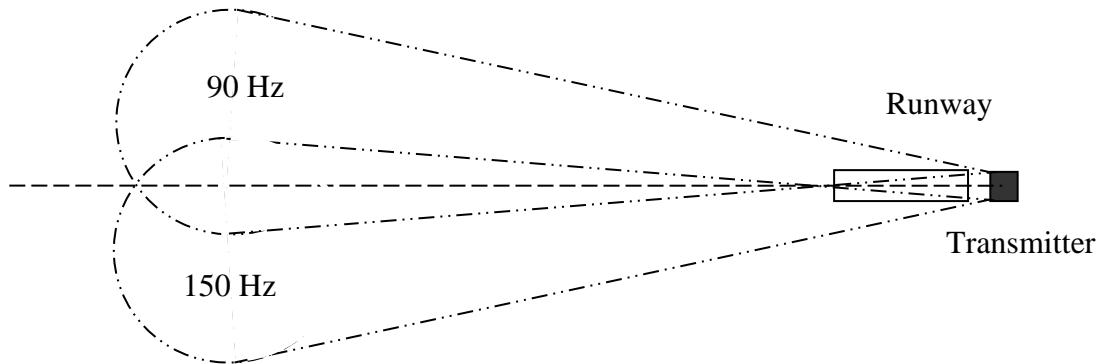


Figure 2: Localiser Beams

90 Hz component while the corresponding frequency for the signal on the right is 150 Hz. The two signals overlap in the middle. The autopilot uses the stronger overlapping signal region to position the aircraft within the ILS approach corridor.

### *The Glideslope System*

The glideslope transmitter is located near the point of touchdown (threshold) on the runway and transmits on a given frequency in the range 329.3 MHz and 335.0 MHz. The radiated signal pattern is similar to that of the localiser but provides vertical guidance relative to a descent path (see Figure 3).

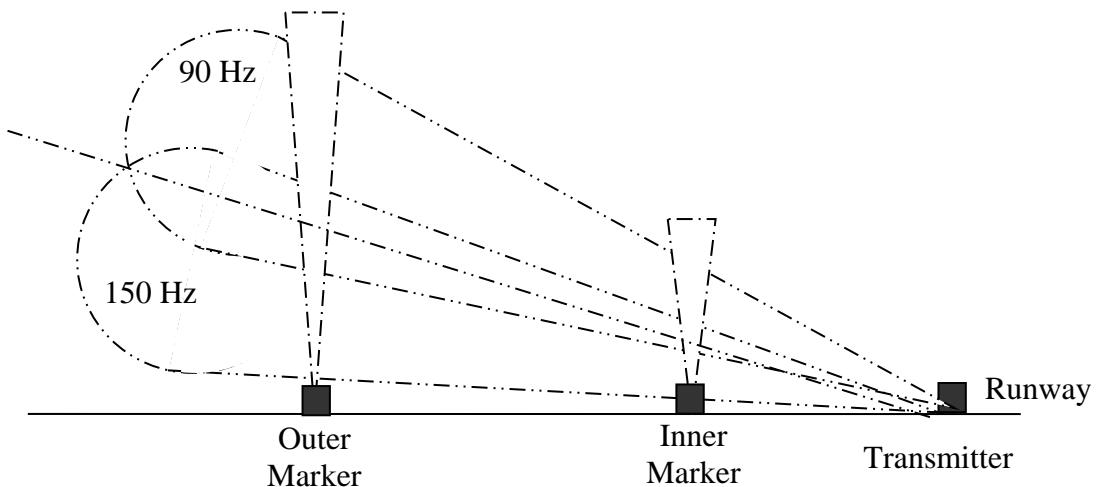


Figure 3: Glideslope and Marker Beams

## The Marker Beacons

Marker beacons transmitters are located along the approach path and provide 75 MHz signals beamed vertically into the approach corridor. The beacons are located 7.4 km (outer marker) and 1.1 km (inner marker) from the runway threshold. These markers provide distance signals so that the speed of descent can be monitored and adjusted.

## Problem Specification

The ILS can be used for automated landing where direction, descent and speed are all controlled through automated control systems. In order to achieve this, the aircraft must be equipped with the necessary systems to ensure the automatic guidance of the aircraft along the approach corridor. The general principle of completely automated landing systems is to feed information from the localiser and glideslope beams into the aircraft's autopilot. The final approach speed is governed by an automatic throttle subsystem.

In this study we will consider the development of a simulation that represents the automated lateral beam guidance system only. This system involves the coupling of the localiser receiver to the lateral autopilot. The glideslope and throttle systems are not considered here.

The geometry of the lateral beam guidance is shown in Figure 4.

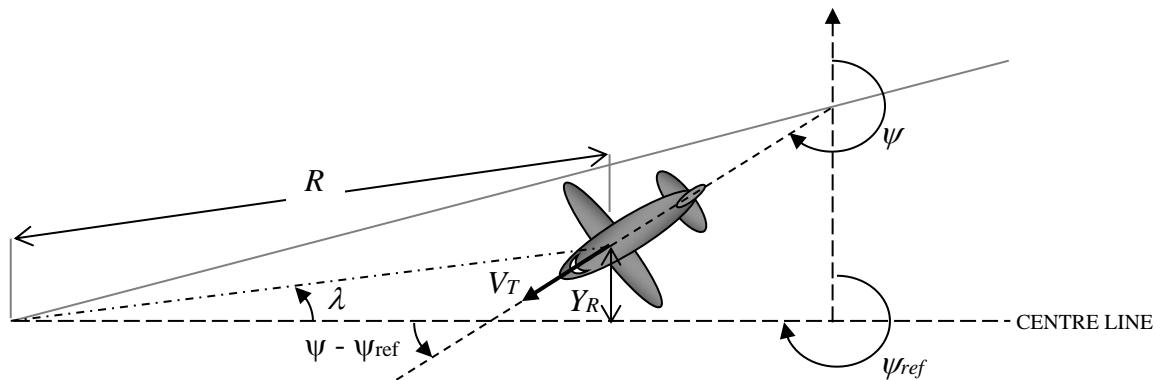


Figure 4: Approximate Geometry of lateral beam guidance

The lateral beam guidance system produces the required aileron commands to generate a coordinated banking manoeuvre that positions the aircraft within the localiser beams. It achieves this by combining the roll control system with the heading control for the aircraft. A diagram of the total system is shown in Figure 5.

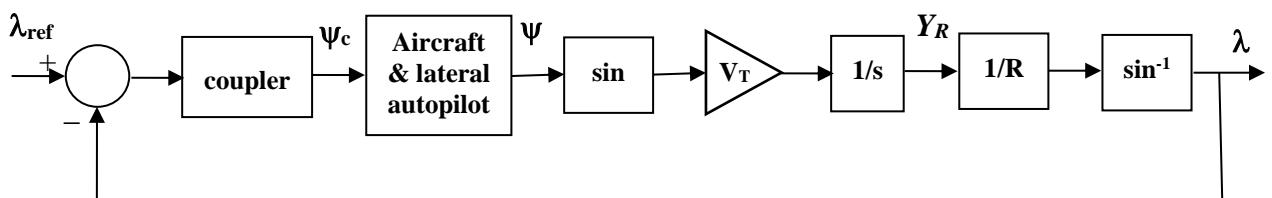


Figure 5: Lateral Beam Guidance System

From Figure 5 it can be seen that the Lateral Beam Guidance System takes a value for the reference angular error between the aircraft and the centre line,  $\lambda_{ref}$ , and compares it with the actual error,  $\lambda$ . In this case the values for  $\lambda_{ref}$  and  $\psi_{ref}$  (the reference heading) are taken to be zero. The comparison of these values is performed by the *coupler* which is in this part of the assignment is a proportional controller of the following form:

$$\psi_c = G_c (\lambda_{ref} - \lambda) \quad (1)$$

Here  $G_c$  is a gain. The resulting commanded heading angle  $\psi_c$  is then fed into the lateral autopilot to generate an appropriate heading for the aircraft to follow ( $\psi$ ). Once the heading has been changed so that the aircraft approaches the centre line of the runway, it directly influences the lateral speed of the aircraft,  $\dot{Y}_R$  (m/s). This is used to calculate the lateral displacement of the aircraft,  $Y_R$  (m), which is then used to estimate the angular error between the aircraft and the centre line. This is then used to estimate the angular error between the aircraft and the centre line by considering the trigonometric relationship between  $Y_R$  and  $\lambda$  i.e.

$$\sin \lambda = \frac{Y_R}{R} \quad (2)$$

This is an overview of the entire system.

A key part of the overall lateral beam guidance system is the lateral autopilot and its interaction with the lateral dynamics of the aircraft. In Figure 5 this system is regarded as the conversion process between the commanded heading,  $\psi_c$  (radians), and the actual heading of the aircraft,  $\psi$  (radians). This process is more involved than this simplified system diagram would lead you to believe.

The Lateral Autopilot has numerous components that provide the actuator commands to the main banking actuators – *the ailerons*. These control surfaces are positioned at the end of the wings and provide the required rolling moments to produce a coordinated banking turn. A detailed description of this system and how it interacts with the aircraft can be seen in Figure 6.

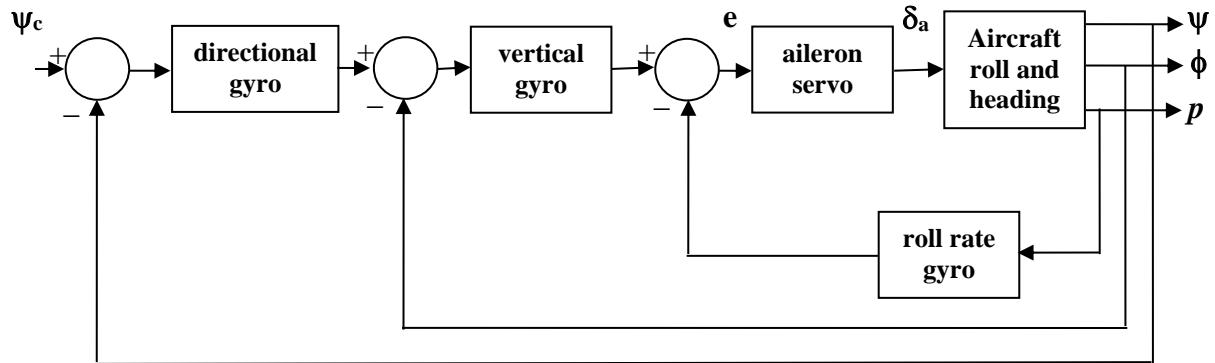


Figure 6: Aircraft and Lateral Autopilot

The Lateral Autopilot forms 3 feedback loops around the aircraft roll and heading dynamics. The outer loop provides a comparison between the commanded heading from the coupler and the actual heading of the aircraft. This comparison passes through the directional gyro which can be represented by a simple gain  $K_D$ . The resulting signal is then a representation of the required roll angle that needs to be

applied in order to provide the banked turn. This commanded roll angle is compared with the actual roll angle of the aircraft,  $\phi$  (radians), by means of the second loop. This comparison passes through the vertical gyro which is represented by a simple gain  $K_V$ . The output from this gyro provides a commanded roll rate to stabilise the speed at which the aircraft is rolling. This forms the input for the final inner loop which measures the aircraft's roll rate,  $p$  (rad/s), via the roll rate gyro (note:  $p = \dot{\phi}$ ). This gyro is represented by the simple gain  $K_R$ .

Ultimately these three feedback loops generate an input signal for the aileron actuator. In this case the actuator is a dc motor, and its electro-mechanics can be represented by the following relationships:

$$L_A \frac{di}{dt} + R_A i + K_E \frac{d\delta_a}{dt} = V_A \quad (3)$$

$$J_M \frac{d^2\delta_a}{dt^2} + B_{SM} \frac{d\delta_a}{dt} = K_T i \quad (4)$$

Here  $i$  is the motor armature current (A),  $\delta_a$  is the angular displacement of the ailerons and associated actuators (radians),  $J_M$  is the moment of inertia for the motor and the aileron ( $\text{kgm}^2$ ),  $L_A$  is the inductance (H),  $R_A$  is the resistance ( $\Omega$ ),  $B_{SM}$  is the damping coefficient,  $K_T$  is the torque constant and  $K_E$  is the back emf constant.

This relationship provides the main control surface input for the aircraft and thus stimulates the aircraft to perform the required banking turn to attain the centre line of the runway. The aileron dc motor is configured as a servo-motor as shown in Figure 7.

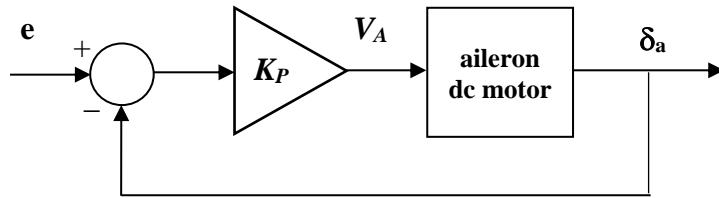


Figure 7: Aileron Servo

This servo-motor configuration regulates the aileron angular so that it follows the reference signal  $e$ . The reference signal is compared to the aileron deflection angle  $\delta_a$ , and the difference is amplified by gain  $K_P$  to produce the input voltage for the dc motor,  $V_A$  (V).

The dynamics of the aircraft are formed through two relationships: the conversion of aileron deflection,  $\delta_a$ , to roll angle,  $\phi$ , and the conversion between the roll angle and the heading angle,  $\psi$ . These form the following two equations:

$$T_A \frac{d^2\phi}{dt^2} + \frac{d\phi}{dt} = K_A \delta_a \quad (5)$$

$$\frac{d\psi}{dt} = \frac{g}{V_T} \phi \quad (6)$$

Here  $g$  is the acceleration due to gravity and  $V_T$  is the forward velocity of the aircraft. These equations represent the behaviour of this ILS Lateral Guidance System.

## Assignment Specifications for Part 1

The combination of all the elements described above produces a mathematical model for the Lateral Beam Guidance System. Using this description as a basis, follow the steps outlined below to complete the first part of your assignment for this course:

### *Mathematical Modelling & Continuous Time Simulation*

1. Use the description given above to derive the state space model for the Lateral Beam Guidance System.
2. Use this model and the parameter values given in the Appendix A to produce an equation or script-based simulation of the Lateral Beam Guidance System in MATLAB.
3. Employ a suitable initial conditions and numerical integration solver with a suitable step-size in the simulation of your system. Justify your choice of the initial conditions, solver, and step-size. **Do not** use the in-built MATLAB integration functions.
4. Analyse the dynamic response of the system. Do you think this a good design for the coupler in this system? Explain your answer.

### *Block Diagram & Validation*

5. Using basic, commonly used blocks in Simulink, construct a block diagram simulation of the Lateral Beam Guidance System.
6. Use the responses from this block diagram simulation to validate your MATLAB model from steps (1) & (2) and simulation responses from step (3).

## Report Part 1 Specifications

Once you have finished this part of the assignment, complete the report form for the first part of the assignment. This report form should outline the development of your mathematical model for this system, your MATLAB and Simulink Simulations, your analysis of this system and the validation of your model responses. The part 1 report template can be found on the Moodle page for this course. Your completed report for this initial part of the assignment should not exceed 6 pages in length and it should be submitted through the Moodle submission portal for part 1 of the assignment before 4:30pm on **25th November 2024**.

## Appendix A: Parameter Values

The following parameters are typical for the Lateral Beam Guidance System:

$$\begin{aligned}B_{SM} &= 0.7 \\g &= 9.81 \text{ m/s}^2 \\G_c &= 45.5 \\J_M &= 0.006 \\K_A &= 1.2 \\K_D &= 0.9 \\K_E &= 0.9 \\K_P &= 52.5 \\K_R &= 1.2 \\K_T &= 1.7 \\K_V &= 1.3 \\L_A &= 0.2 \text{ H} \\R_A &= 10 \Omega\end{aligned}$$

$T_A = 2.0$  seconds

Typical initial conditions are:

$$\psi_0 = -20^\circ$$

$$\phi_0 = 0^\circ$$

$$R_o = 6000\text{m}$$

$$Y_{Ro} = 150\text{m}$$

$$V_T = 55 \text{ m/s}$$

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October 2024