

Numerical Algorithms for ODEs/DAEs (Transient Analysis)

Solving Differential Equation Systems

$$\frac{d}{dt}\vec{q}(\vec{x}(t)) + \vec{f}(\vec{x}(t)) + \vec{b}(t) = \vec{0}$$

- DAEs: many types of solutions useful
 - ✓ DC steady state: no time variations
 - transient: ckt. waveforms changing with time
 - periodic steady state: changes periodic w time
 - linear(ized): all sinusoidal waveforms: AC analysis
 - nonlinear steady state: shooting, harmonic balance
 - noise analysis: random/stochastic waveforms
 - sensitivity analysis: effects of changes in circuit parameters

Transient Analysis

$$\frac{d}{dt}\vec{q}(\vec{x}(t)) + \vec{f}(\vec{x}(t)) + \vec{b}(t) = \vec{0}$$

- **What**
 - inputs $b(t)$ changing with time
 - find waveforms of $x(t)$ as they change with time
- **Why**
 - most general analysis typically needed
 - sine wave, pulse, etc. inputs typical in many applications
- **How**
 - solve DAE using numerical methods
 - “discretize time”: replace d/dt term
 - convert DAE to nonlinear algebraic equation at each discrete time point
 - solve this using NR

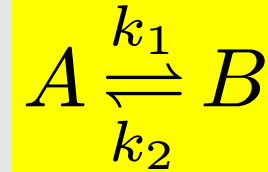
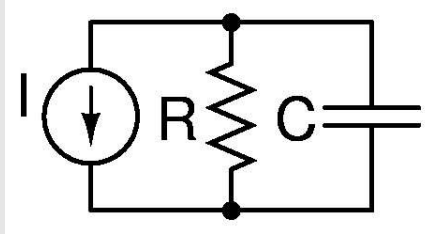
Solving DAEs: Preliminaries

- Given a DAE: does it have a solution?
 - Depends. Various conditions need to hold.
- Easier to analyze if DAEs are really ODEs
 - Ordinary Differential Equations: i.e., $\vec{q}(\vec{x}) \equiv \vec{x}$

$$\frac{d}{dt}\vec{x}(t) + \vec{f}(\vec{x}(t)) + \vec{b}(t) = \vec{0} \Rightarrow \frac{d}{dt}\vec{x}(t) = \vec{g}(\vec{x}, t)$$

- Existence/Uniqueness conditions well known for ODEs
 - $f(x)$ needs to be Lipschitz
 - device models must be smooth / bounded / “physically reasonable”
 - watch those if conditions, $1/x$, $\log(x)$, $\text{sqrt}(x)$, etc. terms!
- DAEs? Much more involved
 - in practice: modifications of ODE methods + heuristics

Analytical Exemplar (Model Problem)



$$C \frac{de}{dt} = -\frac{e}{R} - I(t)$$

$$\frac{d[A]}{dt} = -(k_1 + k_2)[A] + k_2$$

$$\dot{x} = \lambda x + b(t)$$

- Useful because
 - has analytical solution
 - vector linear systems reducible to this form
 - locally approximates nonlinear systems
- Prototype for
 - stability analysis of ODE solution methods

Existence and Uniqueness

- Does a solution exist? Examples:

- $\dot{x} = \lambda x + b(t)$

- yes: $x(t) = x(t_0)e^{\lambda(t-t_0)} + \int_0^t e^{\lambda(t-\tau)} b(\tau) d\tau$

- Solution is unique, given an initial condition

- $\dot{x} = -\frac{1}{2x}, \quad x(0) = x_0$

- $x(t) = \sqrt{x_0^2 - t}$: no solution for $t > x_0^2$

- $\dot{x} = \frac{3}{2}x^{\frac{1}{3}}$

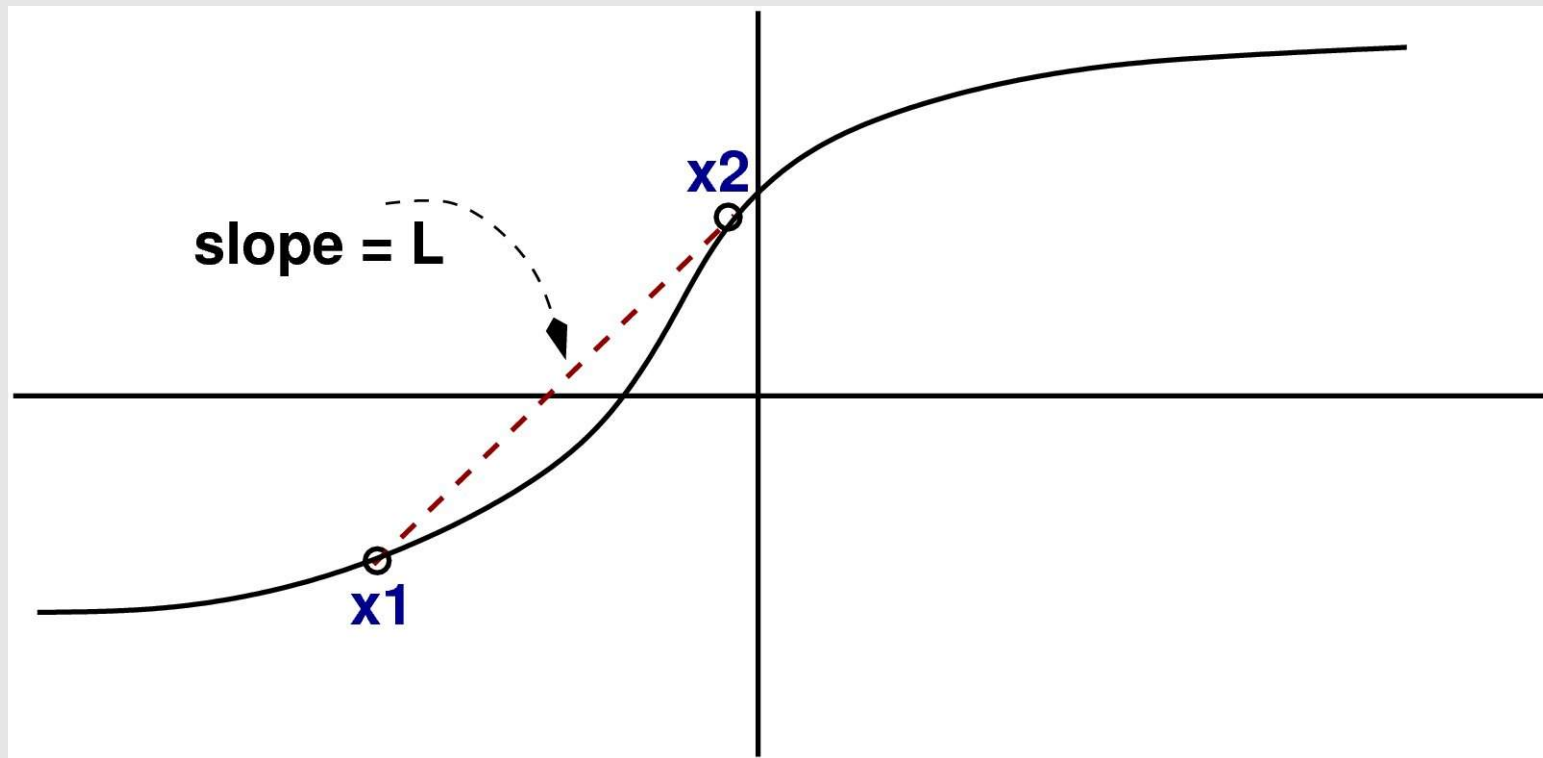
- $x(t) = \begin{cases} 0, & 0 \leq t \leq k \\ (t - k)^{\frac{3}{2}}, & t > k \end{cases}$, for ANY $k > 0$!

- Infinite number of solutions!

Existence/Uniqueness Theorem

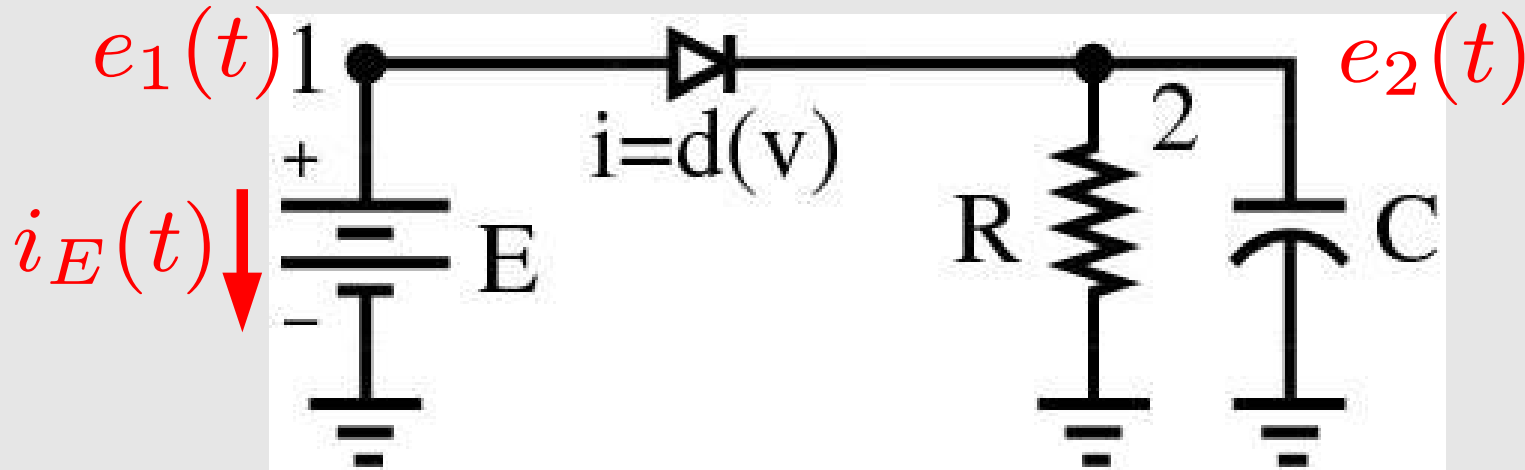
- Picard-Lindelöf Theorem (roughly)
 - If $\vec{g}(\vec{x}, t)$ is
 - defined over all t, x
 - **Lipschitz for all x**
 - then $\dot{\vec{x}}(t) = \vec{g}(\vec{x}, t), \quad \vec{x}(t_0) = \vec{x}_0$ has a **unique global solution**
- $\vec{g}(\vec{x}, t)$ is **Lipschitz if**
 - there exists some finite L such that:
 - $\|\vec{g}(\vec{x}_1, t) - \vec{g}(\vec{x}_2, t)\| < L\|\vec{x}_1 - \vec{x}_2\|, \quad \forall \vec{x}_1, \vec{x}_2$

The Lipschitz Condition



- Linear systems: Lipschitz
- $\sqrt[3]{x}$, $\frac{1}{x - x_0}$: not Lipschitz

Is this globally Lipschitz?



$$\text{n1 KCL: } i_E + d(e_1 - e_2) = 0$$

$$\text{n2 KCL: } -d(e_1 - e_2) + \frac{e_2}{R} + \frac{d}{dt}(Ce_2) = 0$$

$$\text{E BCR: } e_1 - E = 0$$

$$\text{n2 KCL: } \frac{d}{dt}e_2 + \frac{e_2}{RC} - \frac{d(E(t) - e_2)}{C} = 0$$

Solving ODEs: Overview of Strategy

- Discretize the time axis (starting from, e.g., $t=0$)

→ $t_0 = 0, t_1, t_2, \dots, t_N$

- Approximate d/dt term by finite difference

→ e.g., $\frac{d\vec{x}}{dt} \simeq \frac{\vec{x}_i - \vec{x}_{i-1}}{t_i - t_{i-1}}$

- ODE becomes algebraic nonlinear equation

$$\underbrace{\frac{\vec{x}_i - \vec{x}_{i-1}}{t_i - t_{i-1}} + \vec{f}(\vec{x}_i) + \vec{b}(t_i)}_{\vec{h}_i(\vec{x}_i)} = \vec{0}$$

- Solve using Newton-Raphson

→ repeat for $i=1,2,3,\dots,N$

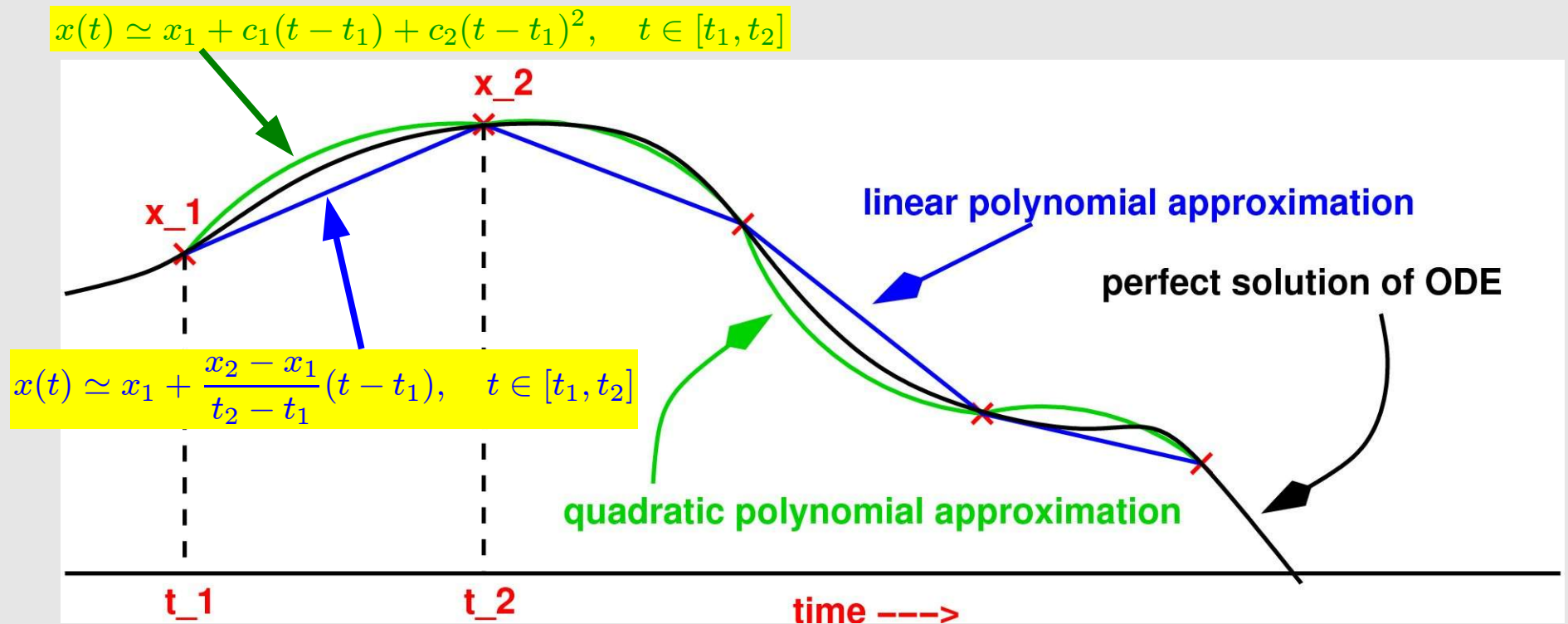
→ using previous solution (or initial condition) at t_{i-1}

- Key issues:

→ how to discretize? errors/accuracy? computation? coding?

Piecewise Polynomial Approximation

- Using locally polynomial bases
 - assume: ODE solution is **locally polynomial**
 - **characterize polynomial with a few numbers**
 - e.g., samples at different points
 - **find those numbers** so that the **local polynomial satisfies the ODE**



Linear Polynomials: FE and BE

- Use of **locally linear** approximations for $x(t)$

- $\vec{x}(t) \simeq \vec{x}_1 + \frac{\vec{x}_2 - \vec{x}_1}{t_2 - t_1} (t - t_1), \quad t \in [t_1, t_2]$

- **Knowns:** t_1, t_2, \vec{x}_1

→ (\vec{x}_1 known from, e.g., initial condition)

- **Unknown:** \vec{x}_2

- Use linear approx. to express $\dot{\vec{x}}(t)$: $\dot{\vec{x}}(t) \simeq \frac{\vec{x}_2 - \vec{x}_1}{t_2 - t_1}$

- Enforce ODE $\dot{\vec{x}}(t) = \vec{g}(\vec{x}, t)$ at t_1 : **Forward Euler (FE)**

→ $\dot{\vec{x}}(t_1) = \vec{g}(\vec{x}_1, t_1) : \frac{\vec{x}_2 - \vec{x}_1}{t_2 - t_1} = \vec{g}(\vec{x}_1, t_1)$

- Enforce ODE $\dot{\vec{x}}(t) = \vec{g}(\vec{x}, t)$ at t_2 : **Backward Euler (BE)**

→ $\dot{\vec{x}}(t_1) = \vec{g}(\vec{x}_2, t_2) : \frac{\vec{x}_2 - \vec{x}_1}{t_2 - t_1} = \vec{g}(\vec{x}_2, t_2)$

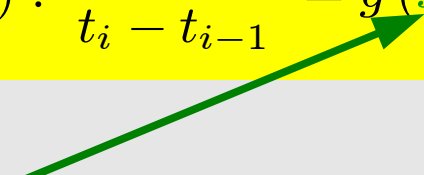
The Forward Euler Method

$$\dot{\vec{x}}(t_{i-1}) = \vec{g}(\vec{x}_{i-1}, t_{i-1}) : \frac{\vec{x}_i - \vec{x}_{i-1}}{t_i - t_{i-1}} = \vec{g}(\vec{x}_{i-1}, t_{i-1})$$

$$\Rightarrow \boxed{\vec{x}_i = \vec{x}_{i-1} + (t_i - t_{i-1})\vec{g}(\vec{x}_{i-1}, t_{i-1})}$$

- **Explicit** integration method
 - \vec{x}_2 available explicitly in terms of knowns
 - **nonlinear solve not needed** (single eval of $\vec{g}(\cdot, \cdot)$ suffices)
 - (we'll see later) **not numerically stable**
 - (we'll see later) **does not work for DAEs**
- “**Time stepping**” ODE solution process
 - 1) start with initial condition: $\vec{x}_0 = \vec{x}(t_0)$, $i=1$
 - 2) find \vec{x}_i using FE equation, above
 - 3) increment i ; stop if $t_i > \text{stoptime}$, else goto 2

The Backward Euler Method

$$\dot{\vec{x}}(t_i) = \vec{g}(\vec{x}_i, t_i) : \frac{\vec{x}_i - \vec{x}_{i-1}}{t_i - t_{i-1}} = \vec{g}(\vec{x}_i, t_i) \Rightarrow \boxed{\frac{\vec{x}_i - \vec{x}_{i-1}}{t_i - t_{i-1}} - \vec{g}(\vec{x}_i, t_i) = \vec{0}}$$


- **Implicit** integration method
 - **Finding \mathbf{x}_2 requires nonlinear solution (N-R)**
 - (we'll see later) **numerically (over)stable**
 - (we'll see later) **does work for DAEs**
- **“Time stepping” ODE solution process**
 - 1) start with initial condition: $\mathbf{x}_0 = \mathbf{x}(t_0)$, $i=1$
 - 2) find \mathbf{x}_i using BE equation, above
 - solve it using Newton-Raphson
 - 3) increment i ; stop if $t_i > \text{stoptime}$, else **goto 2**

The Trapezoidal Method

- “Average” FE and BE:

$$\dot{\vec{x}}(t_1) = \vec{g}(\vec{x}_1, t_1)$$

$$+ \quad \dot{\vec{x}}(t_2) = \vec{g}(\vec{x}_2, t_2)$$

$$\frac{\dot{\vec{x}}(t_1) + \dot{\vec{x}}(t_2)}{2} = \frac{\vec{g}(\vec{x}_1, t_1) + \vec{g}(\vec{x}_2, t_2)}{2}$$

- PWL assumption $\Rightarrow \dot{\vec{x}}(t_1) = \dot{\vec{x}}(t_2) = \frac{\vec{x}_2 - \vec{x}_1}{t_2 - t_1}$

- **Trapezoidal Method:** $\frac{\vec{x}_2 - \vec{x}_1}{t_2 - t_1} = \frac{\vec{g}(\vec{x}_1, t_1) + \vec{g}(\vec{x}_2, t_2)}{2}$

- at i^{th} timestep:

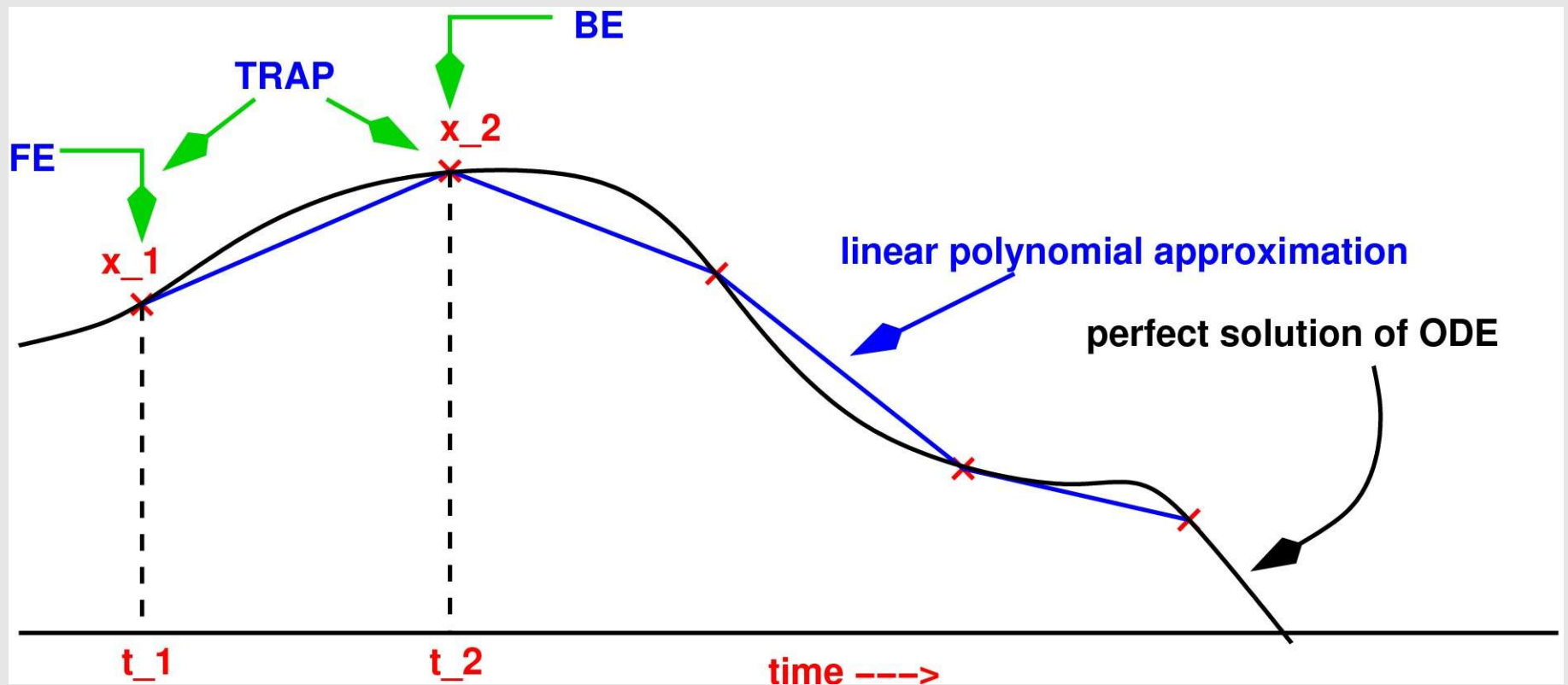
Implicit (N-R needed)

$$\frac{\vec{x}_i - \vec{x}_{i-1}}{t_i - t_{i-1}} = \frac{\vec{g}(\vec{x}_{i-1}, t_{i-1}) + \vec{g}(\vec{x}_i, t_i)}{2}$$

**Perfectly stable numerically
(we'll see later)**

FE, BE, TRAP: Pictorial Summary

- Difference: where/how ODE is “enforced”



Linear Multi Step (LMS) Methods

- FE: $\vec{x}_i - \vec{x}_{i-1} = h_i \vec{g}(\vec{x}_{i-1}, t_{i-1}), \quad h_i \equiv t_i - t_{i-1}.$
- BE: $\vec{x}_i - \vec{x}_{i-1} = h_i \vec{g}(\vec{x}_i, t_i)$
- TRAP: $\vec{x}_i - \vec{x}_{i-1} = h_i \frac{\vec{g}(\vec{x}_i, t_i) + \vec{g}(\vec{x}_{i-1}, t_{i-1})}{2}$
- Generic: $\alpha_0 \vec{x}_i + \alpha_1 \vec{x}_{i-1} = \beta_0 \vec{g}(\vec{x}_i, t_i) + \beta_1 \vec{g}(\vec{x}_{i-1}, t_{i-1})$
 - FE: $\alpha_0 = 1, \alpha_1 = -1, \beta_0 = 0, \beta_1 = h_i$
 - BE: $\alpha_0 = 1, \alpha_1 = -1, \beta_0 = h_i, \beta_1 = 0$
 - TRAP: $\alpha_0 = 1, \alpha_1 = -1, \beta_0 = \frac{h_i}{2}, \beta_1 = \frac{h_i}{2}$
- p^{th} -order Linear Multi Step integration formula

$$\sum_{i=0}^p \alpha_i \vec{x}_{n-i} = \sum_{i=0}^p \beta_i \vec{g}(\vec{x}_{n-i}, t_{n-i})$$

Use of ODE LMS Methods for DAEs

$$\frac{d}{dt}\vec{q}(\vec{x}(t)) + \vec{f}(\vec{x}(t)) + \vec{b}(t) = \vec{0} \Rightarrow \frac{d}{dt}\vec{q}(\vec{x}(t)) = \vec{g}(\vec{x}, t)$$

- The (simple) idea: re-do all derivations with $\vec{q}(t) \equiv \vec{q}(\vec{x}(t))$ on LHS, instead of $\vec{x}(t)$.

- Generic LMS for $p=1$ (1-step LMS):

$$\rightarrow \alpha_0 \vec{q}(\vec{x}_i) + \alpha_1 \vec{q}(\vec{x}_{i-1}) = \beta_0 \vec{g}(\vec{x}_i, t_i) + \beta_1 \vec{g}(\vec{x}_{i-1}, t_{i-1})$$

- BE: $\vec{q}(\vec{x}_i) - \vec{q}(\vec{x}_{i-1}) = h_i \vec{g}(\vec{x}_i, t_i)$ Implicit (N-R needed)

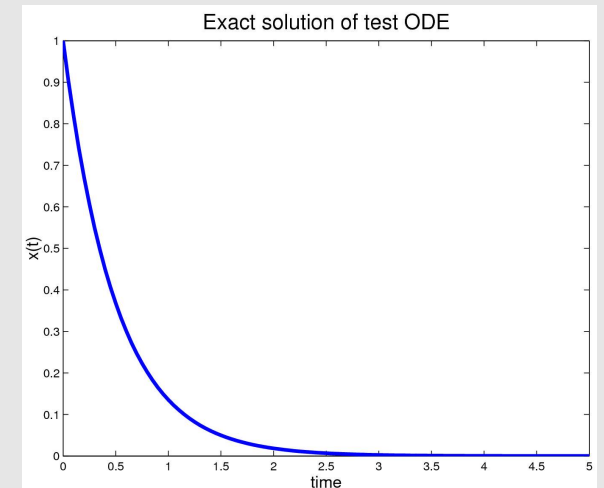
- TRAP: $\vec{q}(\vec{x}_i) - \vec{q}(\vec{x}_{i-1}) = h_i \frac{\vec{g}(\vec{x}_i, t_i) + \vec{g}(\vec{x}_{i-1}, t_{i-1})}{2}$

- FE: $\vec{q}(\vec{x}_i) - \vec{q}(\vec{x}_{i-1}) = h_i \vec{g}(\vec{x}_{i-1}, t_{i-1})$.

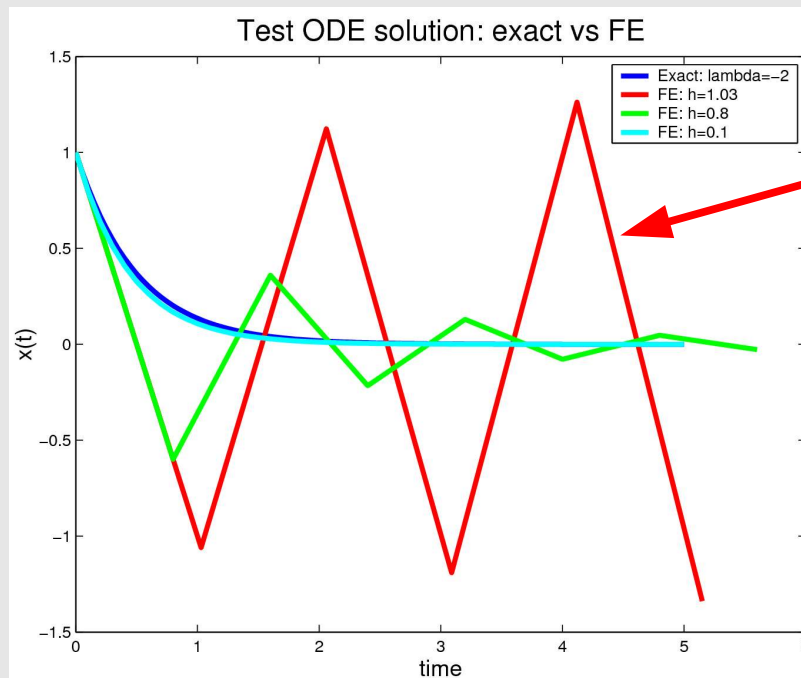
Implicit?

Stability of LMS Methods

- Test ODE: $\dot{x}(t) = \lambda x(t), \quad x(0) = x_0.$
- exact solution: $x(t) = x_0 e^{\lambda t}.$
 - solution decays if $\lambda < 0.$



- What do FE/BE/TRAP produce?



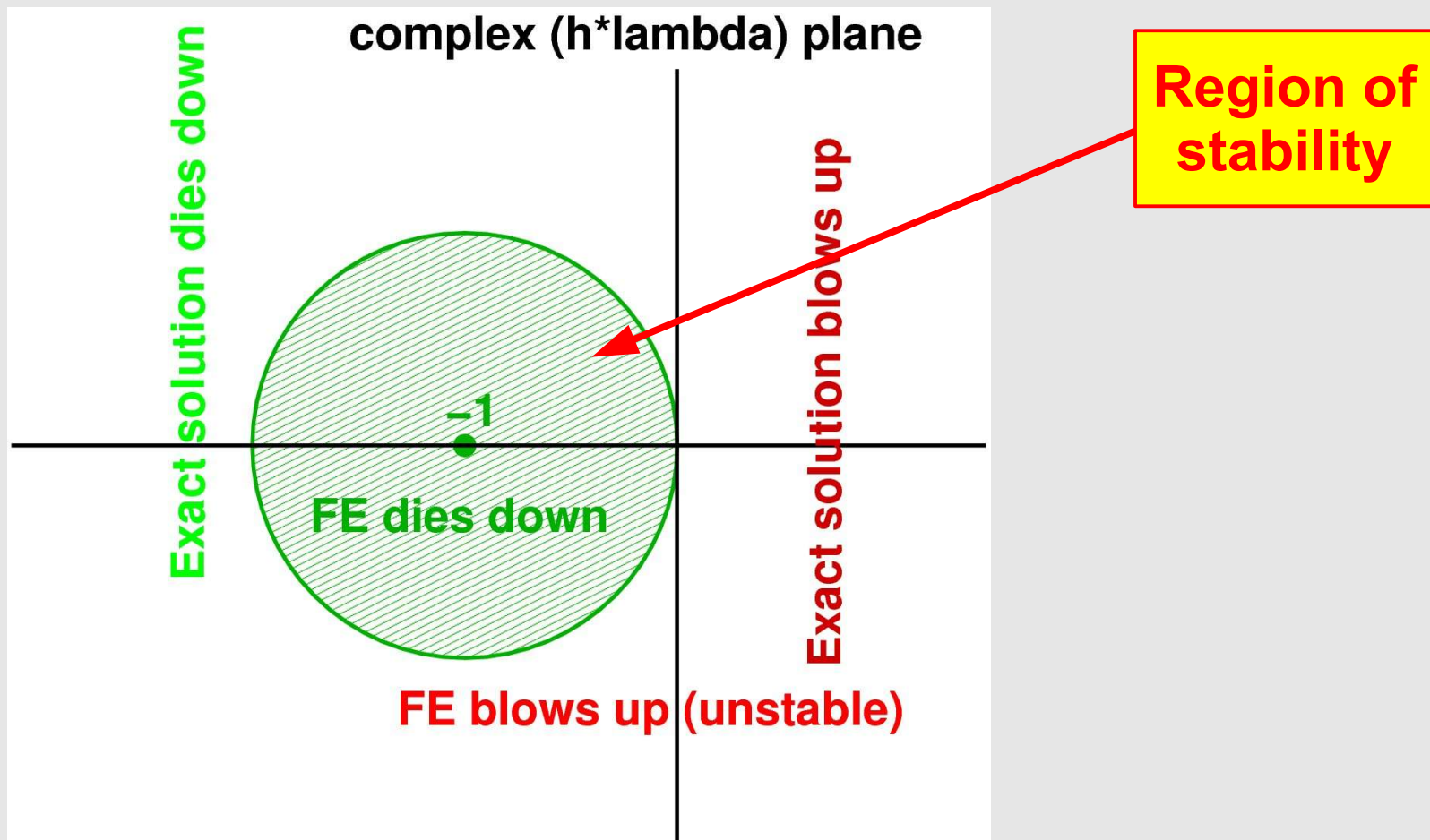
FE is qualitatively wrong

Why FE Explodes

- FE (with constant timestep h)
 - $x_n = (1 + h\lambda)x_{n-1} \Rightarrow x_n = x_0(1 + h\lambda)^n$.
 - if $|1 + h\lambda| > 1$, solution blows up w.r.t n .
 - solution is **qualitatively wrong** for $\lambda < 0$.
- Basic requirement for FE
 - h should be small enough s.t. $|1 + h\lambda| < 1$.
 - Example: $\lambda = 10^9 \Rightarrow h < 2 \times 10^{-9}$.
 - **FE limited to small timesteps**
 - for even “qualitative” accuracy
- FE said to be (numerically) **unstable**
 - if $|1 + h\lambda| > 1$

FE: Stability Picture for Complex λ

- In general: eigenvalues can be complex
- stability condition $|1 + h\lambda| < 1$: **circle** in $h\lambda$ plane



Stability of BE

- BE with constant timestep h

- $x_n(1 - h\lambda) = x_{n-1} \Rightarrow x_n = x_0 \frac{1}{(1 - h\lambda)^n}$

- solution will die down if $|1 - h\lambda| > 1$.

- i.e., all of left half plane.

- but also

- much of right half plane

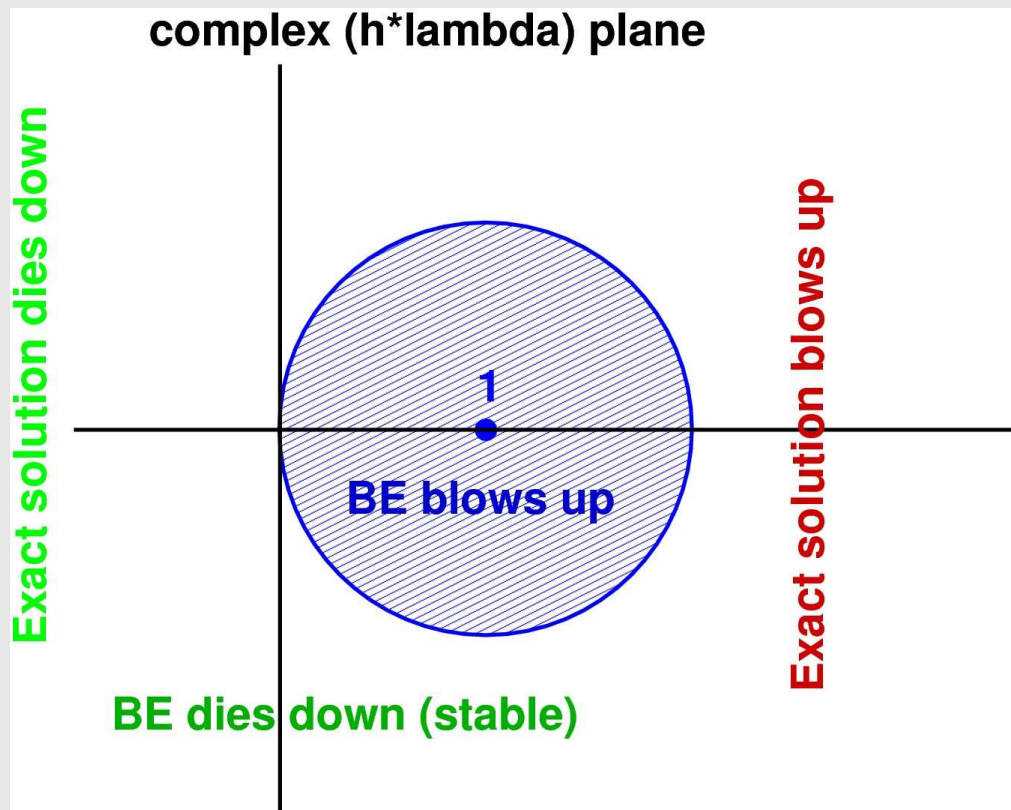
- **BE is overstable**

- **OK only within circle**

- **Applications**

- $\lambda < 0$ more important

- **much better than FE**



Stability of TRAP

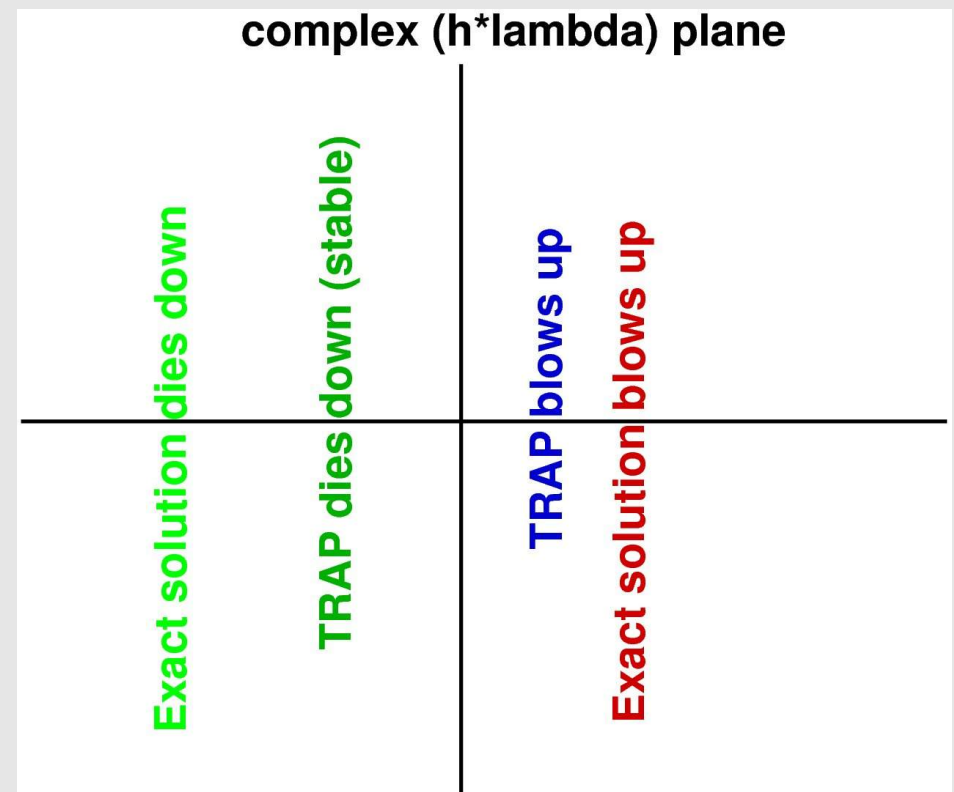
- TRAP with constant timestep h

- $$x_n \left(1 - \frac{h\lambda}{2}\right) = x_{n-1} \left(1 + \frac{h\lambda}{2}\right) \Rightarrow x_n = x_0 \left(\frac{2 + h\lambda}{2 - h\lambda}\right)^n.$$

- solution will die down if $\text{Re}(\lambda) < 0$
- solution will blow up if $\text{Re}(\lambda) > 0$

→ i.e, perfect stability

- Also very accurate
 - (we'll see later)
- Only concern
 - DAE initial consistency
 - (we'll see later)
 - (easy practical workaround)



Accuracy and Truncation Error

- Even if stable: is the method accurate?
- Test problem exact solution: $x(nh) = x_0 e^{\lambda n h}$.
- How do numerical method solutions compare?
 - FE: $x(nh) \simeq x_0 (1 + h\lambda)^n$.
 - BE: $x(nh) \simeq x_0 \frac{1}{(1 - h\lambda)^n}$.
 - TRAP: $x(nh) \simeq x_0 \left(\frac{2 + h\lambda}{2 - h\lambda} \right)^n$.
- None are identical, but how different?

Taylor Expansion Error

- **Exact:** $x(nh) = x_0 e^{\lambda nh} = x_0 \left(1 + nh\lambda + \frac{n^2 h^2 \lambda^2}{2!} + \dots \right)$
- **FE:** $x(nh) \simeq x_0 \left(1 + nh\lambda + \frac{n(n-1)}{2} h^2 \lambda^2 + \dots \right)$
→ first-order accurate
- **BE:** $x(nh) \simeq x_0 \left(1 + nh\lambda + \frac{n(n+1)}{2} h^2 \lambda^2 + \dots \right)$
→ also first-order accurate
- **TRAP:** $x(nh) \simeq x_0 \left(1 + nh\lambda + \frac{n^2}{2} h^2 \lambda^2 + \dots \right)$
→ second-order accurate

Transient: Timestep Control

- Choosing the next timestep dynamically
- LTE based control
 - apply LTE formulae to estimate error
 - change timestep to meet some specified error
 - error specification: like reltol-abstol (reltol=percentage)
 - make sure these are looser than NR tolerances!
 - element-by-element vs vector norm based
 - 2-norm vs max norm; DAE issues
 - (change integration method based on timestep)
- NR convergence based control
 - cut timestep if NR does not converge
 - also: increase maxiter
 - increase timestep if NR converges “too easily”
 - also: decrease maxiter

ODE/DAE Packages Out There

- **MATLAB** has various ODE/DAE integrators
 - ode23, ode45, ...; ode23t, ode15s, ...
- **DASSL/DASPK: general purpose DAE packages**
 - Linda Petzold, UCSB
 - Fortran
 - some tweaking helpful for circuit applications
- **Easy (and often worthwhile) to roll your own**
 - tweaking, special heuristics, debugging, ...

Transient: Other Important Issues

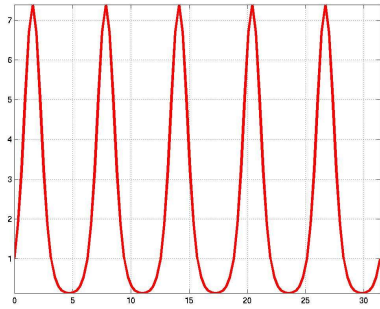
- **What integration method to use?**
 - stability?
 - nonlinear solution required? (implicit vs explicit)
 - accuracy loss due to discretization?
 - Local Truncation Error (LTE)
 - higher order methods (more than 1 previous timepoint)
- **Vast body of work on ODE integration**
 - linear multi-step methods (LMS), Runge-Kutta, symmetric, symplectic, “energy-conserving”, etc.
- **Stiff differential equations**
 - different variables have very different time constants
 - stiffly stable methods allow you to take larger time steps
- **DAE issues**
 - initial condition consistency; stability; index; ...
- **Dynamic timestep control, NR heuristics, ...**

Solving the Circuit's Equations

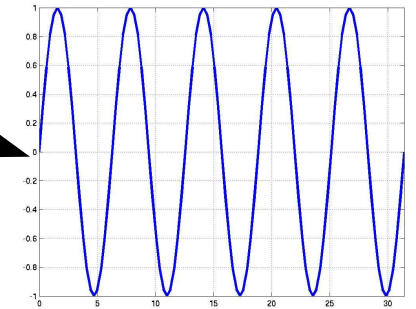
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 - ✓ transient: ckt. waveforms changing with time
 - periodic steady state: changes periodic w time
 - linear(ized): all sinusoidal waveforms: AC analysis
 - nonlinear steady state: shooting, harmonic balance
 - noise analysis: random/stochastic waveforms
 - sensitivity analysis: effects of changes in circuit parameters

The Periodic Steady State Problem



$$\frac{d}{dt} \vec{q}(\vec{x}(t)) + \vec{f}(\vec{x}(t)) + \vec{b}(t) = \vec{0}$$



- What

- inputs $b(t)$ are periodic – e.g., sinusoidal
- **suppose “outputs” $x(t)$ also become periodic**
 - (happens for “stable” circuits and systems ...
 - ... eventually – can take a long time)
- **want to find this periodic steady state directly**
 - without using general/expensive transient analysis

- Why

- audio amps, RF amps, mixers, oscillators, clocks, ...
 - ckt nonlinear => sinusoids will in general be distorted
- **linear circuits: frequency-domain analysis important**
 - much easier and more insightful than transient

- How (for linear circuits): **AC analysis**

