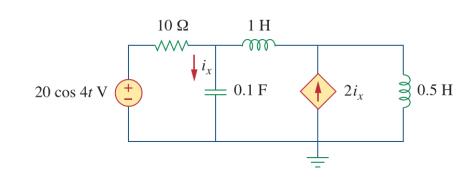
# Lecture 9

- Sinusoidal Steady-State Analysis



## **Outline**

- Kirchhoff's laws in phasor domain
- Generalized impedance
- General AC phasor analysis
- Phasor diagram



## Kirchhoff's Laws in the Phasor Domain

• Let  $v_1, v_2, \cdots v_n$  be the voltages around a closed loop. Then according to KVL

$$v_1 + v_2 + \cdots + v_n = 0$$

$$\mathbf{V}_1 + \mathbf{V}_2 + \dots + \mathbf{V}_n = 0$$

Similarly, KCL holds for phasors:

$$i_1+i_2+\cdots+i_n=0$$

$$\mathbf{I}_1 + \mathbf{I}_2 + \cdots + \mathbf{I}_n = 0,$$

### **Proof**

lf

$$v_1 + v_2 + \dots + v_n = 0$$

where  $v_i$  are sinusoidal voltages of the same frequency, then

 $V_1 + V_2 + \cdots + V_n = 0$ 

$$\mathbf{V}_{1} + \mathbf{V}_{2} + \dots + \mathbf{V}_{n} = 0$$

$$v_{1} + v_{2} + \dots + v_{n} = 0$$

$$\mathbf{V}_{m1} \cos(\omega t + \theta_{1}) + V_{m2} \cos(\omega t + \theta_{2}) + \dots + V_{mn} \cos(\omega t + \theta_{n}) = 0$$

$$\mathbf{Re}(V_{m1}e^{j\theta_{1}} \cdot e^{j\omega t}) + \dots + \mathbf{Re}(V_{mn}e^{j\theta_{n}} \cdot e^{j\omega t}) = 0$$

$$\mathbf{Re}\left((\mathbf{V}_{1} + \dots + \mathbf{V}_{n}) \cdot e^{j\omega t}\right) = 0 \quad Where \mathbf{V}_{k} = V_{mk}e^{j\theta_{k}}$$

$$\mathbf{Re}\left((\mathbf{V}_{1} + \dots + \mathbf{V}_{n}) \cdot e^{j\omega t}\right) = 0 \quad Where \mathbf{V}_{k} = V_{mk}e^{j\theta_{k}}$$

## **Outline**

- Kirchhoff's laws in phasor domain
- Generalized impedance
- General AC phasor analysis
- Phasor diagram

# **Review: Impedance and Admittance**

Resistor	$\mathbf{Z} = R$	$\mathbf{Y} = 1/R$
Inductor	$\mathbf{Z} = j\omega L$	$\mathbf{Y} = 1/j\omega L$
Capacitor	$\mathbf{Z} = 1/j\omega C$	$\mathbf{Y} = j\omega C$

# Impedance is voltage/current

$$\mathbf{Z} = R + jX$$

R = resistance = Re(Z)

X = reactance = Im(Z)

# Admittance is current/voltage

$$\mathbf{Y} = \frac{1}{\mathbf{Z}} = G + jB$$

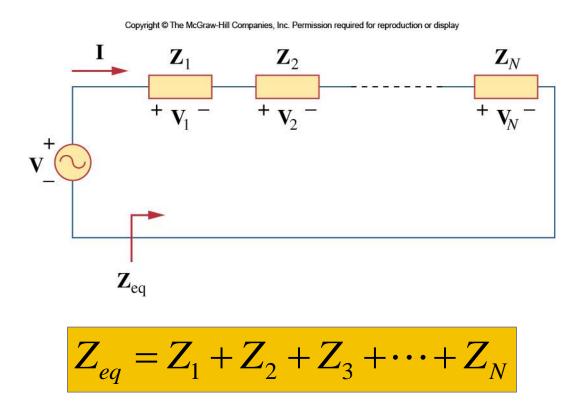
G = conductance = Re(Y)

B = susceptance = Im(Y)

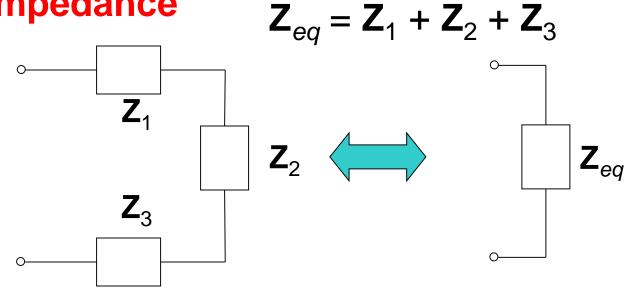


## **Series Impedance**

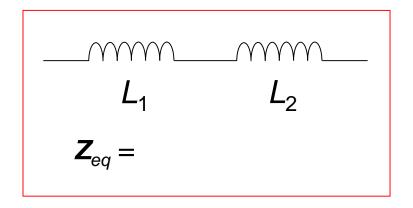
 Once in frequency domain, the impedance elements are generalized, combinations will follow the rules for resistors:



## **Series Impedance**

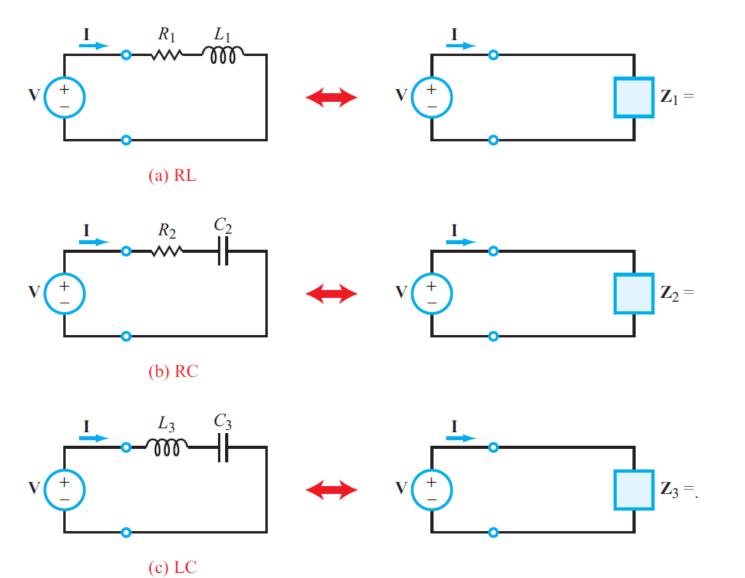


### For example:



$$C_1$$
  $C_2$ 
 $\mathbf{Z}_{eq} = \mathbf{Z}_{eq}$ 

# Impedance combination for RLC Circuit

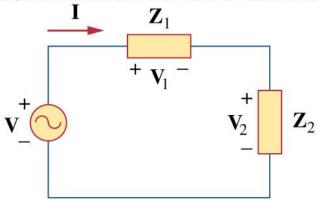




## **Voltage Divider**

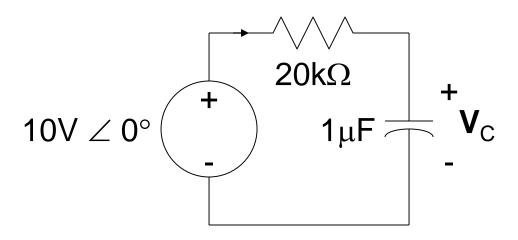
Two elements in series can act like a voltage divider





$$\dot{V}_1 = \frac{Z_1}{Z_1 + Z_2} \dot{V} \quad \dot{V}_2 = \frac{Z_2}{Z_1 + Z_2} \dot{V}$$

## **Example**

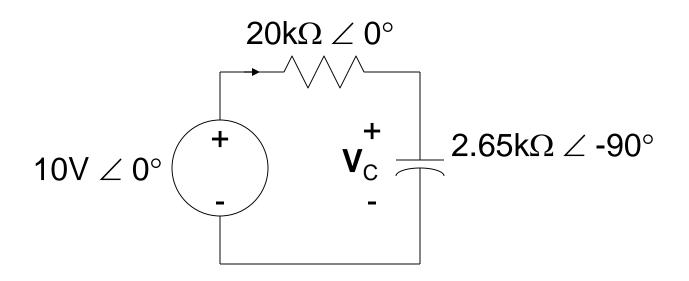


1. 
$$f=60 \text{ Hz}, V_C=?$$

First compute impedances for resistor and capacitor:

$$\mathbf{Z}_R = R = 20 \mathrm{k}\Omega = 20 \mathrm{k}\Omega \angle 0^\circ$$

$$\mathbf{Z}_{C} = 1/j (2\pi f \times 1\mu F) = 2.65 k\Omega \angle -90^{\circ}$$



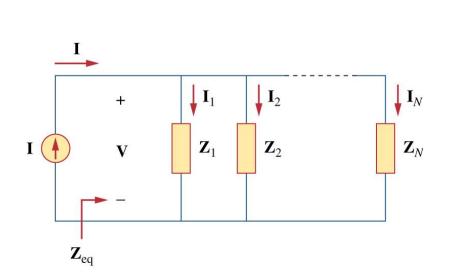
Now use the voltage divider to find  $V_C$ :

$$\mathbf{V}_C = 10 \text{V} \angle 0^{\circ} \left( \frac{2.65 \text{k}\Omega \angle -90^{\circ}}{2.65 \text{k}\Omega \angle -90^{\circ} + 20 \text{k}\Omega \angle 0^{\circ}} \right)$$

$$V_C = 1.31 V \angle -82.4^{\circ}$$

## **Parallel Combination**

 Likewise, elements combined in parallel will combine in the same fashion as resistors in parallel:



$$\frac{1}{Z_{eq}} = \frac{1}{Z_1} + \frac{1}{Z_2} + \frac{1}{Z_3} + \dots + \frac{1}{Z_N}$$

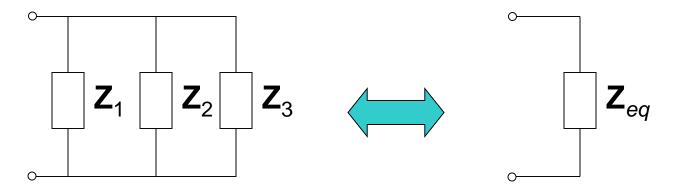
$$Y_{eq} = Y_1 + Y_2 + Y_3 + \dots + Y_N$$

$$I_1 = \frac{Y_1}{Y_1 + \dots + Y_N} I$$

$$I_2 = \frac{Y_2}{Y_1 + \dots + Y_N} I$$

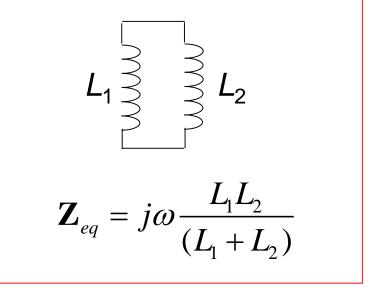
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## **Parallel Impedance**



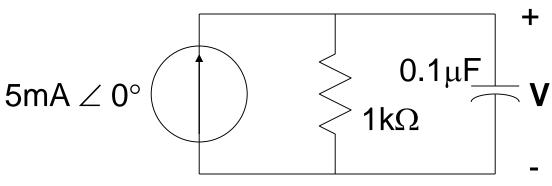
For example:

$$1/\mathbf{Z}_{eq} = 1/\mathbf{Z}_1 + 1/\mathbf{Z}_2 + 1/\mathbf{Z}_3$$

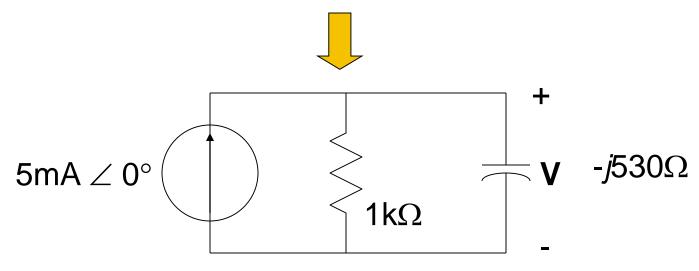


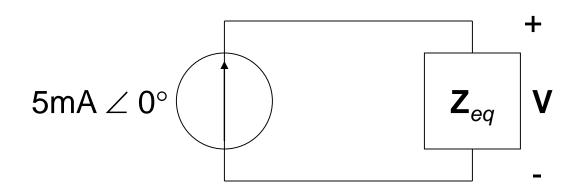
$$\mathbf{Z}_{eq} = \frac{1}{j\omega(C_1 + C_2)}$$

## **Example**



Find v(t) for  $\omega = 2\pi \times 3000$ 





$$\mathbf{Z}_{eq} = \frac{1000 \times (-j530)}{1000 - j530} = \frac{10^3 \angle 0^\circ \times 530 \angle -90^\circ}{1132 \angle -27.9^\circ}$$

$$\mathbf{Z}_{eq} = 468.2\Omega\angle - 62.1^{\circ}$$

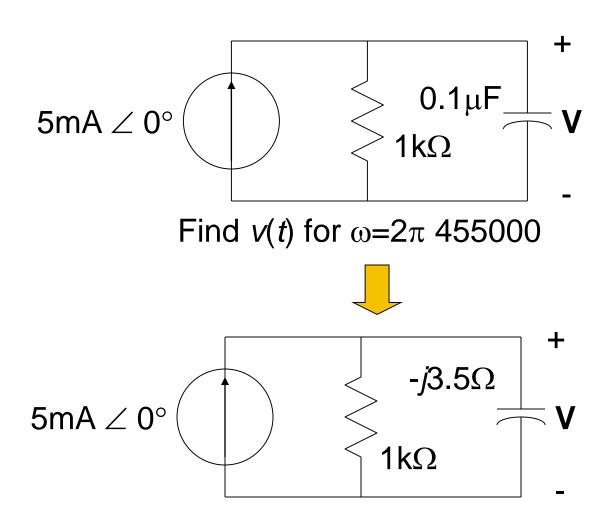
$$\mathbf{V} = \mathbf{IZ}_{eq} = 5 \text{mA} \angle 0^{\circ} \times 468.2 \Omega \angle -62.1^{\circ}$$

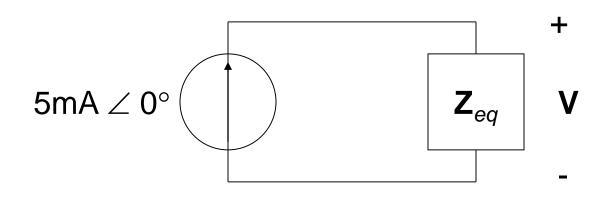
$$V = 2.34V \angle -62.1^{\circ}$$

$$v(t) = 2.34\cos(2\pi 3000t - 62.1^{\circ})V$$



# **Change the Frequency**





$$\mathbf{Z}_{eq} = \frac{1000 \times (-j3.5)}{1000 - j3.5} = \frac{10^3 \angle 0^\circ \times 3.5 \angle -90^\circ}{1000 \angle -0.2^\circ}$$

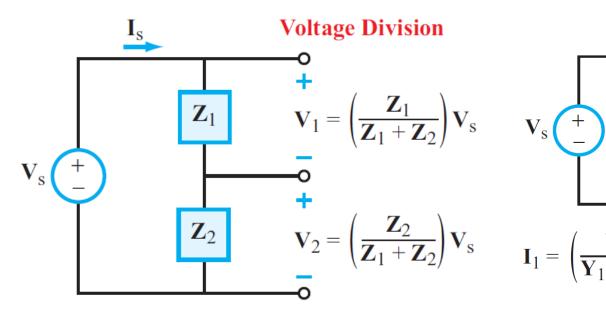
$$\mathbf{Z}_{eq} = 3.5 \angle -89.8^{\circ}\Omega$$

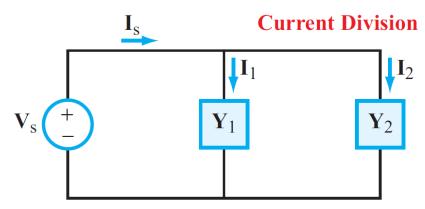
$$V = IZ_{eq} = 5\angle 0^{\circ} \text{mA} \times 3.5\angle - 89.8^{\circ}\Omega$$
  $V = 17.5\angle - 89.8^{\circ} \text{mV}$ 

$$v(t) = 17.5\cos(2\pi 455000t - 89.8^{\circ}) \text{mV}$$



## **Summary: Voltage & Current Division**



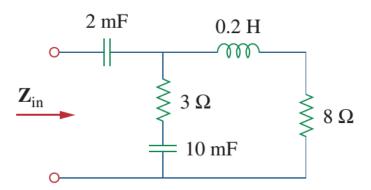


$$\mathbf{V}_2 = \left(\frac{\mathbf{Z}_2}{\mathbf{Z}_1 + \mathbf{Z}_2}\right) \mathbf{V}_{s} \qquad \mathbf{I}_1 = \left(\frac{\mathbf{Y}_1}{\mathbf{Y}_1 + \mathbf{Y}_2}\right) \mathbf{I}_{s} \qquad \mathbf{I}_2 = \left(\frac{\mathbf{Y}_2}{\mathbf{Y}_1 + \mathbf{Y}_2}\right) \mathbf{I}_{s}$$



## **Exercise**

• Find the input impedance of the circuit below.  $\omega = 50$  rad/s.



## **Outline**

- Kirchhoff's laws in phasor domain
- Generalized impedance
- General AC phasor analysis
  - Nodal/mesh analysis
  - Superposition
  - Source transformation/Thevenin/Norton
- Phasor diagram

# **AC Phasor Analysis General Procedure**

#### Step 1: Adopt cosine reference

$$v_s(t) = 12 \sin(\omega t - 45^\circ)$$
  
=  $12 \cos(\omega t - 45^\circ - 90^\circ) = 12 \cos(\omega t - 135^\circ) \text{ V}.$   
 $V_s = 12e^{-j135^\circ} \text{ V}.$ 

#### Step 2: Transform circuit to phasor domain

#### Step 3: Cast KCL and/or KVL equations in phasor domain

$$\mathbf{Z}_{R}\mathbf{I} + \mathbf{Z}_{C}\mathbf{I} = \mathbf{V}_{s},$$

which is equivalent to

$$\left(R + \frac{1}{j\omega C}\right)\mathbf{I} = 12e^{-j135^{\circ}}.$$

#### Step 1

Adopt Cosine Reference (Time Domain)



#### Step 2

Transfer to Phasor Domain

$$R \longrightarrow \mathbf{Z}_{\mathbf{R}} = R$$

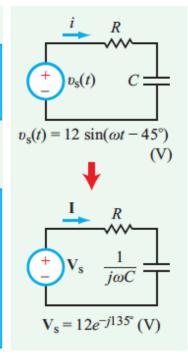
$$L \longrightarrow \mathbf{Z}_{\mathbf{L}} = j\omega L$$

$$C \longrightarrow \mathbf{Z}_{\mathbf{C}} = 1/j\omega C$$



#### Step 3

Cast Equations in Phasor Form





$$\mathbf{I}\left(R + \frac{1}{j\omega C}\right) = \mathbf{V}_{s}$$

# **AC Phasor Analysis General Procedure**

#### Step 4: Solve for unknown variable

$$\mathbf{I} = \frac{12e^{-j135^{\circ}}}{R + \frac{1}{j\omega C}} = \frac{j12\omega C e^{-j135^{\circ}}}{1 + j\omega RC}.$$

Using the specified values, namely  $R = \sqrt{3} \text{ k}\Omega$ ,  $C = 1 \mu\text{F}$ , and  $\omega = 10^3 \text{ rad/s}$ ,

$$\mathbf{I} = \frac{j12 \times 10^3 \times 10^{-6} e^{-j135^{\circ}}}{1 + j10^3 \times \sqrt{3} \times 10^3 \times 10^{-6}} = \frac{j12 e^{-j135^{\circ}}}{1 + j\sqrt{3}} \text{ mA}.$$

$$\mathbf{I} = \frac{12e^{-j135^{\circ}} \cdot e^{j90^{\circ}}}{2e^{j60^{\circ}}} = 6e^{j(-135^{\circ} + 90^{\circ} - 60^{\circ})} = 6e^{-j105^{\circ}} \text{ mA}.$$

#### Step 5: Transform solution back to time domain

To return to the time domain, we apply the fundamental relation between a sinusoidal function and its phasor counterpart, namely

$$i(t) = \Re[\mathbf{I}e^{j\omega t}] = \Re[\mathbf{G}e^{-j105^{\circ}}e^{j\omega t}] = 6\cos(\omega t - 105^{\circ}) \text{ mA}.$$

#### Step 1

Adopt Cosine Reference (Time Domain)



#### Step 2

Transfer to Phasor Domain

$$v \longrightarrow V$$

$$R \longrightarrow \mathbf{Z}_{\mathbf{R}} = R$$

$$L \longrightarrow \mathbf{Z}_{\mathbf{L}} = j\omega L$$

$$C \longrightarrow \mathbf{Z}_{\mathbf{C}} = 1/j\omega C$$



#### Step 3

Cast Equations in Phasor Form



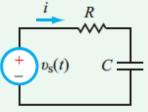
#### Step 4

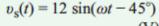
Solve for Unknown Variable (Phasor Domain)

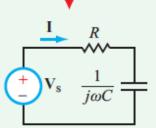


#### Step 5

Transform Solution Back to Time Domain

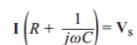




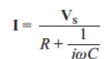


$$V_s = 12e^{-j135^\circ} (V)$$













$$= 6\cos(\omega t - 105^{\circ})$$
(mA)

# **Example: RL Circuit**

$$v_{\rm s}(t) = 15\sin(4 \times 10^4 t - 30^\circ) \text{ V}.$$

Also,  $R = 3 \Omega$  and L = 0.1 mH. Obtain an expression for the voltage across the inductor.

#### **Solution:**

Step 1: Convert  $v_s(t)$  to the cosine reference

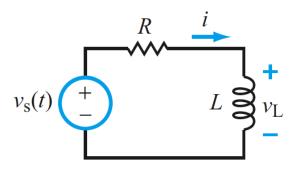
$$v_s(t) = 15\sin(4 \times 10^4 t - 30^\circ) = 15\cos(4 \times 10^4 t - 120^\circ) \text{ V},$$

$$V_{\rm s} = 15e^{-j120^{\circ}} V.$$

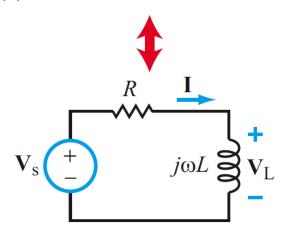
Step 2: Transform circuit to the phasor domain

Step 3: Cast KVL in phasor domain

$$R\mathbf{I} + j\omega L\mathbf{I} = \mathbf{V}_{s}.$$



(a) Time domain



(b) Phasor domain

Step 4: Solve for unknown variable

$$\mathbf{I} = \frac{\mathbf{V}_{s}}{R + j\omega L} = \frac{15e^{-j120^{\circ}}}{3 + j4 \times 10^{4} \times 10^{-4}}$$
$$= \frac{15e^{-j120^{\circ}}}{3 + j4} = \frac{15e^{-j120^{\circ}}}{5e^{j53.1^{\circ}}} = 3e^{-j173.1^{\circ}} \text{ A}.$$

The phasor voltage across the inductor is related to I by

$$\mathbf{V_L} = j\omega L\mathbf{I}$$

$$= j4 \times 10^4 \times 10^{-4} \times 3e^{-j173.1^{\circ}}$$

$$= j12e^{-j173.1^{\circ}}$$

$$= 12e^{-j173.1^{\circ}} \cdot e^{j90^{\circ}} = 12e^{-j83.1^{\circ}} \, \text{V},$$

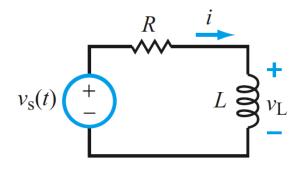
where we replaced j with  $e^{j90^{\circ}}$ .

#### Step 5: Transform solution to the time domain

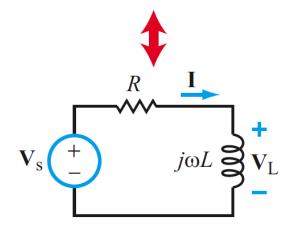
$$v_{L}(t) = \Re [V_{L}e^{j\omega t}]$$

$$= \Re [12e^{-j83.1^{\circ}}e^{j4\times10^{4}t}]$$

$$= 12\cos(4\times10^{4}t - 83.1^{\circ}) \text{ V}.$$



(a) Time domain

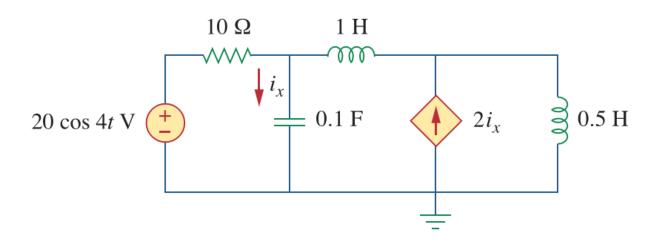


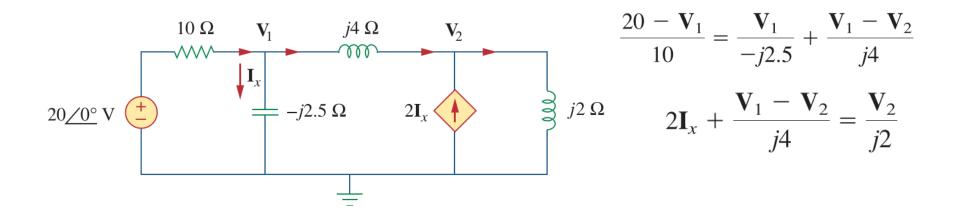
(b) Phasor domain



# **Nodal Analysis**

• Example---Find  $i_x$ 





$$i_x = 7.59 \cos(4t + 108.4^\circ) \text{ A}$$

#### **10.5** Find $i_o$ in the circuit of Fig. 10.54.

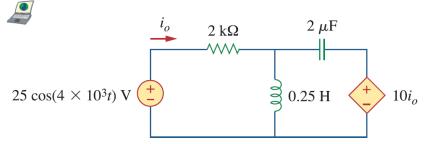
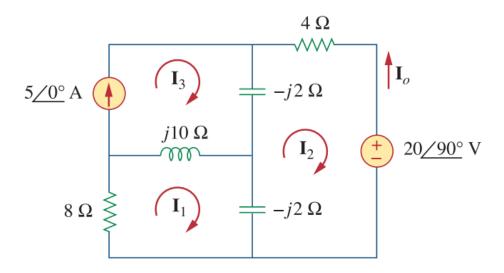


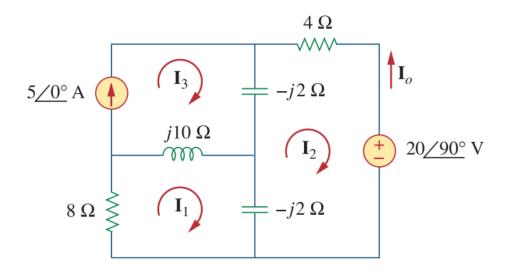
Figure 10.54

For Prob. 10.5.

# **Mesh Analysis**



## Mesh Analysis



Applying KVL to mesh 1, we obtain

$$(8 + j10 - j2)\mathbf{I}_1 - (-j2)\mathbf{I}_2 - j10\mathbf{I}_3 = 0$$
 (10.3.1)

For mesh 2,

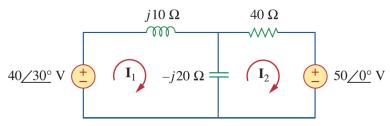
$$(4 - j2 - j2)\mathbf{I}_2 - (-j2)\mathbf{I}_1 - (-j2)\mathbf{I}_3 + 20/90^\circ = 0$$
 (10.3.2)

For mesh 3,  $I_3 = 5$ . Substituting this in Eqs. (10.3.1) and (10.3.2), we get

$$(8 + j8)\mathbf{I}_1 + j2\mathbf{I}_2 = j50 (10.3.3)$$

$$j2\mathbf{I}_1 + (4 - j4)\mathbf{I}_2 = -j20 - j10$$
 (10.3.4)

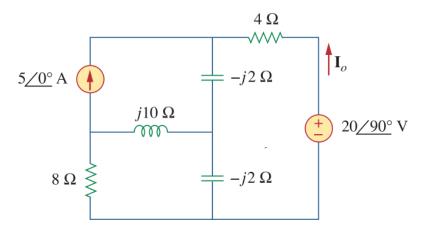
10.27 Using mesh analysis, find  $I_1$  and  $I_2$  in the circuit of Fig. 10.75.

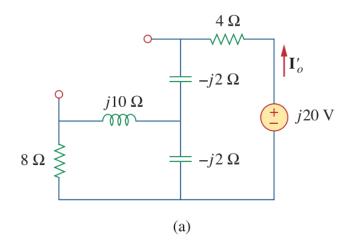


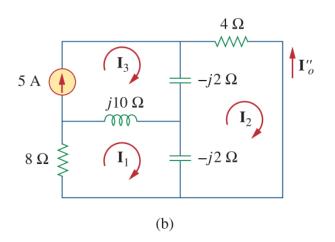
**Figure 10.75** For Prob. 10.27.



## **Superposition-Example**







# **Multiple Frequencies**

**10.46** Solve for  $v_o(t)$  in the circuit of Fig. 10.91 using the superposition principle.

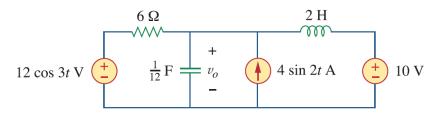
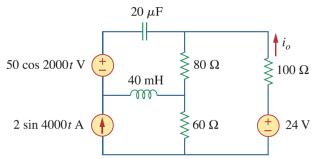


Figure 10.91

For Prob. 10.46.

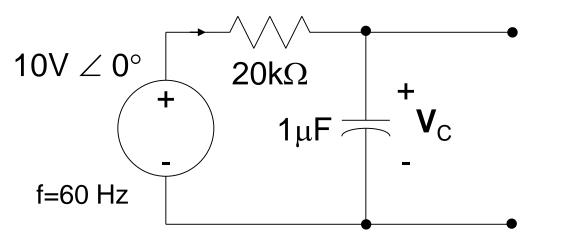
**10.48** Find  $i_o$  in the circuit of Fig. 10.93 using superposition.

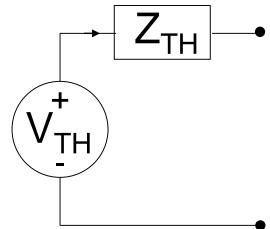




**Figure 10.93** For Prob. 10.48.

## **Thevenin Equivalent**



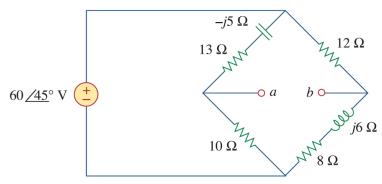


$$ZR = R = 20kΩ = 20kΩ ∠ 0°$$
 $ZC = 1/j (2πf x 1μF) = 2.65kΩ ∠ -90°$ 

$$\mathbf{V}_{TH} = \mathbf{V}_{OC} = 10 \,\text{V} \,\angle 0^{\circ} \left( \frac{2.65 \,\text{k}\Omega \,\angle -90^{\circ}}{2.65 \,\text{k}\Omega \,\angle -90^{\circ} + 20 \,\text{k}\Omega \,\angle 0^{\circ}} \right) = 1.31 \,\angle -82.4$$

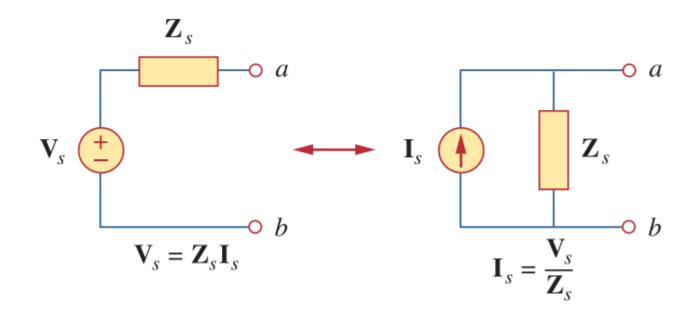
$$\mathbf{Z}_{TH} = \mathbf{Z}_{R} \parallel \mathbf{Z}_{C} = \left(\frac{20k\Omega\angle0^{\circ} \cdot 2.65k\Omega\angle - 90^{\circ}}{2.65k\Omega\angle - 90^{\circ} + 20k\Omega\angle0^{\circ}}\right) = 2.62\angle - 82.4$$

10.67 Find the Thevenin and Norton equivalent circuits at terminals *a-b* in the circuit of Fig. 10.110.



**Figure 10.110** For Prob. 10.67.

## Source transformation/Norton



$$\mathbf{V}_s = \mathbf{Z}_s \mathbf{I}_s \qquad \Leftrightarrow \qquad \mathbf{I}_s = \frac{\mathbf{V}_s}{\mathbf{Z}_s}$$

# **AC Op Amp Circuits**

Question 1: Are op amps used in ac circuits?

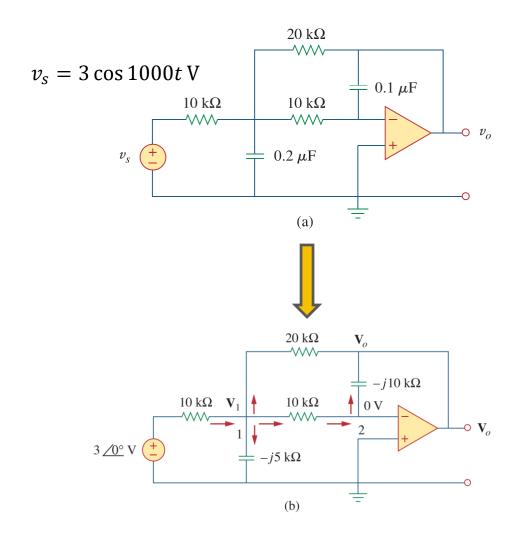
Answer 1: Yes.

 $v_s \stackrel{20 \text{ k}\Omega}{\longleftarrow} 0.1 \mu\text{F}$   $v_s \stackrel{+}{\longleftarrow} 0.2 \mu\text{F}$ 

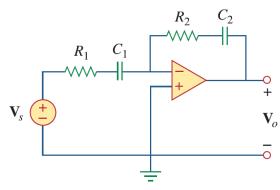
Question 2: Is the ideal op-amp model applicable to ac circuits?

Answer 2: The ideal op-amp model is based on the assumption that the open-loop gain A is very large (>  $10^4$ ), which is true at dc and low frequencies, but not necessarily so at high frequencies. The range of frequencies over which A is large depends on the specific op-amp design.

# Example –find $v_o$



**10.74** Evaluate the voltage gain  $\mathbf{A}_v = \mathbf{V}_o/\mathbf{V}_s$  in the op amp circuit of Fig. 10.117. Find  $\mathbf{A}_v$  at  $\omega = 0$ ,  $\omega \to \infty$ ,  $\omega = 1/R_1C_1$ , and  $\omega = 1/R_2C_2$ .



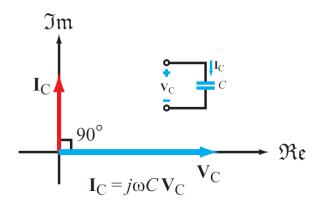
**Figure 10.117** For Prob. 10.74.

## **Outline**

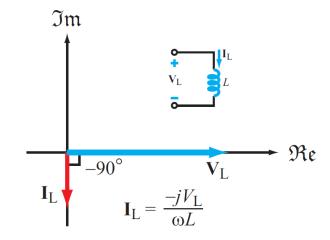
- Kirchhoff's laws in phasor domain
- Generalized impedance
- General AC phasor analysis
- Phasor diagram

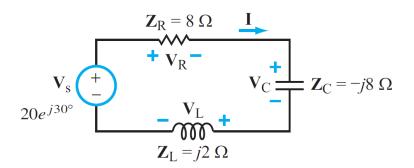
# **Phasor Diagrams**

### **Capacitor**

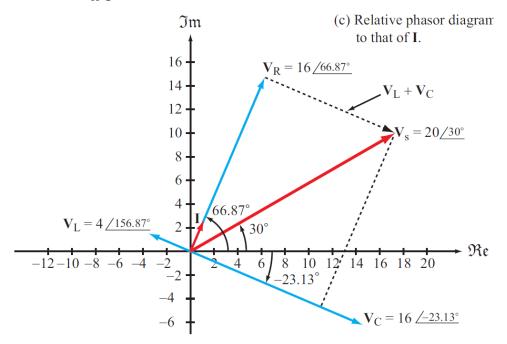


### **Inductor**

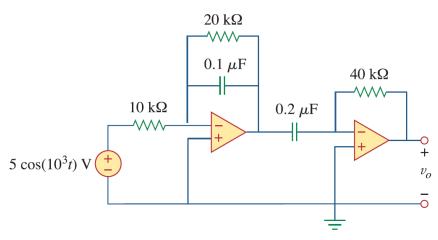




$$\mathbf{I} = \frac{\mathbf{V}_{s}}{R + j\omega L - \frac{j}{\omega C}} = \frac{20e^{j30^{\circ}}}{8 + j2 - j8} = \frac{20e^{j30^{\circ}}}{8 - j6} = \frac{20e^{j30^{\circ}}}{10e^{-j36.87^{\circ}}} = 2e^{j66.87^{\circ}} \,\mathbf{A}$$



#### **10.79** For the op amp circuit in Fig. 10.122, obtain $v_o(t)$ .



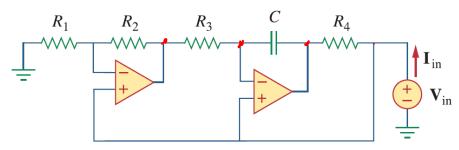
**Figure 10.122** For Prob. 10.79.

**10.89** The op amp circuit in Fig. 10.131 is called an *inductance simulator*. Show that the input impedance is given by

$$\mathbf{Z}_{\rm in} = \frac{\mathbf{V}_{\rm in}}{\mathbf{I}_{\rm in}} = j\omega L_{\rm eq}$$

where

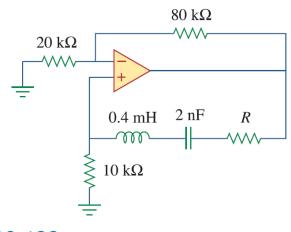
$$L_{\rm eq} = \frac{R_1 R_3 R_4}{R_2} C$$



#### Figure 10.131

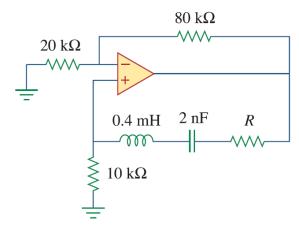
For Prob. 10.89.

- **10.91** Consider the oscillator in Fig. 10.133.
  - (a) Determine the oscillation frequency.
  - (b) Obtain the minimum value of *R* for which oscillation takes place.



**Figure 10.133** For Prob. 10.91.

- **10.91** Consider the oscillator in Fig. 10.133.
  - (a) Determine the oscillation frequency.
  - (b) Obtain the minimum value of *R* for which oscillation takes place.



**Figure 10.133** For Prob. 10.91.