

Formulae Sheet for EE1002: Introduction to Circuits and Systems

Part 1

Resistors in series : $R_{eq} = R_1 + R_2 + R_3$; Resistors in parallel: $\frac{1}{R_{eq}} = \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3}$

Capacitors in series: $\frac{1}{C_{eq}} = \frac{1}{C_1} + \frac{1}{C_2} + \frac{1}{C_3}$; Capacitors in parallel: $C_{eq} = C_1 + C_2 + C_3$

Inductors in series: $L_{eq} = L_1 + L_2 + L_3$; Inductors in parallel: $\frac{1}{L_{eq}} = \frac{1}{L_1} + \frac{1}{L_2} + \frac{1}{L_3}$

Charge in capacitor: $Q = CV$, Energy stored in Capacitor: $E_C = \frac{1}{2} CV^2$

Flux - linkage for inductor: $\lambda = LI$, Energy stored in Inductor: $E_L = \frac{1}{2} LI^2$

Capacitor voltage transient in an RC circuit: $v_c(t) = v_c(0)e^{-\frac{t}{\tau}} + v_c(\infty)\left(1 - e^{-\frac{t}{\tau}}\right)$, $\tau = RC$

Inductor Current transient in an RL circuit: $i_L(t) = i_L(0)e^{-\frac{t}{\tau}} + i_L(\infty)\left(1 - e^{-\frac{t}{\tau}}\right)$, $\tau = \frac{L}{R}$

AC:

Impedance for R, L, C: $Z_C = \frac{1}{jC\omega}$, $Z_L = j\omega L$, $Z_R = R$

where $\omega = 2\pi f = 2\pi \frac{1}{T}$, $V_m = \sqrt{2}V_{RMS}$, $I_m = \sqrt{2}I_{RMS}$

AC Power:

AC supply connected to AC load: $Z = R + jX = \sqrt{R^2 + X^2} \angle \phi$, $\phi = \tan^{-1}\left(\frac{X}{R}\right)$, $X = \omega L$ or $X = -\frac{1}{\omega C}$

Given $v(t) = V_m \cos(\omega t)$, $i(t) = I_m \cos(\omega t - \phi)$,

Apparent power = $V_{RMS} I_{RMS}$

Average power (Real power) = $V_{RMS} I_{RMS} \cos \phi$

Imaginary power = $V_{RMS} I_{RMS} \sin \phi$

Power factor = $\cos \phi$,

(lagging power factor if current lags voltage, else leading power factor if current leads voltage)

Part 2

Chapter 1: Magnetic Circuits and transformers	
Magnetic flux	$B = \frac{\phi}{A} \quad (1.2a)$
Flux-linkage	$\lambda = N \times \phi \quad (1.3)$
Faraday's Law	$e = N \frac{d\phi}{dt} = \frac{d(N\phi)}{dt} = \frac{d\lambda}{dt} \quad (1.4a)$
Voltage Induced in Field-cutting Conductors	$e = \frac{d\lambda}{dt} = Bl \frac{dx}{dt} = Bl(u = \frac{dx}{dt}) = Blu \quad (1.5)$
Voltage Induced by Time-varying Flux	$\phi = \phi_m \sin(\omega t),$ $e = N \frac{d\phi}{dt} = N\phi_m \omega \cos(\omega t) \text{ volts} \quad (1.6)$
Magnetic Field Intensity and Ampere's Law	$B = \mu H = \mu_r \mu_0 H \quad (1.7) \quad \oint H \cdot dl = \sum i \quad (1.8)$
Magnetic Field around a long Straight Wire	$Hl = \sum i = H \times (2\pi r) = I \Rightarrow H = \frac{I}{2\pi r} \Rightarrow B = \mu H$ $= \frac{\mu I}{2\pi r} \quad (1.9)$
Magnetic Field in a Toroidal Core	$Hl = \sum i = H \times (2\pi R) = NI \Rightarrow H = \frac{NI}{2\pi R} \Rightarrow B = \mu H = \frac{\mu NI}{2\pi R}$ \Rightarrow $\phi = B \times A = \frac{\mu NI}{2\pi R} \times (\pi r^2) = \frac{\mu NI r^2}{2R} \Rightarrow \lambda = N\phi$ $= \frac{\mu N^2 I r^2}{2R} \quad (1.9a)$
Magnetic Circuits, MMF	$\mathcal{F} = N \times i \quad A - \text{turns} \quad (1.10)$
Reluctance of magnetic path	$\mathcal{R} = \frac{l}{\mu A} \quad (1.11)$
MMF	$\mathcal{F} = \mathcal{R} \times \phi \quad (1.12)$
Self-Inductance	$L = \frac{\lambda}{i} = \frac{N\phi}{i} = \frac{N(\frac{Ni}{\mathcal{R}})}{i} = \frac{N^2}{\mathcal{R}} \quad (1.13)$
Voltage induced in the self-inductance	$e = \frac{d\lambda}{dt} = \frac{d(Li)}{dt} = L \frac{di}{dt} = v_L \quad (1.14)$
Self-inductances of coils	$L_1 = \frac{\lambda_{11}}{i_1} \text{ and } L_2 = \frac{\lambda_{22}}{i_2} \quad (1.15)$
Mutual inductances between coils	$M = \frac{\lambda_{21}}{i_1} = \frac{\lambda_{12}}{i_2} \quad (1.16)$
Total flux-linkage	$\lambda_1 = \lambda_{11} \pm \lambda_{12} = L_1 i_1 \pm M i_2 \text{ and } \lambda_2 = \pm M i_1 + L_2 i_2 \quad (1.17)$
Transformer voltage relationship	$v_2(t) = \frac{N_2}{N_1} v_1(t) \quad (1.22)$
Transformer current relationship	$\mathcal{F} = N_1 i_1(t) - N_2 i_2(t) = 0 \Rightarrow i_2(t) = \frac{N_1}{N_2} i_1(t) \quad (1.23)$

Ideal transformer power relationship	$p_2(t) = v_2(t) \times i_2(t) = v_1(t) \times i_1(t) = p_1(t) \quad (1.24)$
Impedance Transformations	$Z_L = \frac{V_2}{I_2} \Rightarrow Z'_L = \frac{V_1}{I_1} = \left(\frac{N_1}{N_2}\right)^2 Z_L \quad (1.25)$
Real transformer	$P = V_{rms} I_{rms} \cos\phi, Q = V_{rms} I_{rms} \sin\phi, S = V_{rms} I_{rms}$
Voltage regulation of transformer	percent regulation = $\frac{V_{no-load} - V_{load}}{V_{load}} \times 100\% \quad (1.26)$
Efficiency of transformer	power efficiency = $\frac{P_{out}}{P_{in}} \times 100\% \quad (1.27)$
Chapter 2: Power Semiconductor Diodes and Rectifiers	
Half-wave rectifier average voltage	$V_{o,avg} = \frac{V_m}{\pi} \quad (2.1)$
Output filter capacitor for half-wave rectifier	$C = \frac{I_L T}{V_{pk-pk}} = \frac{I_L}{V_{pk-pk} \times f} \quad (2.6)$
Full-wave bridge rectifier average voltage	$V_{o,avg} = \frac{1}{\pi} \left[\int_0^\pi V_m \sin(\omega t) d(\omega t) \right] = \frac{2V_m}{\pi} \quad (2.7)$
Output filter capacitor for full-wave bridge rectifier	$C = \frac{I_L \times T}{2 \times V_{pk-pk}} = \frac{I_L}{2 \times f_s \times V_{pk-pk}} \quad (2.8)$
Chapter 3: Introduction to Electromechanical Energy Converters	
Torque in an electrical machine	$T = k(\mathbf{B}_s \times \mathbf{B}_r) = k B_s B_r \sin(\gamma) \quad (3.2)$
Linear DC machine	$\mathbf{F}_{ind} = i(l \times \mathbf{B}) \quad (3.3)$ $e_{ind} = (\mathbf{u} \times \mathbf{B}) \bullet \mathbf{l} \quad (3.4)$ $\mathbf{KVL}: V_T - i_A R_A - e_{ind} = 0 \quad (3.5)$ $\mathbf{Newton's Law}: \mathbf{F}_{net} = m \times \mathbf{a} \quad (3.6)$
Steady-state linear velocity	$V_T = e_{ind} = Bl u_{ss} \Rightarrow u_{ss} = \frac{V_T}{Bl} \quad (3.11)$
Converted power in linear DC machine	$P_{conv} = e_{ind} \times i_A = F_{ind} \times u \quad (3.13)$
Field-circuit voltage in rotating DC machine	$V_F = R_F I_F \quad (3.16)$
Back-emf in DC machine	$E_A = K_A \phi \omega_m \quad (3.17)$
Motor torque in DC machine	$T_{dev} = K_T \phi I_A \quad (3.18)$
Converted power in rotating DC machine	$P_{dev} = T_{dev} \omega_m = E_A \times I_A \quad (3.19)$
Armature and field circuit voltages under steady-state condition	$V_T \text{ or } V_A = E_A + I_A R_A \quad \text{armature circuit} \quad (3.21)$ $V_F = I_F R_F \quad \text{field circuit} \quad (3.22)$

Armature and field circuit voltages under dynamic condition	$v_T(t) \text{ or } v_A(t) = e_A(t) + i_A(t)R_A + L_a \frac{di_A}{dt} \text{ (armature circuit) (3.23)}$ $v_F = i_F(t)R_F + L_f \frac{di_F}{dt} \text{ (field circuit) (3.24)}$
Equation of motion	$T_{dev}(t) = k_T \phi(t) i_A(t) = T_L + b(t) \omega_m + J \frac{d\omega_m}{dt} \quad (3.25)$
Generator voltage relationship with speed	$\frac{E_{A1}}{E_{A2}} = \frac{n_1}{n_2} = \frac{\omega_1}{\omega_2} \quad (3.26)$
Motor torque-speed characteristic	$\omega_m = \frac{V_T}{K_A \phi} - \frac{R_A T_{dev}}{(K_T \phi)(K_A \phi)} = \frac{V_T}{K \phi} - \frac{R_A}{(K \phi)^2} T_{dev} \quad (3.29)$
Chopper output voltage	$V_o = \frac{1}{T} \int_0^T v_o(t) dt = V_s \times \frac{T_{on}}{T} = V_s \times D \quad (3.33)$