

Mathematical modelling of IPIS and its state space models

Structure of IPIS in three dimensions is given in Fig. 1 as follows:

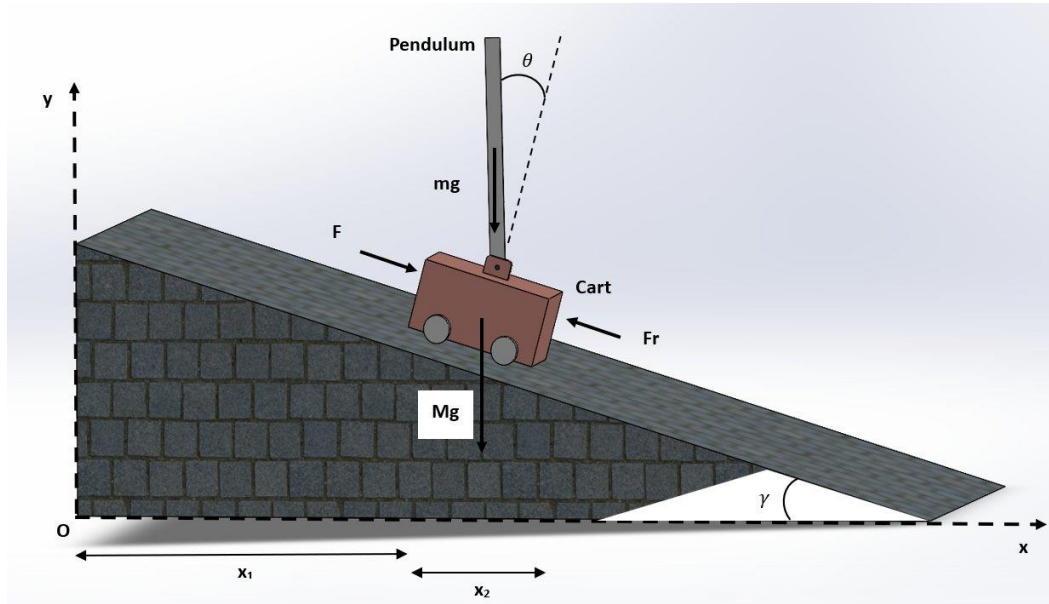


Fig. 1 Structure of IPIS in 3D

Before figuring out the mathematical modelling of IPIS based on Fig. 1, we define the system parameters in Tab. 1 as follows:

Tab. 1 Notation and unit of constant parameters of IPIS

<i>Parameter</i>	<i>Unit</i>	<i>Description</i>
M	$[kg]$	Mass of cart
m	$[kg]$	Mass of pendulum
l_c	$[meter]$	Length of the cart
b	kgm^2/s	Viscous friction co-efficient of pendulum section
γ	$[rad]$	Angle of inclined plane
L	$[meter]$	Distance from pivot joint to the centre of mass of pendulum
g	$[m/s^2]$	Gravity acceleration
I	$[kgm^2]$	Pendulum moment of inertia
F	$[N]$	External force
x	$[meter]$	Cart position
θ	$[rad]$	Angular of pendulum

According to [1], the mathematical modelling of IPIS is given in Equations as follows:

$$(M + m)\ddot{x} - (ml_c \cos\theta)\ddot{\theta} + (b \cos\gamma)\dot{x} + (ml_c \sin\gamma)\dot{\theta}^2 = F \cos\gamma \quad (1)$$

$$(ml_c \cos\theta + ml_c \tan\gamma \sin\theta)\ddot{x} - (I + mL^2)\ddot{\theta} + mgL \sin\theta = 0 \quad (2)$$

Let:

$$A_1 = M + m \quad (4)$$

$$B_1 = -ml_c \cos \theta \quad (5)$$

$$C_1 = F \cos \gamma - (b \cos \gamma) \dot{x} - (ml_c \sin \gamma) \dot{\theta}^2 \quad (6)$$

$$A_2 = ml_c \cos \theta + ml_c \tan \gamma \sin \theta \quad (7)$$

$$B_2 = I + mL^2 \quad (8)$$

$$C_2 = -mgL \sin \theta \quad (9)$$

$$x_1 = x, x_2 = \dot{x}, x_3 = \theta, x_4 = \dot{\theta} \quad (10)$$

From equations (1) and (2), we have:

$$\begin{cases} A_1 \ddot{x} + B_1 \ddot{\theta} = C_1 \\ A_2 \ddot{x} + B_2 \ddot{\theta} = C_2 \end{cases} \quad (11)$$

$$\Rightarrow \begin{cases} \ddot{x} = \frac{C_1 B_2 - C_2 B_1}{A_1 B_2 - A_2 B_1} \\ \ddot{\theta} = \frac{C_2 A_1 - C_1 A_2}{A_1 B_2 - A_2 B_1} \end{cases} \quad (12)$$

$$\Rightarrow \begin{cases} \ddot{x} = \frac{-(mL^2 + I)(l_c m \sin \gamma x_4^2 - F \cos \gamma + b x_2 \cos \gamma) + gl_c^2 m^2 \cos(x_3)}{(M + m) * (mL^2 + I) - l_c^2 m^2 \cos(x_3)(\cos(x_3) + \tan(\gamma) \sin(x_3))} \\ \ddot{\theta} = \frac{-\left(l_c m (\cos(x_3) + \tan \gamma \sin(x_3))(l_c m \sin \gamma x_4^2 - F \cos \gamma + b x_2 \cos \gamma) - gl_c m \sin(x_3)(M + m)\right)}{(M + m) * (mL^2 + I) - l_c^2 m^2 \cos(x_3)(\cos(x_3) + \tan(\gamma) \sin(x_3))} \end{cases} \quad (13)$$

The nonlinear state space equations of IPIS are described as follows:

$$\begin{cases} \dot{x}_1 = x_2 \\ \dot{x}_2 = f_{cn_1} = \frac{-(mL^2 + I)(l_c m \sin \gamma x_4^2 - F \cos \gamma + b x_2 \cos \gamma) + gl_c^2 m^2 \cos(x_3)}{(M + m) * (mL^2 + I) - l_c^2 m^2 \cos(x_3)(\cos(x_3) + \tan(\gamma) \sin(x_3))} \\ \dot{x}_3 = x_4 \\ \dot{x}_4 = f_{cn_2} = \frac{-\left(l_c m (\cos(x_3) + \tan \gamma \sin(x_3))(l_c m \sin \gamma x_4^2 - F \cos \gamma + b x_2 \cos \gamma) - gl_c m \sin(x_3)(M + m)\right)}{(M + m) * (mL^2 + I) - l_c^2 m^2 \cos(x_3)(\cos(x_3) + \tan(\gamma) \sin(x_3))} \end{cases} \quad (14)$$

$$\Rightarrow \dot{x} = f(x, F) \quad (15)$$

On the other hand, system (14) can be simplified into a linear system through Taylor expansion as $x_1, x_2 \rightarrow 0$, and this simplified form is given by:

$$\dot{x} = (A)x(t) + (B)u(t) \quad (16)$$

Where $u(t) = F(t)$, and

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ \frac{\partial f_{cn_1}}{\partial x_1} & \frac{\partial f_{cn_1}}{\partial x_2} & \frac{\partial f_{cn_1}}{\partial x_3} & \frac{\partial f_{cn_1}}{\partial x_4} \\ 0 & 0 & 0 & 1 \\ \frac{\partial f_{cn_2}}{\partial x_1} & \frac{\partial f_{cn_2}}{\partial x_2} & \frac{\partial f_{cn_2}}{\partial x_3} & \frac{\partial f_{cn_2}}{\partial x_4} \end{bmatrix} \quad (17)$$

$$B = \begin{bmatrix} 0 & \frac{\partial f_{cn_1}}{\partial F} & 0 & \frac{\partial f_{cn_2}}{\partial F} \end{bmatrix}^T$$