

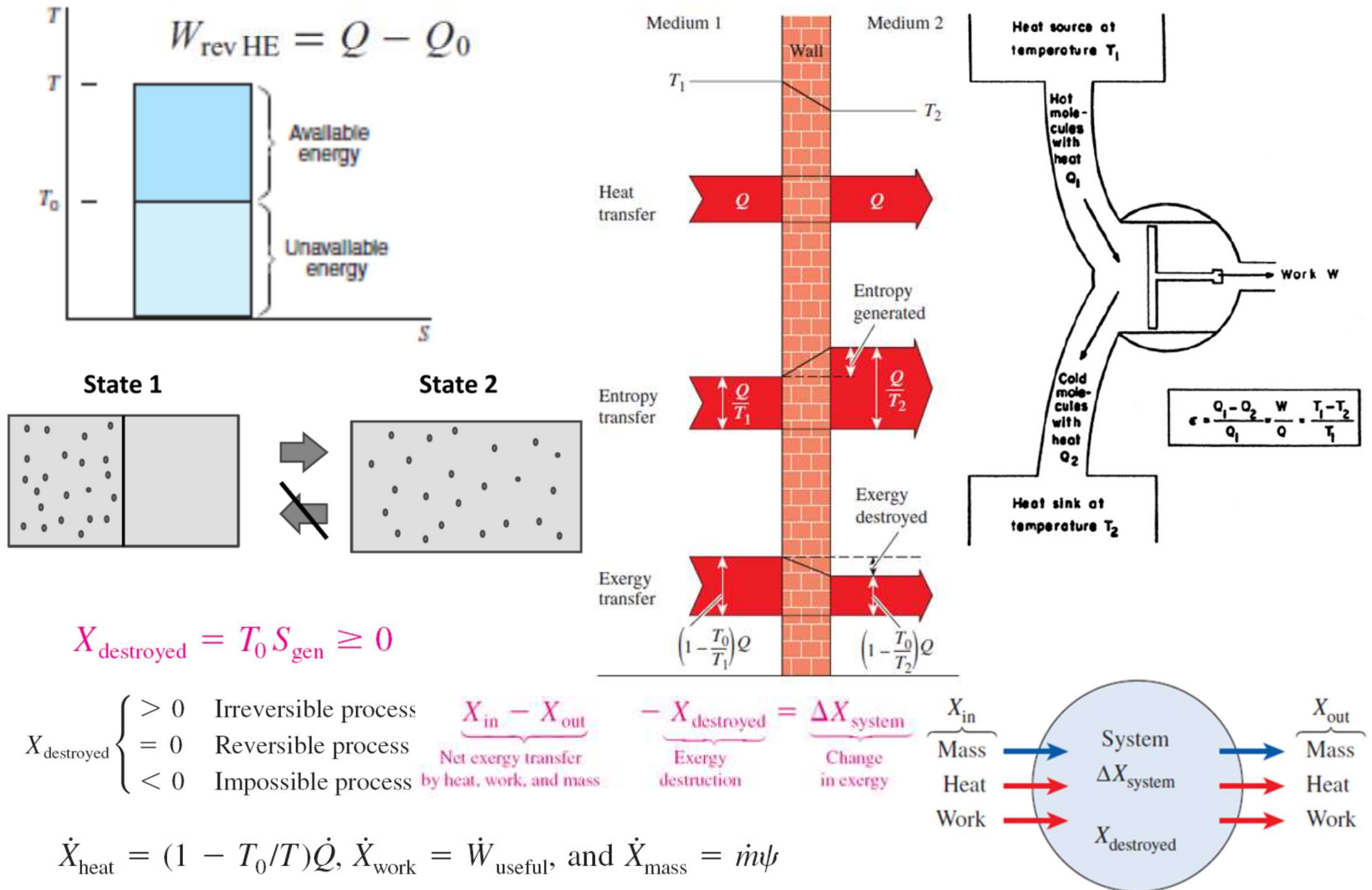
Exergy Balance Over Control Volume

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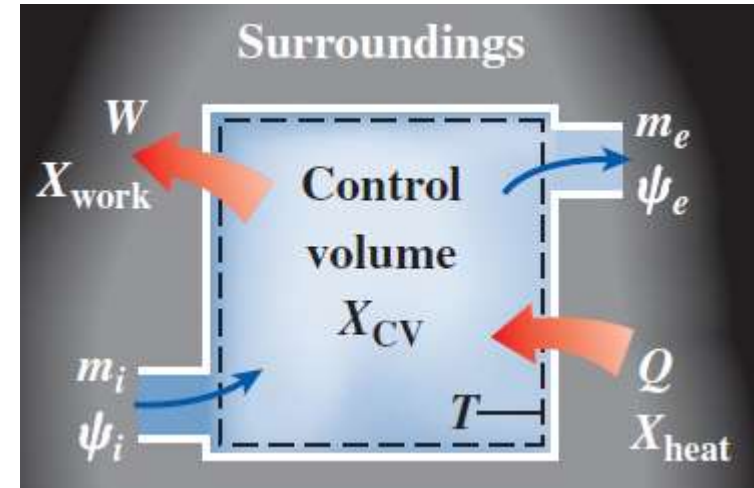
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Previously: Exergy Destruction & Balance



Figs-TD-Borgnakke & Sonntag; Cengel & Boles Modern Electrochemistry 2B, Bockris & Reddy

Exergy Balance Over Control Volume



$$X_{\text{heat}} - X_{\text{work}} + X_{\text{mass,in}} - X_{\text{mass,out}} - X_{\text{destroyed}} = (X_2 - X_1)_{\text{CV}}$$

$$\sum \left(1 - \frac{T_0}{T_k}\right) Q_k - [W - P_0(V_2 - V_1)] + \sum_{\text{in}} m\psi - \sum_{\text{out}} m\psi - X_{\text{destroyed}} = (X_2 - X_1)_{\text{CV}}$$

$$\sum \left(1 - \frac{T_0}{T_k}\right) \dot{Q}_k - \left(\dot{W} - P_0 \frac{dV_{\text{CV}}}{dt}\right) + \sum_{\text{in}} \dot{m}\psi - \sum_{\text{out}} \dot{m}\psi - \dot{X}_{\text{destroyed}} = \frac{dX_{\text{CV}}}{dt}$$

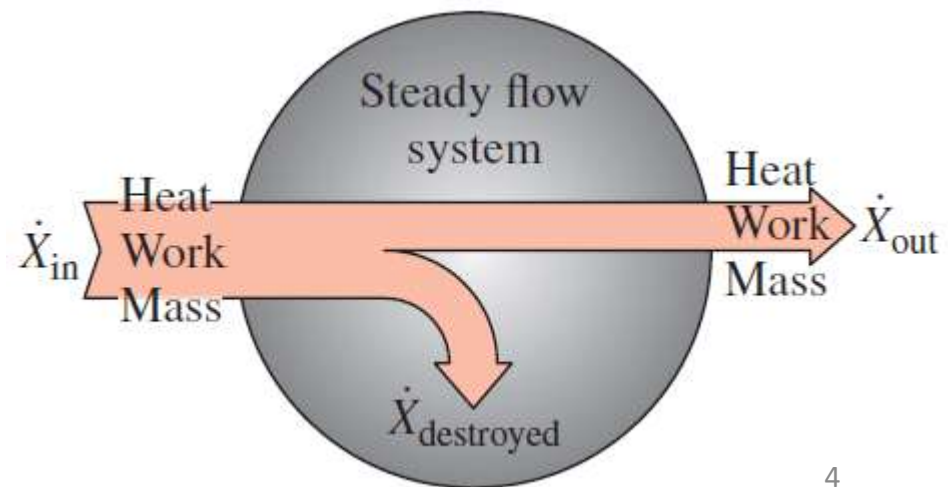
Exergy Balance For Steady Flow Systems

Steady-flow: $\sum \left(1 - \frac{T_0}{T_k}\right) \dot{Q}_k - \dot{W} + \sum_{\text{in}} \dot{m}\psi - \sum_{\text{out}} \dot{m}\psi - \dot{X}_{\text{destroyed}} = 0$

Single-stream: $\sum \left(1 - \frac{T_0}{T_k}\right) \dot{Q}_k - \dot{W} + \dot{m}(\psi_1 - \psi_2) - \dot{X}_{\text{destroyed}} = 0$

$$\psi_1 - \psi_2 = (h_1 - h_2) - T_0(s_1 - s_2) + \frac{V_1^2 - V_2^2}{2} + g(z_1 - z_2)$$

Per-unit mass: $\sum \left(1 - \frac{T_0}{T_k}\right) q_k - w + (\psi_1 - \psi_2) - x_{\text{destroyed}} = 0$



Reversible Work

Single-stream:
$$\sum \left(1 - \frac{T_0}{T_k} \right) \dot{Q}_k - \dot{W} + \dot{m}(\psi_1 - \psi_2) - \dot{X}_{\text{destroyed}} = 0$$

General:
$$W = W_{\text{rev}} \quad \text{when } X_{\text{destroyed}} = 0$$

Single stream:
$$\dot{W}_{\text{rev}} = \dot{m}(\psi_1 - \psi_2) + \sum \left(1 - \frac{T_0}{T_k} \right) \dot{Q}_k \quad (\text{kW})$$

Adiabatic, single stream:
$$\dot{W}_{\text{rev}} = \dot{m}(\psi_1 - \psi_2)$$

Second law efficiency for turbines

$$\eta_{II,turb} = \frac{w}{w_{rev}} = \frac{h_1 - h_2}{\psi_1 - \psi_2} \quad \text{or} \quad \eta_{II,turb} = 1 - \frac{T_0 s_{gen}}{\psi_1 - \psi_2} \quad (\text{Adiabatic turbine})$$

$$\underbrace{\dot{E}_{in} - \dot{E}_{out}}_{\text{Rate of net energy transfer by heat, work, and mass}} = \underbrace{\frac{dE_{system}}{dt}}_{\text{Rate of change in internal, kinetic, potential, etc., energies}} \xrightarrow{0 \text{ (steady)}} = 0$$

$$\dot{E}_{in} = \dot{E}_{out}$$

$$\dot{m}h_1 = \dot{W}_{out} + \dot{Q}_{out} + \dot{m}h_2 \quad (\text{since } ke \equiv pe \equiv 0)$$

$$\dot{W}_{out} = \dot{m}(h_1 - h_2) - \dot{Q}_{out}$$

$$\underbrace{\dot{X}_{in} - \dot{X}_{out}}_{\text{Rate of net exergy transfer by heat, work, and mass}} - \underbrace{\dot{X}_{destroyed}}_{\text{Rate of exergy destruction}} \xrightarrow{0 \text{ (reversible)}} = \underbrace{\frac{dX_{system}}{dt}}_{\text{Rate of change in exergy}} \xrightarrow{0 \text{ (steady)}} = 0$$

$$\eta_{II} = \frac{\dot{W}_{out}}{\dot{W}_{rev,out}}$$

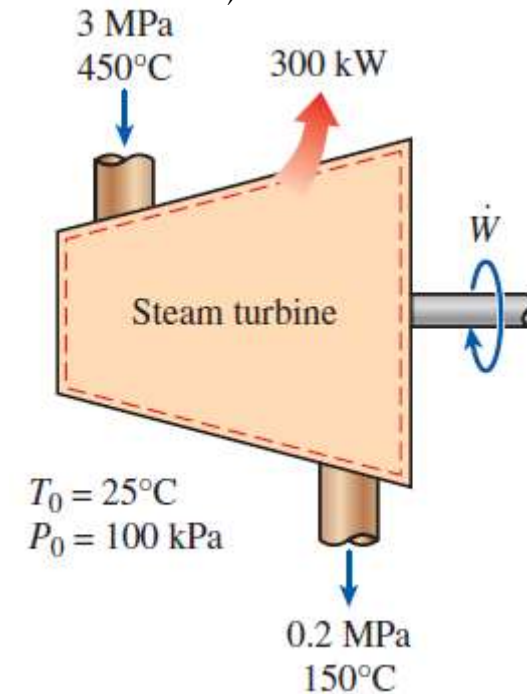
$$\dot{X}_{in} = \dot{X}_{out}$$

$$\dot{m}\psi_1 = \dot{W}_{rev,out} + \dot{X}_{heat} + \dot{m}\psi_2$$

$$\dot{W}_{rev,out} = \dot{m}(\psi_1 - \psi_2)$$

$$= \dot{m}[(h_1 - h_2) - T_0(s_1 - s_2) - \Delta ke \xrightarrow{0} - \Delta pe \xrightarrow{0}]$$

$$\dot{X}_{destroyed} = \dot{W}_{rev,out} - \dot{W}_{out}$$



Second law efficiency for compressor

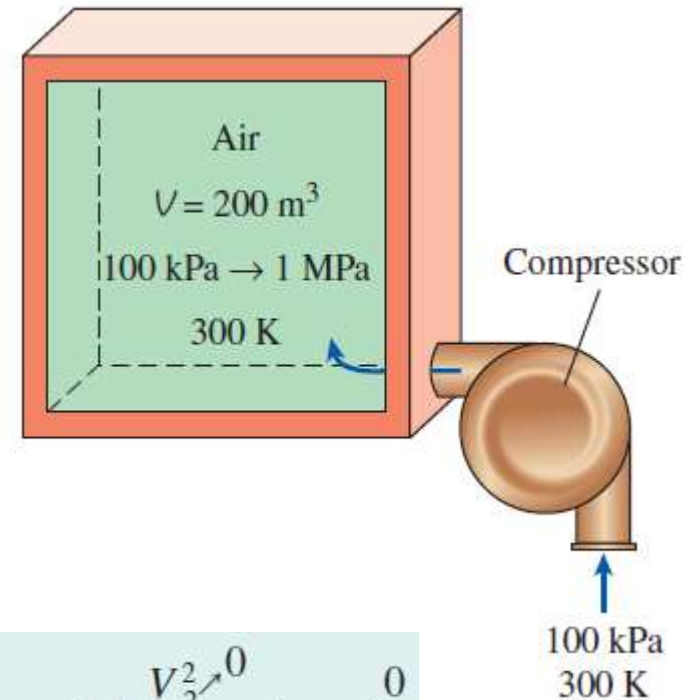
$$\eta_{II,comp} = \frac{w_{rev,in}}{w_{in}} = \frac{\psi_2 - \psi_1}{h_2 - h_1} \quad \text{or} \quad \eta_{II,comp} = 1 - \frac{T_0 s_{gen}}{h_2 - h_1}$$

$$\underbrace{X_{in} - X_{out}}_{\text{Net exergy transfer by heat, work, and mass}} - \underbrace{X_{destroyed}}_{\substack{\nearrow 0 \text{ (reversible)} \\ \text{Exergy destruction}}} = \underbrace{\Delta X_{system}}_{\text{Change in exergy}}$$

$$X_{in} - X_{out} = X_2 - X_1$$

$$W_{rev,in} + m_1 \psi_1 \nearrow 0 = m_2 \phi_2 - m_1 \phi_1 \nearrow 0$$

$$W_{rev,in} = m_2 \phi_2$$



$$\phi_2 = (u_2 - u_0) \nearrow 0 \text{ (since } T_2 = T_0) + P_0(\nu_2 - \nu_0) - T_0(s_2 - s_0) + \frac{V_2^2}{2} \nearrow 0 + gz_2 \nearrow 0$$

$$= P_0(\nu_2 - \nu_0) - T_0(s_2 - s_0)$$

$$P_0(\nu_2 - \nu_0) = P_0 \left(\frac{RT_2}{P_2} - \frac{RT_0}{P_0} \right) = RT_0 \left(\frac{P_0}{P_2} - 1 \right) \quad \text{(since } T_2 = T_0)$$

$$T_0(s_2 - s_0) = T_0 \left(c_p \ln \frac{T_2}{T_0} - R \ln \frac{P_2}{P_0} \right) = -RT_0 \ln \frac{P_2}{P_0} \quad \text{(since } T_2 = T_0)$$

Second law efficiency for other flow devices

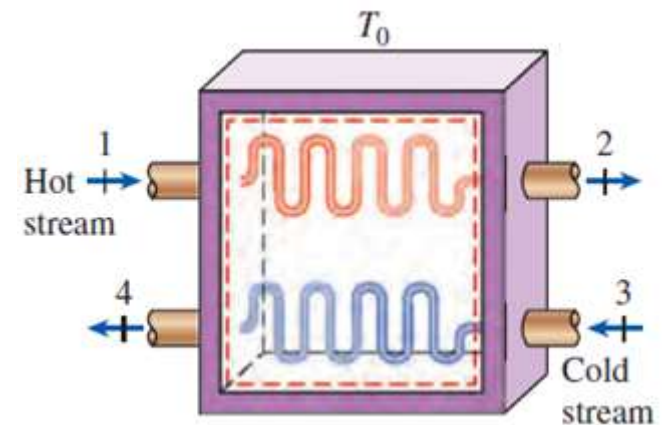
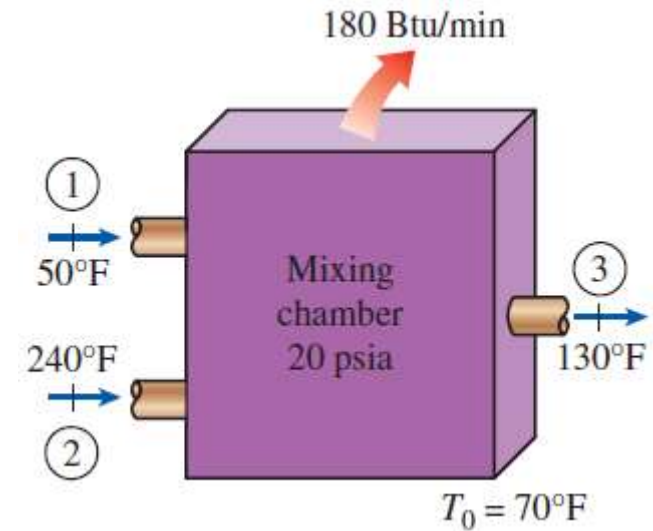
$$\eta_{II, \text{mix}} = \frac{\dot{m}_3 \psi_3}{\dot{m}_1 \psi_1 + \dot{m}_2 \psi_2}$$

$$\eta_{II, \text{mix}} = 1 - \frac{T_0 \dot{S}_{\text{gen}}}{\dot{m}_1 \psi_1 + \dot{m}_2 \psi_2}$$

$$\dot{S}_{\text{gen}} = \dot{m}_3 s_3 - \dot{m}_2 s_2 - \dot{m}_1 s_1$$

$$\eta_{II, \text{HX}} = \frac{\dot{m}_{\text{cold}}(\psi_4 - \psi_3)}{\dot{m}_{\text{hot}}(\psi_1 - \psi_2)}$$

$$\eta_{II, \text{HX}} = 1 - \frac{T_0 \dot{S}_{\text{gen}}}{\dot{m}_{\text{hot}}(\psi_1 - \psi_2)}$$



What's next?

- Thermodynamic property relationships