Problem 1 (6 points) - Boost converter

In Lab9, we learned a boost converter circuit as shown in Fig.1. For this circuit,

- 1) Find the ratio of T_{on}/T_{off} .
- 2) Find the value of inductance L when $\Delta I_L = 2 \text{mA}$ and $T = 3 \mu \text{s}$.

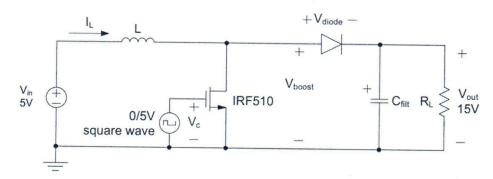


Fig. 1 (a) Boost Converter used in Lab 9.

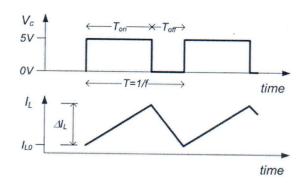


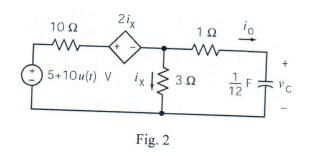
Fig. 1 (b) Timing diagram of the boost converter shown in Fig. 1(a).

Your answer: $V = L \frac{di}{dt} \Rightarrow \Delta i = \frac{1}{L} \cdot 5t$ $\Delta I_{on} = \Delta I_{off}$ $\frac{5V}{L} \cdot T_{on} = \frac{15-5}{L} \cdot T_{off} \Rightarrow \frac{7-M}{T_{off}} = 2iI$ $\frac{5V}{L} \cdot T_{on} = 2mA, \quad T_{on} = \frac{2}{3}T = 2MS$ $L = \frac{5V \cdot 2MS}{2mA} = 5mH$ $\frac{3}{3} + 3 = 6$

Problem 2 (20 points) - First-order circuit analysis

You must show your work to get full credit.

Determine the current $i_o(t)$ in the circuit shown in Fig. 2.



Your answer:

Consider the circuit for time t < 0.

Step 1: Determine the initial capacitor voltage.

The circuit will be at steady state before the source voltage changes abruptly at time t = 0.

The source voltage will be 5 V, a constant.

The capacitor will act like an open circuit.

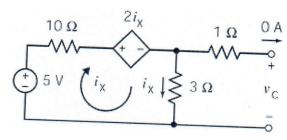
Apply KVL to the mesh to get:

$$(10+2+3)i_x-5=0 \implies i_x=\frac{1}{3}$$
 A

Then

$$v_{\rm C}(0) = 3i_{\rm x} = 1 \text{ V}$$

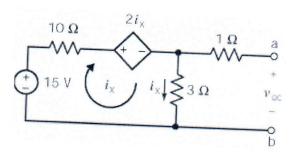
t < 0, at steady state:





Consider the circuit for time t > 0.

Step 2. The circuit will not be at steady state immediately after the source voltage changes abruptly at time t=0. Determine the Thevenin equivalent circuit for the part of the circuit connected to the capacitor. First, determine the open circuit voltage, v_{oc} :



Next, determine the short circuit current, i_{sc} :

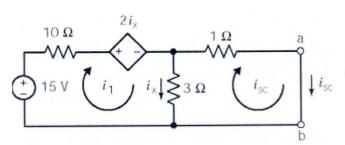
Apply KVL to the mesh to get:

$$(10+2+3)i_x-15=0 \implies i_x=1 \text{ A}$$

Then

$$v_{\text{oc}} = 3 i_x = 3 \text{ V}$$

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Express the controlling current of the CCVS in terms of the mesh currents:

$$i_{\rm x} = i_1 - i_{\rm s}$$

The mesh equations are

$$10 i_1 + 2(i_1 - i_{sc}) + 3(i_1 - i_{sc}) - 15 = 0 \implies 15 i_1 - 5 i_{sc} = 15$$
$$i_{sc} - 3(i_1 - i_{sc}) = 0 \implies i_1 = \frac{4}{3} i_{sc}$$

And so

$$15\left(\frac{4}{3}i_{\rm sc}\right) - 5i_{\rm sc} = 15 \quad \Rightarrow \quad i_{\rm sc} = 1 \text{ A}$$

The Thevenin resistance is

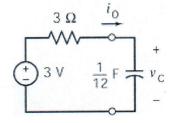


Step 3. The time constant of a first order circuit containing an capacitor is given by

$$\tau = R, C$$

Consequently

$$\tau = R_t C = 3 \left(\frac{1}{12} \right) = 0.25 \text{ s and } a = \frac{1}{\tau} = 4 \frac{1}{\text{s}}$$



Step 4. The capacitor voltage is given by:

$$v_{\rm C}(t) = v_{\rm oc} + (v_{\rm C}(0) - v_{\rm oc})e^{-at} = 3 + (1 - 3)e^{-4t} = 3 - 2e^{-4t}$$
 for $t \ge 0$

Step 5. Express the output current as a function of the source voltage and the capacitor voltage.

$$i_{o}(t) = C \frac{d}{dt} v_{C}(t) = \frac{1}{12} \frac{d}{dt} v_{C}(t)$$

Step 6. The output current is given by

$$i_o(t) = \frac{1}{12} \frac{d}{dt} (3 - 2e^{-4t}) = \frac{1}{12} (-2)(-4)e^{-4t} = \frac{2}{3}e^{-4t} \quad \text{for } t \ge 0$$

Problem 3 (15 points) – Bandstop filter

You must show your work to get full credit.

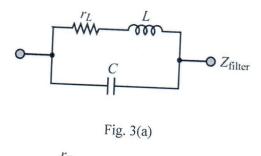
It is very common to see interference caused by the power lines, at a frequency of 60 Hz. This problem outlines the design of a notch filter, shown in Fig. 3(a), to reject a band of frequencies around 60 Hz.

- a) Write the impedance function for the filter of Fig. 3(a) (the resistor r_L represents the internal resistance of
- b) For what value of C will the <u>center frequency</u> of the filter equal 60 Hz if $L = 100 \, mH$ and $r_L = 5\Omega$?
- c) Assume that the filter is used to eliminate the 60-Hz noise from a signal generator with output frequency of 1 kHz in Fig. 3(b). Evaluate the frequency response $V_L(j\omega)/V_{in}(j\omega)$ at both frequencies (60Hz and 1 kHz)

$$V_g(t) = \sin(2\pi 1000t)~\textrm{V}~,~r_g = 50\Omega$$

$$V_n(t) = 3\sin(2\pi 60t) \text{ V}, \ R_L = 300\Omega$$

and if L and C are as in part (b).



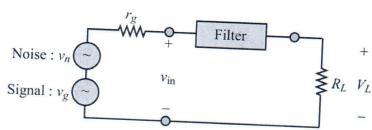


Fig. 3(b)

Your answer:

a)
$$Z_{filter} = (r_L + sL)||\frac{1}{sC} = \frac{1}{\frac{1}{r_L + sL} + sC} = \frac{r_L + sL}{(r_L + sL)sC + 1}, \quad s = j\omega$$

b)
$$\frac{1}{V} = Y = \frac{1}{Z_{filter}} = \frac{1}{r_L + j\omega L} + j\omega C = \frac{r_L}{r_L^2 + \omega^2 L^2} + j(\omega C - \frac{\omega L}{r_L^2 + \omega^2 L^2})$$
At resonance, $\omega_0 C - \frac{\omega_0 L}{r_L^2 + \omega_0^2 L^2} = 0$

Which leads $C = \frac{L}{r_L^2 + \omega_0^2 L^2} = \frac{0.1}{25 + (2\pi * 60)^2 0.1^2} = 7 \times 10^{-5} C.$

L= Cr2+ 20°L2 C

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c)

$$\frac{V_L(j\omega)}{V_{in}(j\omega)} = \frac{R_L}{Z_{filter} + R_L} = \frac{YR_L}{1 + YR_L}.$$

When $\omega = 2\pi 1000$,

$$Y = \frac{5}{25 + (2\pi 1000)^2 0.1^2} + j \left(0.14\pi - \frac{2\pi 1000 \times 0.1}{25 + (2\pi 1000)^2 0.1^2} \right) \approx 0.14\pi j \text{ or } 0.44j$$

Then

$$\frac{V_L(2\pi 1000)}{V_{ln}(2\pi 1000)} = \frac{j132}{1+j132}$$

When $\omega = 2\pi 60$,

$$Y = \frac{5}{25 + (2\pi60)^2 \cdot 0.1^2} = 3.45 \times 10^{-3}$$

Then

$$\frac{V_L(2\pi 1000)}{V_{ln}(2\pi 1000)} = \frac{3.45 \times 10^{-3} \times 300}{1 + 3.45 \times 10^{-3} \times 30} = 0.51.$$

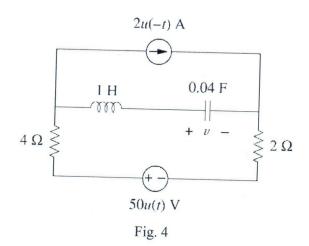
[5=3+5+3+2+2

Problem 4 (33 points) - Second-order circuit analysis

You must show your work to get full credit.

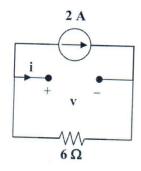
For the circuit in Fig. 4,

- (a) Find the t-domain differential equations for t > 0 and solve for v(t) in time domain.
- (b) Construct the s-domain equivalent circuit for t > 0, then find v(t) in s-domain.



Your answer:

a) For t = 0 –, the equivalent circuit is shown below.



$$i(0-) = 0, v(0-) = -2 \times 6 = -12V$$

For t > 0, we have a series RLC circuit with a step input.

$$\alpha = \frac{R}{2L} = \frac{6}{2} = 3, \quad \omega_0 = \frac{1}{\sqrt{RC}} = \frac{1}{\sqrt{0.04}}, \quad s = -3 \pm \sqrt{9 - 25} = -3 \pm j4$$

$$s + [(A\cos 4t + B\sin 4t)e^{-3t}] \leftarrow (2)$$

Thus, $v(t) = V_{\infty} + [(A\cos 4t + B\sin 4t)e^{-3t}] \leftarrow 2$ where $V_{\infty} = 50V \leftarrow 0$

$$v(t) = 50 + [(A\cos 4t + B\sin 4t)e^{-3t}]$$

$$v(0) = -12 = 50 + A$$
 which gives $A = -62$.

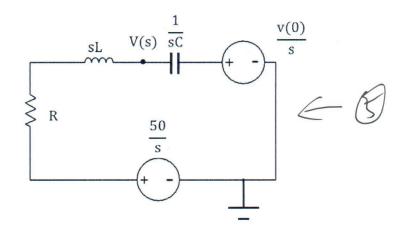
$$i(0) = 0 = C \frac{dv}{dt}|_{t=0}$$

$$\frac{dv}{dt}|_{t=0} = \left[-3(A\cos 4t + B\sin 4t)e^{-3t}\right] + \left[4(-A\sin 4t + B\cos 4t)e^{-3t}\right]|_{t=0} = -3A + 4B = 0$$
Thus $B = -46.5$

$$v(t) = \{50 + [(-62\cos 4t - 46.5\sin 4t)e^{-3t}]\}V \leftarrow (5)$$

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b) In s-domain the equivalent circuit is shown below.



where $R = 6\Omega$, L = 1H, C = 0.04F

$$V(s) = \frac{v(0)}{s} + \frac{\frac{1}{sC}}{R + sL + \frac{1}{sC}} \left[\frac{50}{s} - \frac{v(0)}{s} \right] = -\frac{12}{s} + \frac{1550}{(s^2 + 6s + 25)s}$$

Let $\frac{1}{(s^2+6s+25)s} = F(s)$, so let

$$F(s) = \frac{A}{s} + \frac{B(s+3) + C}{(s+3)^2 + 4^2} = \frac{(A+C)s^2 + (3A+B+6C)s + 25C}{(s^2+6s+25)s} = \frac{1}{(s^2+6s+25)s}$$

So

$$\begin{cases} A + C = 0 \\ 3A + B + 6C = 0 \\ 25C = 1 \end{cases} \xrightarrow{\text{yields}} \begin{cases} A = -\frac{1}{25} \\ B = -\frac{3}{25} \\ C = \frac{1}{25} \end{cases}$$
 2 \chi 3 \tag{7}

So

$$V(s) = -62 \frac{(s+3)+3}{(s+3)^2+4^2} + \frac{50}{s}$$

$$V(t) = \left[-62 \left(e^{-3t} \cos 4t + \frac{3}{4} e^{-3t} \sin 4t \right) + 50 u(t) \right] V$$

$$v(t) = [-62(e^{-5t}\cos 4t + \frac{1}{4}e^{-5t}\sin^2 4t + \frac{1}{4}e^{-5t}\sin^2$$

Problem 5 (26 points) - Fourier series

You must show your work to get full credit.

The transfer function for the narrowband band-pass filter circuit in Fig. 5(a) is

$$H(s) = \frac{-K_0 \beta s}{s^2 + \beta s + \omega_0^2}$$

- a) Find K_0 , β and ω_0^2 as functions of the circuit parameters R_1 , R_2 , R_3 , C_1 and C_2 .
- b) Write the first three terms in the Fourier series that represents v_0 if v_g is the periodic voltage in Fig. 5(b).

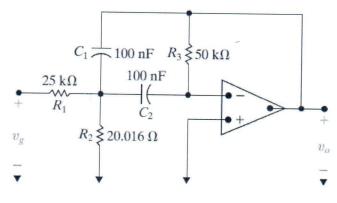


Fig. 5(a)

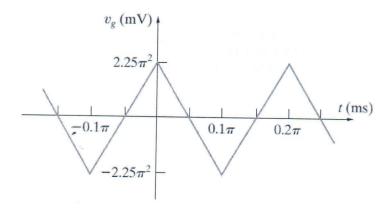


Fig. 5(b)

Your answer:

Let V_a represent the node voltage across R_2 , then the node-voltage equations are

$$\frac{V_a - V_g}{R_1} + \frac{V_a}{R_2} + V_a s C_2 + (V_a - V_0) s C_1 = 0$$

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$$(0 - V_a)sC_2 + \frac{0 - V_o}{R_3} = 0$$

Solving for V_o in terms of V_g yields

$$\frac{V_o}{V_g} = H(s) = \frac{\frac{-1}{R_1 C_1} s}{s^2 + \frac{1}{R_3} \left(\frac{1}{C_1} + \frac{1}{C_2}\right) s + \frac{R_1 + R_2}{R_1 R_2 R_3 C_1 C_2}}$$

It follows that

$$\omega_o^2 = \frac{R_1 + R_2}{R_1 R_2 R_3 C_1 C_2} \ \, \mathcal{E} \ \, \mathcal{O}$$

$$\beta = \frac{1}{R_3} \left(\frac{1}{C_1} + \frac{1}{C_2} \right) \leftarrow \bigcirc$$

Note that

$$H(s) = \frac{-\frac{R_3}{R_1} \left(\frac{C_2}{C_1 + C_2}\right) \frac{1}{R_3} \left(\frac{1}{C_1} + \frac{1}{C_2}\right) s}{s^2 + \frac{1}{R_3} \left(\frac{1}{C_1} + \frac{1}{C_2}\right) s + \left(\frac{R_1 + R_2}{R_1 R_2 R_3 C_1 C_2}\right)}$$

[b] For the given values of
$$R_1, R_2, R_3, C_1$$
, and C_2 we have
$$H(s) = \frac{-400s}{s^2 + 400s + 10^8}$$

$$v_g = \frac{(8)(2.25\pi^2)}{\pi^2} \sum_{n=1,3,5,}^{\infty} \frac{1}{n^2} \cos n\omega_o t$$

$$= 18 \left[\cos \omega_o t + \frac{1}{9} \cos 3\omega_o t + \frac{1}{25} \cos 5\omega_o t + \cdots\right] \text{ mV}$$

$$= \left[18 \cos \omega_o t + 2 \cos 3\omega_o t + 0.72 \cos 5\omega_o t + \cdots\right] \text{ mV}$$

$$\omega_o = \frac{2\pi}{0.2\pi} \times 10^3 = 10^4 \text{ rad/s}$$

$$H(jk10^4) = \frac{-400jk10^4}{10^8 - k^210^8 + j400k10^4} = \frac{-jk}{25(1-k^2) + jk}$$

$$H_1 = -1 = 1/\underline{180^\circ}$$

$$H_3 = \frac{-j3}{-200 + j3} = 0.015/90.86^{\circ}$$

$$H_5 = \frac{-j5}{-600 + j5} = 0.0083/90.48^{\circ}$$

$$v_o = -18\cos\omega_o t + 0.03\cos(3\omega_o t + 90.86^{\circ})$$

$$H_5 = \frac{-j5}{-600 + j5} = 0.0083/90.48^{\circ}$$

$$v_o = -18\cos\omega_o t + 0.03\cos(3\omega_o t + 90.86^\circ)$$

+ $0.006\cos(5\omega_o t + 90.48^\circ) + \cdots \text{ mV}$

- [c] The fundamental frequency component dominates the output, so we expect the quality factor Q to be quite high.
- [d] $\omega_o = 10^4$ rad/s and $\beta = 400$ rad/s. Therefore, Q = 10,000/400 = 25. We expect the output voltage to be dominated by the fundamental frequency component since the bandpass filter is tuned to this frequency!

$$2+2+2+2+2+2+2+3 + 8+1+2+2+3 + 16 = 26$$