

Indian Institute of Technology Gandhinagar



**CL 317 Process Synthesis, Design, and Simulation**

**Interim project report (mid-semester)**

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**Conversion of CO<sub>2</sub> to Methanol**

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## Introduction :

The increasing levels of carbon dioxide (CO<sub>2</sub>) emissions have raised significant concerns about climate change and environmental sustainability. One promising approach to mitigating CO<sub>2</sub> accumulation is its utilization in chemical synthesis, particularly in the production of methanol through CO<sub>2</sub> hydrogenation. Methanol is a valuable chemical feedstock widely used in fuel production, energy storage, and the synthesis of formaldehyde, acetic acid, and other industrial chemicals.

This project focuses on modeling and simulating the methanol production process using Aspen Plus. A critical aspect of this study involves selecting an appropriate thermodynamic model to accurately describe phase equilibria and gas solubilities. The RKSMHV2 model was chosen due to its predictive capability and flexibility, and its performance was compared with other models, including NRTL, NRTL-RK, and Peng-Robinson, by generating Txy and Pxy diagrams.

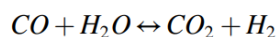
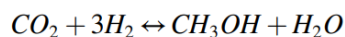
Further, a process flow sheet was developed, incorporating a reactor (RPlug), compressors, and separation units to simulate the methanol synthesis process. The simulation results were analyzed to determine the methanol yield and evaluate the efficiency of different process configurations. This study aims to identify optimal thermodynamic models and process setups that enhance methanol production efficiency while addressing sustainability challenges related to CO<sub>2</sub> utilization.

## System description :

### Scheme 1 :

- The model includes six components: carbon dioxide (CO<sub>2</sub>), hydrogen (H<sub>2</sub>), carbon monoxide (CO), methanol (CH<sub>3</sub>OH), nitrogen (N<sub>2</sub>), and water (H<sub>2</sub>O).
- To account for mixture properties, the RK MHV2 thermodynamic model is applied.

### Reaction :



	Rxn No.	Reaction type	Stoichiometry	Delete
▶	1	Kinetic	CO + 2 H2 --> CH3OH(MIXED)	✗
▶	2	Kinetic	CO2 + H2 --> CO(MIXED) + H2O(MIXED)	✗
▶	3	Kinetic	CO2 + 3 H2 --> CH3OH(MIXED) + H2O(MIXED)	✗

Method used: PENG ROB

## CO<sub>2</sub>-to-Methanol Production Process:

### 1. CO<sub>2</sub> Compression and Mixing with Hydrogen

Carbon dioxide (CO<sub>2</sub>) is compressed using a three-stage compressor to increase its pressure for efficient reaction. The compressed CO<sub>2</sub> is then mixed with hydrogen (H<sub>2</sub>) to form a reactant mixture in the desired stoichiometric ratio for methanol synthesis.

### 2. Heating and Reactor Stage

The CO<sub>2</sub>-H<sub>2</sub> mixture is heated to the required temperature for methanol synthesis. The heated gas is fed into an RPlug reactor, where the reaction occurs.

	Rxn No.	Reaction type	Stoichiometry	Delete
▶	1	Kinetic	CO + 2 H <sub>2</sub> --> CH <sub>3</sub> OH(MIXED)	✗
▶	2	Kinetic	CO <sub>2</sub> + H <sub>2</sub> --> CO(MIXED) + H <sub>2</sub> O(MIXED)	✗
▶	3	Kinetic	CO <sub>2</sub> + 3 H <sub>2</sub> --> CH <sub>3</sub> OH(MIXED) + H <sub>2</sub> O(MIXED)	✗

Inside the reactor, methanol and water are formed as products, along with some unreacted gases.

### 3. Cooling and Pressure Reduction

The reactor's product stream is cooled to condense methanol and water while keeping unreacted gases in vapor form. The pressure is reduced using a control valve, preparing the stream for separation.

### 4. Flash Separation

- The cooled stream undergoes further chilling to reach a lower temperature, enhancing phase separation.
- It enters a flash separator, where the mixture is split:
- 30% of the contents (mainly unreacted gases) are removed.
- 70% of the vapor is recycled to improve process efficiency.

## 5. Vapor Recompression and Condensation

- The recycled vapor is compressed and converted into liquid form.
- This liquid is then processed to extract methanol.

## 6. Distillation for Methanol Purification

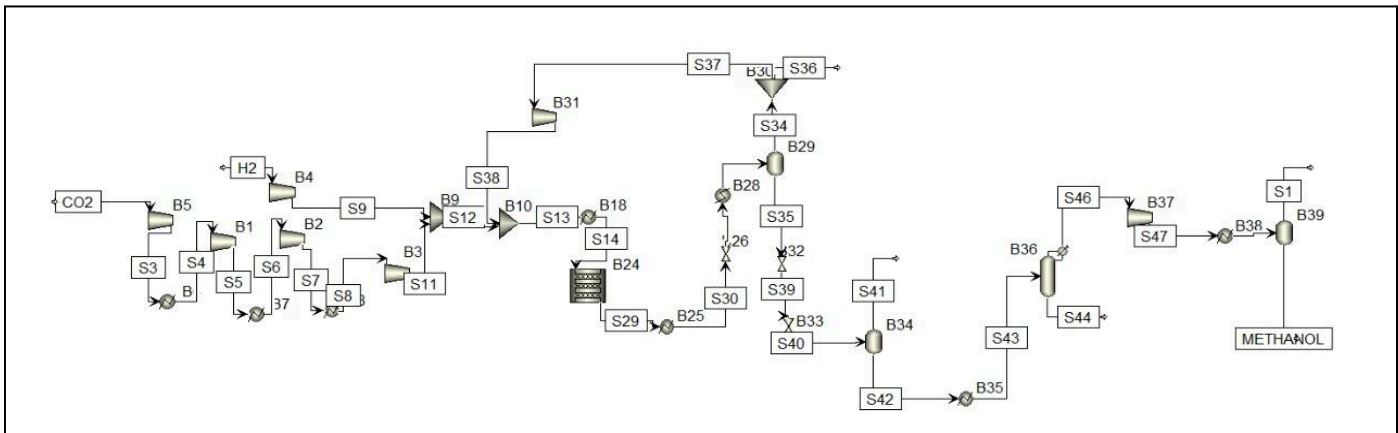
The condensed liquid is sent to a distillation column where Methanol is obtained as the distillate and water and other impurities are removed as bottoms.

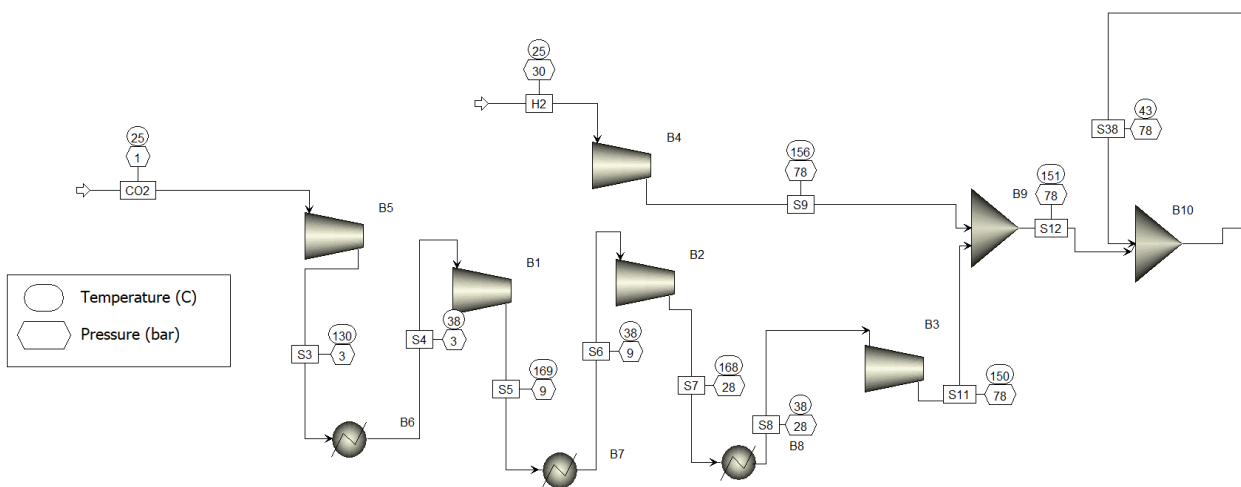
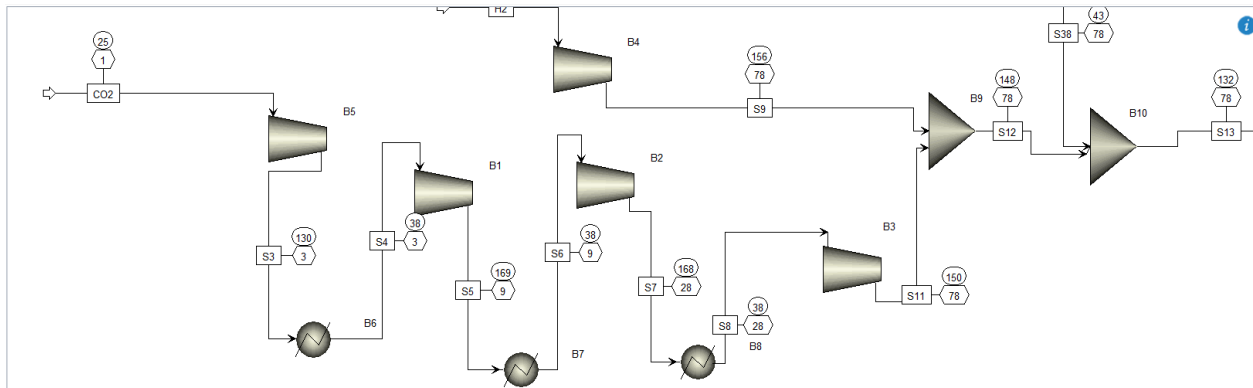
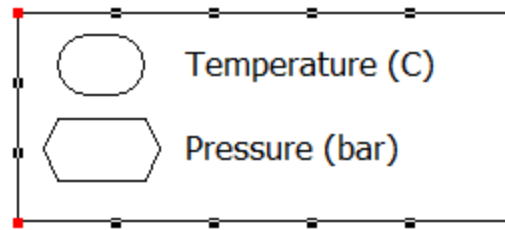
## 7. Final Methanol Compression

The methanol vapor is compressed to obtain liquid methanol, which is the final product ready for storage or further use.

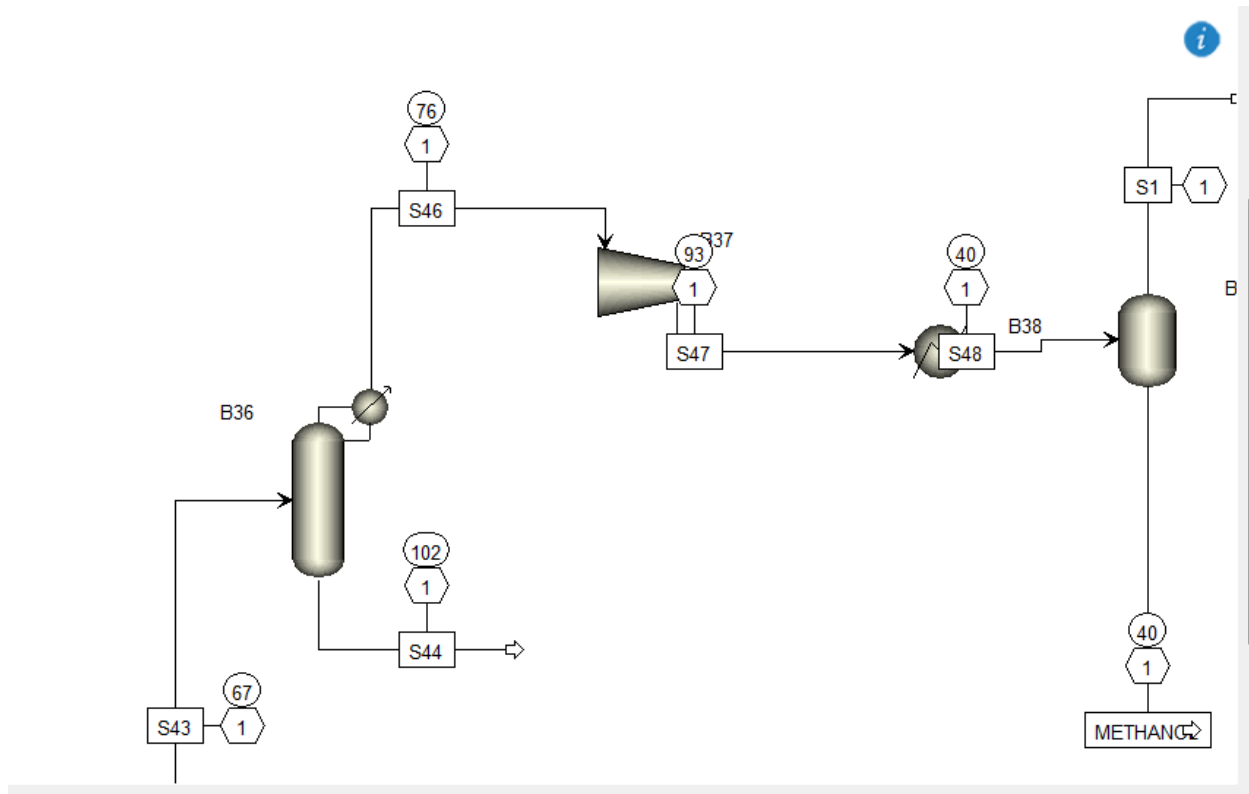
## Methodology :

### Flowsheet designed :









## PARAMETERS FOR FEED:

Main Flowsheet **CO2 (MATERIAL)**

☒ Mixed ☐ CI Solid ☐ NC Solid ☐ Flash Options ☐ EO Options ☐ Costing ☐ Comments

Specifications

Flash Type: **Temperature** **Pressure**

State variables

Temperature: **25** **C**

Pressure: **1** **bar**

Vapor fraction:

Total flow basis: **Mole**

Total flow rate: **2500** **kmol/hr**

Solvent:

Reference Temperature

Volume flow reference temperature: **C**

Component concentration reference temperature: **C**

Composition

Mole-Frac

Component	Value
CO	<b>0.3</b>
CO2	<b>0.7</b>
H2O	<b>0</b>
CH3OH	<b>0</b>
H2	<b>0</b>

Total: **1**

Component Attributes

Particle Size Distribution

Main Flowsheet × H2 (MATERIAL) × +

Mixed CI Solid NC Solid Flash Options EO Options Costing Comments

Specifications

Flash Type **Temperature** **Pressure**

State variables

Temperature **25** **C**

Pressure **30** **bar**

Vapor fraction

Total flow basis **Mass**

Total flow rate **15000** **kg/hr**

Solvent

Reference Temperature

Volume flow reference temperature

Component concentration reference temperature

Composition

**Mass-Frac**

Component	Value
CO	0
CO2	0
H2O	0
CH3OH	0
H2	1

Total 1

Component Attributes

Particle Size Distribution

Methods × +

Global Flowsheet Sections Referenced Comments

Property methods & options

Method filter **CHEMICAL**

Base method **PENG-ROB**

Henry components

Petroleum calculation options

Free-water method **STEAM-TA**

Water solubility **3**

Electrolyte calculation options

Chemistry ID

☒ Use true components

Method name **PENG-ROB** Methods Assistant...

☐ Modify

EOS **ESPRSTD**

Data set **1**

Liquid gamma

Data set

Liquid molar enthalpy **HLMX106**

Liquid molar volume **VLMX20**

☐ Heat of mixing

☐ Poynting correction

☐ Use liquid reference state enthalpy

## Preliminary results :

Results obtained :



We can see the molar flow rates, mole fractions, mass flow rates, temperature, etc in the results obtained below :

Flowsheet × B29 (Flash2) × B39 (Flash2) × B38 (Heater) × B37 (Compr) × <b>Results Summary - Streams (All)</b> × Main Flowsheet × B36 (RadFrac) × B35 (Heater) × B34 (Flash2) × +										
Material	Heat	Load	Work	Power	Vol.% Curves	Wt. % Curves	Petroleum	Polymers	Solids	
	Units	CO2	H2	METHANOL	S1	S3	S4	S5	S6	S7
- MIXED Substream										
Phase		Vapor Phase	Vapor Phase	Liquid Phase	Vapor Phase	Vapor Phase	Vapor Phase	Vapor Phase	Vapor Phase	Vapor Phase
Temperature	C	25	25	40	40	130.481	38	169.236	38	
Pressure	bar	1	30	1	1	2.7	2.7	8.8	8.8	
Molar Vapor Fraction		1	1	0	1	1	1	1	1	
Molar Liquid Fraction		0	0	1	0	0	0	0	0	
Molar Solid Fraction		0	0	0	0	0	0	0	0	
Mass Vapor Fraction		1	1	0	1	1	1	1	1	
Mass Liquid Fraction		0	0	1	0	0	0	0	0	
Mass Solid Fraction		0	0	0	0	0	0	0	0	
Molar Enthalpy	cal/mol	-73718.9	6.24324	-60220	-15824.4	-72802.5	-73621.3	-72464	-73663.9	
Mass Enthalpy	cal/gm	-1880.11	3.09703	-2148.78	-1319.05	-1856.73	-1877.62	-1848.1	-1878.7	
Molar Entropy	cal/mol-K	8.10143	-6.74435	-51.3056	-4.88667	8.76045	6.45993	7.22248	4.01232	
Mass Entropy	cal/gm-K	0.206616	-3.34561	-1.83069	-0.40733	0.223424	0.164752	0.1842	0.102329	
Molar Density	mol/cc	4.04779e-05	0.00118784	0.0218496	3.851e-05	8.06438e-05	0.000105194	0.000240208	0.000349144	

Flowsheet × B29 (Flash2) × B39 (Flash2) × B38 (Heater) × B37 (Compr) × <b>Results Summary - Streams (All)</b> × Main Flowsheet × B36 (RadFrac) × B35 (Heater) × B34 (Flash2) × +										
Material	Heat	Load	Work	Power	Vol.% Curves	Wt. % Curves	Petroleum	Polymers	Solids	
	Units	S8	S9	S11	S12	S13	S14	S29	S30	S31
- MIXED Substream										
Phase		Vapor Phase	Vapor Phase	Vapor Phase	Vapor Phase	Vapor Phase	Vapor Phase	Vapor Phase		
Temperature	C	38	156.084	150.384	151.425	136.355	210	284	92	
Pressure	bar	28.3	78	78	78	78	75	75	74	
Molar Vapor Fraction		1	1	1	1	1	1	1	0.384195	
Molar Liquid Fraction		0	0	0	0	0	0	0	0.615805	
Molar Solid Fraction		0	0	0	0	0	0	0	0	
Mass Vapor Fraction		1	1	1	1	1	1	1	0.101395	
Mass Liquid Fraction		0	0	0	0	0	0	0	0.898605	
Mass Solid Fraction		0	0	0	0	0	0	0	0	
Molar Enthalpy	cal/mol	-73807.4	936.797	-72891.3	-17629.9	-15226.1	-14655.7	-30699.8	-37684.8	
Mass Enthalpy	cal/gm	-1882.36	464.709	-1859	-1550.61	-1490.29	-1434.47	-1749.44	-2147.48	
Molar Entropy	cal/mol-K	1.34559	-6.10952	1.96854	-2.96662	-3.41561	-2.05485	-14.3075	-29.8396	
Mass Entropy	cal/gm-K	0.0343176	-3.03069	0.050205	-0.260924	-0.334313	-0.201125	-0.815316	-1.70042	
Molar Density	mol/cc	0.00119453	0.00210593	0.00230729	0.00215961	0.00223572	0.00181995	0.00174801	0.0052646	

Flowsheet × B29 (Flash2) × B39 (Flash2) × B38 (Heater) × B37 (Compr) × <b>Results Summary - Streams (All)</b> × Main Flowsheet × B36 (RadFrac) × B35 (Heater) × B34 (Flash2) × +										
Material	Heat	Load	Work	Power	Vol.% Curves	Wt. % Curves	Petroleum	Polymers	Solids	
	Units	S31	S33	S34	S35	S36	S37	S38	S39	S40
- MIXED Substream										
Phase				Vapor Phase	Liquid Phase	Vapor Phase	Vapor Phase	Vapor Phase		
Temperature	C	91.9807	35	35	35	35	35	42.5796	36.2394	
Pressure	bar	73.6	73.4	73.4	73.4	73.4	73.4	78	10	
Molar Vapor Fraction		0.384336	0.369691	1	0	1	1	1	0.0212589	
Molar Liquid Fraction		0.615664	0.630309	0	1	0	0	0	0.978741	
Molar Solid Fraction		0	0	0	0	0	0	0	0	
Mass Vapor Fraction		0.101512	0.0783246	1	0	1	1	0.999996	0.00387181	
Mass Liquid Fraction		0.898488	0.921675	0	1	0	0	4.37395e-06	0.996128	
Mass Solid Fraction		0	0	0	0	0	0	0	0	
Molar Enthalpy	cal/mol	-37684.8	-38697.6	-1729.44	-60380.2	-1729.44	-1729.44	-1675.02	-60380.2	
Mass Enthalpy	cal/gm	-2147.48	-2205.19	-465.168	-2353.06	-465.168	-465.168	-450.528	-2353.06	
Molar Entropy	cal/mol-K	-29.8346	-32.8385	-6.61597	-48.2186	-6.61597	-6.61597	-6.56754	-47.963	
Mass Entropy	cal/gm-K	-1.70013	-1.87131	-1.7795	-1.87911	-1.7795	-1.7795	-1.76646	-1.86915	
Molar Density	mol/cc	0.00523991	0.0062275	0.00274487	0.0243422	0.00274487	0.00274487	0.00284057	0.0104668	

Material	Heat	Load	Work	Power	Vol.% Curves	Wt. % Curves	Petroleum	Polymers	Solids					
				Units	S7	S8	S9	S11	S12	S13	S14	S29	S	
Phase					Vapor Phase	Vapor Phase	Vapor Phase	Vapor Phase	Vapor Phase	Vapor Phase	Vapor Phase	Vapor Phase		
Temperature					168.312	38	156.084	150.384	151.425	136.355	210	284		
Pressure	bar				28.3	28.3	78	78	78	78	75	75		
Molar Vapor Fraction					1	1	1	1	1	1	1	1		
Molar Liquid Fraction					0	0	0	0	0	0	0	0		
Molar Solid Fraction					0	0	0	0	0	0	0	0		
Mass Vapor Fraction					1	1	1	1	1	1	1	1		
Mass Liquid Fraction					0	0	0	0	0	0	0	0		
Mass Solid Fraction					0	0	0	0	0	0	0	0		
Molar Enthalpy	cal/mol				-72537.3	-73807.4	936.797	-72891.3	-17629.9	-15226.1	-14655.7	-30699.8		
Mass Enthalpy	cal/gm				-1849.97	-1882.36	464.709	-1859	-1550.61	-1490.29	-1434.47	-1749.44		
Molar Entropy	cal/mol-K				4.7542	1.34559	-6.10952	1.96854	-2.96662	-3.41561	-2.05485	-14.3075		
Mass Entropy	cal/gm-K				0.12125	0.0343176	-3.03069	0.050205	-0.260924	-0.334313	-0.201125	-0.815316		
Molar Density	mol/cc				0.000780563	0.00119453	0.00210593	0.00230729	0.00215961	0.00223572	0.00181995	0.00174801		
Mass Density	gm/cc				0.0306059	0.0468374	0.0024553	0.0904689	0.0245541	0.0228419	0.0185941	0.0306747		
Enthalpy Flow	W				5.63731E-07	5.23551E-07	1.6362E-06	5.05168E-07	1.65637E-07	1.65633E-07	1.76167E-07	5.04111E-07		

## Molar flow rate and Mass flow rate :

Material	Heat	Load	Work	Power	Vol.% Curves	Wt. % Curves	Petroleum	Polymers	Solids																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																							
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Capital: \_\_\_USD Utilities: \_\_\_USD/Year Energy Savings: \_\_\_MW (\_\_\_%) Exchangers - Unknown: 0 OK: 0 Risk: 0 CO2e Scope 1 -77014 kg/hr

Flowsheet x B29 (Flash2) x B39 (Flash2) x B38 (Heater) x B37 (Compr) x Results Summary - Streams (All) x Main Flowsheet x B36 (RadFrac) x B35 (Heater) x B34 (Flash2) x

Material	Heat	Load	Work	Power	Vol.% Curves	Wt. % Curves	Petroleum	Polymers	Solids																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																							

Flowsheet x B29 (Flash2) x B39 (Flash2) x B38 (Heater) x B37 (Compr) x Results Summary - Streams (All) x Main Flowsheet x B36 (RadFrac) x B35 (Heater) x B34 (Flash2) x

Material	Heat	Load	Work	Power	Vol.% Curves	Wt. % Curves	Petroleum	Polymers	Solids					
	Units	S30	S31	S33	S34	S35	S36	S37	S38	S				
▶	Mass Density	gm/cc	0.0923852	0.0919519	0.109282	0.0102051	0.624628	0.0102051	0.0102051	0.0105609				
▶	Enthalpy Flow	cal/sec	-7.1333e+07	-7.1333e+07	-7.325e+07	-1.21023e+06	-7.20397e+07	-363070	-847162	-820502				
▶	Average MW		17.5484	17.5484	17.5484	3.71789	25.6603	3.71789	3.71789	3.7179				
▶	— Mole Flows	kmol/hr	6814.38	6814.38	6814.38	2519.21	4295.17	755.764	1763.45	1763.45				
▶	CO	kmol/hr	163.189	163.189	163.189	154.649	8.54048	46.3947	108.254	108.255				
▶	CO2	kmol/hr	0.135414	0.135414	0.135414	0.0894157	0.045998	0.0268247	0.062591	0.062596				
▶	H2O	kmol/hr	1750.85	1750.85	1750.85	1.31882	1749.53	0.395647	0.923177	0.923157				
▶	CH3OH	kmol/hr	2450.65	2450.65	2450.65	8.08754	2442.57	2.42626	5.66128	5.66116				
▶	H2	kmol/hr	2449.55	2449.55	2449.55	2355.07	94.481	706.521	1648.55	1648.54				
▶	— Mole Fractions													
▶	CO		0.0239478	0.0239478	0.0239478	0.0613878	0.00198839	0.0613878	0.0613878	0.0613885				
▶	CO2		1.98718e-05	1.98718e-05	1.98718e-05	3.54935e-05	1.07093e-05	3.54935e-05	3.54935e-05	3.54964e-05				
▶	H2O		0.256935	0.256935	0.256935	0.000523506	0.407326	0.000523506	0.000523506	0.000523496				
▶	CH3OH		0.35963	0.35963	0.35963	0.00321035	0.568678	0.00321035	0.00321035	0.00321028				
▶	H2		0.359468	0.359468	0.359468	0.934843	0.0219971	0.934843	0.934843	0.934843				

		Units	CO2	H2	METHANOL	S1	S3	S4	S5	S6	S7
- Mole Fractions											
CO			0.3	0	3.84611e-06	0	0.3	0.3	0.3	0.3	0.3
CO2			0.7	0	3.13483e-06	0	0.7	0.7	0.7	0.7	0.7
H2O			0	0	0.28413	0	0	0	0	0	0
CH3OH			0	0	0.715847	0	0	0	0	0	0
H2			0	1	1.57025e-05	0	0	0	0	0	0
+ Mass Flows		kg/hr	98025	15000	95930.4		98025	98025	98025	98025	98025
- Mass Fractions											
CO			0.214311	0	3.83982e-06	0	0.214311	0.214311	0.214311	0.214311	0.214311
CO2			0.785689	0	4.91738e-06	0	0.785689	0.785689	0.785689	0.785689	0.785689
H2O			0	0	0.182444	0	0	0	0	0	0
CH3OH			0	0	0.817546	0	0	0	0	0	0
H2			0	1	1.12825e-06	0	0	0	0	0	0
Volume Flow		l/min	1.02919e+06	103968	1995.48		516225	395887	173005	119147	52944.8

Material	Heat	Load	Work	Power	Vol.% Curves	Wt. % Curves	Petroleum	Polymers	Solids						
					Units	S31	S33	S34	S35	S36	S37	S38	S39	S40	
- Mole Fractions															
						0.0239478	0.0239478	0.0613878	0.00198839	0.0613878	0.0613878	0.0613885	0.00198839		
						1.98718e-05	1.98718e-05	3.54935e-05	1.07093e-05	3.54935e-05	3.54935e-05	3.54964e-05	1.07093e-05		
						0.256935	0.256935	0.000523506	0.407326	0.000523506	0.000523506	0.000523496	0.407326		
						0.35963	0.35963	0.00321035	0.568678	0.00321035	0.00321035	0.00321028	0.568678		
						0.359468	0.359468	0.934843	0.0219971	0.934843	0.934843	0.934842	0.0219971		
- Mass Flows						kg/hr	119581	119581	9366.15	110215	2809.85	6556.31	6556.32	110215	
						kg/hr	4571	4571	4331.78	239.222	1299.53	3032.24	3032.27	239.222	
						kg/hr	5.95953	5.95953	3.93517	2.02436	1.18055	2.75462	2.75484	2.02436	
						kg/hr	31542.1	31542.1	23.759	31518.3	7.12769	16.6313	16.6309	31518.3	
						kg/hr	78524.3	78524.3	259.142	78265.1	77.7427	181.4	181.396	78265.1	
						kg/hr	4938	4938	4747.54	190.462	1424.26	3323.28	3323.27	190.462	
+ Mass Fractions															
						l/min	21674.6	18237.3	15296.5	2940.82	4588.95	10707.6	10346.8	6839.38	
+ Vapor Phase															
+ Liquid Phase															

Material	Heat	Load	Work	Power	Vol.% Curves	Wt.% Curves	Petroleum	Polymers	Solids	
		Units	S40	S41	S42	S43	S44	S46	S47	S48
<b>– Mole Fractions</b>										
CO			0.00198839	0.0668898	3.71897e-05	3.71897e-05	1.0795e-173	4.56953e-05	4.56953e-05	4.56953e-05
CO2			1.07093e-05	0.000304024	1.89099e-06	1.89099e-06	8.24577e-136	2.32348e-06	2.32348e-06	2.32348e-06
H2O			0.407326	0.027171	0.418755	0.418755	1	0.285819	0.285819	0.285819
CH3OH			0.568678	0.161652	0.580915	0.580915	2.04895e-37	0.713775	0.713775	0.713775
H2			0.0219971	0.743983	0.000291174	0.000291174	5.92307e-173	0.000357767	0.000357767	0.000357767
<b>– Mass Flows</b>	<b>kg/hr</b>		<b>110215</b>	<b>1135.27</b>	<b>109080</b>	<b>109080</b>	<b>13982.6</b>	<b>95097.2</b>	<b>95097.2</b>	<b>95097.2</b>
CO	kg/hr		239.222	234.879	4.34368	4.34368	2.34687e-169	4.34368	4.34368	4.34368
CO2	kg/hr		2.02436	1.67734	0.34702	0.34702	2.81662e-131	0.34702	0.34702	0.34702
H2O	kg/hr		31518.3	61.3636	31456.9	31456.9	13982.6	17474.3	17474.3	17474.3
CH3OH	kg/hr		78265.1	649.332	77615.8	77615.8	5.09568e-33	77615.8	77615.8	77615.8
H2	kg/hr		190.462	188.015	2.44756	2.44756	9.26743e-170	2.44756	2.44756	2.44756
<b>+ Mass Fractions</b>										
Volume Flow	l/min		46164.7	44832.2	2885.32	4984.61	328.799	1.61619e+06	1.41163e+06	2871.3
<b>+ Vapor Phase</b>										

CONCLUSION FROM ASPEN SIMULATION:

CH3OH	0	0	0.715847
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The final methanol conversion is 0.715847 as shown in the desired methanol stream.

CO	0.3	0	3.84611e-06
CO2	0.7	0	3.13483e-06

The final mole fractions of Carbon monoxide and Carbon dioxide is :  $3.84 \times 10^{-6}$  and  $3.13 \times 10^{-6}$ . The conversion efficiency of CO is 99.96 % and CO2 is 99.99% from these results obtained from Aspen.

## P-x Diagram Analysis for CO<sub>2</sub> Solubility

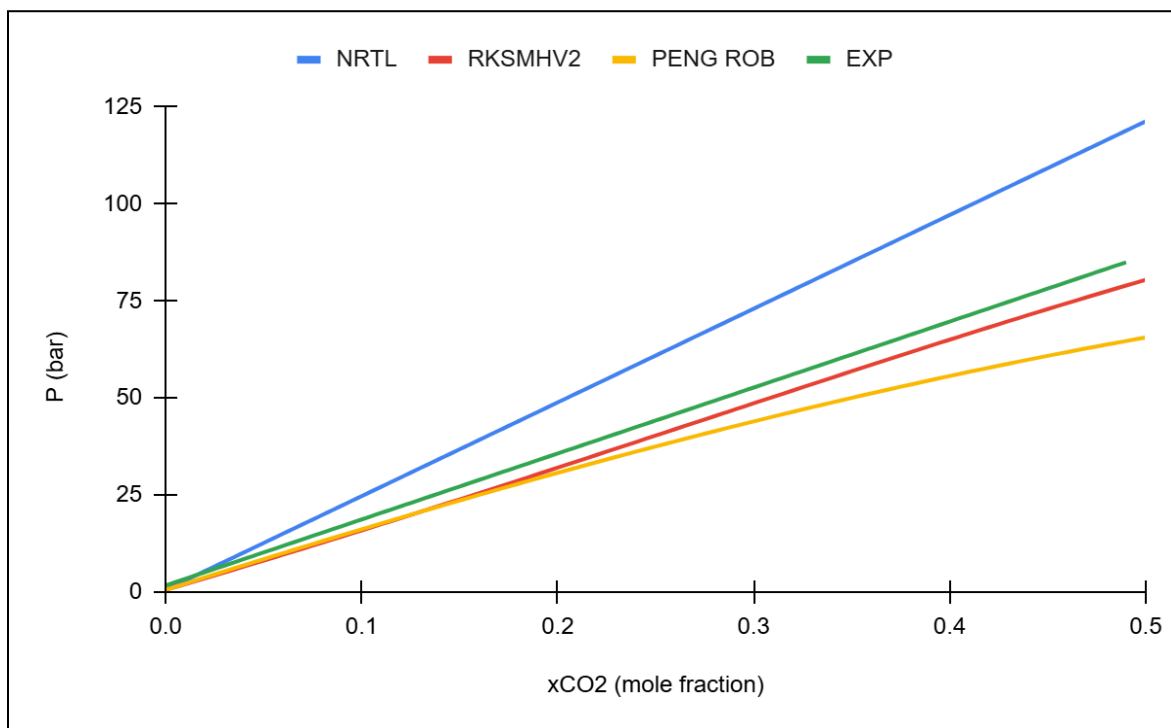


Figure: P-x of CO<sub>2</sub> in CH<sub>3</sub>OH(Methanol) at 323.15K

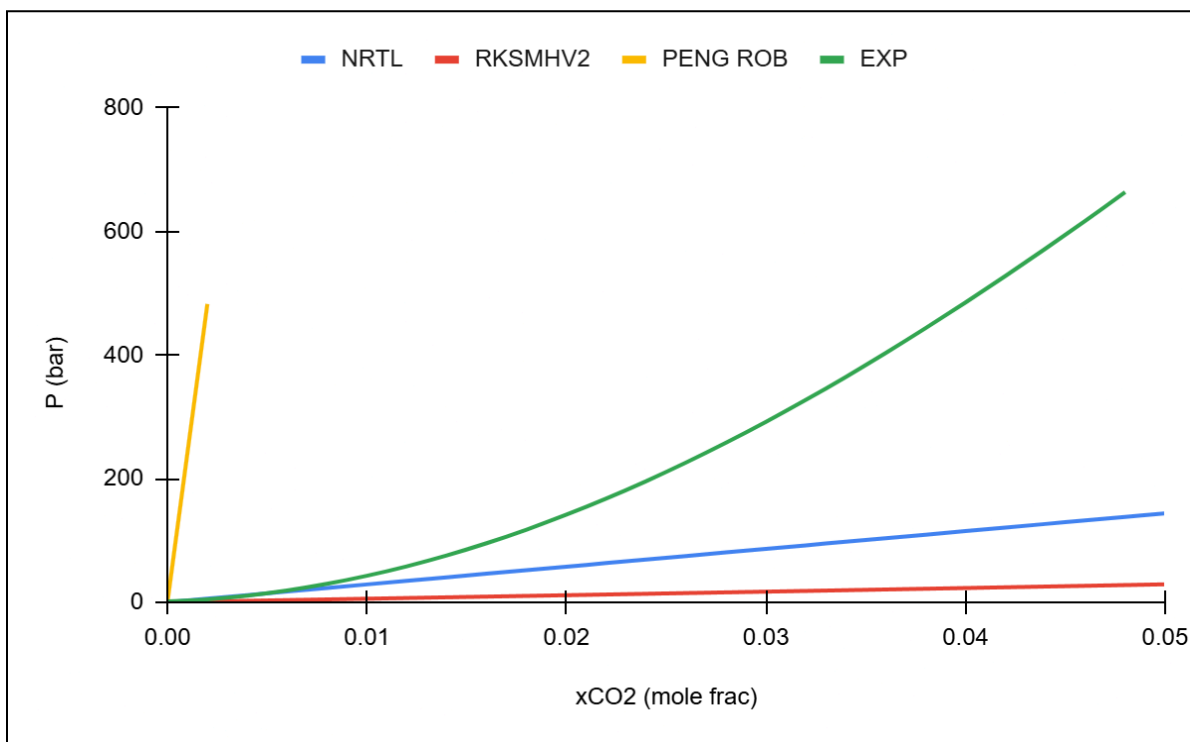


Figure: P-x of CO<sub>2</sub> in H<sub>2</sub>O(water) at 323.15K.

In this study, the solubility of CO<sub>2</sub> in methanol and water was analyzed using three thermodynamic models: **RKSM V2, Peng-Robinson (PR), and NRTL**. The predicted solubilities were compared against experimental data at **323.15 K** to assess the accuracy of these models.

### **Key Observations from P-x Diagrams:**

#### **1. CO<sub>2</sub> Solubility in Methanol:**

- **RKSMHV2** provided the best solubility predictions, with minimal deviations from experimental values.
- **Peng-Robinson (PR)** under-predicted solubility, except for the CO<sub>2</sub>-methanol system, where the results were more accurate.
- **NRTL** produced relatively accurate solubility estimates, particularly when Henry's constants were specified.

#### **2. CO<sub>2</sub> Solubility in Water:**

- **Both RKSMHV2 and NRTL overestimated solubility**, with RX MHV2 showing greater deviation.
- The solubility of CO<sub>2</sub> in water was significantly lower than in methanol, meaning these deviations had minimal impact on process simulation results.
- **PR performed the worst for CO<sub>2</sub>-water predictions**, further confirming its limitations in handling polar systems.

### **Conclusion:**

The analysis of P-x diagrams confirmed that RKSMHV2 is a **suitable thermodynamic model for methanol-based systems**, as it **accurately predicts CO<sub>2</sub> solubility in methanol while maintaining computational efficiency**. Despite its minor overestimation in water, the deviations do not significantly impact the overall process design. The results from this study align with previous literature, reinforcing the choice of RKSMHV2 for reactor and separation unit simulations.

## T-x-y Diagram Analysis for Methanol-Water System

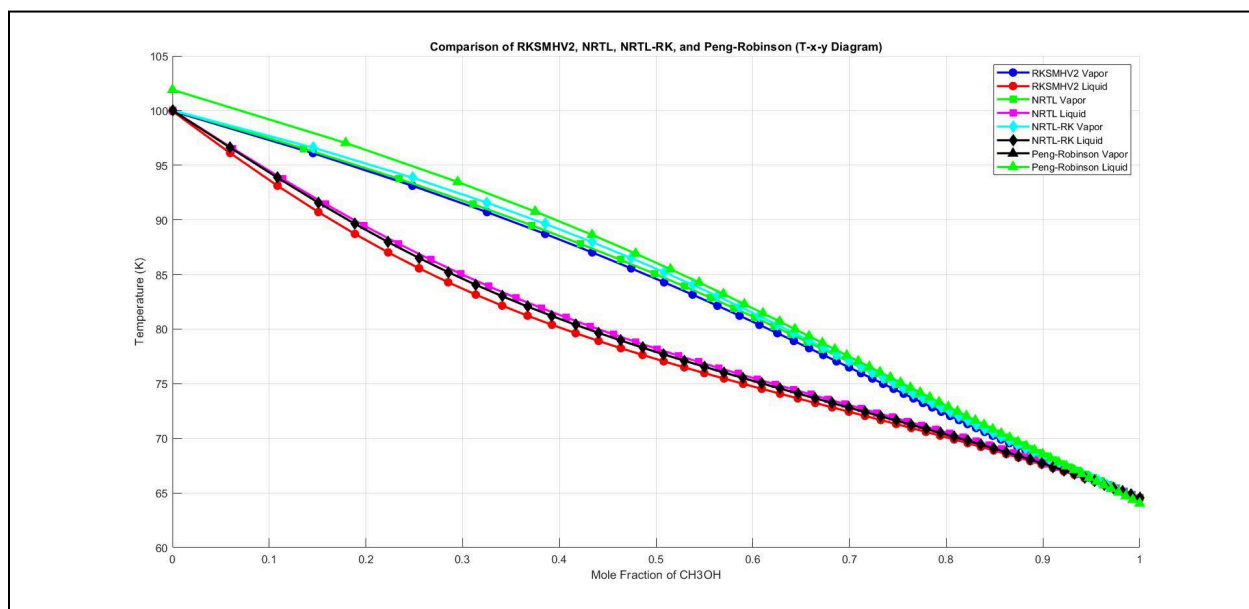


Figure: Comparison of RKSMHV2, NRTL, NRTL-RK, and Peng Robinson(T-x-y diagram).

The phase equilibrium behavior of the methanol-water system was analyzed by generating T-x-y diagrams using four thermodynamic models: RKSMV2, NRTL, NRTL-RK, and Peng-Robinson (PR). The objective was to compare their accuracy in predicting vapor-liquid equilibrium (VLE) and determine the most suitable model for process simulation.

### Key Observations from T-x-y Diagrams:

#### 1. Overall Agreement Between Models:

- The **bubble point** (liquid-to-vapor transition) and **dew point** (vapor-to-liquid transition) curves were closely aligned for all models, confirming their reliability for VLE calculations.
- RKSMHV2, NRTL, and NRTL-RK provided **similar temperature predictions**, with minor deviations in composition regions.
- **Peng-Robinson showed slight deviations** in the vapor phase region, likely due to its cubic equation of state approach.

#### 2. Model-Specific Differences:

- **Bubble Point Temperatures:**
  - RKSMHV2 predicted slightly **lower bubble point temperatures** compared to NRTL models.
  - NRTL and NRTL-RK showed **higher bubble points**, likely due to their explicit treatment of molecular interactions.



- **Dew Point Temperatures:**
  - RKSMHV2 and Peng-Robinson predicted **higher dew point temperatures**, suggesting that equation-of-state models overestimate vapor-phase methanol concentrations.
  - NRTL-based models provided **more accurate liquid-phase equilibrium data** due to their activity coefficient approach.

## Conclusion :

The T-x-y diagram analysis confirms that all models provide reasonable phase equilibrium predictions, with RKSMHV2 emerging as the preferred choice due to its balance between predictive accuracy and computational efficiency. While NRTL-based models offer precise liquid-phase data, RKSMHV2's ability to model polar and non-polar compounds without requiring binary interaction parameters makes it ideal for methanol-water and methanol-hydrogen systems.

This validation ensures that RKSMHV2 can be confidently used for reactor and separation unit simulations in Aspen Plus, supporting accurate process design and optimization.

## Future Work :

For our future work, we plan to implement an optimized dual-stage reactor system that integrates both non-adiabatic and adiabatic reactors to enhance methanol synthesis efficiency. The first-stage non-adiabatic reactor will enable higher conversion at lower temperatures, while the second-stage adiabatic reactor will sustain reaction rates under reduced reactant concentrations.

We also aim to optimize heat recovery by effectively utilizing waste heat to generate steam, minimizing energy deficits, and improving overall process sustainability. This approach will not only enhance conversion efficiency but also reduce operational costs, making the process more economically and environmentally viable.

We also aim to design and develop and develop a flowsheet for the conversion of methanol to formaldehyde.

## References:

(1)Chiou, H.-H.; Lee, C.-J.; Wen, B.-S.; Lin, J.-X.; Chen, C.-L.; Yu, B.-Y. Evaluation of Alternative Processes of Methanol Production from CO<sub>2</sub>: Design, Optimization, Control, Techno-Economic, and Environmental Analysis. *Fuel* 2023, 343, 127856–127856. <https://doi.org/10.1016/j.fuel.2023.127856>.