

National University of Singapore
Department of Electrical & Computer Engineering

<h2 style="margin: 0;">EE3331C Feedback Control Systems</h2> <h3 style="margin: 0;">Mid-Term Quiz</h3>
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Instructions :

1. There are TWO (2) questions, carrying a total of TWENTY (20) marks. Answer BOTH questions.
2. A formula list is provided on Page 8.
3. Please show all working clearly.
4. Time allowed : 1 hour

Name : _____

Matriculation Number : _____

Q1	
Q2	
Total	

1. A closed-loop control system and its root locus plot are shown in Figures 1 and Figure 2 respectively.

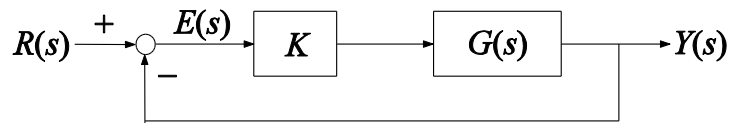


Figure 1: Feedback System

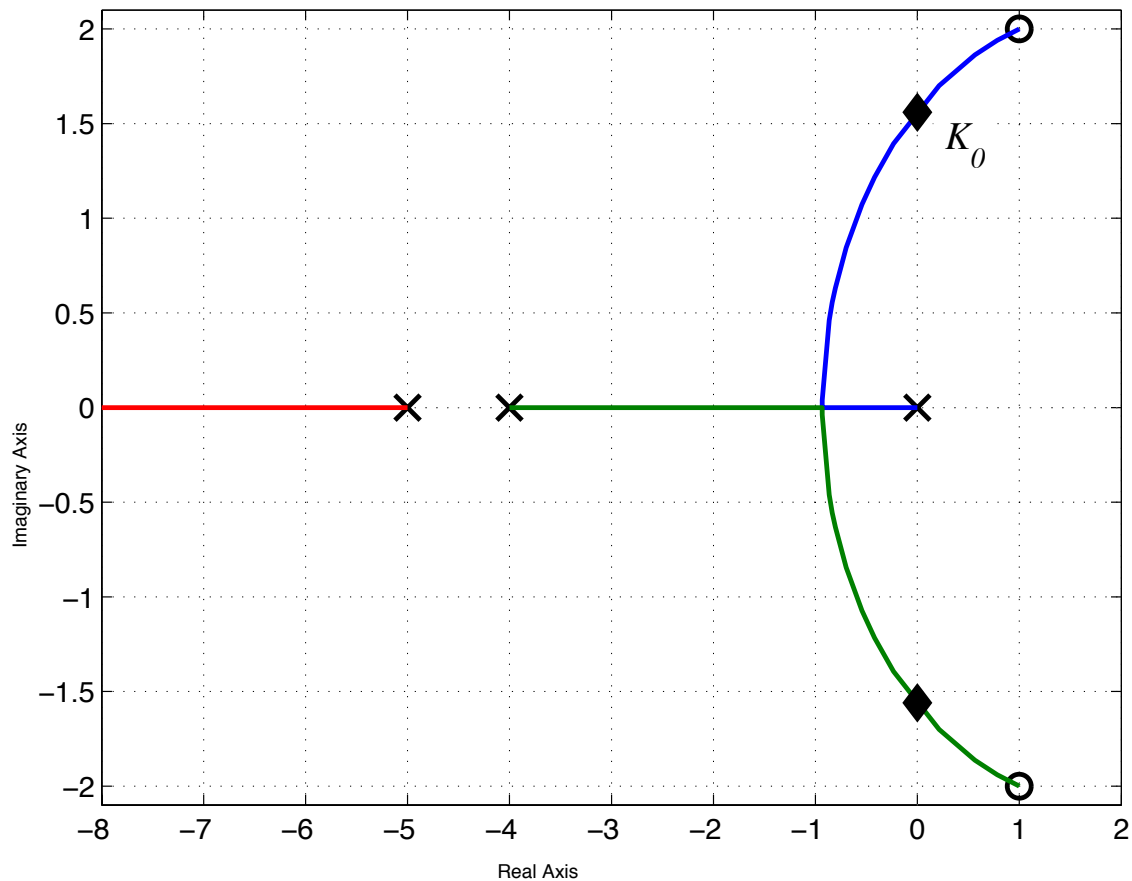
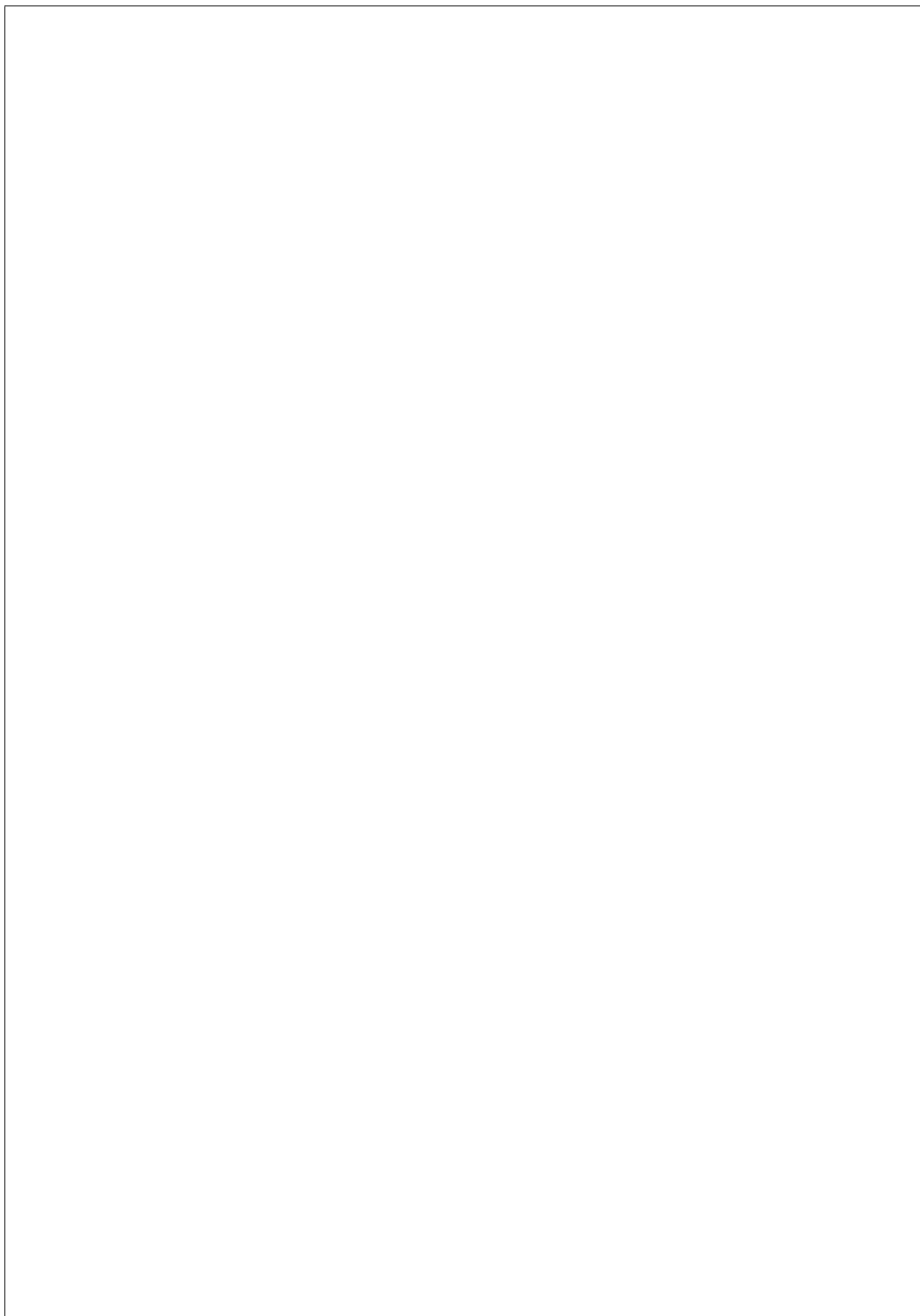
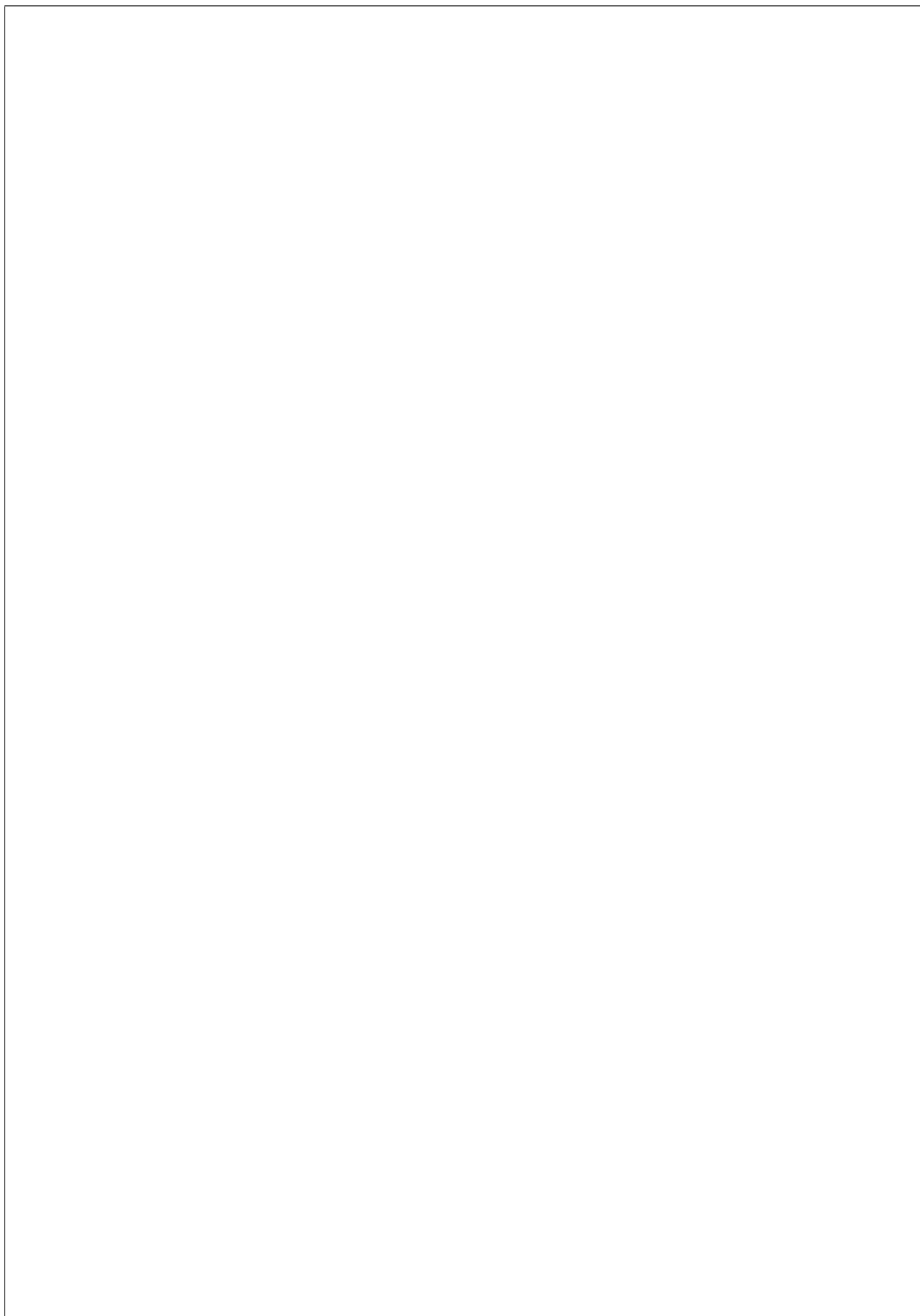


Figure 2: Root Locus Plot

- The transfer function of the plant is $G(s) = \frac{s^2 + as + b}{s^3 + cs^2 + ds}$. Find a , b , c and d .
- Find the value of K_0 in Figure 2.
- What is the steady-state error ($E(s) = R(s) - Y(s)$), when the reference signal, $r(t)$ is a unit ramp function, t . You may assume that $K < K_0$, i.e. the closed-loop system is stable.

(10 MARKS)





2. Figures 3 and 4 shows a series RLC circuit and its output voltage, $v_o(t)$.

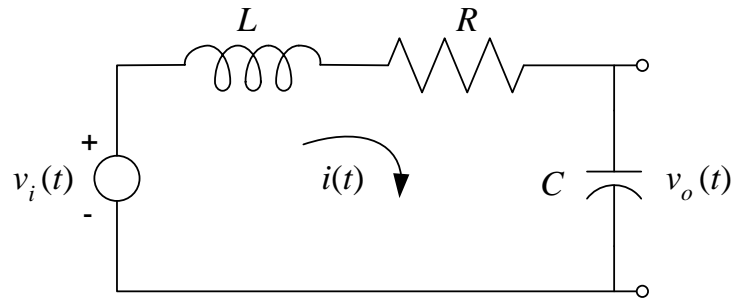


Figure 3: Series RLC circuit

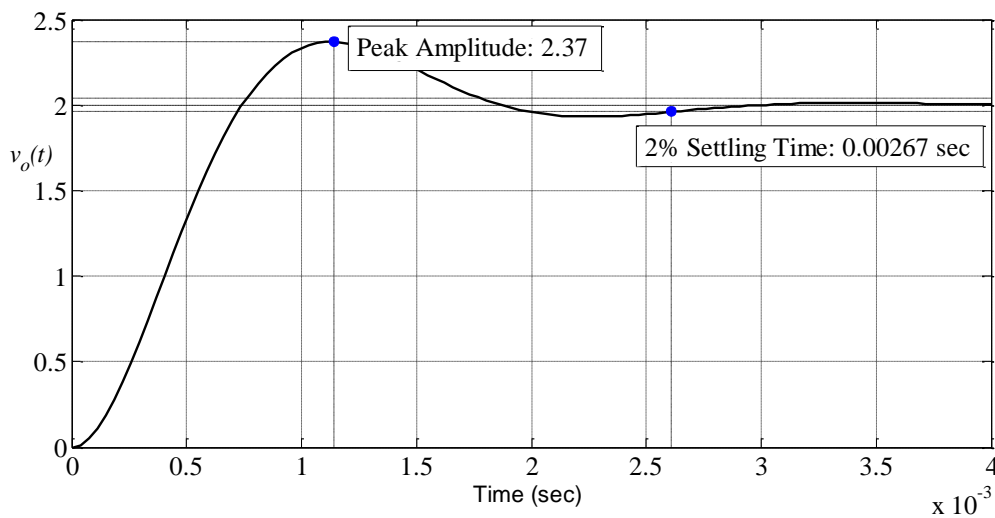


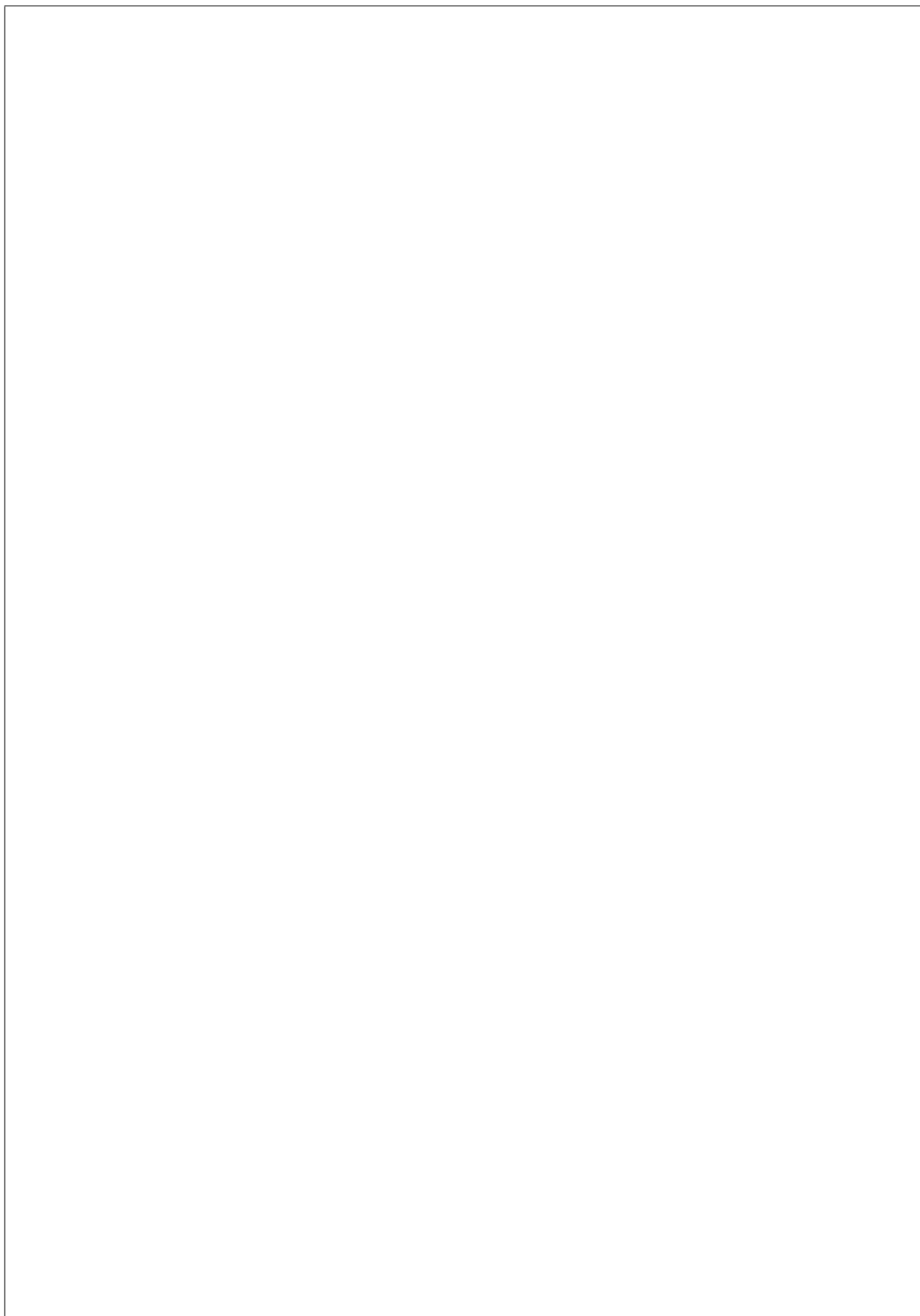
Figure 4: Output voltage of series RLC circuit

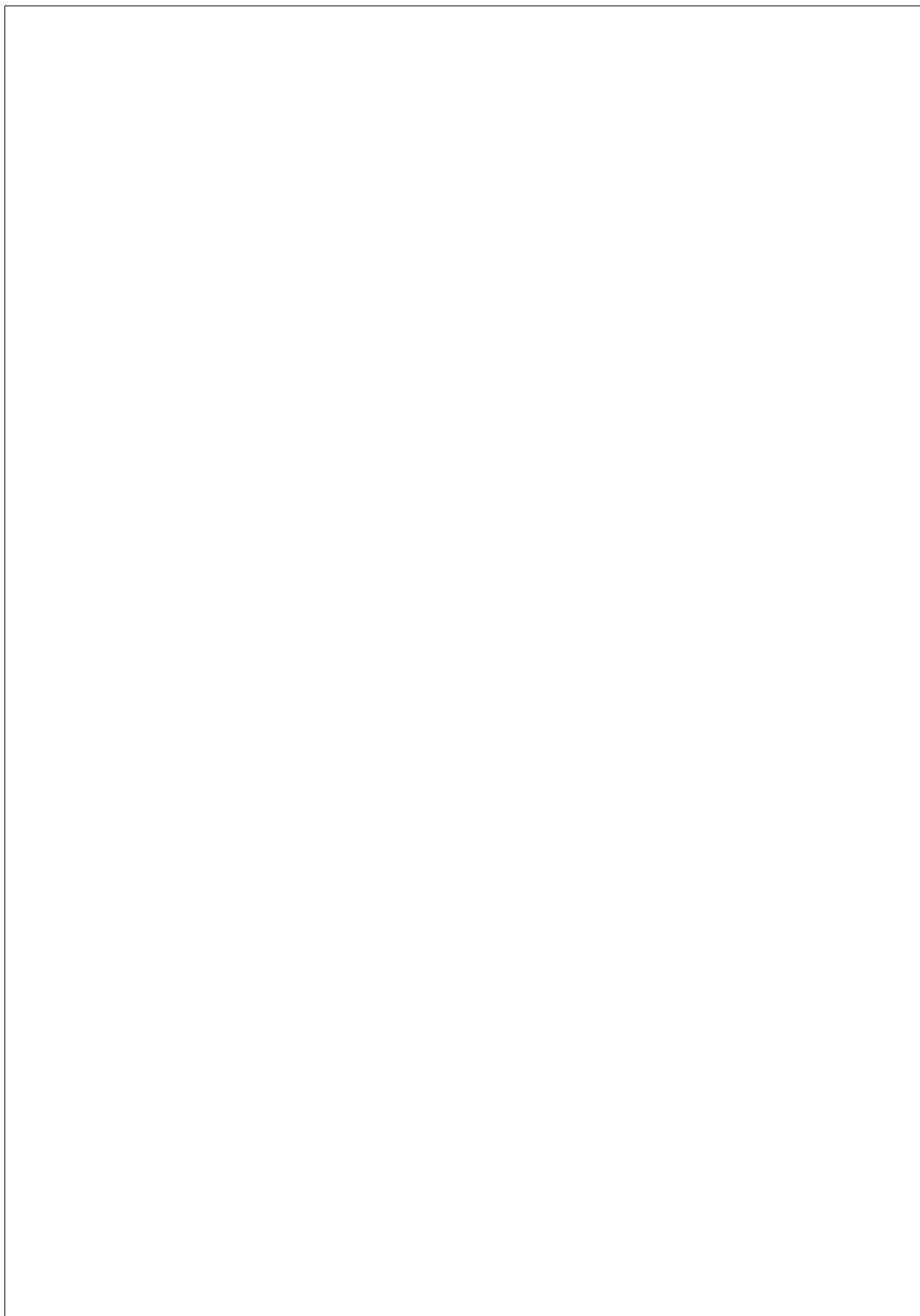
- (a) Derive the differential equation relating the input voltage, $v_i(t)$, and output voltage, $v_o(t)$. Assuming zero initial conditions, show that

$$H(s) = \frac{V_o(s)}{V_i(s)} = \frac{1}{LCs^2 + RCs + 1}$$

- (b) Figure 4 shows the output voltage, $v_o(t)$, of the series RLC circuit in part (a) when $v_i(t)$ is a step voltage of 2V. Estimate L and C given that $R = 3\Omega$.

(10 MARKS)

A large, empty rectangular box with a thin black border, occupying the central portion of the page. It is intended for the student to write their answers to the quiz questions.



SOME USEFUL LAPLACE TRANSFORM RULES

Transform of derivatives, $\mathcal{L}\left\{\frac{dy(t)}{dt}\right\}$	$sY(s) - y(0)$
Transform of integral, $\mathcal{L}\left\{\int_0^t y(\tau)d\tau\right\}$	$\frac{Y(s)}{s}$
Shift in time domain, $\mathcal{L}\{y(t-L)u(t-L)\}$	$Y(s)e^{-sL}$
Shift in s-domain, $\mathcal{L}\{y(t)e^{-at}\}$	$Y(s+a)$
Final Value Theorem	$\lim_{t \rightarrow \infty} y(t) = \lim_{s \rightarrow 0} sY(s)$

SOME USEFUL LAPLACE TRANSFORMS

Function, $f(t)$	Laplace Transform, $F(s)$	Function, $f(t)$	Laplace Transform, $F(s)$
delta function, $\delta(t)$	1	$\sin \omega t$	$\frac{\omega}{s^2 + \omega^2}$
unit step function, $u(t)$	$\frac{1}{s}$	$\cos \omega t$	$\frac{s}{s^2 + \omega^2}$
t	$\frac{1}{s^2}$	$1 - e^{-at}$	$\frac{a}{s(s+a)}$
ke^{-at}	$\frac{k}{s+a}$	$t - \frac{1}{a}(1 - e^{-at})$	$\frac{a}{s^2(s+a)}$

SOME DESIGN FORMULAE FOR UNDERDAMPED 2nd ORDER SYSTEM

Standard 2nd order system : $\frac{K\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$

Maximum overshoot, M_p	$M_p = Ke^{-\frac{\pi\zeta}{\sqrt{1-\zeta^2}}}$
Settling time (2%), t_s	$t_s = \frac{4}{\zeta\omega_n}$
Rise time, t_r	$t_r = \frac{1.8}{\omega_n}$
Peak time, t_p	$t_p = \frac{\pi}{\omega_n\sqrt{1-\zeta^2}}$

Q1.

(a). zeros: $s = 1 \pm j2$
 $(s-1+j2)(s-1-j2) = s^2 - 2s + 5$
 $\Rightarrow a = -2, b = 5$

poles: $s = 0, -4, -5$
 $\Rightarrow c = 9, d = 20$

(b) $K = K_0$,

poles: $-1 + GK = 0$
 $\Rightarrow 1 + \frac{K(s^2 - 2s + 5)}{s(s^2 + 9s + 20)} = 0$

$\Rightarrow s^3 + 9s^2 + 20s + Ks^2 - 2Ks + 5K = 0$

$s = j\omega, -j\omega^3 - (9\omega^2 + K\omega^2) + j(20 - 2K)\omega + 5K = 0$

real: $-(9+K)\omega^2 + 5K = 0$
 $\Rightarrow -(9+K)(20-2K) + 5K = 0$

imag: $-\omega^3 + (20-2K)\omega = 0$
 $\Rightarrow \omega^2 = 20-2K$
 $\Rightarrow 2K^2 - 2K - 180 + 5K = 0$
 $2K^2 + 3K - 180 = 0$
 $\Rightarrow K = 8.77, -10.27$

$K = \frac{-3 \pm \sqrt{9 + 4(2)(180)}}{4}$

(c).

$e_{ss} = \lim_{s \rightarrow 0} sE(s)$

$= \lim_{s \rightarrow 0} s \frac{1}{1+GK} R(s)$

$= \lim_{s \rightarrow 0} s \frac{1}{1 + \frac{K_1(s^2 - 2s + 5)}{s(s^2 + 9s + 20)}} \cdot \frac{1}{s^2}$

$= \lim_{s \rightarrow 0} s \frac{s}{s + \frac{K_1(5)}{20}} \cdot \frac{1}{s^2}$

$= \frac{20}{5K_1} = \frac{4}{K_1} \neq$

Q2. (a). KVL, $V_o(t) + L \frac{di(t)}{dt} + Ri(t) = v_i(t)$, $i(t) = C \frac{dv(t)}{dt}$

$$\Rightarrow LC \frac{d^2 v_o(t)}{dt^2} + RC \frac{dv_o(t)}{dt} + v_o(t) = v_i(t).$$

Take LT,

$$(LCs^2 + RCs + 1)V_o(s) = V_i(s)$$

$$\Rightarrow \frac{V_o(s)}{V_i(s)} = \frac{1}{LCs^2 + RCs + 1}$$

$$= \frac{1/LC}{s^2 + \frac{R}{L}s + \frac{1}{LC}}$$

(b). c.f. $s^2 + 2\zeta\omega_n s + \omega_n^2$

$$\Rightarrow \omega_n^2 = \frac{1}{LC}, \quad 2\zeta\omega_n = \frac{R}{L}, \quad R = 3\Omega$$

From the graph,

$$\% M_p = e^{-\pi\zeta/\sqrt{1-\zeta^2}} = \frac{0.37}{2}$$

$$\Rightarrow \zeta = \sqrt{\frac{(\ln(\frac{0.37}{2}))^2}{\pi^2 + (\ln(\frac{0.37}{2}))^2}} \approx 0.47$$

$$2\% f_s = \frac{4}{\zeta\omega_n} = 0.00267 \Rightarrow \omega_n = \frac{4}{(0.47)(0.00267)} = 3187.5$$

$$\Rightarrow \zeta\omega_n = \frac{4}{0.00267}$$

$$L = \frac{R}{2} \frac{0.00267}{4} = 1 \text{ mH. } *$$

$$C = \frac{1}{L\omega_n^2} = 100 \mu\text{F} *$$