### NATIONAL UNIVERSITY of SINGAPORE

# **Department of Electrical and Computer Engineering**

#### **EE2021 – Devices and Circuits**

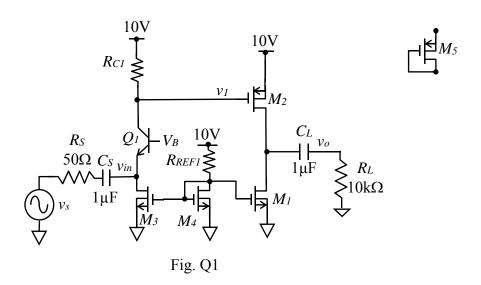
#### **Homework 4 Solutions**

## **Homework 4:**

You have to submit the homework assignment (Q.1) in hardcopy in class on <u>Wednesday</u> 8 April 2015.

Unless otherwise stated, you may use the tables of the amplifier configurations and equivalent resistances in your lecture notes in your solutions to the questions.

# **Q.1**



In the two-stage amplifier circuit shown in Fig. Q1, assume that the npn BJT, the NMOS transistors and the PMOS transistors have the following device parameters:

- $V_A = 100 \text{ V}$  and  $\beta = 100 \text{ for the BJT}$ ,  $Q_I$ ;
- $K_n = 2 \text{ m A/V}^2$ ,  $V_{THN} = 1 \text{ V}$ ,  $\lambda_n = 0.001 \text{ V}^{-1}$  and no body effect for the NMOS transistors,  $M_1$ ,  $M_3$  and  $M_4$ .
- $K_p = 2 \text{ m A/V}^2$ ,  $V_{THP} = -1 \text{ V}$ ,  $\lambda_p = 0.001 \text{ V}^{-1}$  and no body effect for the PMOS transistors,  $M_5$  and  $M_2$ .

Further assume that  $R_{REF1}$  is chosen such that  $M_1$ ,  $M_3$  and  $M_4$  each has a drain current of 1 mA. (You are not required to find  $R_{REF1}$ .)

(i) Identify the configuration of each stage of the multi-stage amplifier.

[2 marks]

(ii) Estimate the small signal parameters of  $M_2$ , i.e.  $g_{m,M2}$ , and  $r_{o,M2}$  and the small signal parameters of  $Q_1$ , i.e.,  $g_{m,Q1}$ ,  $r_{\pi,Q1}$ ,  $r_{o,Q1}$ .

[3 marks]

(iii) Design  $R_{CI}$  to ensure that  $M_2$  has the same current as  $M_1$  assuming these transistors are operating in the saturation region.

[2 marks]

(iv) Estimate the overall gain, i.e.,  $v_o/v_s$ .

[6 marks]

(v) What is the minimum  $V_B$  value allowed such that  $M_3$  is operating in the saturation region?

[4 marks]

(vi) If  $R_{CI}$  is replaced with  $M_5$ , would it create any biasing issue? Would the overall gain be larger or smaller?

[3 marks]

1. (i) Identify the configuration of each stage of the multi-stage amplifier.

Common base - Common Source

(ii) Estimate the small signal parameters of M<sub>2</sub>, i.e.  $g_{m,M2}$ , and  $r_{o,M2}$  and the small signal parameters of Q<sub>1</sub>, i.e.,  $g_{m,Q1}$ ,  $r_{\pi Q1}$ ,  $r_{o,Q1}$ .

$$I_{C,QI} \approx I_{E,QI} = I_{D,M3} = I_{D,MI} = I_{D,M2} = 1 \text{ mA}.$$

$$g_{m,Q1} = \frac{I_C}{V_T} = \frac{1 \text{ mA}}{0.025 \text{ V}} = 40 \text{ mA/V}.$$

$$r_{\pi,Q1} = \frac{\beta}{g_m} = \frac{100}{0.04} = 2.5 \text{ k}\Omega.$$

$$r_{o,Q1} = \frac{V_A}{I_C} = \frac{100}{1 \times 10^{-3}} = 100 \text{ k}\Omega.$$

$$g_{m,M2} = 2\sqrt{K_p I_{D,M2}} = 2\sqrt{2 \times 10^{-3} \times 1 \times 10^{-3}} = 2.83 \text{ mA/V}.$$

$$r_{o,M2} = \frac{1}{\lambda_n I_D} = \frac{1}{0.001 \times 1 \times 10^{-3}} = 1 \text{ M}\Omega.$$

(iii) Design  $R_{CI}$  to ensure that  $M_2$  has the same current as  $M_1$  assuming these transistors are operating in the saturation region.

$$I_{D,M2} = K_p (V_{GS,M2} - |V_{THP}|)^2 = 1 \text{ mA}$$

 $\Rightarrow$   $|V_{GS,M2}| = 1.71 \text{ V} = I_{C,Q1}R_{C1}$  (The other solution, 0.293 V is rejected as it is less than the magnitude of the threshold voltage.)

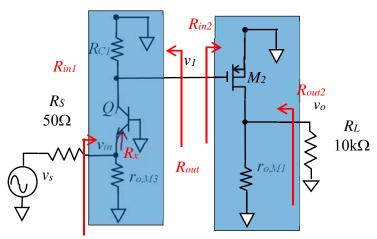
$$R_{CI} = 1.71 \text{ k}\Omega$$

(iv) Estimate the overall gain, i.e.,  $v_o/v_s$ .

#### Note:

- Students are not required to draw the circuits shown below, nor state the values of the two-port parameters as given below. If they could get the answer to the overall gain correct, they get full (6) marks. However, if they do not get the answer, then these circuits, or parameter values, if given correctly, will earn partial credits as shown.
- Some of the answers below are calculated after making approximations. Students may calculate the values without using approximations. They should be marked correct in those cases. Anyway, the answers would not be different by more than 10%.

# **AC** Equivalent Circuit:



#### Two port network prameters:

For CB Amplifier,  $G_{ml} = -g_{m,Ql} = -40 \text{ mA/V}$ ,

For CS amplifier,  $G_{m2} = g_{m,M2} = 2.83 \text{ mA/V}$ ,

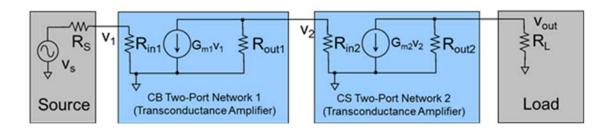
$$R_{in2} = \infty,$$

$$R_{out1} = r_{o,Q1} \left\{ 1 + g_{m,Q1} \left[ \left( r_{\pi,Q1} + R_S \right) / \left( r_{\sigma,M3} \right) \left( \frac{r_{\pi,Q1}}{r_{\pi,Q1} + R_S} \right) \right\} / \left( R_{C1} \approx R_{C1} = 1.71 \text{ k}\Omega \right) \right\}$$

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$$R_{in1} = \left[ \frac{1}{g_{m,Q1}} \times \frac{r_{o,Q1} + R_C}{r_{o,Q1} + R_C/\beta} \right] // r_{o,M3} \approx \frac{1}{g_{m,Q1}} = 25 \Omega$$

 $R_{out2} = r_{o,M2} // r_{o,M1} = 500 \text{ k}\Omega.$ 



$$\frac{v_o}{v_s} = \frac{v_1}{v_s} \times \frac{v_2}{v_1} \times \frac{v_o}{v_2}$$

$$= \frac{R_{in1}}{R_s + R_{in1}} \times \left[ -G_{m,Q1} (R_{out1} / / R_{in2}) \right] \times \left[ -G_{m,M2} (R_{out2} / / R_L) \right]$$

$$\approx \frac{\frac{1}{g_{m,Q1}}}{R_s + \frac{1}{g_{m,Q1}}} \times g_{m,Q1} R_{C1} \times \left( -g_{m,M2} R_L \right)$$

$$= \frac{25}{50 + 25} \times 40 \times 10^{-3} \times 1.71 \times 10^3 \times \left( -2.83 \times 10^{-3} \times 10 \times 10^3 \right)$$

$$= 0.33 \times 68.4 \times \left( -28.3 \right) = -638.8$$

(v) What is the minimum  $V_B$  value allowed such that  $M_3$  is operating in the saturation region?

$$I_{D,M3} = K_n (V_{GS,M3} - V_{THN})^2 = 1 \text{ mA}$$

For  $M_3$  to operate in saturation, the minimum drain-source voltage,

$$V_{DSsat,M3} = V_{GS,M3} - V_{THN} = \sqrt{\frac{I_{D,M3}}{K_n}} = 0.707 \text{ V}.$$

$$V_{E,Q1} = V_{DSsat,M3} = 0.707 \text{ V}$$

Minimum 
$$V_{B,QI} = V_{E,QI} + 0.7 = 1.407 \text{ V}.$$

(vi) If  $R_{CI}$  is replaced with  $M_5$ , would it create any biasing issue? Would the overall gain be larger or smaller?

Biasing would not be an issue as the  $M_5$  will produce the  $V_{GS}$  needed for 1 mA to flow through it.

The small signal resistance of  $M_5$  (diode connected resistor) is

$$\frac{1}{g_{m,M5}} = 353 \,\Omega.$$

As this value is less than RC1, the gain would be smaller.