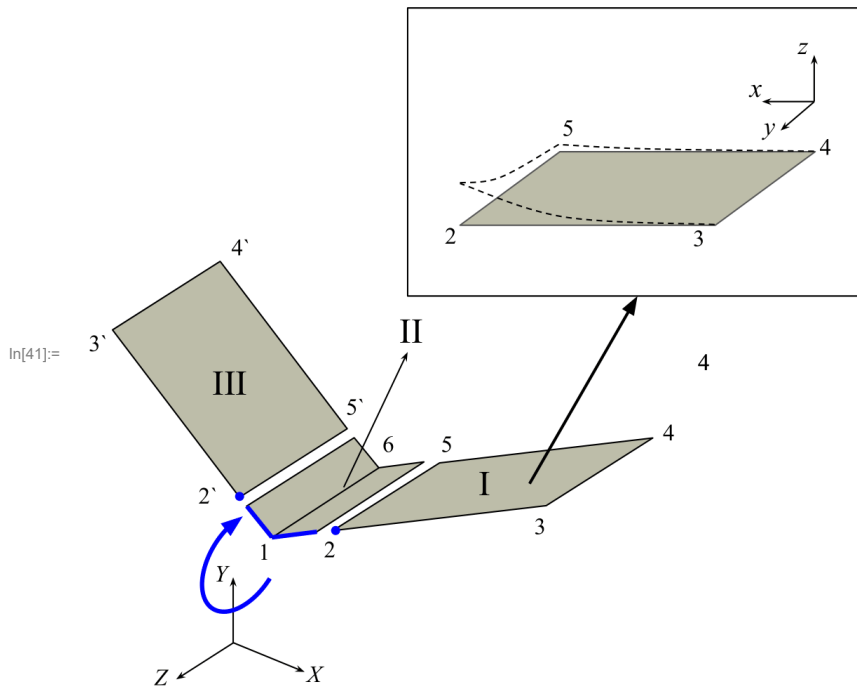


# Derivation of stiffness of equivalent torsion spring

The problem of deriving the stiffness of an equivalent torsion spring of a hexagonal honeycomb unit-cell reduces (due to symmetry) to finding the stiffness of the system shown below. Here  $\theta$  is angle of honeycomb.  $l$ ,  $w$ , and  $t_w$  are the length 2-3, width 3-4 and thickness of the plate respectively.  $d$  is the width of the attached bilayer (not shown) and is equal to length 2-2'.




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```
In[1]:= $Assumptions = E2 > 0 && w > 0 && t_w > 0 && l > 0 &&
          {x, y, z,  $\psi$ ,  $\theta$ , u, v, w, a, b, c, d, e, f} \in \text{Reals};
```

\* We assume all the material properties and dimensions are positive and restrict ourselves to the Reals.

---

```
In[2]:= u_y = f y x^3;
u_z = (a + b y^2 + c y^4) (x^3);
u_x = u_z Tan[ $\theta$ ];
```

\* Polynomial approximation of displacement in section I. Here,  $a$ ,  $b$ ,  $c$ , and  $e$  are constants to be found through energy minimization.  $\theta$  is angle of honeycomb.

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```
In[5]:= bEliminate = Simplify[Flatten[Solve[
    {(D[(u_z / Cos[θ]), y] /. {x → l, y → w / 2}) == ψ}, {b}]]];
(*Solving for b as function of tip angle*)
u_x = u_x /. bEliminate; (*Substituting b*)
u_z = u_z /. bEliminate; (*Substituting b*)
u_y = u_y /. bEliminate; (*Substituting b*)
```

```
In[9]:= ε_xx = Simplify[-z D[u_z, {x, 2}] + D[u_x, x]];
ε_yy = Simplify[-z D[u_z, {y, 2}] + D[u_y, y]];
ε_xy = Simplify[(D[u_x, y] + D[u_y, x]) / 2 - z D[D[u_z, x], y]];
```

**\* Evaluating the strains and simplifying the equations**

```
In[12]:= σ_xx = E2 (ε_xx) / (1);
σ_yy = E2 (ε_yy) / (1);
σ_xy = (E2 / 2) ε_xy;
```

**\* Evaluating the stresses. Here 'E2' is used in place of 'E' since 'E' is reserved in MATHEMATICA.**

```
In[15]:= dU = Simplify[1/2 (σ_xx ε_xx + σ_xy ε_xy + σ_yy ε_yy)]
(* Writing the energy of infinitesimal element*)
```

```
Out[15]= 1/16 l^6 w^2 E2 x^2 (8 x^4 (1^3 w (f + c (w^2 - 12 y^2) z) - 2 z ψ Cos[θ])^2 +
    18 (1^3 w (2 a - c w^2 y^2 + 2 c y^4) + 2 y^2 ψ Cos[θ])^2 (-2 z + x Tan[θ])^2 + x^2 y^2
    (-12 z ψ Cos[θ] + 2 x ψ Sin[θ] + 1^3 w (3 (f + 2 c (w^2 - 4 y^2) z) - c x (w^2 - 4 y^2) Tan[θ]))^2)
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```
In[16]:= U1 = Integrate[dU, {z, -t_w/2, t_w/2}];
(*Integrating wrt z*)
U2 = Integrate[U1, {y, 0, w/2}]; (*Integrating wrt y*)
U3 = Integrate[U2, {x, 0, 1}]; (*Integrating wrt x*)
U = Simplify[U3] (*Simplifying the total energy*)
```

```
Out[19]= 
$$\frac{1}{11289600 l^3 w} E2 \cos[\theta] t_w \left( 7 \left( 403200 a^2 l^6 w^2 - 23520 a c l^6 w^6 + 3840 c^2 l^{10} w^6 + 576 c^2 l^8 w^8 + 535 c^2 l^6 w^{10} + 9600 l^4 \psi^2 + 5040 l^2 w^2 \psi^2 + 2520 w^4 \psi^2 + 24 l^3 w^3 \left( 2800 a - 3 c w^2 \left( 56 l^2 + 45 w^2 \right) \right) \psi \cos[\theta] + 120 \left( 80 l^4 + 42 l^2 w^2 + 21 w^4 \right) \psi^2 \cos[2\theta] \right) \sec[\theta] t_w^2 + 3 l^2 w^2 \left( 20 l^2 \sec[\theta]^3 \left( 441 f^2 l^4 w^2 + 8 c^2 l^6 w^6 + 35 \psi^2 + l^4 w^2 \left( 441 f^2 - 8 c^2 l^2 w^4 \right) \cos[2\theta] + 28 c l^3 w^3 \psi \cos[3\theta] - 35 \psi^2 \cos[4\theta] + 245 f l^2 w \psi \sin[3\theta] \right) + 504 l^3 w \left( 560 a - 27 c w^4 \right) \psi \tan[\theta]^2 - 140 l^4 w \psi \sec[\theta]^2 \left( 4 c l w^2 - 35 f \tan[\theta] \right) + 7 \sec[\theta] \left( 19200 f^2 l^8 - 560 c f l^7 w^4 \tan[\theta] + 3 \left( 80640 a^2 l^6 - 4704 a c l^6 w^4 + 107 c^2 l^6 w^8 + 504 w^2 \psi^2 + 504 w^2 \psi^2 \cos[2\theta] \right) \tan[\theta]^2 \right) \right)$$

```

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```
In[26]:= eqn1 = Simplify[D[U, a] == 0];
(*Minimization equation wrt a*)
eqn2 = Simplify[D[U, c] == 0];
(*Minimization equation wrt c*)
eqn3 = Simplify[D[U, f] == 0];
(*Minimization equation wrt e*)
eqn4 = Simplify[D[U, ψ] == M];
(*Minimization equation wrt ψ, i.e. dU/dψ=M *)

solution = Simplify[
  Flatten[Solve[{eqn1, eqn2, eqn3, eqn4}, {a, c, f, ψ}]]]
(*Solving the 4 equations simultaneuosly*)
```

```

Out[26]= {a → (525 M w2 (9 l2 Sin[θ]2 + 5 Cos[θ]2 tw2)
  (-3 l2 (32 256 000 l6 + 3 000 960 l4 w2 - 656 509 l2 w4 - 70 560 w6) Sin[θ]2 tw2 -
  140 (384 000 l6 + 37 440 l4 w2 - 4901 l2 w4 - 420 w6) Cos[θ]2 tw4 +
  27 l4 w2 (28 800 l4 + 48 965 l2 w2 + 7056 w4) Sin[θ]2 Tan[θ]2) ) /
  (E2 tw (45 l4 (2 903 040 000 l10 + 2 858 976 000 l8 w2 + 1 821 083 520 l6 w4 +
  288 250 417 l4 w6 + 15 648 780 l2 w8 + 635 040 w10) Cos[θ] Sin[θ]4 tw4 +
  25 l2 (5 806 080 000 l10 + 4 940 352 000 l8 w2 + 2 124 365 040 l6 w4 +
  289 303 959 l4 w6 + 13 496 980 l2 w8 + 423 360 w10) Cos[θ]3 Sin[θ]2 tw6 + 3500
  (11 520 000 l10 + 9 288 000 l8 w2 + 3 212 760 l6 w4 + 388 521 l4 w6 + 16 430 l2 w8 + 420 w10)
  Cos[θ]5 tw8 + 405 l6 w2 (51 840 000 l8 + 101 506 800 l6 w2 +
  20 043 625 l4 w4 + 1 473 612 l2 w6 + 84 672 w8) Sin[θ]5 tw2 Tan[θ] +
  729 l8 w4 (240 000 l6 + 672 875 l4 w2 + 215 180 l2 w4 + 21 168 w6) Sin[θ]5 Tan[θ]3) ) ,
c → (882 000 M (9 l2 Sin[θ]2 + 5 Cos[θ]2 tw2) (l2 (410 880 l4 + 278 203 l2 w2 + 30 240 w4)
  Sin[θ]2 tw2 + 20 (10 080 l4 + 4523 l2 w2 + 420 w4) Cos[θ]2 tw4 +
  9 l4 (9600 l4 + 23 075 l2 w2 + 3024 w4) Sin[θ]2 Tan[θ]2) ) /
  (E2 tw (45 l4 (2 903 040 000 l10 + 2 858 976 000 l8 w2 + 1 821 083 520 l6 w4 +
  288 250 417 l4 w6 + 15 648 780 l2 w8 + 635 040 w10) Cos[θ] Sin[θ]4 tw4 +
  25 l2 (5 806 080 000 l10 + 4 940 352 000 l8 w2 + 2 124 365 040 l6 w4 +
  289 303 959 l4 w6 + 13 496 980 l2 w8 + 423 360 w10) Cos[θ]3 Sin[θ]2 tw6 + 3500
  (11 520 000 l10 + 9 288 000 l8 w2 + 3 212 760 l6 w4 + 388 521 l4 w6 + 16 430 l2 w8 + 420 w10)
  Cos[θ]5 tw8 + 405 l6 w2 (51 840 000 l8 + 101 506 800 l6 w2 +
  20 043 625 l4 w4 + 1 473 612 l2 w6 + 84 672 w8) Sin[θ]5 tw2 Tan[θ] +
  729 l8 w4 (240 000 l6 + 672 875 l4 w2 + 215 180 l2 w4 + 21 168 w6) Sin[θ]5 Tan[θ]3) ) ,
f → - ( (1176 000 l M w2 (9 l2 Sin[θ]2 + 5 Cos[θ]2 tw2) Tan[θ]
  (18 l2 (2100 l4 + 107 l2 w2 + 70 w4) Sin[θ]2 tw2 +
  35 (600 l4 + 27 l2 w2 + 10 w4) Cos[θ]2 tw4 + 81 l4 w2 (5 l2 + 14 w2) Sin[θ]2 Tan[θ]2) ) ) /
  (E2 tw (45 l4 (2 903 040 000 l10 + 2 858 976 000 l8 w2 + 1 821 083 520 l6 w4 +
  288 250 417 l4 w6 + 15 648 780 l2 w8 + 635 040 w10) Cos[θ] Sin[θ]4 tw4 +
  25 l2 (5 806 080 000 l10 + 4 940 352 000 l8 w2 + 2 124 365 040 l6 w4 +
  289 303 959 l4 w6 + 13 496 980 l2 w8 + 423 360 w10) Cos[θ]3 Sin[θ]2 tw6 +
  3500 (11 520 000 l10 + 9 288 000 l8 w2 + 3 212 760 l6 w4 + 388 521 l4 w6 +
  16 430 l2 w8 + 420 w10) Cos[θ]5 tw8 + 405 l6 w2 (51 840 000 l8 + 101 506 800 l6 w2 +
  20 043 625 l4 w4 + 1 473 612 l2 w6 + 84 672 w8) Sin[θ]5 tw2 Tan[θ] +
  729 l8 w4 (240 000 l6 + 672 875 l4 w2 + 215 180 l2 w4 + 21 168 w6) Sin[θ]5 Tan[θ]3) ) ) ,
ψ → (25 200 l3 M w Sec[θ]2 (840 (3200 l6 + 900 l4 w2 + 223 l2 w4 + 21 w6) tw2 +
  l2 w2 (96 000 l4 + 245 945 l2 w2 + 31 752 w4) Tan[θ]2) ) /
  (E2 tw (140 (11 520 000 l10 + 9 288 000 l8 w2 + 3 212 760 l6 w4 +
  388 521 l4 w6 + 16 430 l2 w8 + 420 w10) tw4 +
  5 l2 w2 (51 840 000 l8 + 101 026 800 l6 w2 + 18 697 875 l4 w4 + 1 043 252 l2 w6 + 42 336 w8)
  tw2 Tan[θ]2 + 9 l4 w4 (240 000 l6 + 672 875 l4 w2 + 215 180 l2 w4 + 21 168 w6) Tan[θ]4) ) ) }

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```
In[27]:=  $\tau_i = \text{Simplify}[(M / (\psi /. \text{solution}))]$ 
(*Stiffness of section I -
moment (M) by tip angle (found as  $\psi$  above)*)
```

```
Out[27]= 
$$\frac{E2 \cos[\theta]^2 t_w (140 (11520000 l^{10} + 9288000 l^8 w^2 + 3212760 l^6 w^4 + 388521 l^4 w^6 + 16430 l^2 w^8 + 420 w^{10}) t_w^4 + 5 l^2 w^2 (51840000 l^8 + 101026800 l^6 w^2 + 18697875 l^4 w^4 + 1043252 l^2 w^6 + 42336 w^8) t_w^2 \tan[\theta]^2 + 9 l^4 w^4 (240000 l^6 + 672875 l^4 w^2 + 215180 l^2 w^4 + 21168 w^6) \tan[\theta]^4)}{(25200 l^3 w (840 (3200 l^6 + 900 l^4 w^2 + 223 l^2 w^4 + 21 w^6) t_w^2 + l^2 w^2 (96000 l^4 + 245945 l^2 w^2 + 31752 w^4) \tan[\theta]^2))}$$

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```
In[28]:=  $\tau_{ii} = E2 I2 / (w / 2);$  (*Stiffness of section II. 'I2'
is used in place of 'I' since it is reserved*)
I2 = ((d / 2) Tan[ $\theta$ ] *  $t_w^3 / 12 + ((d / 2) \tan[\theta])^3 * t_w / 12$ ) +
((d / 2) Tan[ $\theta$ ] *  $t_w^3 / 12 - ((d / 2) \tan[\theta])^3 * t_w / 12$ ) * Cos[2  $\theta$ ];
(* Area moment of inertia of section II found
by rotating that of a rectangular section by
 $\theta$  and invoking symmetry to double the value*)
 $\tau_{ii} = \text{Simplify}[E2 I2 / (w / 2)]$  (*Substituting*)
```

```
Out[29]= 
$$\frac{d E2 \sin[\theta] t_w (4 \cos[\theta] t_w^2 + d^2 \sin[\theta] \tan[\theta]^3)}{24 w}$$

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```
In[30]:=  $\tau = \text{Simplify}[\tau_{ii} + 2 \tau_i]$ 
(*Total  $\tau$ . Since  $\tau_i = \tau_{iii}$  by symmetry*)
```

```
Out[30]= 
$$\frac{1}{12600 w} E2 t_w (525 d \sin[\theta] (4 \cos[\theta] t_w^2 + d^2 \sin[\theta] \tan[\theta]^3) + (\cos[\theta]^2 (140 (11520000 l^{10} + 9288000 l^8 w^2 + 3212760 l^6 w^4 + 388521 l^4 w^6 + 16430 l^2 w^8 + 420 w^{10}) t_w^4 + 5 l^2 w^2 (51840000 l^8 + 101026800 l^6 w^2 + 18697875 l^4 w^4 + 1043252 l^2 w^6 + 42336 w^8) t_w^2 \tan[\theta]^2 + 9 l^4 w^4 (240000 l^6 + 672875 l^4 w^2 + 215180 l^2 w^4 + 21168 w^6) \tan[\theta]^4)) / (840 (3200 l^9 + 900 l^7 w^2 + 223 l^5 w^4 + 21 l^3 w^6) t_w^2 + l^5 w^2 (96000 l^4 + 245945 l^2 w^2 + 31752 w^4) \tan[\theta]^2))$$

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