EE3331C/EE3331E Feedback Control Systems Part II: Frequency Response Methods

Chapter 3: Stability Analysis

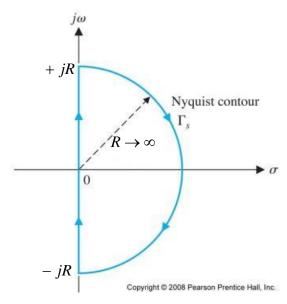
Part 3B – Nyquist Stability Criterion

Closed loop transfer function

$$G_{CL}(s) = \frac{L(s)}{1 + L(s)} = \frac{L(s)}{F(s)}$$

 \circ Stability check: Is there any pole of G_{CL} in the RHP?

- O Nyquist Contour:
 - A closed contour that surrounds the entire RHP
 - \circ Radius of the semicircle $R \rightarrow \infty$



Stability check objective using the Nyquist contour:

Is there any pole of G_{CL} in the area bounded by the Nyquist contour?

$$G_{CL}(s) = \frac{L(s)}{1 + L(s)} = \frac{L(s)}{F(s)}$$

○ A pole of $G_{CL}(s)$ is a zero of F(s)

$$G_{CL}(s_1) = \infty \qquad \Rightarrow \qquad F(s_1) = 0$$

Transfer Function Pole:

if $G(s_1) = \infty$ then $s = s_1$ is a pole of G(s)

Transfer Function Zero: if $G(s_1)=0$ then $s=s_1$ is a zero of G(s)

 Stability check objective using the Nyquist contour and the transfer function F(s):

Is there any zero of F(s) in the area bounded by the Nyquist contour?

$$F(s) = 1 + L(s)$$

Example 3b-1: Closed loop pole is zero of the transfer function F(s)

$$L(s) = \frac{10}{s(s+5)}$$

Then,

$$F(s) = 1 + L(s)$$

$$= 1 + \frac{10}{s(s+5)}$$

$$= \frac{s(s+5) + 10}{s(s+5)}$$

$$F(s) = \frac{s^2 + 5s + 10}{s(s+5)}$$

$$s^2 + 5s + 10 = 0$$

$$s_{1,2} = -2.5 \pm j1.94$$
 [zeros of F(s)]

The closed loop transfer function,

$$G_{CL}(s) = \frac{L(s)}{1 + L(s)} = \frac{L(s)}{F(s)}$$

$$= \frac{\frac{10}{s(s+5)}}{\frac{s^2 + 5s + 10}{s(s+5)}}$$

$$= \frac{10}{s^2 + 5s + 10}$$

$$s^{2} + 5s + 10 = 0$$

 $s_{1,2} = -2.5 \pm j1.94$ [Closed loop poles]

Closed Loop Stability Check

Search for a pole of G_{CL}(s) in the RHP?



Search for a pole of G_{CL}(s) inside the Nyquist Contour?



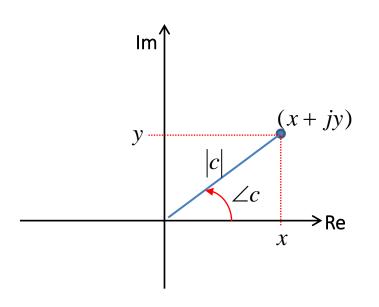
Search for a zero of F(s) inside the Nyquist Contour?

Define a closed contour that surrounds the entire RHP ⇒ the Nyquist Contour

A pole of $G_{CL}(s)$ is also a zero of F(s) where F(s) = 1+L(s)

Cauchy's Principle of Argument or the Argument Principle

a. Argument of a Complex Number c = (x + jy)



Modulus (magnitude) – distance from the origin

$$|c| = \sqrt{x^2 + y^2}$$

Argument – angle between the line drawn from the point to the origin and the positive real-axis

$$\angle c = \tan^{-1} \frac{y}{x}$$

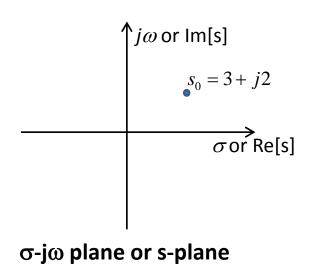
If a function F(s) of complex variable s is evaluated for $s=s_0$, the result is a complex number $F(s_0)$

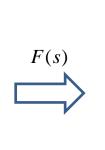
• Example 3b-2:
$$F(s) = \frac{s+2}{s+3}$$
 $F(s_0) = \frac{5+j2}{6+j2}$ $s_0 = 3+j2$ $\sqrt{29} \angle 21.8^{\circ}$

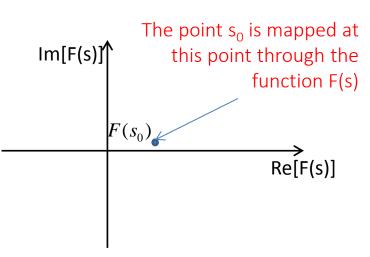
$$F(s_0) = \frac{5 + j2}{6 + j2}$$
$$= \frac{\sqrt{29} \angle 21.8^{\circ}}{\sqrt{40} \angle 18.4^{\circ}}$$

$$|F(s_0)| = \frac{\sqrt{29}}{\sqrt{40}} = 0.85$$

 $\angle F(s_0) = 21.8^\circ - 18.4^\circ = 3.4^\circ$







Re[F]-Im[F] plane or the F(s)-plane

- The point s_0 is mapped to the point $F(s_0)$
 - \circ Principle of Argument (PoA) deals with the $\angle F(s)$

Consider the point $s_0 = 3+j2$ mapped to $F(s_0)$ where F(s) has one real-axis zero and no pole, e.g., F(s)=(s+2)

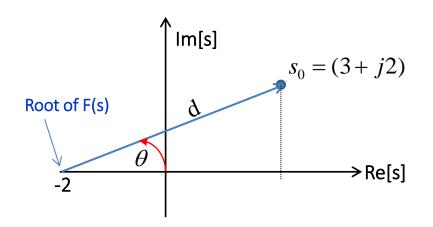
$$F(s) = s + 2$$

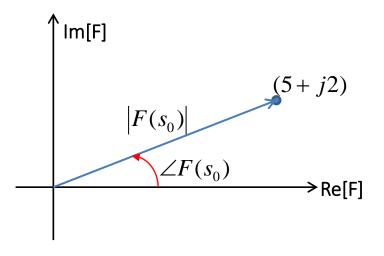
$$F(s_0) = (3 + j2) + 2$$

$$= 5 + j2$$

$$|F(s_0)| = \sqrt{5^2 + 2^2} = \sqrt{29}$$

$$\angle F(s_0) = \tan^{-1} \frac{2}{5}$$





 $|F(s_0)|$ is equal to the distance between s_0 and the root of F(s).

$$d = \sqrt{5^2 + 2^2} = \sqrt{29}$$

 $\angle F(s_0)$ is equal to the angle between the line drawn from the root of F(s) to s_0 and the +ve real axis

$$\theta = \tan^{-1} \frac{2}{5}$$

 \circ Now consider the mapping of 3+j2 when F(s) has one real-axis pole and no zero

$$F(s) = \frac{1}{s+2}$$

$$F(s_0) = \frac{1}{3+j2+2} = \frac{1}{5+j2} = (a-jb)$$

$$|F(s_0)| = \frac{1}{\sqrt{5^2+2^2}}$$

$$\angle F(s_0) = -\tan^{-1}\frac{2}{5}$$

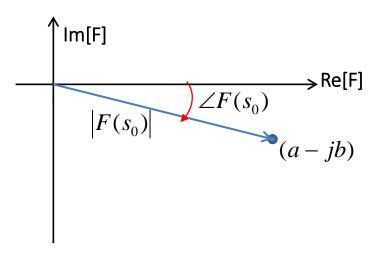
$$\lim[s]$$

$$S_0 = (3+j2)$$

$$Re[s]$$

$$d = \sqrt{5^2+2^2}$$

$$\theta = \tan^{-1}\frac{2}{5}$$



|F(s)| is equal to the reciprocal of d

$$|F(s_0)| = \frac{1}{d}$$

 $\angle F(s)$ is equal to $-\theta$

$$\angle F(s_0) = -\theta$$

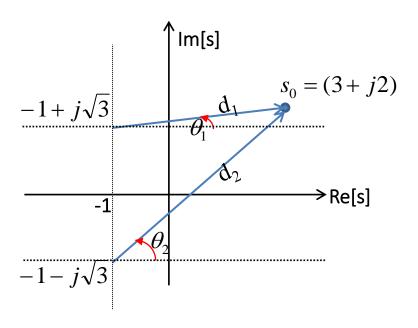
One more example: F(s) with two complex zeros

$$F(s) = s^{2} + 2s + 4, \quad s_{1,2} = -1 \pm j\sqrt{3}$$

$$s_{0} = 3 + j2$$

$$F(s_{0}) = (3 + j2)^{2} + 2(3 + j2) + 4 \qquad |F(s_{0})| = \sqrt{15^{2} + 16^{2}} \qquad \angle F(s_{0}) = \tan^{-1} \frac{16}{15}$$

$$= 15 + j16 \qquad = 21.9 \qquad = 46.8^{\circ}$$



$$d_1 = \sqrt{4^2 + (2 - \sqrt{3})^2} \cong 4$$

$$d_2 = \sqrt{4^2 + (2 + \sqrt{3})^2} \cong 5.47$$

$$d_1 \times d_2 \cong 21.9$$

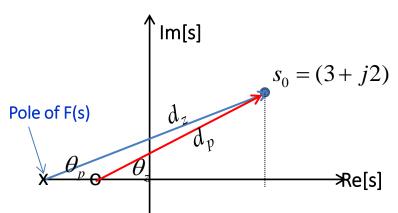
$$\theta_1 = \tan^{-1} \frac{(2 - \sqrt{3})}{4} = 3.8^{\circ}$$

$$\theta_2 = \tan^{-1} \frac{2 + \sqrt{3}}{4} = 43.0^{\circ}$$

$$\theta_1 + \theta_2 = 46.8^{\circ}$$

 \circ Another one: F(s) having one pole and one zero

$$F(s) = \frac{s+1}{s+2}$$



$$F(s_0) = \frac{4+j2}{5+j2}$$

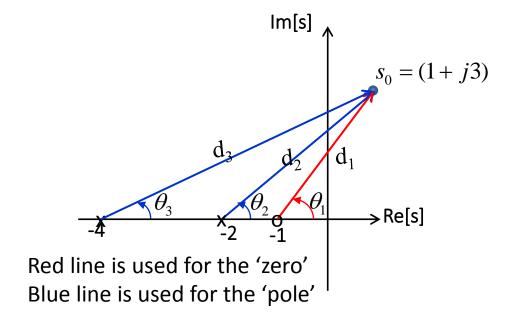
$$|F(s_0)| = \frac{\sqrt{4^2+2^2}}{\sqrt{5^2+2^2}} = \frac{d_z}{d_p}$$

$$\angle F(s_0) = \tan^{-1}\frac{2}{4} - \tan^{-1}\frac{2}{5} = \theta_z - \theta_p$$

- In general, if
 - \circ θ_{z1} , θ_{z2} , θ_{z3} , etc. are the angles formed by the lines drawn from s_0 to the zeros of F(s) and
 - \circ θ_{p1} , θ_{p2} , θ_{p3} , etc. are the angles formed by the lines drawn from s_0 to the poles of F(s), then

$$\angle F(s_0) = (\theta_{z1} + \theta_{z2} + \theta_{z3} + ...) - (\theta_{z1} + \theta_{z2} + \theta_{z3} + ...)$$

$$F(s) = \frac{(s+1)}{(s+2)(s+5)}$$



$$F(s_0) = \frac{d_1 \angle \theta_1}{(d_2 \angle \theta_2)(d_2 \angle \theta_2)}$$

$$\left| F(s_0) \right| = \frac{d_1}{d_2 \times d_3}$$

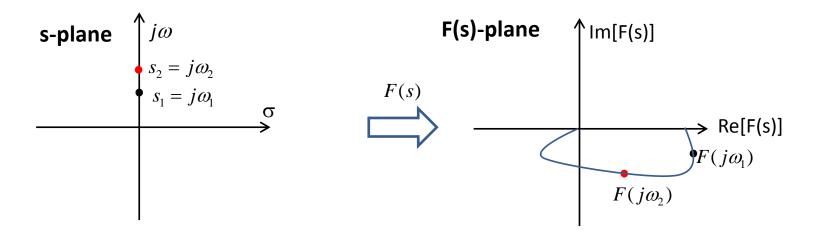
$$\angle F(s_0) = \theta_1 - \theta_2 - \theta_3$$

 \circ For the Principle of Argument, we are interested to know the variations in the **argument of** F(s) as s_0 is varied around a **closed contour**

b. Mapping of a line, i.e., when s is varied

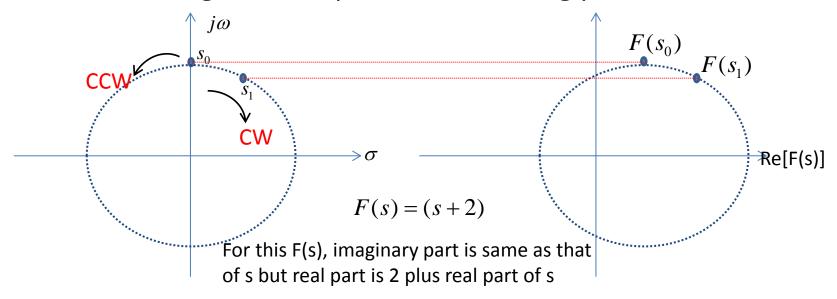
 \circ For example, consider s varied along the +j ω -axis

$$F(s)|_{s=+j\omega} = F(j\omega), \quad 0 \le \omega \le \infty$$



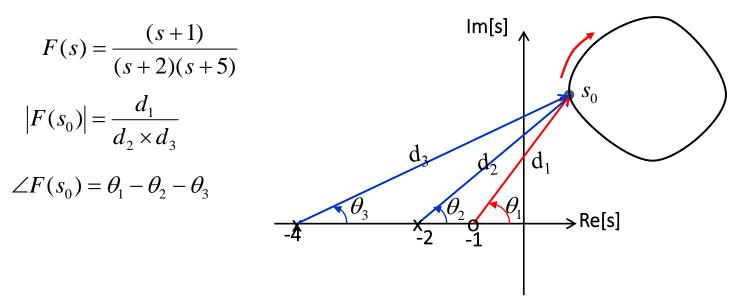
- o $F(j\omega)$ for ω : $0\rightarrow\infty$, is the frequency response of the transfer function F(s)
 - O Mapping of the $+j\omega$ axis is the frequency response plot on the $F(j\omega)$ plane. It is also called the **polar plot** of $F(j\omega)$.

 \supset If s is varied along a closed path, the resulting plot is also closed



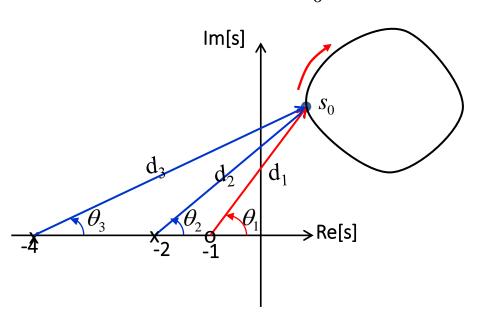
- While mapping a closed path, we need to define the direction
 - Clockwise (CW) or
 - Counter-clockwise (CCW)
- The Nyquist Stability Criterion is based on the properties of the argument of a transfer function while s is varied along the Nyquist contour (which is a closed path)

- \circ When a closed contour is mapped through a complex function F(s),
 - Variation in $\angle F(s)$ is determined by the variations in angles θ_1 , θ_2 , θ_3 , etc. as the point s_0 is moved around the contour



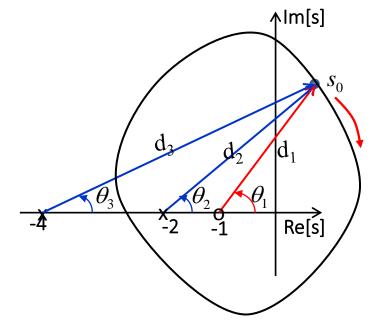
- O How $\angle F(s)$ is varied depends on the positions of the poles and zeros of F(s) with respect to the closed contour
 - o Is a pole (or zero) inside the contour or outside?

\circ Assume, the point s_0 is moved around the contour in CW direction



All poles and zeros are outside the closed contour ⇒ pole or zero is **not enclosed** by the contour

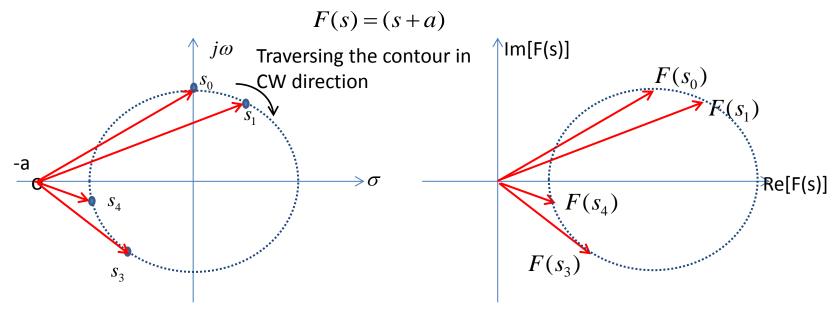
Variations in all the angles (θ_1 , θ_2 , and θ_3) are less than 360° as s_0 is moved around the contour



One pole and one zero are inside the closed contour (**enclosed** by the contour)

 θ_1 and θ_2 goes through net change of 360° as s_0 is moved around the contour

O Illustration # 1: F(s) with a single zero outside the contour

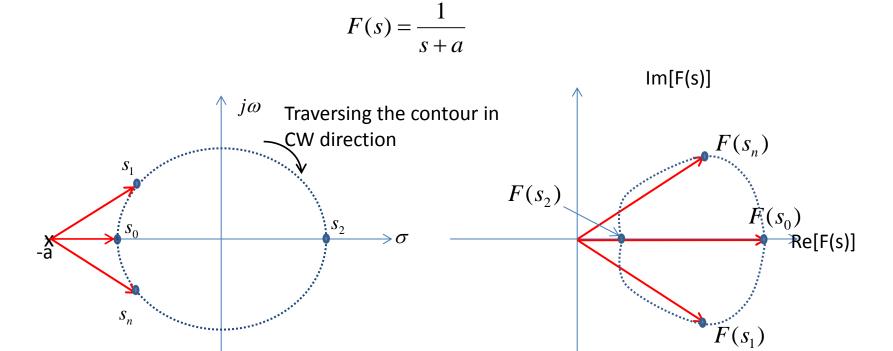


Here and in the examples that follow, the contour is traversed in the CW direction

- Observation:
 - \circ The zero of F(s) is **outside** the contour
 - Net change in $\angle F(s)$ is less than $360^\circ \Rightarrow$ The plot of F(s) doesn't encircle the origin

[Only argument, not the modulus, of F(s) is of interest for PoA]

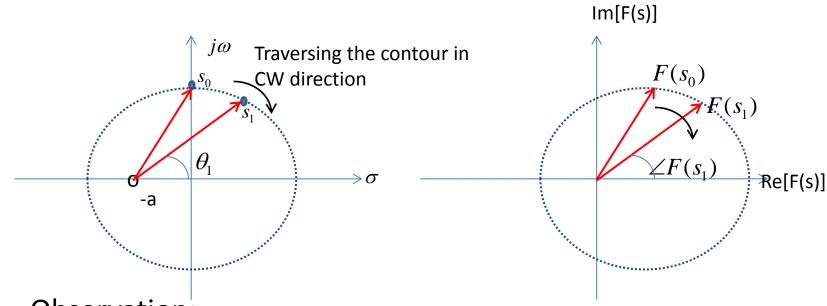
 \circ *Illustration* # 2: F(s) with a single pole outside the contour



- Observation:
 - \circ The pole of F(s) is **outside** the contour
 - Net change in $\angle F(s)$ is less than $360^\circ \Rightarrow$ The plot of F(s) doesn't encircle the origin

O Illustration # 3: F(s) with a single zero enclosed by the contour

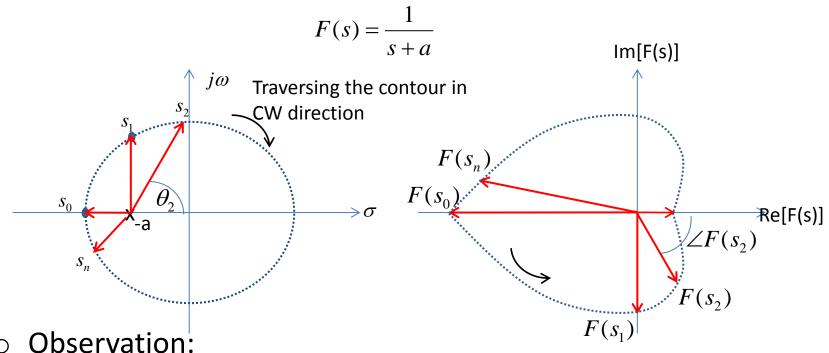
$$F(s) = (s+a)$$



- Observation:
 - \circ The zero of F(s) is **enclosed** the contour
 - \angle F(s) goes through a net change of 360° \Rightarrow The plot of F(s) encircles the origin in the same direction as traversing the contour in s-plane

$$\angle F(s) = \theta$$

Illustration # 4: F(s) with a single pole enclosed by the contour



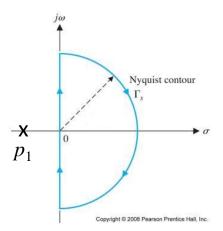
- - \circ The pole of F(s) is **enclosed** by the contour
 - \circ \angle F(s) goes through a net change of 360° \Rightarrow The plot of F(s)encircles the origin in the direction opposite to the traversing direction in s-plane

$$\angle F(s) = -\theta$$

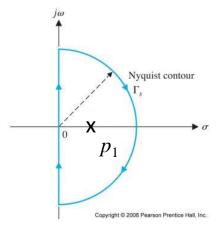
Summary:

- o If zeros and poles of F(s) are **not** enclosed by the contour, none of the vectors drawn from the zeros and poles to the CW traversing point on the contour rotate through 360°
 - \circ $\angle F(s)$ is not varied by 360° or more
 - \circ Resulting F(s)-plot doesn't encircle the origin of F(s) plane
- If a zero (or a pole) is enclosed by the contour, the vector drawn from the zero (or pole) to the CW traversing point rotates through 360°
 - \circ $\angle F(s)$ is changed through 360° for each pole or zero
 - Origin of the F(s)-plane is encircled (CW for zero and CCW for pole)

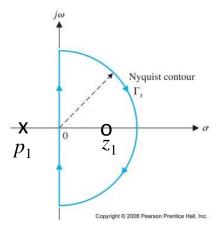
Illustration (enclosure of pole or zero in the s-plane)



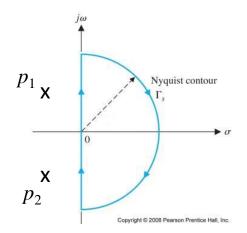
Pole p_1 is not enclosed



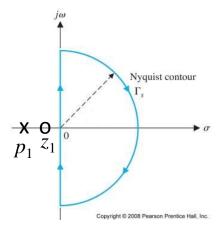
Pole p_1 is enclosed



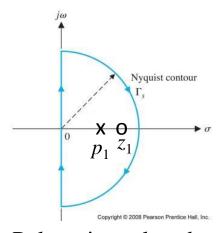
Pole p_1 is not enclosed Zero z_1 is enclosed



Pole p_1 is not enclosed Pole p_2 is not enclosed

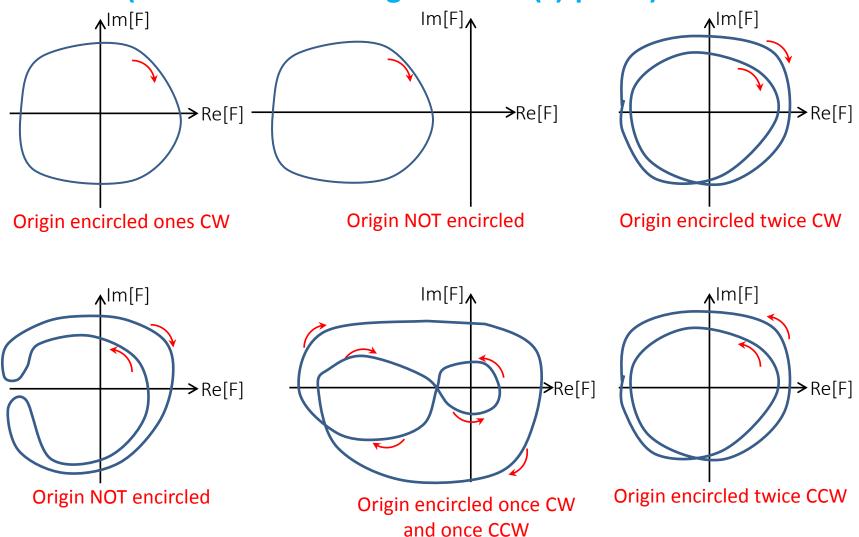


Pole p_1 is not enclosed Zero z_1 is not enclosed



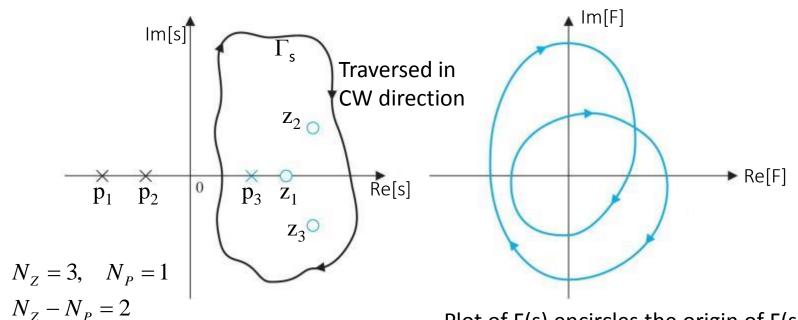
Pole p_1 is enclosed Zero z_1 is enclosed

Illustration (encirclement of origin in the F(s)-plane)



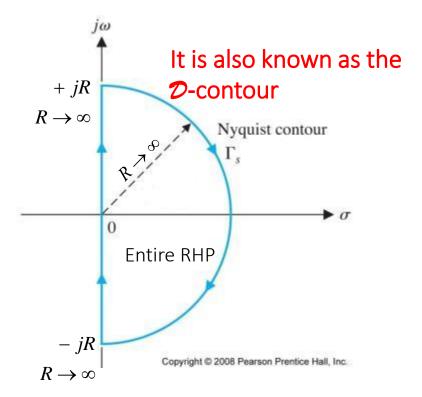
Statement of the Principle of Argument

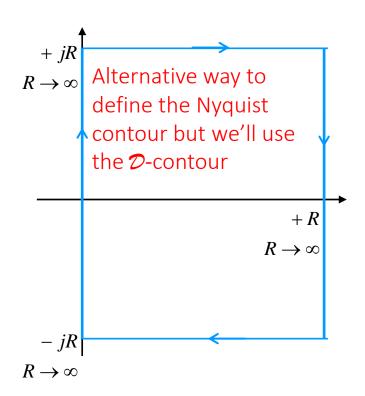
o If a complex function F(s) has $\mathbf{N_Z}$ number of zeros and $\mathbf{N_P}$ number of poles enclosed by a contour Γ_s then the contour mapping encircles the origin $(\mathbf{N_Z-N_P})$ times in the same direction as the direction of traversing the contour



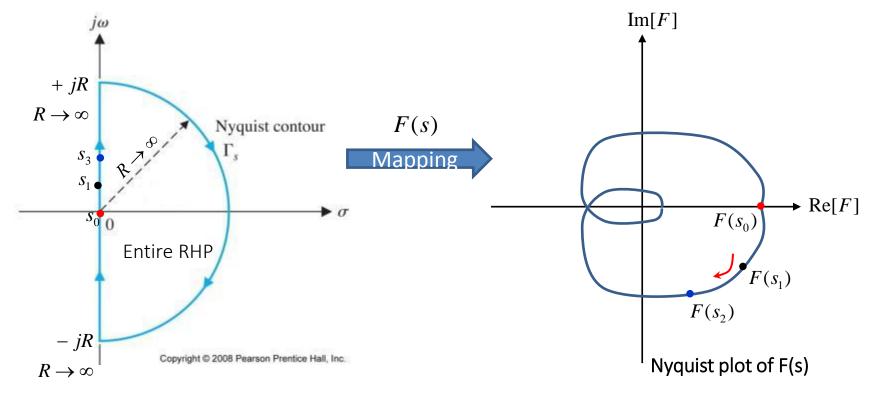
Plot of F(s) encircles the origin of F(s)plane twice in the CW direction

- Argument Principle defines the relation between encirclement of origin by F(s)-plot and number of poles and zeros enclosed in a predefined contour
- Stability Check: is there any zero of F(s) = 1 + L(s) enclosed by the Nyquist contour?





- Mapping the Nyquist contour is a key step in applying PoA for testing stability
- O Nyquist Plot: The F(s)-plot generated by evaluating F(s) as s is varied in a particular direction (CW) along the Nyquist contour.



 We'll learn soon how to sketch the Nyquist plot for a given transfer function

CL stability check \Rightarrow is there any zero of F(s) inside the Nyquist contour?

$$F(s) = 1 + L(s)$$
$$= 1 + KG(s)$$

o If there are N_Z zeros of F(s) and N_P poles of F(s) inside the Nyquist contour, then mapping of the contour in clockwise (CW) direction results in CW encirclement of the origin N_{CW} times where

$$N_{CW} = N_Z - N_P$$

- \circ We want to find the value of N_Z
- We can determine N_{CW} from the Nyquist plot of F(s)
- \circ What is N_P ?

What is N_P ?

$$L(s) = KG(s) = K\frac{N_L(s)}{D_L(s)}$$

O If $s=s_1$ is an open loop pole then, $D_L(s_1)=0$

$$F(s) = 1 + K \frac{N_L(s)}{D_L(s)} = \frac{D_L(s) + KN_L(s)}{D_L(s)}$$

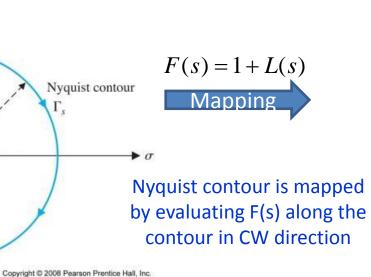
- $O \quad \text{If } D_L(s_1) = 0 \text{ then } s = s_1 \text{ is a pole of } F(s)$
 - \circ A pole of F(s) is also a pole of L(s), i.e., open loop pole
- As L(s) is already known, we know how many of its poles are inside the Nyquist contour \Rightarrow we know the value of N_P
 - o If OL is stable, no pole of L(s) is in RHP, i.e., $N_P=0$
 - \circ If OL is unstable, N_P is the number of unstable poles of L(s)

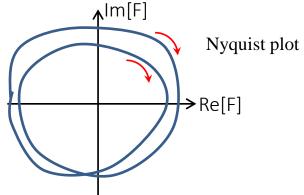
$$L(s) = G_c G_p H$$

$$= KG(s)$$

$$\int_{j\omega}^{j\omega}$$
Nyquist contour

$$G_{CL}(s) = \frac{L(s)}{1 + L(s)} = \frac{L(s)}{F(s)}$$





 Count number of CW encirclement (N_{CW}) of origin by the Nyquist plot

$$N_{CW} = N_Z - N_P$$

- \circ Count N_{CW} from the Nyquist plot
- Get N_P from the open loop transfer function L(s)
- \circ N_Z is the number of unstable zero of F(s), *i.e.* unstable pole of $G_{CL}(s)$
 - For CL to be stable, N_Z must be 0

Can we use L(s) to Check Stability?

$$F(s) = 1 + L(s) \implies L(s) = F(s) - 1$$

$$F(s_1) = a + jb$$
 $L(s_1) = F(s_1) - 1$
= $(a-1) + jb$

 \circ Example 3b-3: Consider the following functions evaluated at $s_1=2+j1$

$$F(s) = \frac{s+1}{s+5}$$

$$F(s_1) = \frac{2+j1+1}{2+j1+5} = \frac{3+j1}{7+j1}$$

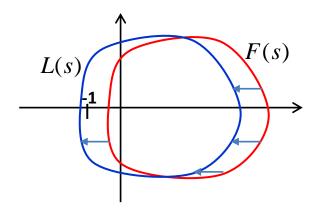
$$L(s_1) = F(s_1) - 1$$

$$= 0.44+j0.08-1$$

$$= -0.56+j0.08$$

$$F(s_1) = \frac{22+j4}{50} = 0.44+j0.08$$

 \circ Plot of $L(s) \Rightarrow \text{plot of } F(s) \text{ shifted to left by 1}$



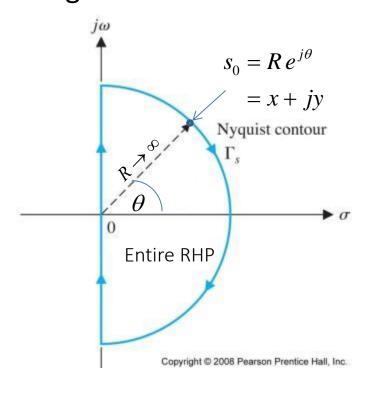
If the F(s) encircles the origin, L(s) will encircle the point (-1,0) or (-1+j0)

Stability check:

- Sketch the Nyquist plot of L(s) and find N_{CW} , the number of clockwise encirclement of the point (-1,0)
- \circ From the knowledge of OL, find the value of N_P
- \circ Find number of unstable CL poles (N_z) by solving

$$N_{CW} = N_Z - N_P$$

 The Nyquist plot of L(s) is the mapping of the Nyquist Contour using the transfer function L(s)



Segment by Segment Mapping

○ Segment 1: $s = j\omega$, $-R \le \omega \le R$ $R \to \infty$

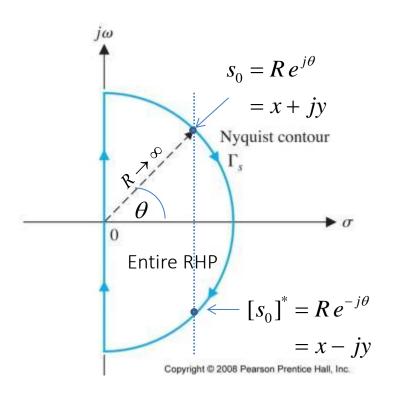
$$L(s)\big|_{seg1} = L(j\omega), \quad -R \le \omega \le R$$
 $R \to \infty$

Segment 2: $s = R\cos\theta + jR\sin\theta$ $= Re^{j\theta}$ $R \to \infty, \theta : +90^{\circ} \to 0^{\circ} \to -90^{\circ}$

$$L(s)|_{seg 2} = L(Re^{j\theta}),$$

 $R \to \infty, \theta : +90^{\circ} \to 0^{\circ} \to -90^{\circ}$

Symmetry of the Nyquist Contour

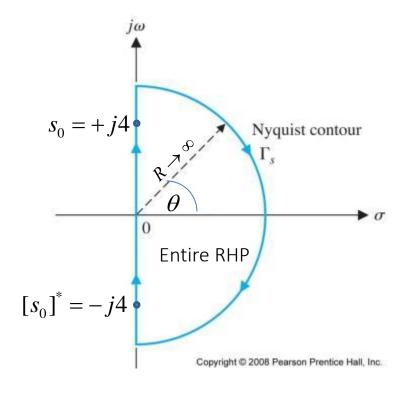


o Then,

$$L([s_0]^*) = [L(s_0)]^*$$
$$= a - jb$$

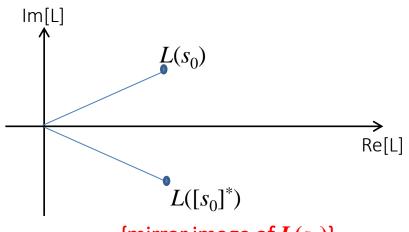
- We can map the upper half of the Nyquist contour, i.e., find
 $L(s_0)$
 - \circ Then $L([s_0]^*)$ is the mirror image of the point $L(s_0)$

Example 3b-4: Evaluate L(s) for $s_0 = +j4$ and $[s_0]^* = -j4$ when $L(s) = \frac{s+2}{s+5}$



$$L(s_0) = \frac{2+j4}{5+j4} = \frac{\sqrt{20}\angle 63.4^{\circ}}{\sqrt{41}\angle 38.7^{\circ}} = 0.7\angle 24.7^{\circ}$$

$$L([s_0]^*) = \frac{2 - j4}{5 - j4} = \frac{\sqrt{20} \angle - 63.4^{\circ}}{\sqrt{41} \angle - 38.7^{\circ}} = 0.7 \angle - 24.7^{\circ}$$



{mirror image of $L(s_0)$ }

Complex variable s along the upper half of the \mathcal{D} -contour

1) Along the +j ω axis: $s = j\omega$, $0 \le \omega \le R$

$$s = j\omega, \quad 0 \le \omega \le R$$

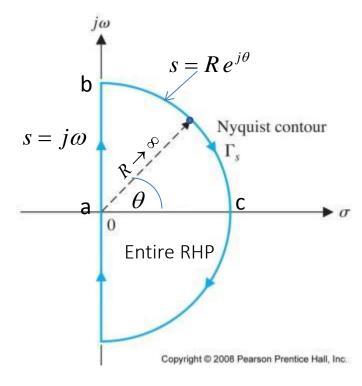
$$R \to \infty$$

[Going upward from point a to **b** in the figure below]

2) Along the top half of the semicircle: $s = R e^{j\theta}$

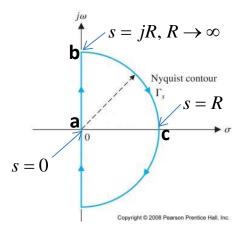
[Going CW from point **b** to **c** in the figure below]

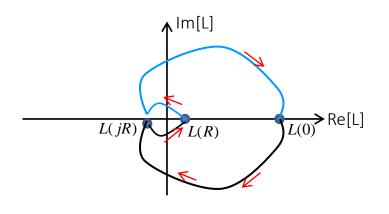
$$R \rightarrow \infty$$
, $\theta : +90^{\circ} \rightarrow 0^{\circ}$



Sketching the Nyquist Plot: L(s) with no Integrator

$$L(s) = K \frac{(s+b_1)(s+b_2)(s^2+c_1s+d_1)....}{(s+a_1)(s+a_2)(s^2+p_1s+q_1)....}$$





1) Map the upper half of the Nyquist contour

- a) Map the points 'a', 'b', and 'c'
 - Determine the points L(0), L(jR) where $R \rightarrow \infty$, and L(R)
- b) Connect L(0) to L(jR)
 - How is $L(j\omega)$ changed as ω is varied from 0 to R
- c) Connect L(jR) to L(R)
 - How L(s) is changed as s is varied along the arc from 'b' to 'c'
- 2) Complete the Nyquist plot by adding the mirror image of the plot obtained in step 1

Example 3b-5: Map the points 'a', 'b' and 'c' of the Nyquist contour for the transfer function (s+10)

$$L(s) = \frac{(s+10)}{(s+1)(s+100)}$$

o Answer:

'a'
$$s = 0$$
, $L(0) = \frac{(0+10)}{(0+1)(0+100)} = 0.1$

$$s = R,$$

$$L(R) = \frac{(R+10)}{(R+1)(R+100)}$$

$$= \frac{R+10}{R^2+101R+100}$$

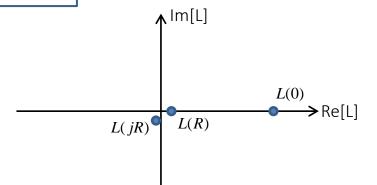
$$as \quad R \to \infty, \quad L(R) \cong \frac{1}{R}$$

$$s = jR,$$

$$L(jR) = \frac{(jR+10)}{(jR+1)(jR+100)}$$

$$= \frac{\sqrt{R^2+100}}{\sqrt{R^2+1}\sqrt{R^2+10000}} \angle \left(\tan^{-1}\frac{R}{10} - \tan^{-1}R - \tan^{-1}\frac{R}{100}\right)$$

$$as \quad R \to \infty, \quad |L(jR)| \cong \frac{1}{R}, \quad \angle L(jR) = -90^{\circ}$$



How to connect L(0) to L(jR) and L(jR) to L(R)?

Connecting L(0) to L(jR), $R \rightarrow \infty$

For this section,

$$s = j\omega$$
, $0 \le \omega \le R$

$$L(s) = K \frac{(s+b_1)(s+b_2)(s^2+c_1s+d_1)....}{(s+a_1)(s+a_2)(s^2+p_1s+q_1)....}$$

$$L(j\omega) = K \frac{(j\omega + b_1)(j\omega + b_2)((j\omega)^2 + jc_1\omega + d_1)...}{(j\omega + a_1)(j\omega + a_2)((j\omega)^2 + jp_1\omega + q_1)...}, \quad 0 \le \omega \le R, \quad R \to \infty$$

- \circ There are different ways to find the variations in $L(j\omega)$
 - 1) Using trigonometric expression of the argument
 - 2) Finding points of intersections with the axes
 - 3) Sketching the Bode (phase) plot

1) Using Trigonometric Expression for $\angle L(j\omega)$

○ *Example* 3b-6: For the following transfer function, determine how ∠L is changed as ω is varied from 0 to R where R→∞

$$L(s) = \frac{K}{(s+2)(s+10)}$$

Answer:

$$L(j\omega) = \frac{K}{(j\omega+2)(j\omega+10)}$$

$$L(0) = \frac{K}{(0+2)(0+10)} = \frac{K}{20}$$

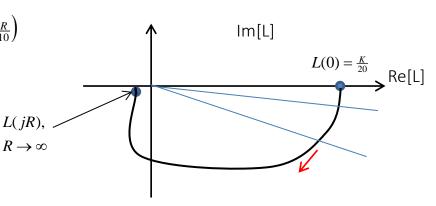
$$L(jR) = \frac{K}{(jR+2)(jR+10)}$$

$$= \frac{K}{\sqrt{R^2 + 100}\sqrt{R^2 + 4}} \angle \left(-\tan^{-1}\frac{R}{2} - \tan^{-1}\frac{R}{10}\right)$$

$$\stackrel{\cong}{=} \frac{K}{R^2} \angle -180^{\circ}$$

$$\angle L = -\tan^{-1}\frac{\omega}{2} - \tan^{-1}\frac{\omega}{10}$$

- 1. $\angle L$ is negative for all $\omega > 0$
- 2. $\angle L \rightarrow (-180^{\circ})$ as $\omega \rightarrow \infty$
- 3. Plot must be in the 4th and the 3rd quadrant



2) Finding points of intersections with the axes

Intersection with real-axis:

$$Im[L(j\omega)] = 0$$

$$\angle L(j\omega) = 0^{\circ} \text{ or } \pm 180^{\circ}$$

Intersection with imaginary-axis:

$$Re[L(j\omega)] = 0$$

$$\angle L(j\omega) = \pm 90^{\circ}$$

○ Example 3b-7: For the following transfer function, determine how \angle L is changed as ω is varied from 0 to R where R→∞

$$L(s) = \frac{K}{(s+2)(s+10)}$$

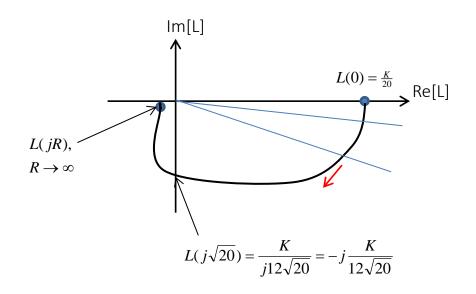
O Answer:

$$L(j\omega) = \frac{K}{(j\omega + 2)(j\omega + 10)}$$
$$= \frac{K}{(20 - \omega^2) + j12\omega}$$

Im[L] = 0 when ω =0. This point is effectively the dc-gain, L(j0)

$$Re[L] = 0$$
 when,

$$(20 - \omega^2) = 0 \implies \omega = \sqrt{20}$$



Example 3b-8: For the following transfer function, find points of intersection of the frequency response curve with the real-axis and the imaginary-axis

$$L(s) = \frac{K}{(s+2)(s^2+2s+5)}$$

o Answer:

$$L(s) = \frac{K}{(s+2)(s^2+2s+5)} = \frac{K}{s^3+4s^2+9s+10}$$

$$L(j\omega) = \frac{K}{-j\omega^{3} - 4\omega^{2} + j9\omega + 10} = \frac{K}{(10 - 4\omega^{2}) + j\omega(9 - \omega^{2})}$$

The curve intersects with real-axis at two points

$$\omega = 0 \implies L(j0) = \frac{K}{10}, \qquad \omega = 3 \implies L(j3) = -\frac{K}{26}$$

And it intersects with imaginary-axis at one point,

$$\omega = \frac{\sqrt{10}}{2} \implies L(j\frac{\sqrt{10}}{2}) = \frac{K}{j\frac{\sqrt{10}}{2}(9 - \frac{10}{4})} = -j\frac{4K}{13\sqrt{10}}$$

 Example 3b-9: For the following transfer function, find points of intersection of the frequency response curve with real-axis and imaginary-axis

$$L(s) = \frac{K(s+2)}{(s^2 + 2s + 5)}$$

Answer:

$$L(j\omega) = \frac{K(j\omega+2)}{-\omega^2 + j2\omega+5} = \frac{K(j\omega+2)}{(5-\omega^2) + j2\omega}$$

[multiply both numerator and denominator by the conjugate of the denominator]

$$L(j\omega) = \frac{K(j\omega+2)}{(5-\omega^2)+j2\omega} \times \frac{(5-\omega^2)-j2\omega}{(5-\omega^2)-j2\omega}$$

$$L(j\omega) = K \frac{10 + j\omega(1 - \omega^2)}{(5 - \omega^2)^2 + 4\omega^2}$$

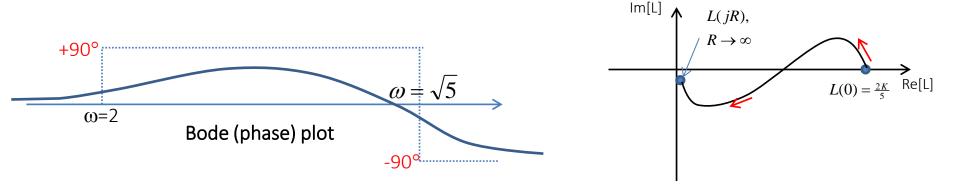
The imaginary part is zero at two frequencies,

$$\omega = 0 \implies L(j0) = \frac{2K}{5}, \qquad \omega = 1 \implies L(j1) = +\frac{K}{2}$$

○ The real part is not zero for any $\infty \ge \omega \ge 0$.

3) Using Bode (Phase) Plot

- O Hand-sketch the Bode (phase) plot of L(jω) to find how \angle L(jω) changes as ω is varied from 0 to ∞
- Example 3b-10: For the following transfer function, find the trend in ∠L(jω) as ω is varied from 0 to ∞ $L(s) = \frac{K(s+2)}{(s^2+2s+5)}$
 - O Answer: The corner frequency of the zero is 2 and natural frequency of the complex poles is $\omega_n = \sqrt{5}$



Phase of the transfer function is bounded between +90° and -90°. $L(j\omega)$ -plot must be on the right side of the $Im[L(j\omega)]$ axis.

 Keeping the same example, let's verify the result using the method of finding the points of inter-section

O Example 3b-11:
$$L(s) = \frac{K(s+2)}{(s^2+2s+5)}$$

Answer:

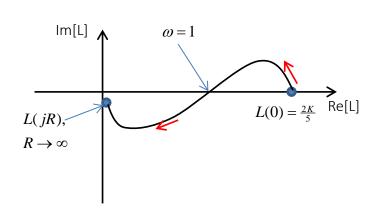
$$L(j\omega) = K \frac{2 + j\omega}{(5 - \omega^2) + j2\omega}$$

$$L(j\omega) = K \frac{2 + j\omega}{(5 - \omega^2) + j2\omega} \times \frac{(5 - \omega^2) - j2\omega}{(5 - \omega^2) - j2\omega}$$

$$L(j\omega) = K \frac{10 + j\omega(1 - \omega^2)}{(5 - \omega^2)^2 + 4\omega^2},$$

$$\therefore (a + jb)(a - jb) = a^2 + b^2$$

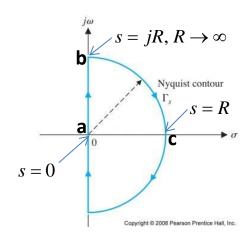
Real part of L is >0 for all ω Imaginary part is zero for ω =0 and ω =1 Imaginary part is positive for ω <1 and negative for ω >1



Connecting L(jR) to L(R), $R \rightarrow \infty$

For this segment (upper half of the semicircle),

$$s = Re^{j\theta}, R \to \infty, \theta: 90^{\circ} \to 0^{\circ}$$



○ Consider L(s) having m poles and n zeros with $m \ge n$

$$L(s) = K \frac{(s+b_1)(s+b_2)(s^2+c_1s+d_1)....}{(s+a_1)(s+a_2)(s^2+p_1s+q_1)....}$$

$$s = Re^{j\theta} \implies s^{2} = R^{2}e^{j2\theta}$$

$$L(s) = K \frac{(Re^{j\theta} + b_{1})(Re^{j\theta} + b_{2})(R^{2}e^{j2\theta} + c_{1}Re^{j\theta} + d_{1})....}{(Re^{j\theta} + a_{1})(Re^{j\theta} + a_{2})(R^{2}e^{j2\theta} + p_{1}Re^{j\theta} + q_{1})....}$$

<u>Linear factor</u>

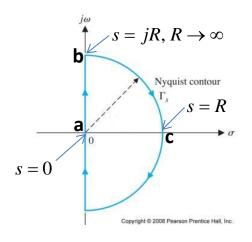
$$(Re^{j\theta} + b_1) = R(e^{j\theta} + b_1R^{-1})$$
$$= R(e^{j\theta}), \quad \therefore R^{-1} \approx 0$$

Quadratic factor

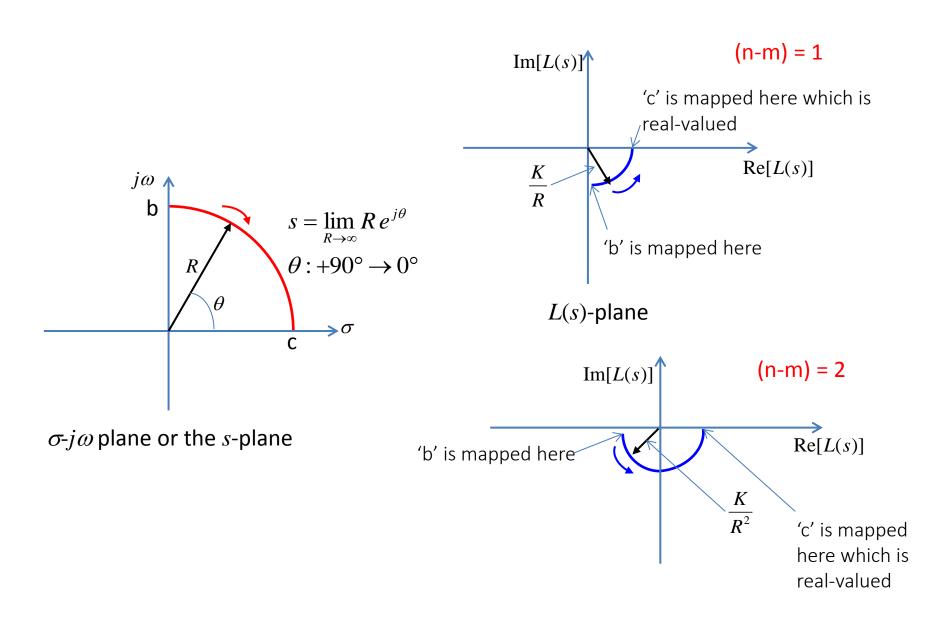
$$(R^{2}e^{j2\theta} + c_{1}Re^{j\theta} + d_{1}) = R^{2}(e^{j2\theta} + c_{1}R^{-1}e^{j\theta} + d_{1}R^{-2})$$

$$= R^{2}(e^{j2\theta}), \quad \therefore R^{-1} \approx 0$$

$$\begin{split} s &= Re^{j\theta}, \quad R \to \infty, \, \theta : 90^{\circ} \to 0^{\circ} \\ L(s) &= K \frac{(Re^{j\theta} + b_{1})...(R^{2}e^{j2\theta} + c_{1}Re^{j\theta} + d_{1})....}{(Re^{j\theta} + a_{1})...(R^{2}e^{j2\theta} + p_{1}Re^{j\theta} + q_{1})....} \\ &= K \frac{(Re^{j\theta})...(R^{2}e^{j2\theta})}{(Re^{j\theta})...(R^{2}e^{j2\theta})} \\ &= K \frac{R^{m}e^{jm\theta}}{R^{n}e^{jn\theta}} \end{split}$$



- Plot of L(s) is an arc of infinitesimally small radius
- \circ Argument of L(s) is changed through –(n-m) θ as θ is varied
 - As θ is varied from 90° to 0° clockwise while going from 'b' to 'c', ∠L(s) is sees a change of (n-m)×90° counterclockwise



Example 3b-12: Sketch the Nyquist plot for

$$L(s) = \frac{K}{(s+2)(s+10)}$$

Answer:

$$L(0) = \frac{K}{(0+2)(0+10)} = \frac{K}{20}$$

$$L(jR) = \frac{K}{(jR+2)(jR+10)}$$

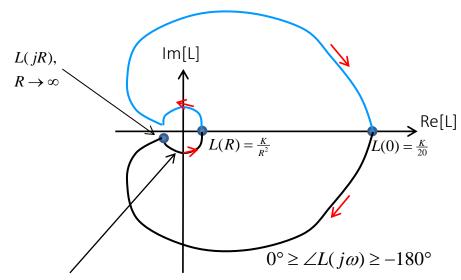
$$|L(jR)| \cong \frac{K}{R^2}, \quad \angle L(jR) \cong -180^{\circ}$$

$$L(R) = \frac{K}{(R+2)(R+10)} \cong \frac{K}{R^2}$$

$$L(j\omega) = \frac{K}{(j\omega + 2)(j\omega + 10)}$$

$$\angle L(j\omega) = \left(-\tan^{-1}\frac{\omega}{2} - \tan^{-1}\frac{\omega}{10}\right)$$

$$0^{\circ} \ge \angle L(j\omega) \ge -180^{\circ}$$



(n-m)=2 means CCW rotation through 180°

Example 3b-13: Sketch the Nyquist Plot of

$$L(s) = \frac{1}{s-3}$$

o Answer:

$$L(0) = \frac{1}{0-3} = -\frac{1}{3}$$

$$L(jR) = \frac{1}{jR-3} = \frac{1}{\sqrt{R^2 + 9} \angle (180^\circ - \tan^{-1} \frac{R}{3})}$$

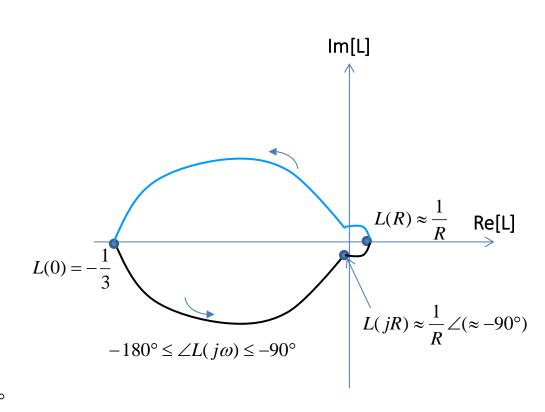
$$|L(jR)| \cong \frac{1}{R}, \quad \angle L(jR) = -90^\circ, \quad \because R \to \infty$$

$$L(R) = \frac{1}{R-3} \cong \frac{1}{R}$$

$$L(j\omega) = \frac{1}{j\omega - 3}, \quad 0 \le \omega \le R, \quad R \to \infty$$

$$\angle L(j\omega) = \frac{1}{\angle (180^\circ - \tan^{-1} \frac{\omega}{3})}$$

$$= \angle (-180^\circ + \tan^{-1} \frac{\omega}{3})$$
as $0^\circ \le \tan^{-1} \frac{\omega}{3} < 90^\circ, \quad -180^\circ \le \angle L(j\omega) \le -90^\circ$



If a pole of L(s) lies on the D-contour, for example, an integrator of L(s), then that point can't be mapped

$$L(s) = \frac{K}{(s)^{N}} \frac{(s+b_1)(s+b_2)(s^2+c_1s+d_1)...}{(s+a_1)(s+a_2)(s^2+p_1s+q_1)...}$$

$$L(j\omega) = \frac{K}{(j\omega)^{N}} \frac{(j\omega + b_1)(j\omega + b_2)((j\omega)^{2} + jc_1\varepsilon + d_1)...}{(j\omega + a_1)(j\omega + a_2)((j\omega)^{2} + jp_1\varepsilon + q_1)...}, \quad 0 \le \omega \le R, \quad R \to \infty$$

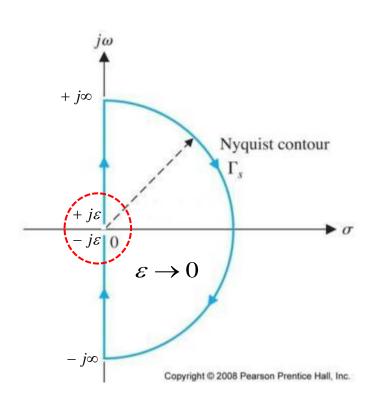
 \circ While mapping the j ω -axis, we can't evaluate L(j0),

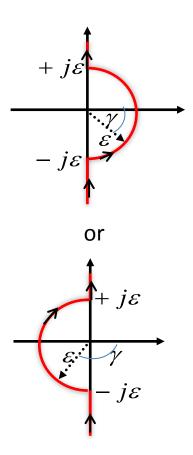
$$|L(j0)| = \infty$$
, $\angle L(j0) = ?$

o Instead of finding L(j0), we find the point for infinitesimally small value of ω

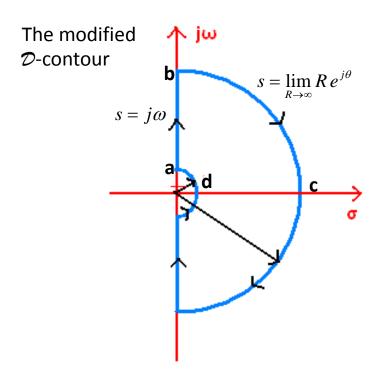
$$L(j\varepsilon)$$
 where $\varepsilon \approx 0$

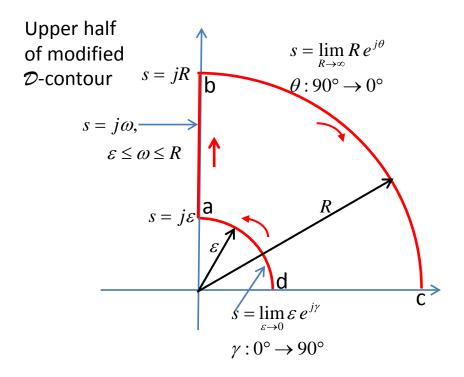
The Nyquist Contour is modified to exclude the point of singularity





 Modified contour is same as the D-contour except for the small semicircle around the pole



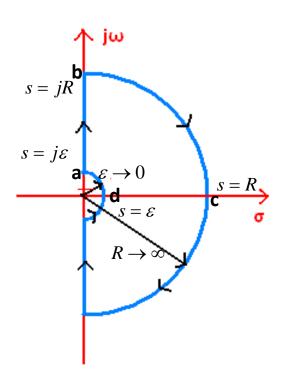


- \circ The modified \mathcal{D} -contour is also symmetric about the real axis
 - We consider only the upper half

$$L(s) = \frac{K}{(s)^{N}} \frac{(s+b_1)(s+b_2)(s^2+c_1s+d_1)...}{(s+a_1)(s+a_2)(s^2+p_1s+q_1)...}$$

1) Map the upper half of the Nyquist contour

- a) Map the points 'd', 'a', 'b', and 'c'
 - Determine the points $L(\varepsilon)$, $L(j\varepsilon)$, L(j)where $R \rightarrow \infty$, and L(R)
- b) Connect $L(\varepsilon)$ to $L(j\varepsilon)$
 - How is L(s) changed as s is varied alother the arc from 'd' to 'a'
- c) Connect $L(j\varepsilon)$ to L(jR)
- d) Connect L(jR) to L(R)
 - Steps c and d are quite similar to wh was done for L(s) without integrator
- 2) Complete the Nyquist plot by adding the milimage of the plot obtained in step 1



Mapping of the points 'd' $[L(\varepsilon)]$

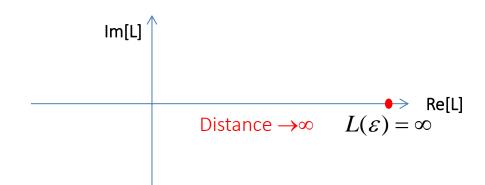
$$L(s) = \frac{K}{(s)^{N}} \frac{(s+b_1)...(s^2 + c_1s + d_1)...}{(s+a_1)...(s^2 + p_1s + q_1)...}$$

$$L(\varepsilon) = \frac{K}{(\varepsilon)^{N}} \frac{(\varepsilon+b_1)...(\varepsilon^2 + c_1\varepsilon + d_1)...}{(\varepsilon+a_1)...(\varepsilon^2 + p_1\varepsilon + q_1)...}$$
 [real-valued]

As $\varepsilon \to 0$,

$$L(\varepsilon) = \frac{K}{(\varepsilon)^{N}} \frac{(b_1)...(d_1)...}{(a_1)...(q_1)...} \to \infty$$

The point $L(\varepsilon)$ lies on the real-axis of the L(s)plane and it is at infinite distance from the
origin



Mapping of the points 'a' $[L(j\varepsilon)]$

$$L(s) = \frac{K}{(s)^{N}} \frac{(s+b_1)...(s^2+c_1s+d_1)...}{(s+a_1)...(s^2+p_1s+q_1)...}$$

$$\Rightarrow$$

$$L(s) = \frac{K}{(s)^{N}} \frac{(s+b_{1})...(s^{2}+c_{1}s+d_{1})...}{(s+a_{1})...(s^{2}+p_{1}s+q_{1})...} \qquad \qquad \Box \qquad L(j\varepsilon) = \frac{K}{(j\varepsilon)^{N}} \frac{(j\varepsilon+b_{1})...(-\varepsilon^{2}+jc_{1}\varepsilon+d_{1})...}{(j\varepsilon+a_{1})...(-\varepsilon^{2}+jp_{1}\varepsilon+q_{1})...}$$

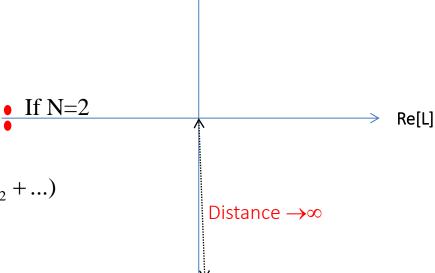
$$L(j\varepsilon)\big|_{\varepsilon\to 0} = \frac{K}{(\varepsilon\angle 90^\circ)^N} \frac{(r_{x1}\angle \delta_{x1})(r_{x2}\angle \delta_{x2})...}{(r_{y1}\angle \delta_{y1})(r_{y2}\angle \delta_{y2})...}$$

 $[\angle \delta_{x1}, \angle \delta_{x2}, \text{ etc. are}]$ infinitesimally small angle]

$$|L(j\varepsilon)| = \frac{K}{(\varepsilon)^N} \frac{(r_{x1})(r_{x2})...}{(r_{v1})(r_{v2})...} \cong \infty$$

$$\angle L(j\varepsilon) = -N \times 90^{\circ} + (\angle \delta_{x1} + \delta_{x2} + ...) - (\angle \delta_{y1} + \delta_{y2} + ...)$$

$$= -N \times 90^{\circ} \pm \delta$$



lm[L]

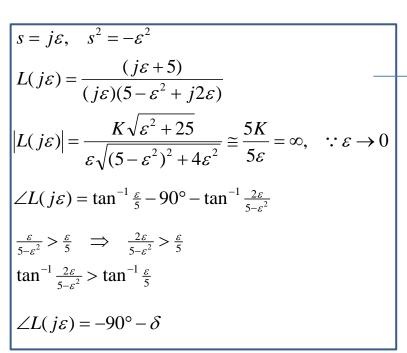
If N=1

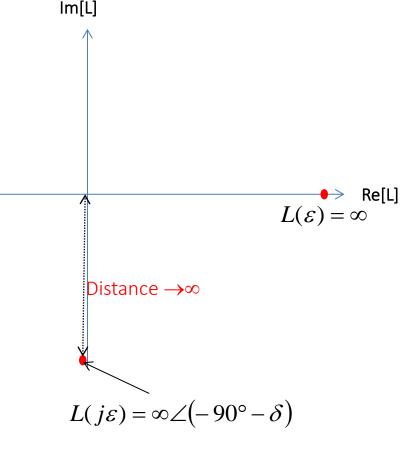
Example 3b-14: Map points $(s=\varepsilon)$ and $(s=j\varepsilon)$ for the transfer function

$$L(s) = \frac{K(s+5)}{s(s^2 + 2s + 5)}$$

Answer:

$$s = \varepsilon, \quad L(\varepsilon) = \frac{K}{\varepsilon} \frac{(\varepsilon + 5)}{(\varepsilon^2 + 2\varepsilon + 5)}$$
$$\varepsilon \to 0, \quad L(\varepsilon) = \frac{K}{\varepsilon} \to \infty$$





Connecting L(ε) to L($j\varepsilon$), $\varepsilon \rightarrow 0$

For this segment (upper half of the small semicircle),

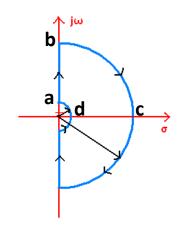
$$s = \varepsilon e^{j\gamma}, \quad \varepsilon \to 0, \gamma : 0^{\circ} \to 90^{\circ}$$

$$L(s) = \frac{K}{(s)^{N}} \frac{(s+b_1)...(s^2+c_1s+d_1)...}{(s+a_1)...(s^2+p_1s+q_1)...}$$

$$s = \varepsilon e^{j\gamma} \implies s^2 = \varepsilon^2 e^{j2\gamma}$$

$$L(s) = \frac{K}{(\varepsilon e^{j\gamma})^N} \frac{(\varepsilon e^{j\gamma} + b_1)...(\varepsilon^2 e^{j2\gamma} + c_1 \varepsilon e^{j2\gamma} + d_1)...}{(\varepsilon e^{j\gamma} + a_1)...(\varepsilon^2 e^{j2\gamma} + p_1 \varepsilon e^{j\gamma} + q_1)...}$$

$$L(s) = \frac{K}{(\varepsilon^N \angle N \times \gamma)} \frac{(b_1)...(d_1)...}{(a_1)...(q_1)...} = \infty \angle (-N \times \gamma)$$



Linear factor

$$(\varepsilon e^{j\gamma} + b_1) \cong b_1$$

Quadratic factor

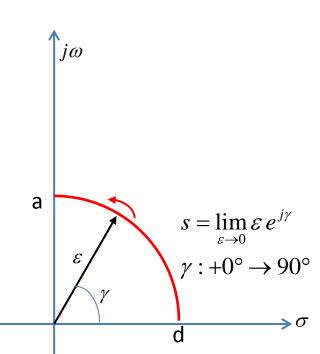
$$(\varepsilon^2 e^{j2\gamma} + c_1 \varepsilon e^{j\gamma} + d_1) \cong d_1$$

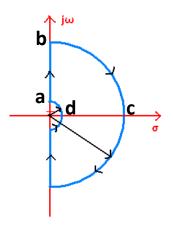
<u>Integrator</u>

$$\frac{K}{\left(\varepsilon e^{j\gamma}\right)^{N}} = \frac{K}{\varepsilon^{N} \angle N \times \gamma}$$

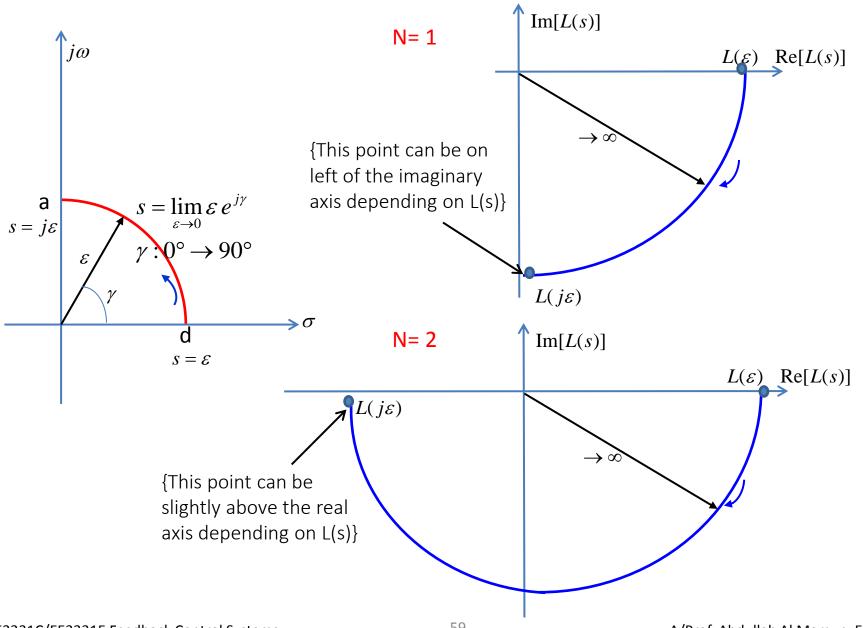
$$L(s) = \frac{K}{(\varepsilon^N \angle N \times \gamma)} \frac{(b_1)...(d_1)...}{(a_1)...(q_1)...} = \infty \angle (-N \times \gamma)$$

- Plot of L(s) is an arc of infinitely large radius
- \circ Argument of L(s) is changed through $-N\gamma$ as γ is varied





- \circ γ is varied from 0° to 90° CCW while going from 'd' to 'a'
 - ∠L(s) goes through a net clockwise change of N×90°



Example 3b-15: For the following transfer function, sketch L(s) when $s = \varepsilon e^{j\gamma}$

$$L(s) = \frac{K}{s^2} \frac{(s+2)}{(s+5)}$$

 $\varepsilon \approx 0, \gamma : +0^{\circ} \rightarrow 90^{\circ}$

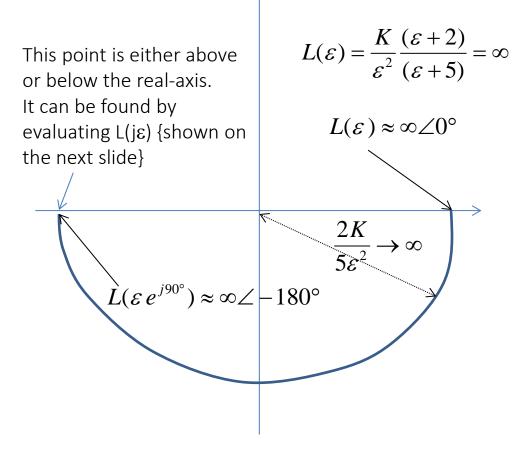
o Answer:

$$L(s) = \frac{K}{(\varepsilon e^{j\gamma})^2} \frac{(\varepsilon e^{j\gamma} + 2)}{(\varepsilon e^{j\gamma} + 5)}$$
$$\approx \frac{K}{(\varepsilon e^{j\gamma})^2} \frac{(2)}{(5)}$$

$$|L(s)| = \frac{2K}{5(\varepsilon)^2} \to \infty,$$

$$\angle L(s) \cong -2 \times \gamma$$

$$\gamma = 0^{\circ}$$
:
 $|L(s)| \to \infty, \quad \angle L(s) = 0^{\circ}$
 $\gamma = 90^{\circ}$:
 $|L(s)| \to \infty, \quad \angle L(s) \cong -180^{\circ}$



$$L(s) = \frac{K}{s^2} \frac{(s+2)}{(s+5)}$$

$$s = \varepsilon e^{j\gamma}$$

$$\varepsilon \approx 0, \gamma : +0^\circ \to 90^\circ$$

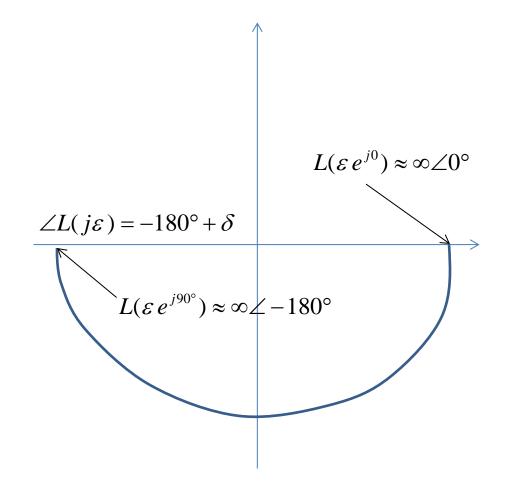
$$\gamma = 90^{\circ}: \quad s = j\varepsilon$$

$$L(s) = \frac{K}{(j\varepsilon)^{2}} \frac{(2+j\varepsilon)}{(5+j\varepsilon)}$$

$$\angle L(s) \cong -2 \times 90^{\circ} + \tan^{-1}\frac{\varepsilon}{2} - \tan^{-1}\frac{\varepsilon}{5}$$

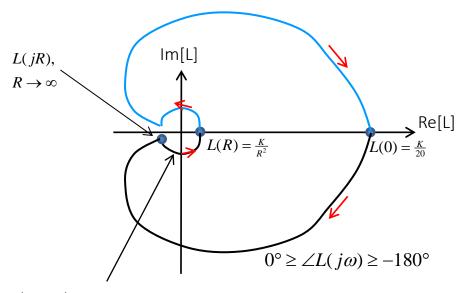
$$\tan^{-1}\frac{\varepsilon}{2} > \tan^{-1}\frac{\varepsilon}{5}, \quad for \ \forall \varepsilon$$

$$\angle L(j\varepsilon) = -180^{\circ} + \delta, \quad \delta > 0$$

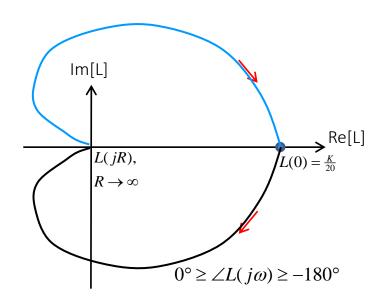


Sketching the Nyquist Plot: Mapping of $Re^{j\theta}$ Ignored

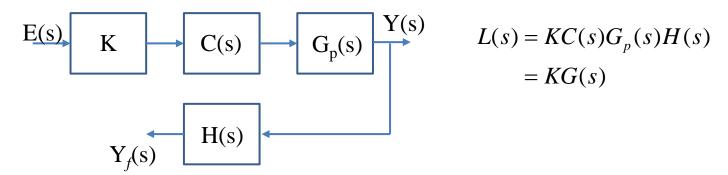
- When the big semicircle is mapped, it gives an arc of infinitesimally small radius $\frac{K}{R^{(n-m)}}$
 - This is too small compared to other parts of the Nyquist plot and hence is often drawn as a point
- O Example 3b-16: $L(s) = \frac{K}{(s+2)(s+10)}$







1. Sketch the Nyquist plot of the loop transfer function L(s) by following the Nyquist contour in CW direction



- 2. Count N_{CW} , the number of CW encirclement of the point (-1,0)
- 3. Determine N_P , the number of OL poles inside the Nyquist contour
- 4. Find N_Z from the equation $N_{CW} = N_Z N_P$
 - N_Z is the number of zeros of F(s) in RHP, i.e., the number of closed loop poles in RHP
 - For CL stability, N_Z must be 0

Example 3b-17: Check stability of the closed loop if the loop transfer function is

$$L(s) = \frac{100}{(s+1)(0.1s+1)}$$

o Answer:

$$L(0) = \frac{100}{(0+1)(0+1)} = 100$$

$$L(jR) = \frac{100}{(jR+1)(j0.1R+1)}$$

$$|L(jR)| = \frac{100}{\sqrt{R^2 + 1}\sqrt{0.01R^2 + 1}}$$

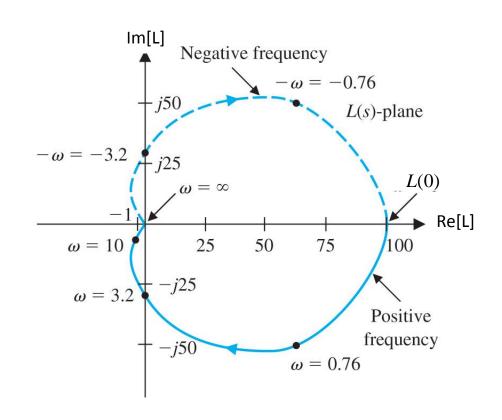
$$\approx 0, \quad \therefore R \to \infty$$

$$\angle L(jR) = -\tan^{-1} R - \tan^{-1}(0.1R)$$

$$\cong -90^{\circ} - 90^{\circ}, \quad \therefore R \to \infty$$

$$\cong -180^{\circ}$$

- o From the Nyquist plot, $N_{CW} = 0$
- \circ L(s) is open loop stable, i.e., $N_P = 0$



$$N_{CW} = N_Z - N_P \implies N_Z = 0$$

CL is stable

Example 3b-18: Check CL stability if

o Answer:

$$L(\varepsilon) = \frac{K}{\varepsilon(\tau\varepsilon + 1)} \to \infty$$

$$L(jR) = \frac{K}{(jR)(jR\tau + 1)}$$

$$\left| L(jR) \right| = \frac{100}{R\sqrt{\tau^2 R^2 + 1}} \cong 0$$

$$\angle L(jR) = -90^{\circ} - \tan^{-1}(\tau R)$$

$$\cong -180^{\circ}. \quad \because R \to \infty$$

$$L(s) = \frac{K}{s(\tau s + 1)}$$

$$L(j\varepsilon) = \frac{K}{(j\varepsilon)(j\varepsilon\tau + 1)}$$
$$|L(j\varepsilon)| \to \infty, \quad \because \varepsilon \to 0$$
$$\angle L(j\varepsilon) = -90^{\circ} - \tan^{-1}(\varepsilon\tau)$$
$$= -90^{\circ} - \delta,$$

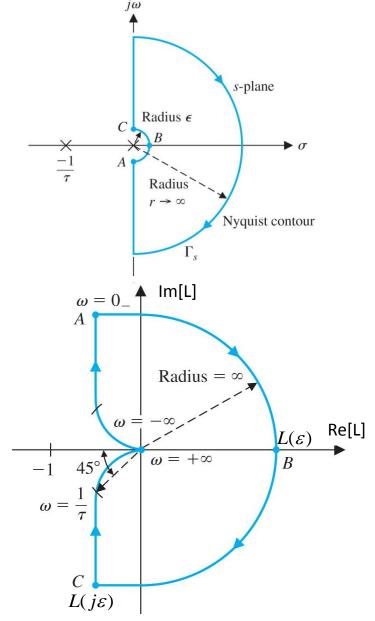
 $\delta \approx 0$, $:: \varepsilon \to \infty$

$$\circ$$
 From the Nyquist plot, N_{CW} = 0

○ L(s) has no pole inside Γ_s , i.e., $N_P = 0$

$$N_{\scriptscriptstyle CW} = N_{\scriptscriptstyle Z} - N_{\scriptscriptstyle P} \quad \Longrightarrow \quad N_{\scriptscriptstyle Z} = 0$$

CL is stable



Example 3b-19: For the following L(s), find the range of K such that CL is stable

Answer:

$$L(s) = \frac{K}{s(s+1)^2}$$

$$L(\varepsilon) = \frac{K}{\varepsilon(\tau_1 \varepsilon + 1)^2} \to \infty$$

$$L(j\omega) = \frac{K}{(j\omega)(j\omega+1)^2}$$

$$\angle L(j\omega) = -90^{\circ} - 2 \tan^{-1}(\omega)$$
$$-90^{\circ} \ge \angle L(j\omega) \ge -270^{\circ}$$

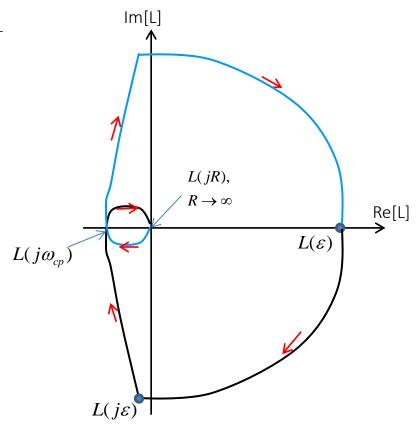
[3rd and 2nd quadrant]

$$|L(j\varepsilon)| \to \infty, \quad :: \varepsilon \to 0$$

$$\angle L(j\varepsilon) = -90^{\circ} - 2 \tan^{-1}(\varepsilon)$$
$$= -90^{\circ} - \delta,$$

$$|L(jR)| = \frac{K}{R(R^2 + 1)} \cong 0$$

$$\angle L(jR) = -90^{\circ} - 2 \tan^{-1}(R)$$
$$\cong -270^{\circ}, \quad \because R \to \infty$$



- \circ The value of $L(j\omega_{cp})$ determines whether (-1,0) is encircled or not
 - We need to find this point

$$L(j\omega) = \frac{K}{(j\omega)(j\omega+1)^2}$$

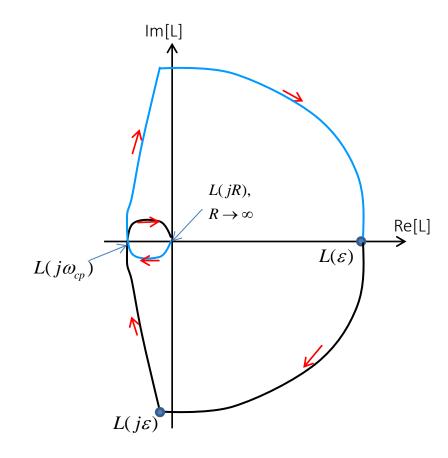
$$L(j\omega) = \frac{K}{j\omega(1-\omega^2+j2\omega)}$$
$$= \frac{K}{-2\omega^2+j\omega(1-\omega^2)}$$

For $L(j\omega_{\rm cp})$, imaginary part is equal to 0

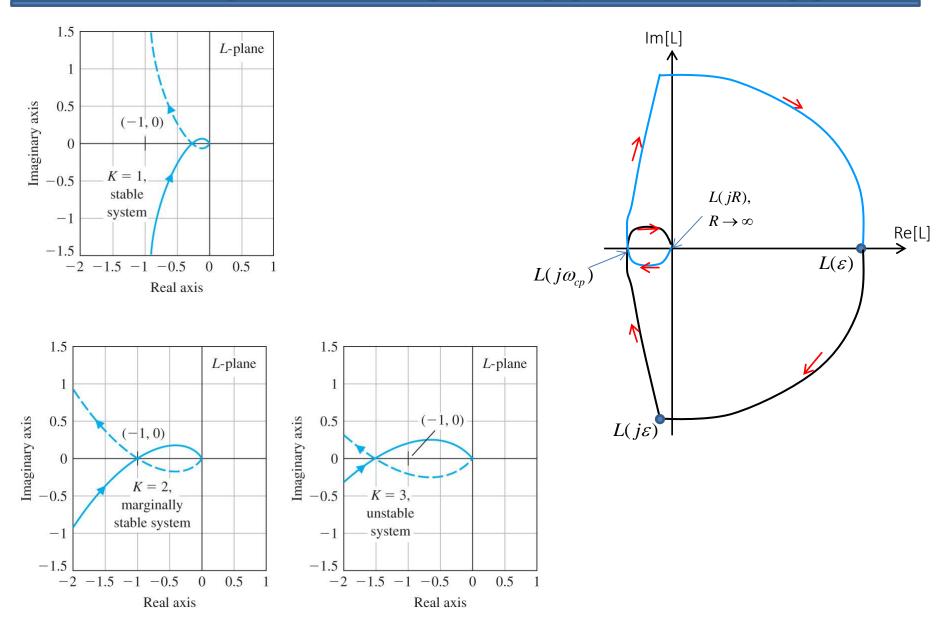
$$\omega_{cp} = 1$$

$$L(j\omega_{cp}) = \frac{K}{-2\omega_{cp}^2} = -\frac{K}{2}$$

- o If K<2, $N_{CW}=0$ and the CL is stable
- Otherwise, CL is unstable



 \circ The next slide shows the situations for three different values of K



[2nd quadrant]

Example 3b-20: Check CL stability if $L(s) = \frac{K}{s^2(\tau s + 1)}$

Answer:

$$L(\varepsilon) = \frac{K}{\varepsilon^{2}(\tau \varepsilon + 1)} \to \infty \qquad L(j\omega) = \frac{K}{(j\omega)^{2}(j\omega\tau + 1)}$$

$$\angle L(j\omega) = -180^{\circ} - \tan^{-1}(\tau\omega)$$

$$-180^{\circ} \ge \angle L(j\omega) \ge -270^{\circ}$$

$$|L(j\varepsilon)| \to \infty, \quad \because \varepsilon \to 0$$

$$\angle L(j\varepsilon) = -180^{\circ} - \tan^{-1}(\varepsilon\tau)$$

$$\cong -180^{\circ} - \delta$$

$$|L(jR)| = \frac{K}{R^{2}\sqrt{\tau^{2}R^{2} + 1}} \cong 0 \quad \because R \to \infty$$

$$\angle L(jR) = -180^{\circ} - \tan^{-1}(\tau R)$$

From the Nyquist plot, $N_{CW} = 2$

 $\approx -270^{\circ}$, $R \rightarrow \infty$

L(s) has no pole inside Γ_s , i.e., $N_P = 0$

$$N_{CW} = N_Z - N_P \quad \Rightarrow \quad N_Z = 2$$

s-plane 2 poles at s=0 Radius ϵ Radius $r \rightarrow \infty$ Nyquist contour $\Gamma_{\rm s}$ Im[L] L(s)-plane $L(j\varepsilon)$ $L(\varepsilon)$ $\omega = 0$ Re[L] Γ_L

CL is unstable with 2 RHP poles