

EE49001: Control and Electronic System Design

Assignment-2: Inverted Pendulum, Part:1

Submitted By:

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1. A pendulum consisting of a mass-less rod of length $l = 0.36m$ and a bob of mass $m = 0.26kg$ is attached to a cart of mass $M = 2.4kg$ moving on a rail. Let the position of the cart on the rail be denoted by x and the angle of the rod with respect to the upward vertical by θ . The cart is propelled by a horizontal force of u along the rail.

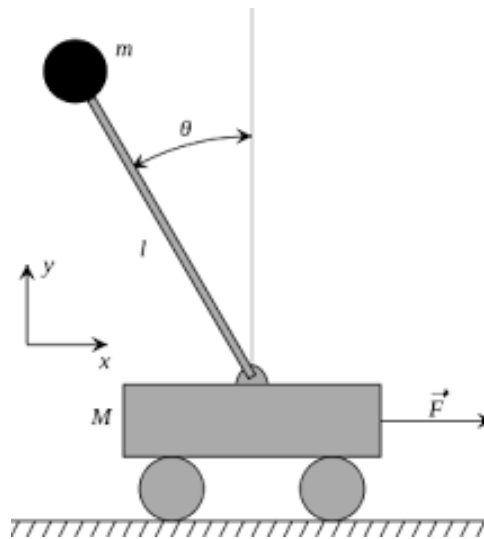


Fig: Diagram for Inverted Pendulum Setup

For the following system, we have 4 states: $z = [x, \dot{x}, \theta, \dot{\theta}]$, where:

$\dot{x} = v \equiv$ Translational velocity of the cart along x —direction

$\dot{\theta} = \omega$ Angular velocity of the rod, $F = u \equiv$ Horizontal force on the cart

- 1.1. Represent the nonlinear dynamics of the plant in the form $\dot{z} = f(z, u)$ where z denotes the states and u denotes the input

We can, using Newton's Laws of Motion, say that:

$$\dot{x} = v$$

$$\dot{\theta} =$$

$$(m + M)\ddot{x} + ml\ddot{\theta} \cos \theta - ml\dot{\theta}^2 \sin \theta = u$$

$$ml^2\ddot{\theta} = mgl \sin \theta - ml\ddot{x} \cos \theta$$

Considering the state space, $z = \begin{bmatrix} x \\ v \\ \theta \\ \omega \end{bmatrix}$

$$\dot{x} = f_1 = v$$

$$\dot{v} = f_2 = \frac{u + ml\omega^2 \sin \theta - mg \sin \theta \cos \theta}{m \sin^2 \theta + M}$$

$$\dot{\theta} = f_3 = \omega$$

$$\dot{\omega} = f_4 = \frac{g(m + M) \sin \theta - u \cos \theta - ml\omega^2 \sin \theta \cos \theta}{(m \sin^2 \theta + M)l}$$

- 1.2. Determine the equilibrium points of the above dynamical system.

The system is at equilibrium, means $\sum \vec{F}_{system} = 0$ and $\sum \vec{\tau}_{system} = 0$. It means, $\dot{x} = \ddot{\theta} = 0$. Putting these values in the non-linear dynamics' equations, we get: $\theta \in \{0, \pi\}$. For equilibrium we have $\dot{z} = 0$. That is: $\dot{x} = \ddot{x} = \dot{\theta} = \ddot{\theta} = 0$.

- 1.3. Linearize the above nonlinear dynamics around the unstable equilibrium point which has $\theta = 0$, and obtain the linearized dynamics of the form: $\dot{z} = Az + Bu$ for suitable matrices A and B . Determine the dimensions of A and B .

For Linearization of the given state equations in the neighbourhood of $\theta = 0$ i.e. $\theta = \Delta\theta$ where $\Delta\theta \rightarrow 0^\circ$, we can assume the small angle approximations to be valid. Therefore, we have $\sin \theta \approx \theta$ and $\cos \theta \approx 1$.

Hence, we can write:

$$ml^2\ddot{\theta} = mgl \theta - ml\ddot{x}$$

$$(m + M)\ddot{x} + ml\ddot{\theta} = u$$

For small θ , assuming $\dot{\theta}^2 \approx 0$

These are the linearized dynamics equations in the neighbourhood of $\theta = 0^\circ$

The 4 nonlinear equations can be linearised in the form $\dot{z} = Az + Bu$, where the matrices are defined as follows:

$$[A_{ij}] = \left[\frac{\partial f_i}{\partial z_j} \right]_{z_0} \text{ and } [B_i] = \left[\frac{\partial f_i}{\partial u} \right]_{z_0}$$

z_0 is the unstable equilibrium point, $z_0 = 0$

Dimensionally, $A \equiv 4 \times 4$ and $B \equiv 4 \times 1$

z_0 is the unstable equilibrium point $z_0 = 0$

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & -\frac{mg}{M} & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & \frac{(m+M)g}{Ml} & 0 \end{bmatrix} \text{ and } B = \begin{bmatrix} 0 \\ 1 \\ 0 \\ -\frac{1}{Ml} \end{bmatrix}$$

- 1.4. Obtain the transfer functions $\frac{\Theta(s)}{U(s)}$ and $\frac{X(s)}{U(s)}$ assuming θ to be close to zero.

Taking Laplace Transform we get

$$(m+M)s^2X + mls^2\Theta = U \quad mls^2\Theta - mg\Theta + ms^2X = 0$$

Where,

$$X = X(s) = \mathcal{L}\{x(t)\} \quad 1\Theta = \Theta(s) = \mathcal{L}\{\theta(t)\} \quad U = U(s) = \mathcal{L}\{u(t)\}$$

On solving and simplifying we get,

$$\frac{X(s)}{U(s)} = \frac{\frac{1}{M}\left(s^2 - \frac{g}{l}\right)}{s^2\left(s^2 - \frac{(M+m)g}{Ml}\right)}$$

$$\frac{\Theta(s)}{U(s)} = -\frac{\frac{1}{Ml}}{s^2 - \frac{(M+m)g}{Ml}}$$

Numerical Values of transfer function:

$$\text{sys1} = \frac{0.4167 s^2 - 12.41}{s^4 - 30.17 s^2}$$

Fig: Transfer function $\frac{X(s)}{U(s)}$

$$\text{sys2} = \frac{-0.15 s^2}{s^4 - 30.17 s^2}$$

Fig: Transfer function $\frac{\theta(s)}{U(s)}$

- 1.5. The pendulum is to be balanced in the inverted position with the cart being within the rail by applying a suitable u . Explain if the pendulum can be balanced using only θ or only x feedback. In other words, determine if the system is controllable when the input u is equal to either θ or x .

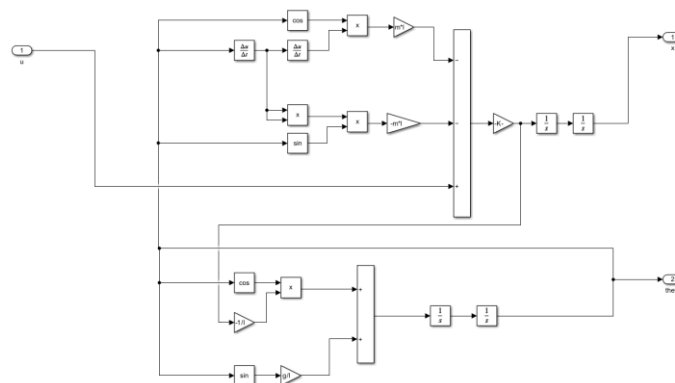
For $G(s) = \frac{\theta(s)}{U(s)}$: There is a pole-zero cancellation for the pole at $s = 0$

$H(s) = \frac{x(s)}{U(s)}$: Though, theoretically, there is no pole-zero cancellation, but pole and zero are very close. Therefore, for all practical purposes, pole-zero cancellation can be considered for the system.

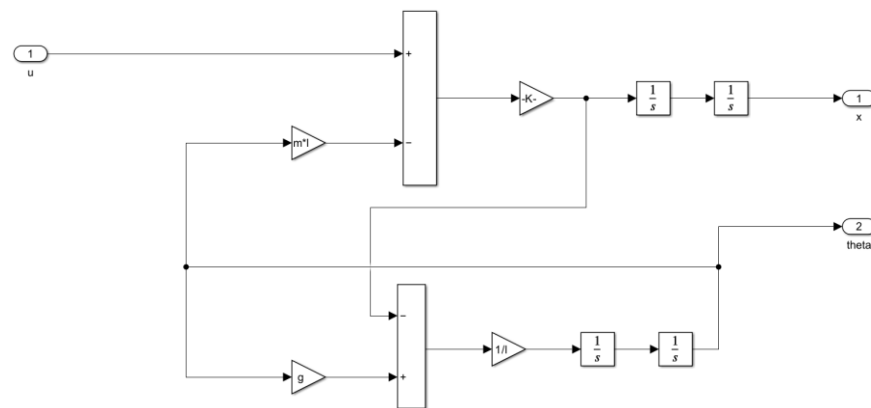
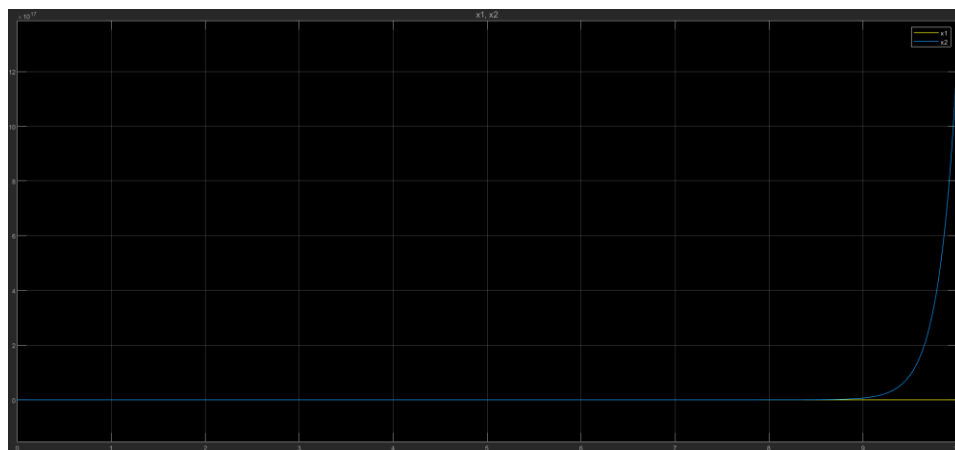
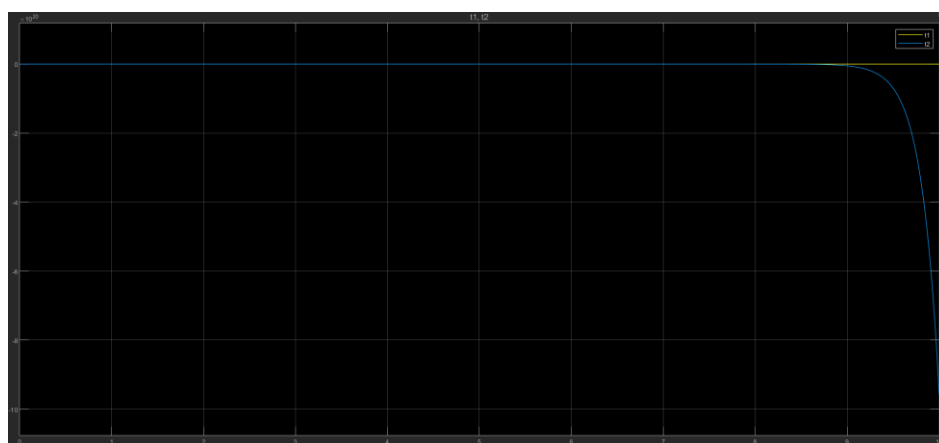
Though it is theoretically possible to control the system by only providing feedback of x , it is not practically possible.

Hence, the system is not controllable by providing feedback of only θ or x

- 1.6. Create a model of the nonlinear dynamical system in SIMULINK



1.7. Create a model of the linearized system in SIMULINK.

1.8. Plots for x and θ Fig. Comparison between x_1 (non-linear) and x_2 (linear)Fig. Comparison between θ_1 (non-linear) and θ_2 (linear)