

# Thermal Performance of the Petal Prototype

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ATLAS Experiment

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## Abstract

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## Acknowledgements

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# 1 Introduction

The high-luminosity upgrade for the LHC planned to be ready to run in 2026 imposes new challenges on detectors. For instance, an enhanced luminosity is immediately related to elevated radiation levels which constitute heat development. To avoid a thermal runaway and ensure reliable measurements, the electronics must be held at a constant temperature which requires some kind of cooling system for all detector components.

## 1.1 Petal

During my time in the DESY summer school, I participated in testing the thermal performance of the inner tracking detector of the ATLAS experiment. Figure 3 illustrates its position within the big detector and the planned upgraded design. The parts studied at DESY are the so-called petals that are assembled perpendicularly around the beampipe to track particles with low transversal energy. Figure 1 displays a picture of the tested petal prototype.



Figure 1: Picture of the tested petal prototype.

## 1.2 Cooling System

Figure 2 shows a prototype of the bare cooling loop. The cooling system is based on the energy needed for a phase change. Liquid  $\text{CO}_2$  is pumped into the cooling loop where some of it evaporates if exposed to heat. This evaporation requires energy (enthalpy of evaporation) which is taken from the heat source.

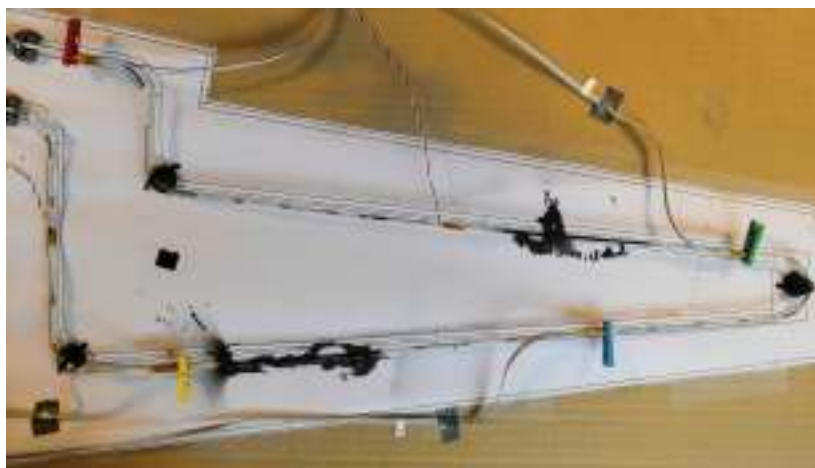


Figure 2: Picture of the a bare cooling loop.

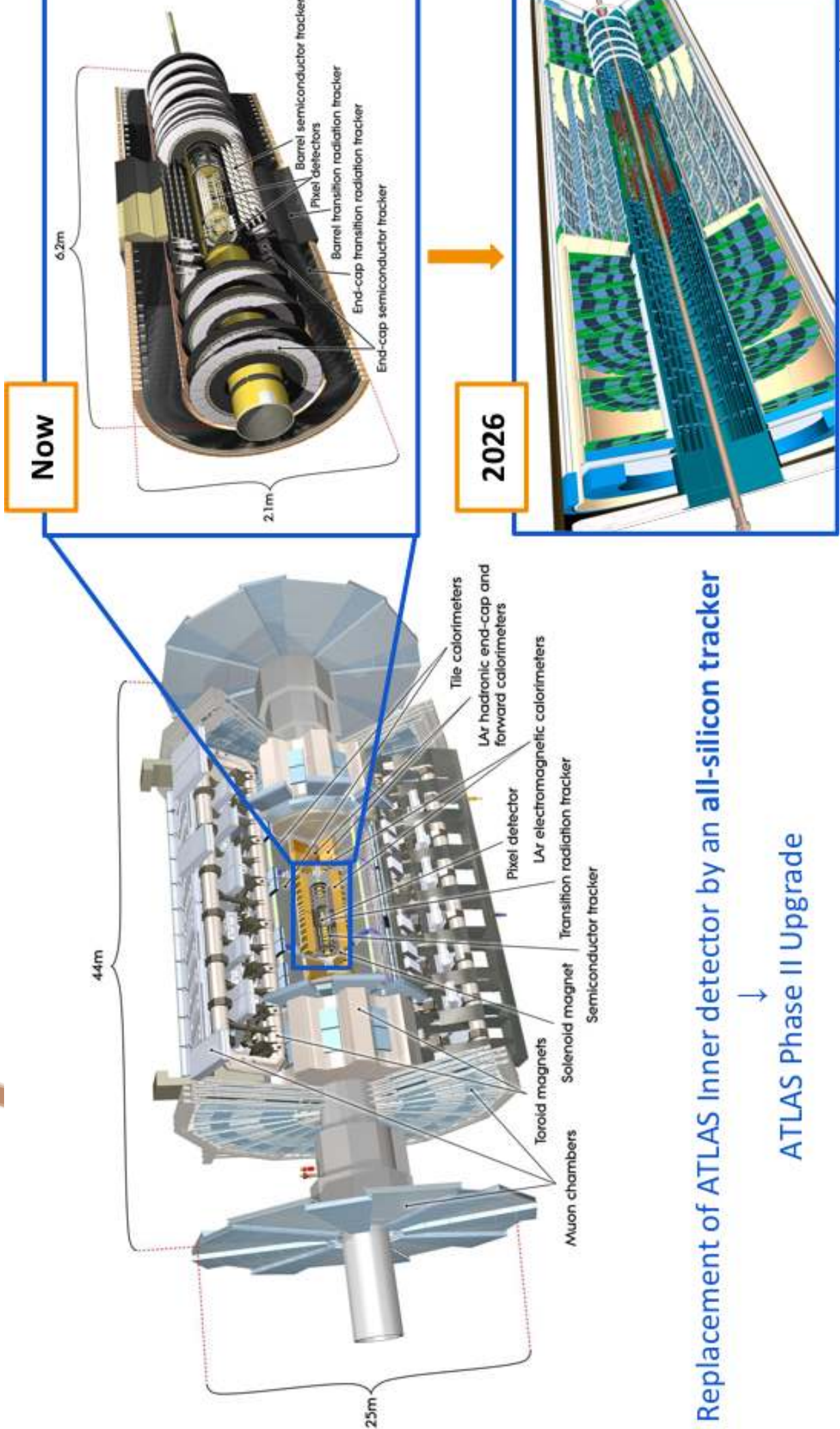


Figure 3: Schematics of the upgrade of the ATLAS inner tracking detector.



## 2 Infrared Theory

To assess the thermal performance of the petal, we measure the emitted radiation in the infrared (IR) spectrum. To properly evaluate the data measured with the IR camera, we need to understand the behaviour of IR radiation and camera software. This section gives an overview over these topics.

### 2.1 Emissivity

Every body emits IR radiation depending on its temperature. Light in the IR spectrum behaves identical to the more intuitive visible light. This means that surfaces can emit, absorb, and reflect IR radiation. Being purely interested in the *emitted* power, we need to minimize reflection in the IR region. The emissivity  $\epsilon$  describes the ability of a surface to emit IR radiation. It is a value between 0 and 1, where 0 corresponds to total reflection, whereas 1 corresponds to no reflection. So, to achieve good results using IR measurements, we cover the petal with a high emissivity coating. The determination of the exact emissivity value for the chosen paint is described in section 3.

### 2.2 Conversion from Temperature to Power

To fully comprehend and also for being able to check the camera data, a theoretical relation between the emitted power and temperature is crucial. As we are trying to approach an ideal black body using the high emissivity paint, Planck's law for black body radiation,

$$p(\lambda, T) = \frac{2hc^2}{\lambda^5} \frac{1}{\exp(hc/(\lambda k_B T)) - 1} , \quad (1)$$

can be a good start. The IR camera measures radiation over a range of wavelengths, so we need to integrate this and obtain

$$F(T) = \int_{\lambda_{\min}}^{\lambda_{\max}} \frac{C_1}{\lambda^5} \frac{1}{\exp(C_2/(\lambda T)) - 1} d\lambda . \quad (2)$$

Taking account of reflections of the ambience, we propose the following equation

$$P(T) = \underbrace{\epsilon F(T)}_{\text{emission}} + \underbrace{(1 - \epsilon) F(T_{\text{amb.}})}_{\text{reflection of ambience}} . \quad (3)$$

### 2.3 Comparing Manual and Camera Computations

In the following, we test the accuracy of equation 3 by varying different variables.

#### Different Wavelength Ranges

We are not entirely sure for which range of wavelengths the camera is sensitive. Therefore, we tried different integration bounds, the result of which is displayed in figure 4. Seemingly, the smaller range approximates the camera values better but still not satisfyingly.

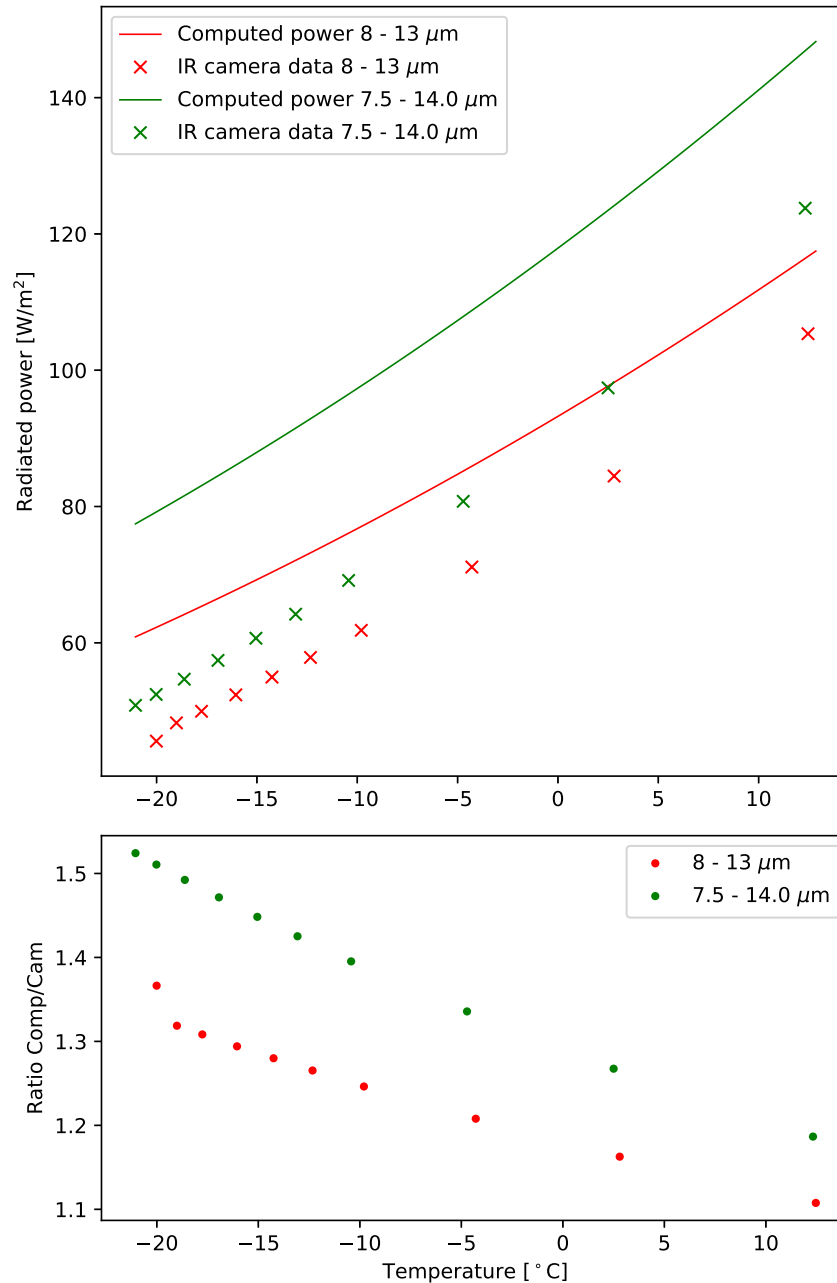


Figure 4: Testing with different wavelength ranges.

## Different Emissivities

Another try is varying the emissivity in the camera as shown in figure 5. The lowest emissivity 0.90 appears to give the best model. Still, we do not want to settle with this result because shape-wise, the curve for  $\epsilon = 1.00$  resembles the camera values most.

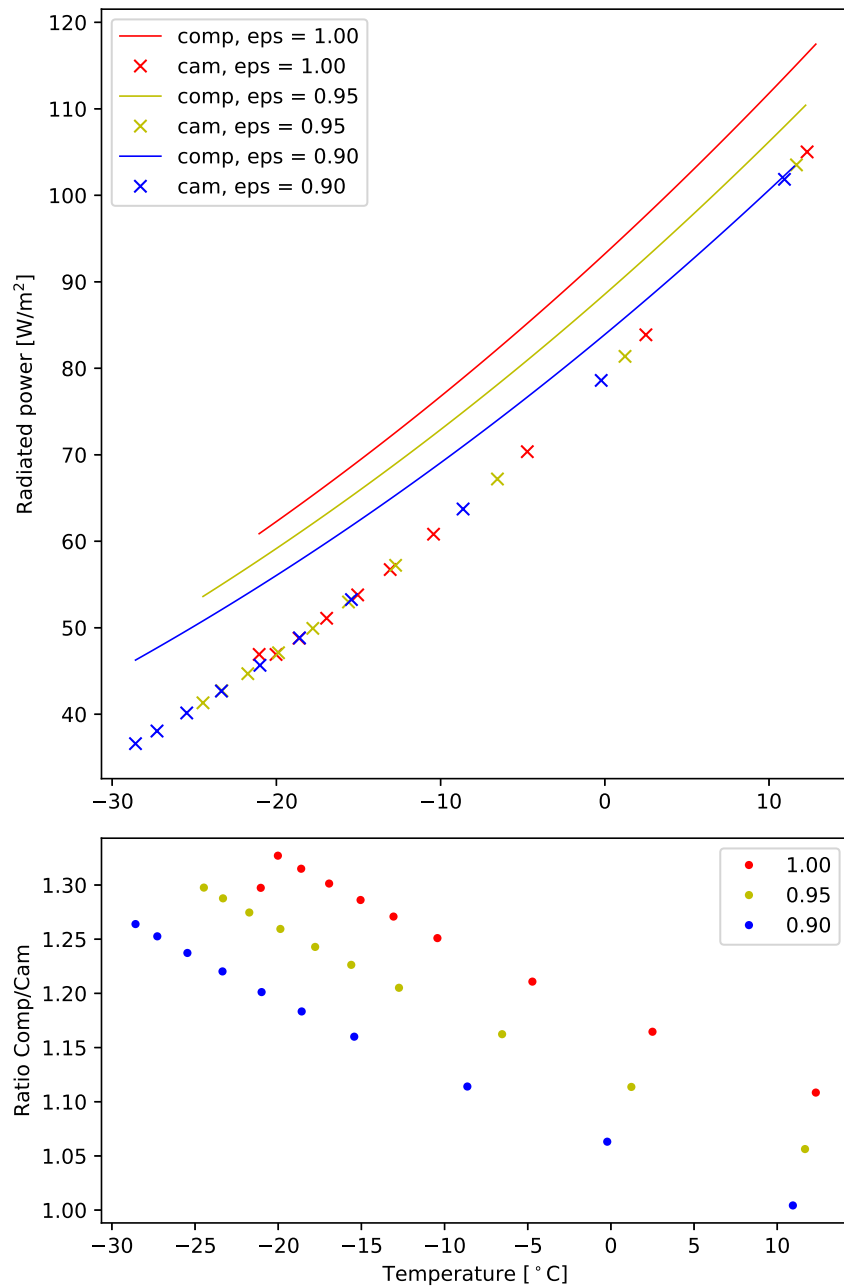


Figure 5: Test with different emissivities.

## Fit with Global Scaling Factor

We also tried fitting the equation to the camera values using a global scaling parameter:

$$P(T) = \tau [\epsilon S(T) + (1 - \epsilon)S(T_{\text{amb}})] . \quad (4)$$

In figure 6, we see the fit obtained with the built in function `curve_fit` of the `python` package `scipy.optimize`. Looking at the plot, one intuitively remarks that this does not seem to be the best fit. Interestingly, this computational deviation is not reflected by extremely high uncertainties:

$$\tau_{1.00} = 0.821 \pm 0.018 ,$$

$$\tau_{0.95} = 0.856 \pm 0.021 ,$$

$$\tau_{0.90} = 0.896 \pm 0.024 .$$

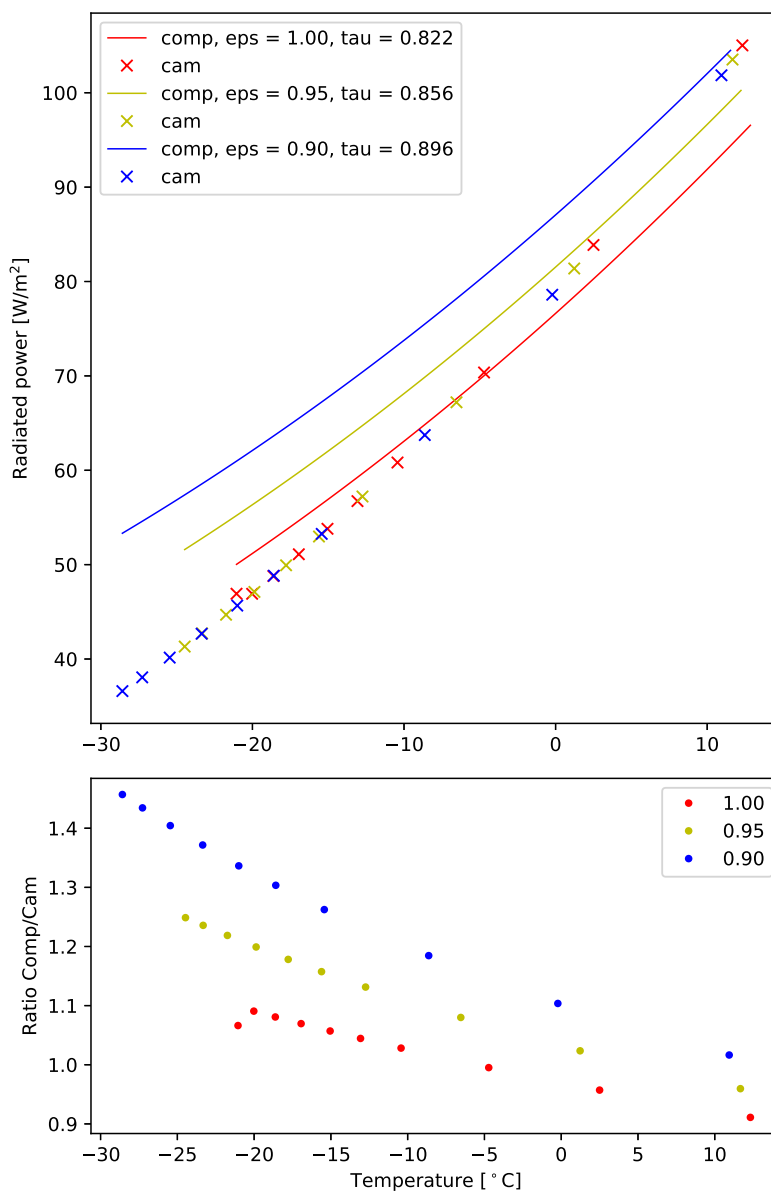


Figure 6: Fitting the function to the camera values using a global scaling factor.



### 3 Emissivity Measurements

This section treats the determination of the emissivity of the paint. To do so, we need the paint to be next to a surface of known emissivity. We use high emissivity tape with  $\epsilon_T = 0.95$ . In terms of equation (3), we can then write

$$\begin{aligned} P_P &= \epsilon_P F(T_P) + (1 - \epsilon_P) F(T_{\text{amb}}) \quad \text{for the paint,} \\ P_T &= \epsilon_T F(T_T) + (1 - \epsilon_T) F(T_{\text{amb}}) \quad \text{for the tape.} \end{aligned}$$

Assuming that both areas have the same real temperature because of their proximity and therefore emit the same amount of IR radiation, we set  $P_P = P_T$ . After rearranging, we obtain an equation for the emissivity of the paint

$$\epsilon_P = \epsilon_T \frac{F(T_T) - F(T_{\text{amb}})}{F(T_P) - F(T_{\text{amb}})} . \quad (5)$$

In the following, we first describe the used set-up for measuring the emissivity of the paint and afterwards analyse the obtained data.

#### 3.1 Set-Up

As the petal will later be used at temperatures below  $0^\circ\text{C}$ , the thermal performance tests need to be adapted to low temperatures too. Therefore, we measure the emissivity of the paint on the cold side of a Peltier element. Actually, we use two Peltier elements next to each other covered by aluminium plates on the both sides. For simplicity, we shall refer to this combination of Peltier elements as 'the Peltier'. Figure 7 shows its cold side with the tape and paint. Additionally, we measure the surface temperature with pt100s. These values are a reference to the IR measurements and to control the Peltier. We calculate the emissivity with the IR data to guarantee comparability with the petal measurements which due to practical reasons cannot be done by pt100s all over the petal.

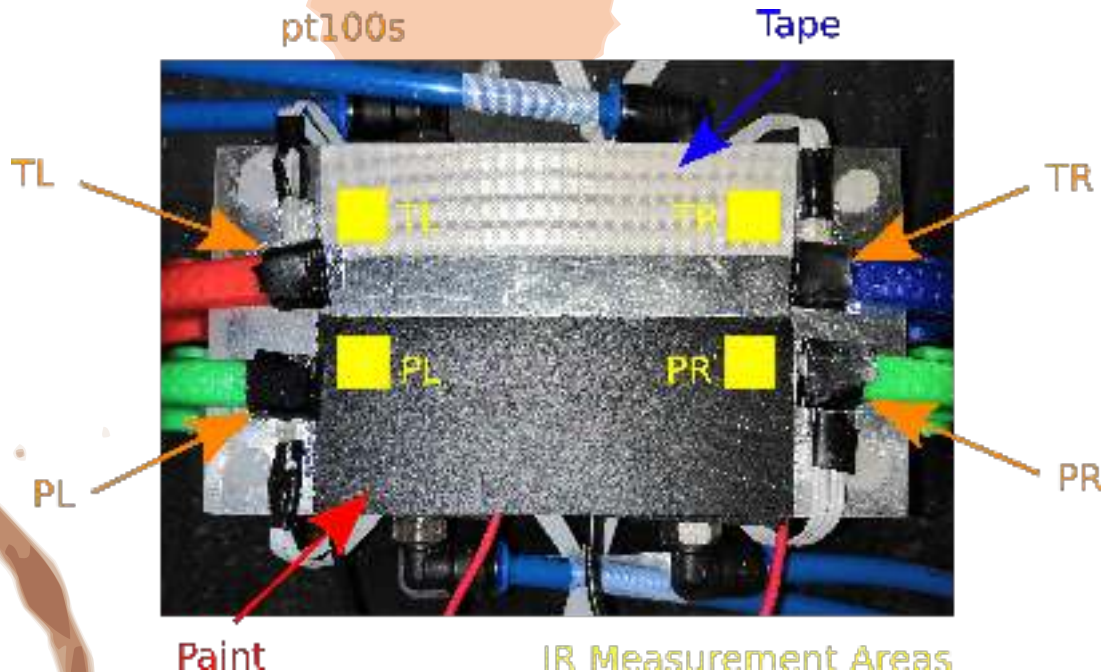


Figure 7: Peltier element used for measuring the emissivity of the paint. We see the cold side with a taped and a painted area. There are also for thermocouples (type: pt100) which are named according to their position (e.g. TL means tape left). Additionally there is an IR camera measurement area next to each of the thermocouples.

To ensure a low humidity to avoid ice formation, the Peltier sits in a cardboard box with dry air flushing that only leaves a hole for the camera lens. Furthermore to secure an optimal cooling of the Peltier, we cool

its warm side using a chiller.

To gather the needed data, we run a current through the Peltier and wait some minutes until the pt100s and the voltage stabilise. Then we note the pt100 values as well as the temperature and radiance power for the four measurement areas as computed by the software. Additionally, we measure the ambient temperature and relative humidity in the box. We stop the measurement when the Peltier stops cooling efficiently (no stable minimum) or when ice forms on the Peltier.

We ran this routine three times trying to lower the humidity. Using humidity pearls worked well. Covering the inside walls of the cardboard box with acrylic glas did not lead to any improvement.

### 3.2 Results

Figure 8 shows the results for the emissivity of the paint for all three runs. The values are all quite stable within the runs but vary a lot among them. We have no explanation for this yet.

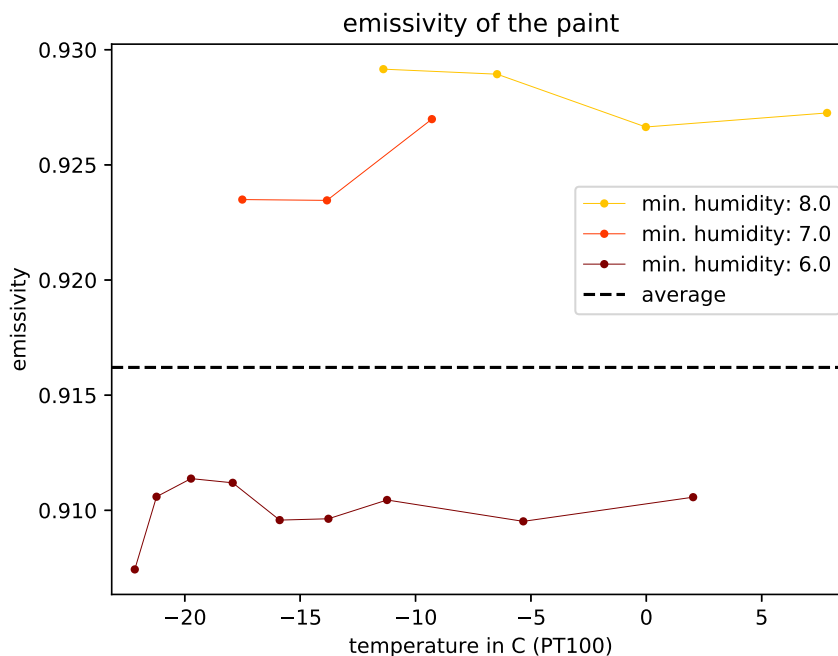


Figure 8: Emissivity values for the three different measurement runs with their absolute average.

Figure 9 displays the difference in temperature between the pt100s and the corresponding IR measurement point taken at the respective emissivity value. For the top and bottom plot this is within an acceptable range, for the middle plot, the deviation reaches 4°C, which is too high.

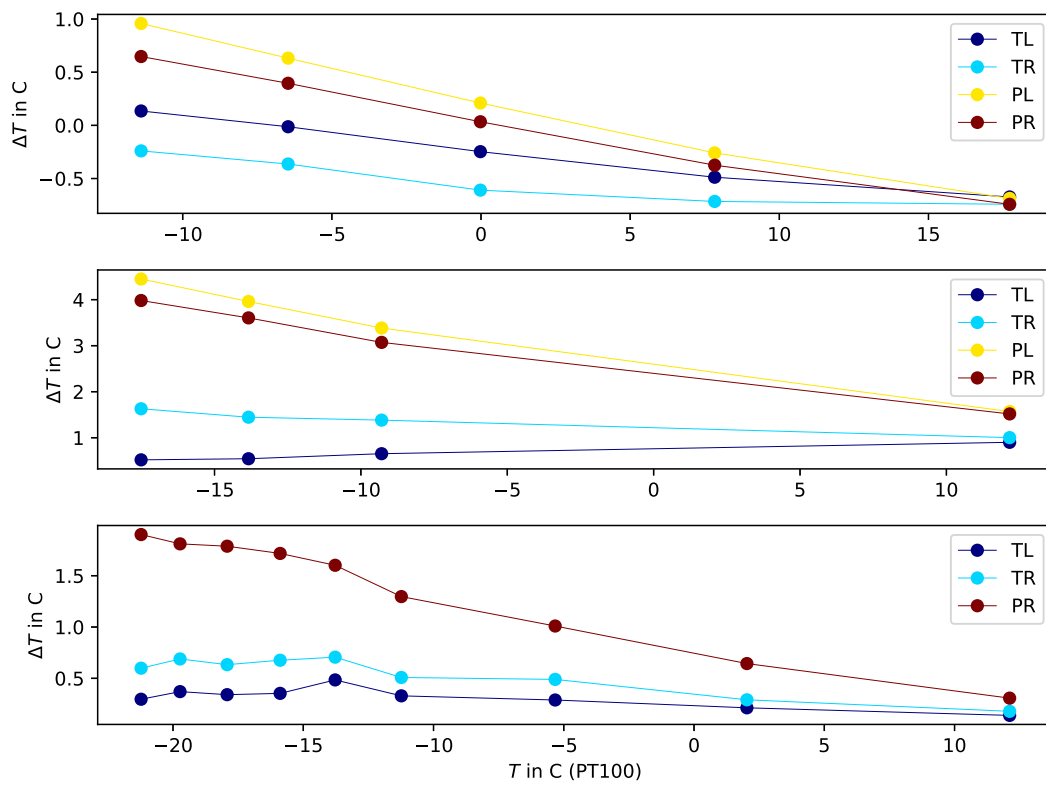


Figure 9: Temperature difference  $\Delta T$  for all available data points in the three different measurement runs (humidity values from top to bottom 0.8, 0.7, 0.6). For the tape the emissivity was set to 0.95. For the paint, the emissivity was set to 0.95 as well in the top and bottom plot, whereas it was set to 0.92 in the middle plot.

## 4 Understanding the Camera Software

When reaching the camera sensor, the IR photons induce a current. The software interprets this signal and displays the corresponding temperature. According to the user's manual, these computations are based on equation (3) (see section 2.2). As described in section 2.2, we are not yet able to reproduce the camera data with it.

To gain confidence in the software nevertheless and intuition for crucial variables in infrared measurements, we conducted studies using the camera software. Figure 10 shows the result. To obtain it, we took one of the thermograms taken during the emissivity measurements described in section 3 and chose one measurement point (paint right). We then manually set different ambient temperatures and varied for each of them the emissivity, keeping all other variables constant. In brief, the plot shows the dependence of the object temperature on ambient temperature and emissivity.

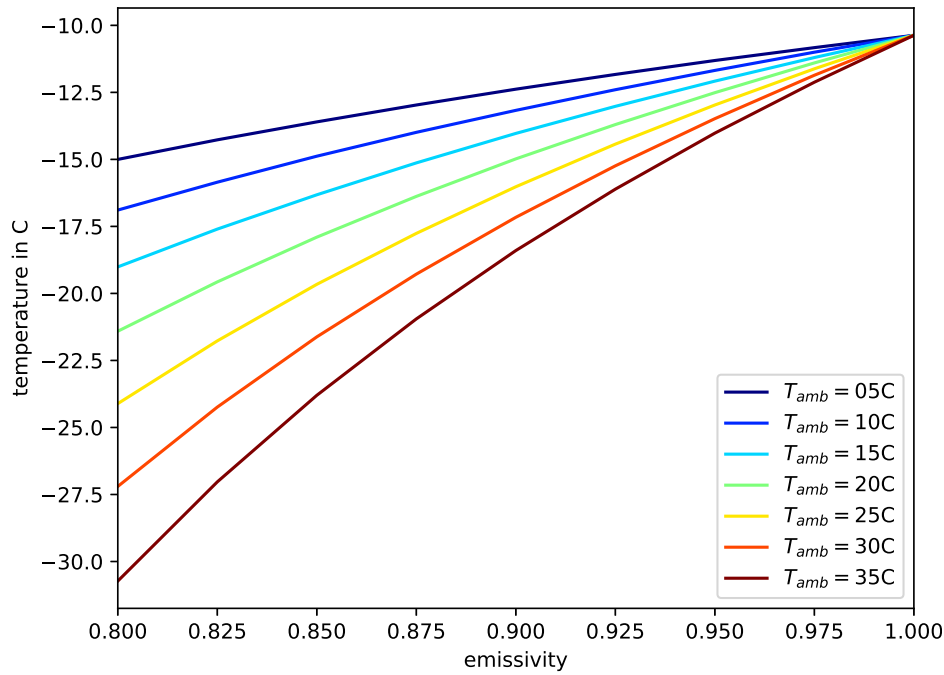


Figure 10: Object temperature on the paint for different emissivities and ambient temperatures computed by the software.

Figure 11 shows the same plot using the same thermogram but using tape right as measurement point. As pointed out by the red dotted line, the emissivity for this measurement with real  $T_{\text{amb}} = 21.9^\circ\text{C}$  and real surface temperature  $T_{\text{pt100}} = -11.54^\circ\text{C}$  should roughly be 0.96. This is close but not identical to the manufacturer value of 0.95. Thus, we can trust the measurement reasonably but there is either still some aspect of the measurement we do not understand or a small error in the software we need to determine.

If we go back to the paint, we can use this kind of plot to evaluate the impact of the uncertainty in the emissivity value (see section 3) on the temperature measurement. Figure 12a shows again the dependency of temperature on the paint on ambient temperature and emissivity. Assuming  $T_{\text{amb}} = 20^\circ\text{C}$ , the emissivity range and the following temperature range is being highlighted by the orange dotted lines. More precisely, the emissivity range of  $0.905 \leq \epsilon \leq 0.930$  determined in section 3 leads to a temperature uncertainty of just above  $1^\circ\text{C}$  at a real surface temperature of roughly  $T_{\text{pt100}} = -10^\circ\text{C}$  (see 12a). For colder temperatures around  $T_{\text{pt100}} = -20^\circ\text{C}$ , the following temperature uncertainty rises to  $2^\circ\text{C}$  (see 12b). To accomplish the uncertainty threshold of  $1^\circ\text{C}$  on the temperature measurement in all temperature ranges, we need to restrict the emissivity some more.

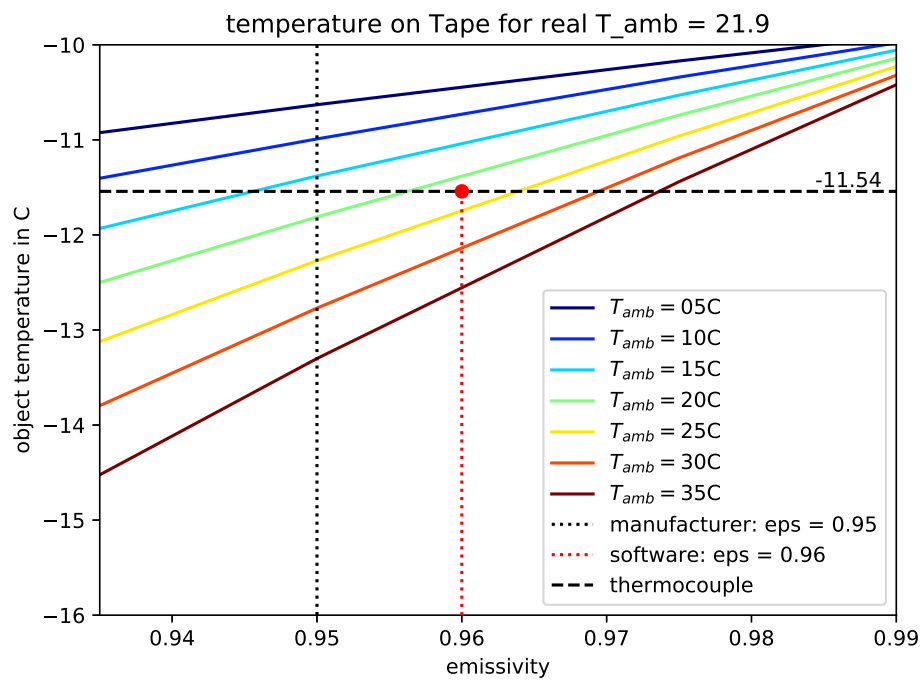
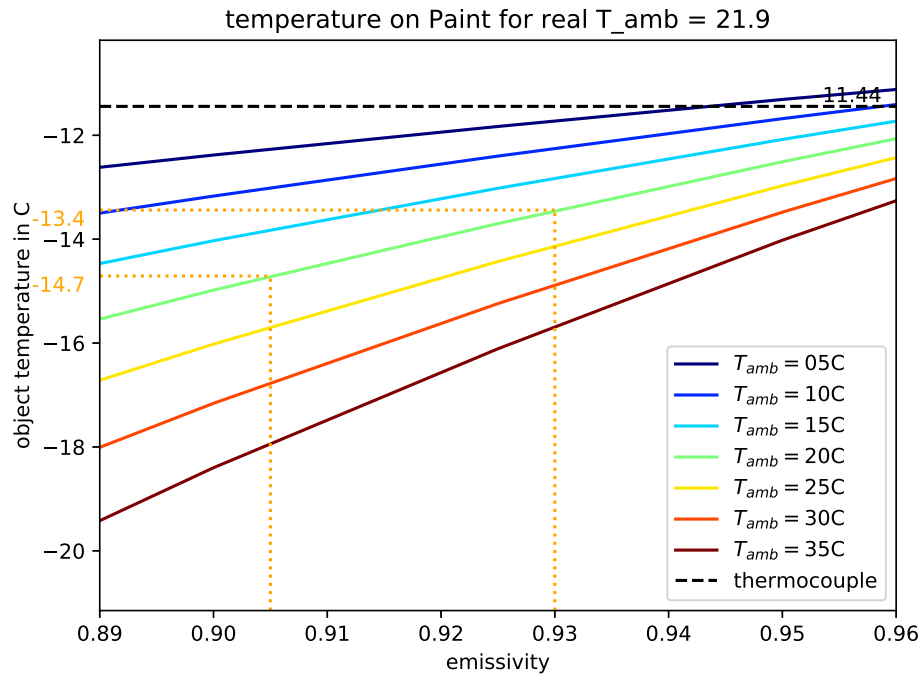
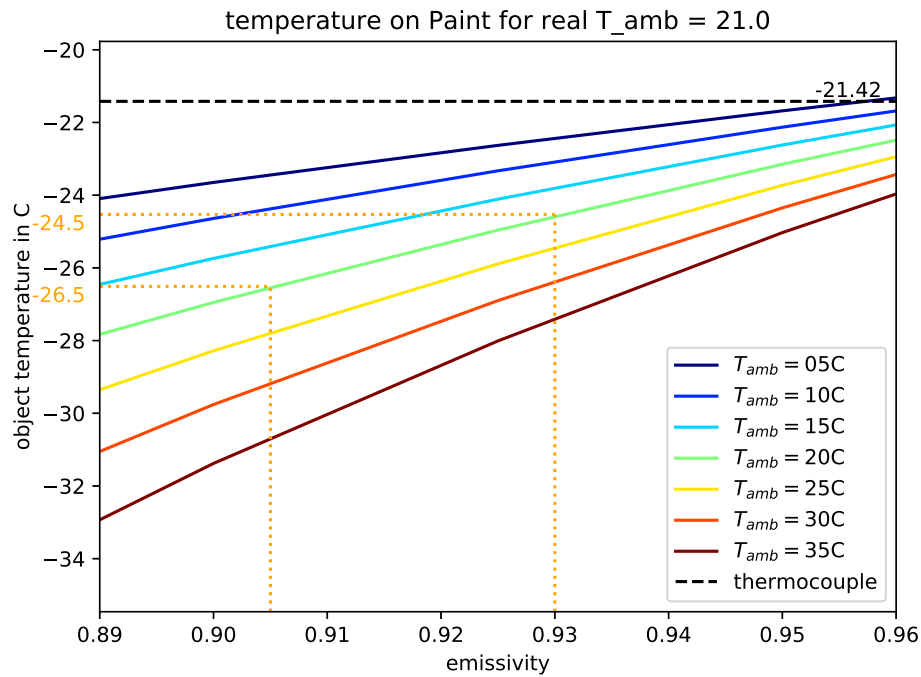


Figure 11: Object temperature on the tape for different emissivities and ambient temperatures computed by the software.



(a)  $T_{\text{pt100}} = -11.44^\circ\text{C}$ .



(b)  $T_{\text{pt100}} = -21.42^\circ\text{C}$ .

Figure 12: Object temperature on the paint for different emissivities and ambient temperatures computed by the software, including a display of the effect of an uncertainty in the emissivity on the temperature for an ambient temperature of  $20^\circ\text{C}$ .



## 5 Tests on the Petal

This section treats the preparation of the petal in the first two subsections and eventually the first results of the thermal performance tests done in late august 2018 in the third subsection.

### 5.1 Last Pre-Study on Gluing pt100s and Paint Emissivity on Si

As outlined in section 2.1, the petal needs to be covered with a high emissivity coating. The chosen paint was examined in section 3. Before the tests could start, we decided to do a last pre-study to check if the paint when sprayed onto Si has the same emissivity as on Aluminium and to check if gluing the pt100s onto Si is as reliable as clamping. The set-up for this test is similar to the one described in 3.1: the same Peltier element sitting in the same cardboard box. The only modifications are on the surface of the Peltier as shown in figure 13.

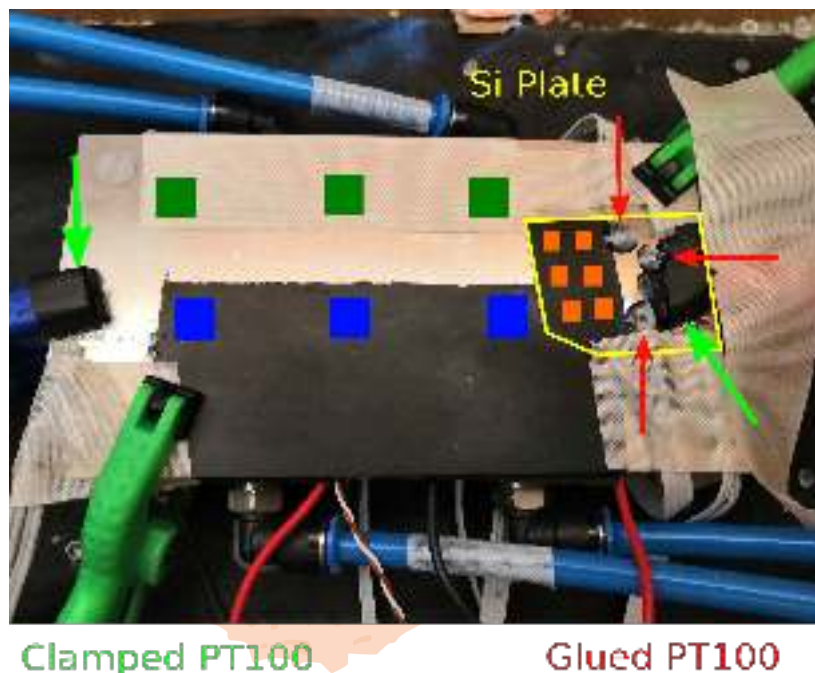


Figure 13: Cold side of the Peltier to test the emissivity of the paint on Si and the reliability of glued pt100s. The Si plate has two parts: one unpainted side with three glued and one clamped pt100, and one painted side with six IR measurement areas. The green and blue squares represent the IR measurement areas on the tape and paint.

#### Reliability of Glued pt100s

Figure 14 compares the temperature measurement of the three glued pt100s and the one clamped pt100s on the Si plate. One of the glued pt100s shows a large deviation whereas the two remaining glued pt100s are rather close to the clamped one. We consider gluing to be a trustworthy measurement overall.

#### Emissivity of the Paint on Si

To obtain an emissivity value for the paint on Si, we use again equation 5, comparing the Si measurement areas with the rightmost tape area. Additionally, we compute again emissivities for the paint on aluminium, comparing each paint area with the closest tape area. Figure 15 shows the resulting emissivities. Notably, the values are relatively stable over a broad temperature range and the values for the paint on aluminium are in the range determined in section 3. We expect to have the same emissivity independent of the underlying material. Unfortunately, the emissivities of the paint on Si are higher than this range. We suspect reflections of the clamps, the glue, and the shiny uncoated part of the Si plate to possibly have caused this result. The grouping of the values for the three left and right Si measurement areas supports this argument.

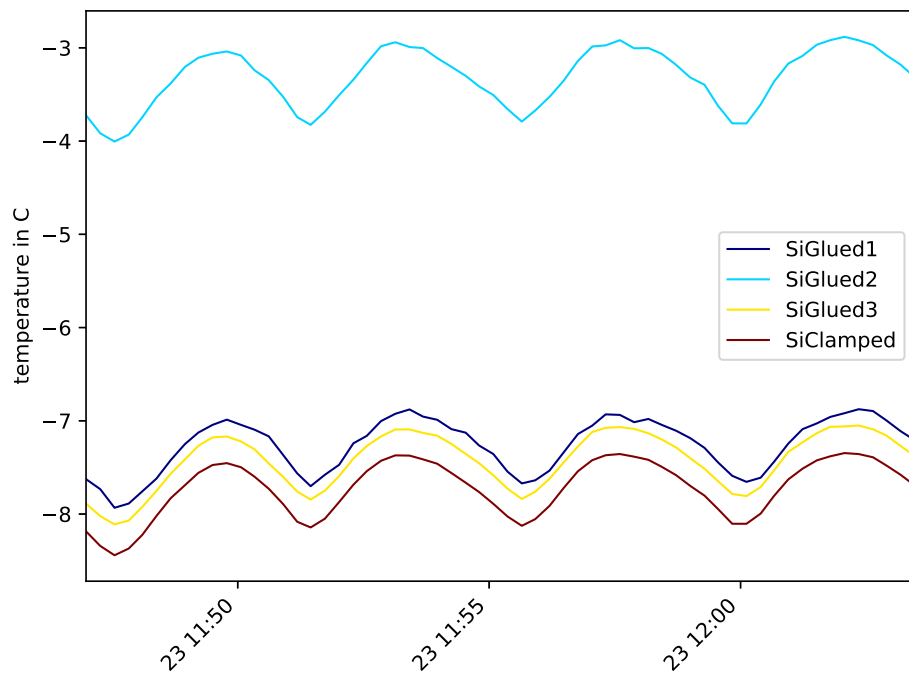


Figure 14: Temperatures as measured by the three glued and the one clamped pt100s on the Si.

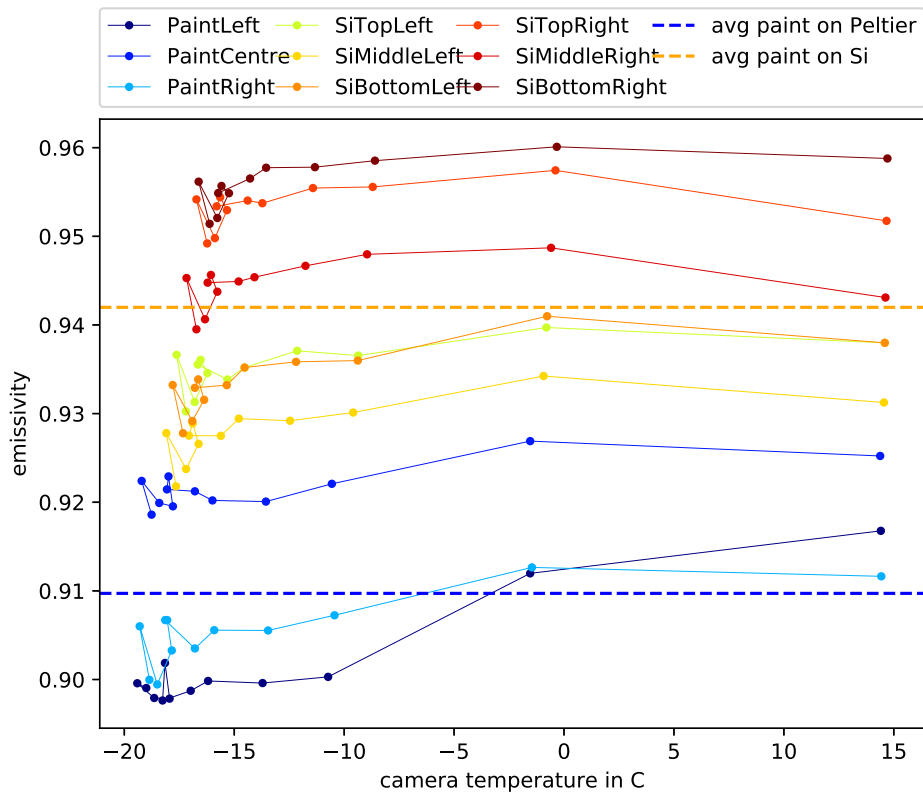


Figure 15: Emissivity values for the paint on the Peltier (aluminium) and paint on the Si plate.

## 5.2 Spraying the Petal

Intuitively, one would spray the paint onto the petal by laying it on a horizontal surface and spraying from above. This would lead the paint to distribute evenly due to gravitational forces and give a sleek layer of paint. However, number one priority in the spraying process is preserving the wirebonds and the electronics in general. Having a big amount of liquid paint on the petal seems to be too risky which is why we choose to apply the paint from a distance while the petal is in a horizontal position. In figure 16, we see the petal before and after the spraying procedure. Figure 17 illustrates the downside of the technique describe above: The paint layer is quite rough and sandy. This does not interfere with the IR measurements given that we cannot observe any Narcissus effect<sup>1</sup>.



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<sup>1</sup>Seeing the reflection of the heat emitted by the IR camera in the thermogram when looking at the surface perpendicularly is called Narcissus effect.



(a) Before



(b) After

Figure 16: Petal before and after applying the paint.



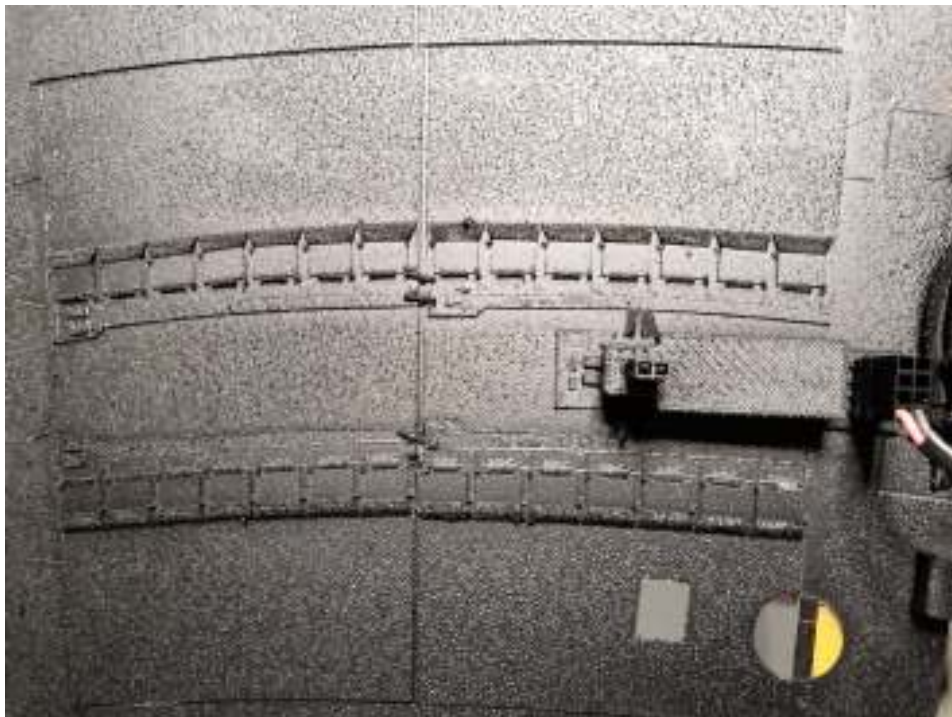
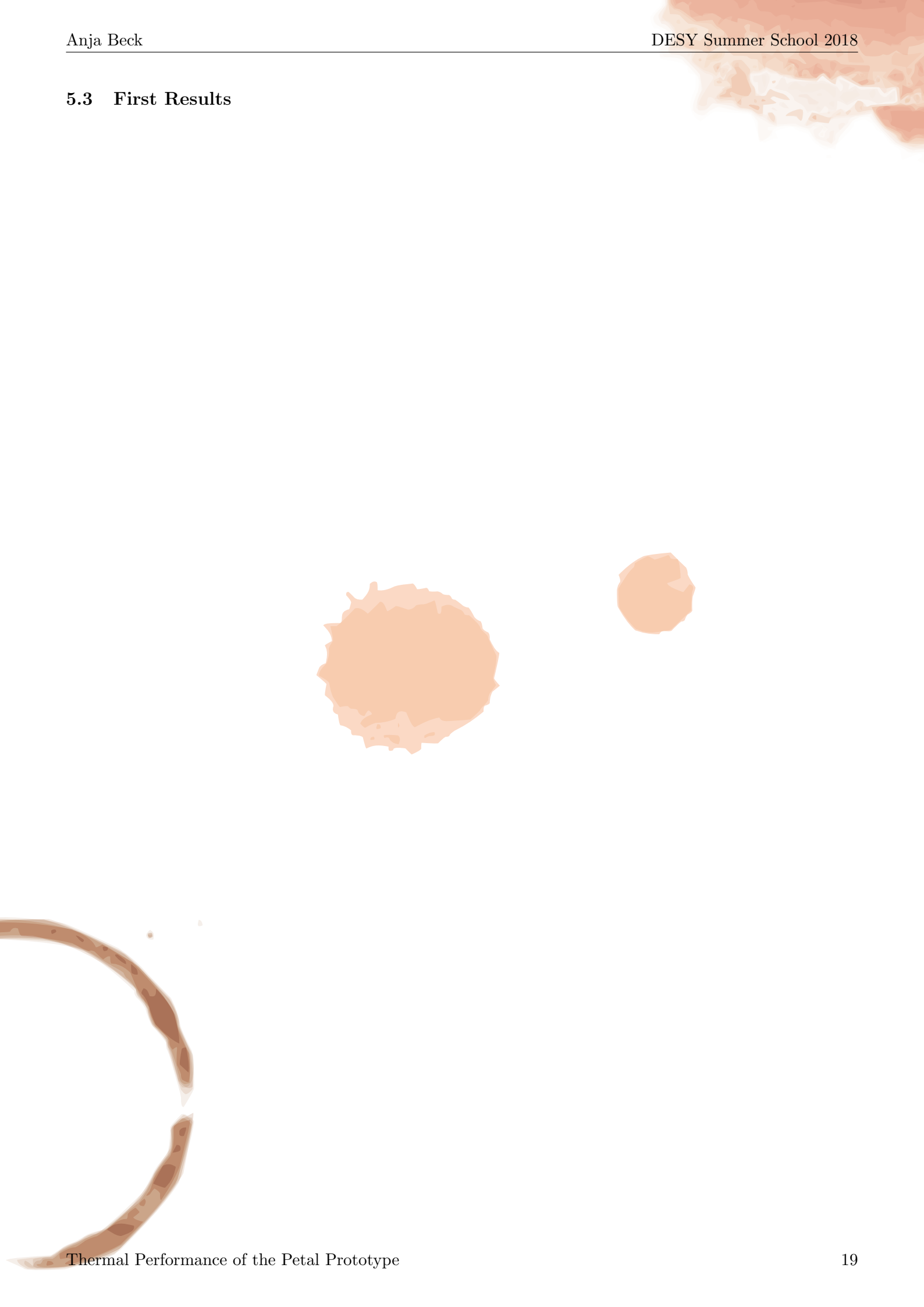


Figure 17: Close up view of the paint structure.

### 5.3 First Results





## 6 Summary and Outlook