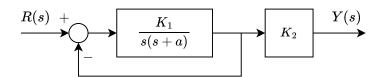
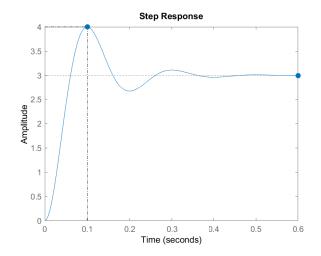
EE160 Homework 2 Solution

1. Consider the following 2nd-order system and its **unit step response**, some performance indices have been given in the figure, determine K_1, K_2 and a, respectively. (9')





Solution. According to the step response, we have

$$\begin{cases} y(\infty) &= 3\\ T_p &= 0.1\\ P.O. &= \frac{4-3}{3} \times 100\% = 33.3\% \end{cases}$$
 (2')

The closed-loop transfer function is

$$\frac{Y(s)}{R(s)} = \frac{K_1 K_2}{s^2 + as + K_1} = K_2 \frac{\omega_n^2}{s^2 + 2\zeta \omega_n s + \omega_n^2} \quad (2')$$

Similarly, we have

$$\begin{cases} T_p &= \frac{\pi}{\omega_n \sqrt{1 - \zeta^2}} = 0.1\\ P.O. &= 100e^{-\zeta \pi / \sqrt{1 - \zeta^2}} = 33.3 \end{cases} \Rightarrow \begin{cases} \zeta &= 0.33\\ \omega_n &= 33.28 \end{cases}$$
 (2'

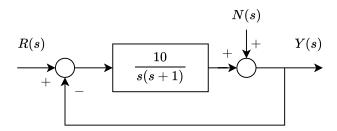
Compared with the coefficients of $\frac{Y(s)}{R(s)}$, we have

$$\begin{cases} K_1 &= \omega_n^2 = 1108 \\ a &= 2\zeta \omega_n = 22 \end{cases}$$
 (2')

Moreover, since we consider the unit step response

$$y(\infty) = \lim_{s \to 0} sY(s) = \lim_{s \to 0} s \cdot \frac{K_1 K_2}{s^2 + as + K_1} \cdot \frac{1}{s} = K_2 = 3$$
 (1')

2. Consider the following 2nd-order system.



(a) When r(t) = 1(t) (unit step signal), n(t) = t, calculate the steady-state error of the system. (6') Solution. According to the block diagram

$$Y(s) = N(s) + [R(s) - Y(s)] \cdot \frac{10}{s(s+1)}$$

$$(1 + \frac{10}{s(s+1)}) \cdot Y(s) = \frac{10}{s(s+1)} \cdot R(s) + N(s) \quad (2')$$

$$Y(s) = \frac{10}{s^2 + s + 10} \cdot R(s) + \frac{s^2 + s}{s^2 + s + 10} \cdot N(s)$$

Based on the definition of error

$$E(s) = R(s) - Y(s)$$

$$= \frac{s^2 + s}{s^2 + s + 10} \cdot R(s) - \frac{s^2 + s}{s^2 + s + 10} \cdot N(s)$$
(2')

By the final value principle,

$$e(\infty) = \lim_{s \to 0} sE(s) = \lim_{s \to 0} s \frac{s^2 + s}{s^2 + s + 10} \left(\frac{1}{s} - \frac{1}{s^2} \right) = -\frac{1}{10}$$
 (2')

(b) When r(t) = 1(t) (unit step signal), n(t) = 0, calculate peak time T_p , settling time T_s and the percent overshoot P.O. of the step response. (7')

Solution. The closed-loop transfer function is

$$\frac{Y(s)}{R(s)} = \frac{10}{s^2 + s + 10} = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$
 (2')

Thus

$$\begin{cases} 2\zeta\omega_n &= 1\\ \omega_n^2 &= 10 \end{cases} \Rightarrow \begin{cases} \zeta &= 0.158\\ \omega_n &= \sqrt{10} \end{cases}$$
 (2')

Peak time and the percent overshoot can be given

$$\begin{cases}
T_p &= \frac{\pi}{\omega_n \sqrt{1-\zeta^2}} = 1.006s \\
T_s &= \frac{4}{\zeta \omega_n} = 8s \\
P.O. &= e^{-\zeta \pi / \sqrt{1-\zeta^2}} \times 100\% = 60.49\%
\end{cases}$$
(3')

- 3. Consider the unity feedback third-order system with open-loop transfer function $G(s) = \frac{1}{s(0.1s+1)(0.5s+1)}$.
 - (a) Calculate the **poles** of the **closed-loop** transfer function. (5') Solution. The closed-loop transfer function is

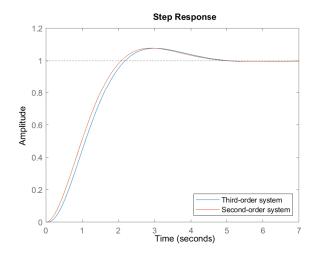
$$T(s) = \frac{G(s)}{1 + G(s)} = \frac{20}{s^3 + 12s^2 + 20s + 20} = \frac{10.24 \cdot 1.954}{(s + 10.24)(s^2 + 1.763s + 1.954)}$$
 (2')

Thus the poles of the closed-loop system are $p_{1,2} = -0.8814 \pm 1.0848j$ and $p_3 = -10.24$. (3')

(b) Determine whether the response of the third-order system can be approximated by the dominant roots of the second-order system. If so, plot the **unit step response** of the **approximated second-order** system and the **original third-order** system on the **same** figure; if not, give your reasons. (7') Solution. Since the real part of the dominant roots is less that one tenth of the real part of the third root, i.e.,

$$\frac{|-0.8814|}{|-10.24|} = 0.086 < \frac{1}{10} \quad (3')$$

Then the response of the third-order system can be approximated by the second-order system. And the step response of the approximated second-order system $T_2(s) = \frac{1.954}{s^2 + 1.763s + 1.954}$ and the original third-order system is given below. (4')



4. Consider two **unity feedback** systems, necessary information of the **open-loop** transfer function has been given in the table.

system type number zeros poles high frequency gain i. 1 -1
$$-4, -1 \pm j$$
 7 ii. 2 $-\frac{1}{2}, -\frac{1}{4}$ $-1 \pm 3j$ 10

(a) Determine the **open-loop** transfer function G(s) of each system. (4') Solution.

i.
$$G(s) = \frac{7(s+1)}{s(s+4)(s^2+2s+2)}$$
 (2')

ii.
$$G(s) = \frac{10(s+\frac{1}{2})(s+\frac{1}{4})}{s^2(s^2+2s+10)}$$
 (2')

(b) Calculate the position error constant K_p , velocity error constant K_v and acceleration error constant K_a of each system, respectively. (6') Solution.

i.

$$K_p = \lim_{s \to 0} G(s) = \infty$$

$$K_v = \lim_{s \to 0} sG(s) = \frac{7}{8} \quad (3')$$

$$K_a = \lim_{s \to 0} s^2 G(s) = 0$$

ii.

$$K_p = \lim_{s \to 0} G(s) = \infty$$

$$K_v = \lim_{s \to 0} sG(s) = \infty$$

$$K_a = \lim_{s \to 0} s^2 G(s) = \frac{1}{8}$$
(3')

(c) Based on the error constants derived in (b), give the steady-state error e_{ss} when the input signal r(t) = 1(t) (unit step signal), r(t) = t and $r(t) = t^2$ of each system, respectively. (6') Solution.

i.

$$r(t) = 1(t) \quad \Rightarrow e_{ss} = \frac{1}{1 + K_p} = 0$$

$$r(t) = t \quad \Rightarrow e_{ss} = \frac{1}{K_v} = \frac{8}{7}$$

$$r(t) = t^2 \quad \Rightarrow e_{ss} = \infty$$

$$(3')$$

ii.

$$r(t) = 1(t)$$
 $\Rightarrow e_{ss} = 0$
 $r(t) = t$ $\Rightarrow e_{ss} = 0$
 $r(t) = t^2$ $\Rightarrow e_{ss} = \frac{2}{K_a} = 16$ (3')

5. Using the Routh-Hurwitz criterion, determine if the system with the following characteristic equation is stable. (10')

(a)
$$s^4 + 2s^3 + s^2 + 2s + 1 = 0$$

(b)
$$s^5 + 8s^4 + 15s^3 + 36s^2 + 42s + 11 = 0$$

Solution.

(a) Unstable

(b) Stable

6. Determine the range of K for a stable system (10')

- (a) a system with a characteristic equation $s^3 + Ks^2 + (1+K)s + 6 = 0$
- (b) A unit negative feedback system with a open-loop transfer function

$$G(s) = \frac{K}{(s+2)(s+3)(s+5)}$$

Solution.

(a)
$$K > 0$$
, $\frac{K(K+1)-6}{K} > 0$, $K > 2$

(b)
$$\frac{K}{s^3+10s^2+31s+K+30}$$
 ,280 > K > -30
$$s^3 \quad 1 \quad 31$$

$$s^2 \quad 10 \quad K+30$$

$$s^1 \quad 28-K/10 \quad 0$$

$$s^0 \quad K+30 \quad 0$$

7. Consider the feedback control system shown in the following Figure. The controller and model transfer functions are given by

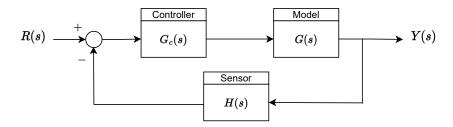
$$G_c(s) = K$$
 and $G(s) = \frac{s+40}{s(s+10)}$

and the sensor transfer function is

$$H(s) = \frac{1}{s+20}$$

.(15')

- (a) Determine the limiting value of gain K for a stable system.
- (b) Let K = 3, determine whether the relative stability of the system is smaller than -1 ($\sigma < -1$).



(a)
$$\frac{K(s^2 + 60s + 800)}{40K + (200 + K)s + 30s^2 + s^3}$$

$$s^3 \quad 1 \quad K + 200$$

$$s^2 \quad 30 \quad 40K$$

$$s^1 \quad 200 - \frac{K}{3} \quad 0$$

$$s^0 \quad 40K \quad 0$$

$$600 > K > 0$$

(b) No.
$$40K + (200 + K)(s - \sigma) + 30(s - \sigma)^2 + (s - \sigma)^3$$
 Let $K = 3, \sigma = 1$
$$s^3 + 27s^2 + 146s - 54$$

$$s^3 + 1 + 146$$

$$s^2 + 27s - 54$$

$$s^1 + 148 + 0$$

$$s^0 + 54 + 0$$

8. Consider a spacecraft attitude control problem. The control system structure is shown below. Suppose we only consider the pitch-axis rotation of the spacecraft, which has a plant transfer function

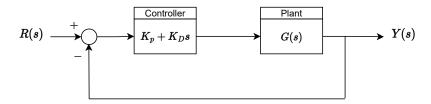
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$$G(s) = \frac{1}{Is^2} + \frac{L/I}{s^2 + 2\zeta\omega s + \omega^2}$$

where $I = 77,076kg/m^2$ is the spacecraft pitch inertia, L = -1.387 the telescope structure gain in the pitch axis, $\omega = 14.068$ rad/s the structure natural frequency, and ζ the passive damping ratio assumed as 0.005. A proportional plus derivative controller is used in the system, where

$$G_c(s) = K_p + K_D s$$

and where $K_p > 0$ and $K_D > 0$. Please give a selection of K_p and K_d via trial and error to stabilize the system and proof the stability. (15')



Solution.

$$G = \frac{D}{N} = \frac{(L+1)s^2 + 2\zeta\omega s + \omega^2}{Is^2(s^2 + 2\zeta\omega s + \omega^2)}$$

$$G_p = \frac{G*G_c}{G*G_c + 1} = \frac{D*G_c}{D*G_c + N}$$

$$D*G_c + N = ((L+1)s^2 + 2\zeta\omega s + \omega^2) * (K_p + K_D s) + Is^2(s^2 + 2\zeta\omega s + \omega^2)$$

I write a script to generate the routh table and verify the system stability given K_p and K_d