

EE2023 TUTORIAL 8 (SOLUTIONS)

Solution to Q.1

Transfer function of suspension system:

$$H(s) = \frac{X_o(s)}{X_i(s)} = \frac{bs + k}{ms^2 + bs + k}$$

Substituting $m = 1 \text{ kg}$, $k = 1 \text{ Nm}^{-1}$, $b = \sqrt{2} \text{ Nm}^{-1}\text{s}$, we get

$$H(s) = \frac{s\sqrt{2} + 1}{s^2 + s\sqrt{2} + 1}$$

Frequency response of suspension system:

$$H(j\omega) = H(s)|_{s=j\omega} = \frac{1 + j\omega\sqrt{2}}{1 - \omega^2 + j\omega\sqrt{2}}$$

$$\rightarrow \begin{cases} \text{Magnitude Response: } |H(j\omega)| = \left(\frac{1 + 2\omega^2}{(1 - \omega^2)^2 + 2\omega^2} \right)^{1/2} = \left(\frac{1 + 2\omega^2}{1 + \omega^4} \right)^{1/2} \\ \text{Phase Response: } \angle H(j\omega) = \angle \left(\frac{1 + j\omega\sqrt{2}}{1 - \omega^2 + j\omega\sqrt{2}} \times \frac{1 - j\omega\sqrt{2}}{1 - j\omega\sqrt{2}} \right) \\ = \angle \left(\frac{1 + 2\omega^2}{1 + \omega^2 + j\omega^3\sqrt{2}} \right) = -\tan^{-1} \left(\frac{\omega^3\sqrt{2}}{1 + \omega^2} \right) \end{cases}$$

Fourier series expansion of input: $x_i(t) = \frac{4}{\pi} \left[\sin(t) + \frac{1}{3} \sin(3t) + \frac{1}{5} \sin(5t) + \dots \right]$

- **Steady-state** response of system due to sinusoidal input $\sin(t)$ is given by

$$|H(j1)| \cdot \sin(t + \angle H(j1)) = 1.2247 \sin(t - 0.6155)$$

- **Steady-state** response of system due to sinusoidal input $\sin(3t)$ is given by

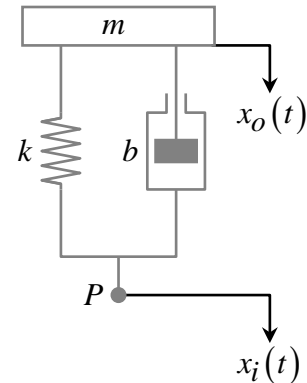
$$|H(j3)| \cdot \sin(3t + \angle H(j3)) = 0.4814 \sin(3t - 1.3147)$$

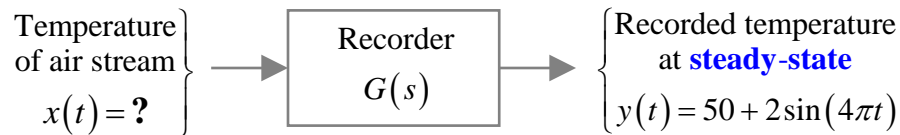
- **Steady-state** response of system due to sinusoidal input $\sin(5t)$ is given by

$$|H(j5)| \cdot \sin(5t + \angle H(j5)) = 0.2854 \sin(5t - 1.4248)$$

Since system is linear, the output of the system can be obtained by superposition. Hence, at **steady state**:

$$\begin{aligned} x_{o,ss}(t) &= \frac{4}{\pi} \left[1.2247 \sin(t - 0.6155) + \frac{1}{3} \times 0.4814 \sin(3t - 1.3147) + \frac{1}{5} \times 0.2854 \sin(5t - 1.4248) + \dots \right] \\ &= \frac{4}{\pi} \left[1.2247 \sin(t - 0.6155) + 0.1065 \sin(3t - 1.3147) + 0.05708 \sin(5t - 1.4248) + \dots \right] \end{aligned}$$



Solution to Q.2

$$G(s) = \frac{1}{s+1} \quad \text{since it is given that } G(s) \text{ has } \left\{ \begin{array}{l} \bullet \text{ DC gain} = 1 \\ \bullet \text{ First order dynamics} \\ \bullet \text{ Time constant} = 1 \text{ min} \end{array} \right\}$$

Therefore,

$$G(j\omega) = \frac{1}{j\omega + 1} \quad \dots\dots \left\{ \begin{array}{ll} \text{Magnitude response:} & |G(j\omega)| = (\omega^2 + 1)^{-1/2} \\ \text{Phase response:} & \angle G(j\omega) = -\tan^{-1}(\omega) \end{array} \right.$$

At STEADY-STATE:

The system output is $y(t) = 50 + 2\sin(4\pi t)$. Let the system input be $x(t) = \alpha + \beta \sin(4\pi t + \gamma)$. Then,

$$\alpha |G(j0)| + \beta |G(j4\pi)| \sin(4\pi t + \gamma + \angle G(j4\pi)) = 50 + 2\sin(4\pi t).$$

where

$$|G(j0)| = 1 \quad \text{and} \quad |G(j4\pi)| = (16\pi^2 + 1)^{-1/2} = 0.0793$$

$$\angle G(j4\pi) = -\tan^{-1}(4\pi) = -1.4914$$

Therefore,

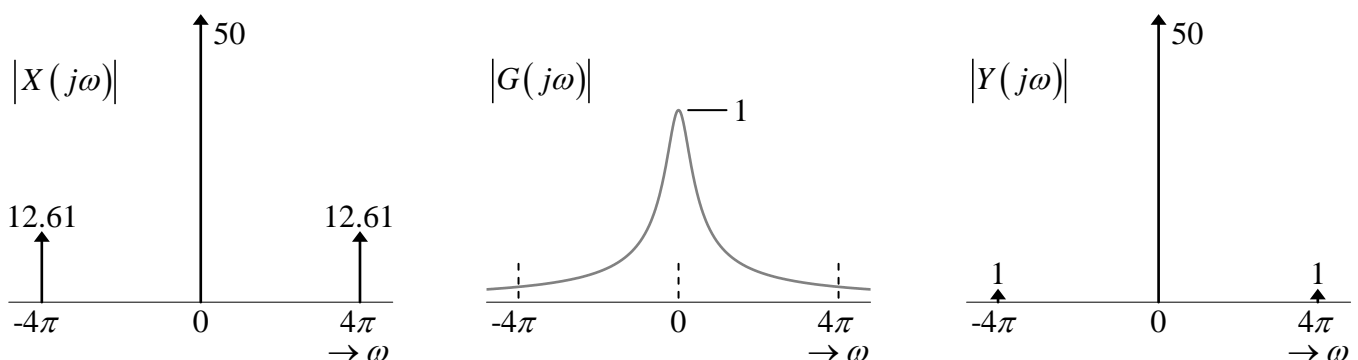
$$\left. \begin{array}{ll} \alpha |G(j0)| = 50 & \rightarrow \alpha = 1 \\ \beta |G(j4\pi)| = 2 & \rightarrow \beta = \frac{2}{0.0793} \approx 25.22 \\ \gamma + \angle H(j4\pi) = 0 & \rightarrow \gamma = 1.4914 \end{array} \right\} \rightarrow \left\{ \begin{array}{l} x(t) = \alpha + \beta \sin(4\pi t + \gamma) \\ \quad = 50 + 25.22 \sin(4\pi t + 1.49) \end{array} \right.$$

which shows that:

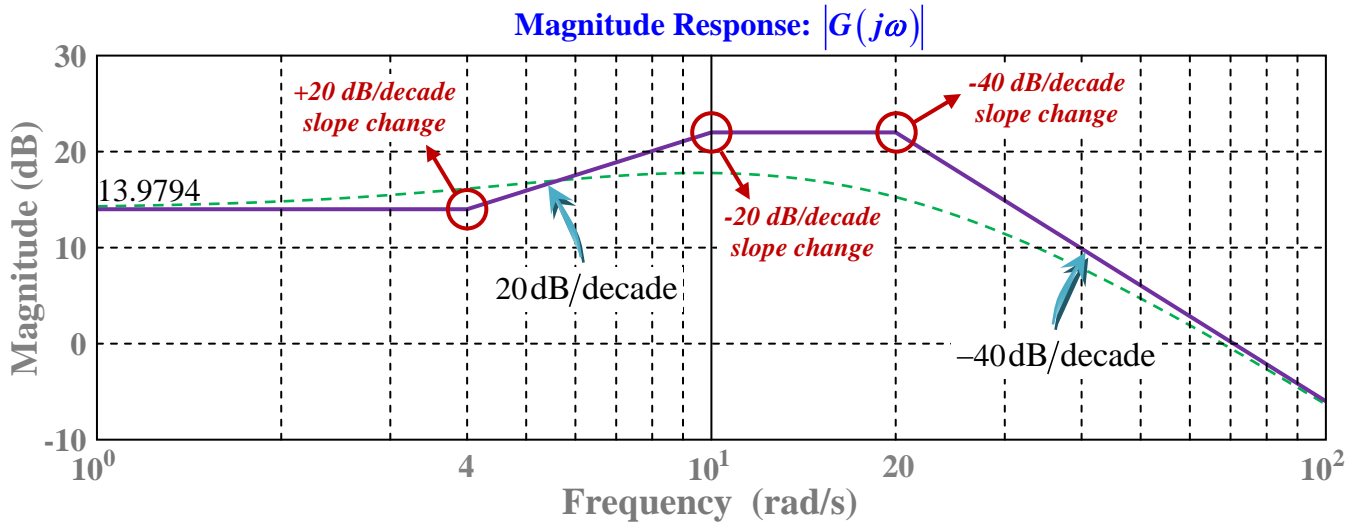
Maximum air temperature: $50 + 25.22 = 75.22^\circ\text{C}$

Minimum air temperature: $50 - 25.22 = 24.78^\circ\text{C}$

We note that the recorded maximum and minimum temperatures are 52°C and 48°C . Clearly, the recorder does not have sufficient bandwidth.



Solution to Q.3



Transfer function:
$$G(s) = \frac{K(s+\alpha)}{(s+\beta)(s+\gamma)(s+\lambda)} = \frac{K_{dc} \left(\frac{s}{\alpha} + 1 \right)}{\left(\frac{s}{\beta} + 1 \right) \left(\frac{s}{\gamma} + 1 \right) \left(\frac{s}{\lambda} + 1 \right)}; \quad K = \frac{\beta\gamma\lambda}{\alpha} K_{dc}$$

- (a)
- At $\omega = 4 \text{ rad/s}$, there is a **slope-change** of 20 dB/decade. This indicates the presence of the zero factor $\left(\frac{s}{4} + 1 \right)$ in $G(s)$.
 - At $\omega = 10 \text{ rad/s}$, there is a **slope-change** of -20 dB/decade. This indicates the presence of the pole factor $\left(\frac{s}{10} + 1 \right)^{-1}$ in $G(s)$.
 - At $\omega = 20 \text{ rad/s}$, there is a **slope-change** of -40 dB/decade. This indicates the presence of the double pole factor $\left(\frac{s}{20} + 1 \right)^{-2}$.
 - DC (or Static) gain: $\left[20 \log_{10} K_{dc} = |G(j0)|_{dB} = 13.9794 \text{ dB} \right]$ or $\left[K_{dc} = 10^{13.9794/20} = 5 \right]$.

Hence, the transfer function is

$$G(s) = \frac{5 \left(\frac{s}{4} + 1 \right)}{\left(\frac{s}{10} + 1 \right) \left(\frac{s}{20} + 1 \right)^2} = \frac{5000(s+4)}{(s+10)(s+20)^2}$$

$$\therefore K = 5000, \alpha = 4, \beta = 10, \gamma = \lambda = 20$$

(b)

CASE A: Magnitude response is invariant to transport delay (or dead-time).

Example: $\tilde{G}(s) = \frac{5000(s+4)}{(s+10)(s+20)^2} e^{-sL}$ and $G(s) = \frac{5000(s+4)}{(s+10)(s+20)^2}$ have the same magnitude response.

Proof:

$$|\tilde{G}(j\omega)| = \frac{5000|j\omega+4|}{|j\omega+10||j\omega+20|^2} \cdot \underbrace{|e^{-j\omega L}|}_{=1} = \frac{5000|j\omega+4|}{|j\omega+10||j\omega+20|^2} = |G(j\omega)|$$

REMARKS: For *unilateral* Laplace transform, this holds only for $L > 0$.
For *bilateral* Laplace transform, L can take any real value.

CASE B: Magnitude response is invariant to the reflection of any zero about the ω axis on the s -plane

Example: $\tilde{G}(s) = \frac{5000(s-4)}{(s+10)(s+20)^2}$ and $G(s) = \frac{5000(s+4)}{(s+10)(s+20)^2}$ have the same magnitude response.

Proof:

$$|\tilde{G}(j\omega)| = \frac{5000|j\omega-4|}{|j\omega+10||j\omega+20|^2} = \frac{5000|j\omega+4|}{|j\omega+10||j\omega+20|^2} = |G(j\omega)|$$

REMARKS: At first sight, it appears that we may also preserve the magnitude response by reflecting any pole about the ω axis on the s -plane. However, this will cause the system to become unstable. For unstable systems, it is erroneous to set $s = j\omega$ in $G(s)$ to obtain the frequency response because $s = j\omega$ lies outside the region of convergence of $G(s)$. Stated another way, frequency response of an unstable system does not exist. It is thus quite meaningless to talk about magnitude response of an unstable system.

Suppose $G(s)$ is stable and has frequency response $G(j\omega)$. By reflecting one or more poles of $G(s)$ to the right-half of the s -plane to form $\tilde{G}(s)$, all we can say is that $|\tilde{G}(j\omega)| = |G(j\omega)|$. It is incorrect to call $|\tilde{G}(j\omega)|$ the magnitude response of $\tilde{G}(s)$ because $\tilde{G}(s)$ is unstable.

Hence, possible transfer functions are:
$$\begin{cases} \frac{5000(s+4)}{(s+10)(s+20)^2}, & \frac{5000(s+4)}{(s+10)(s+20)^2} \exp(-sL) \\ \frac{5000(s-4)}{(s+10)(s+20)^2}, & \frac{5000(s-4)}{(s+10)(s+20)^2} \exp(-sL) \end{cases}$$