

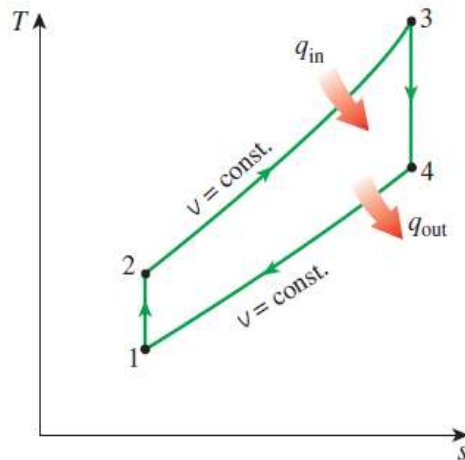
# *Vapor Power Cycles*

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# Previously: Otto-, Diesel-, Brayton- & Stirling-Cycles



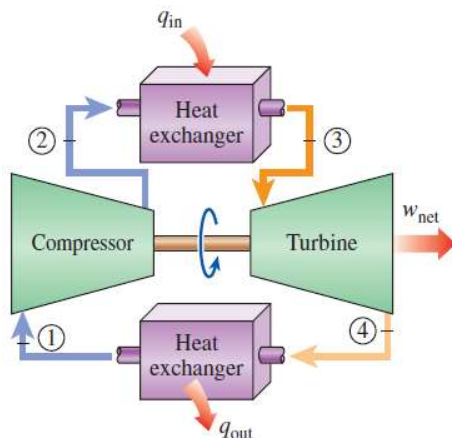
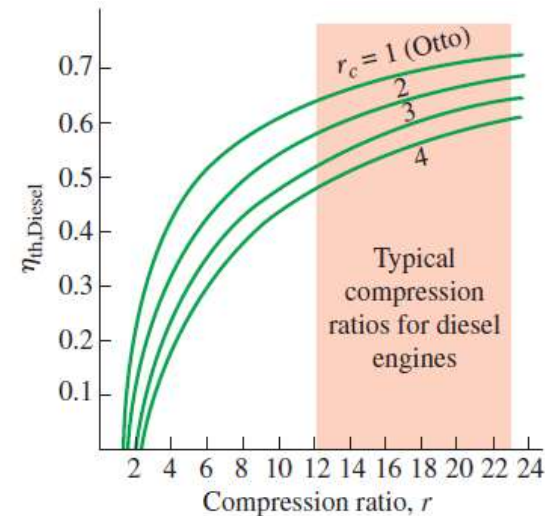
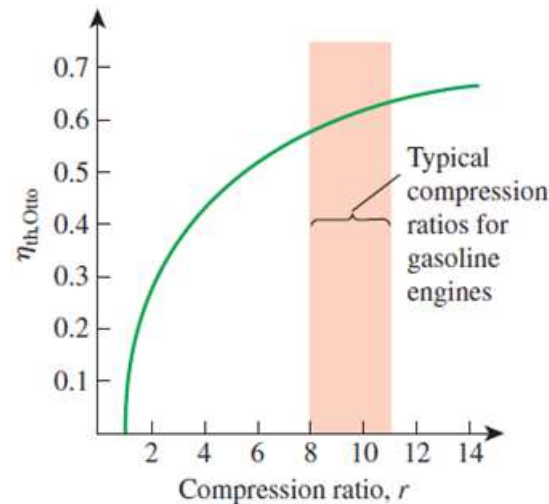
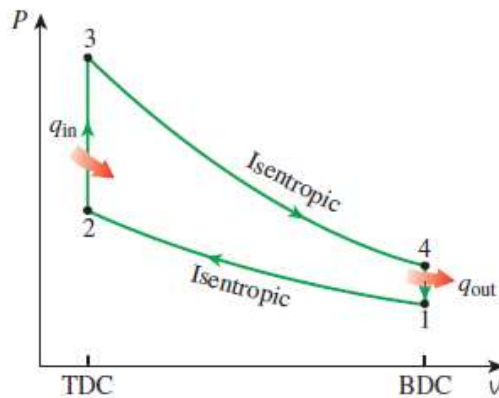
$$q_{in} - w_{b,out} = u_3 - u_2 \rightarrow q_{in} = P_2(v_3 - v_2) + (u_3 - u_2)$$

$$= h_3 - h_2 = c_p(T_3 - T_2)$$

$$\eta_{th,Otto} = \frac{w_{net}}{q_{in}} = 1 - \frac{q_{out}}{q_{in}} = 1 - \frac{T_4 - T_1}{T_3 - T_2} = 1 - \frac{T_1(T_4/T_1 - 1)}{T_2(T_3/T_2 - 1)}$$

Isoentropic gas results for  $1 \rightarrow 2$  &  $3 \rightarrow 4$

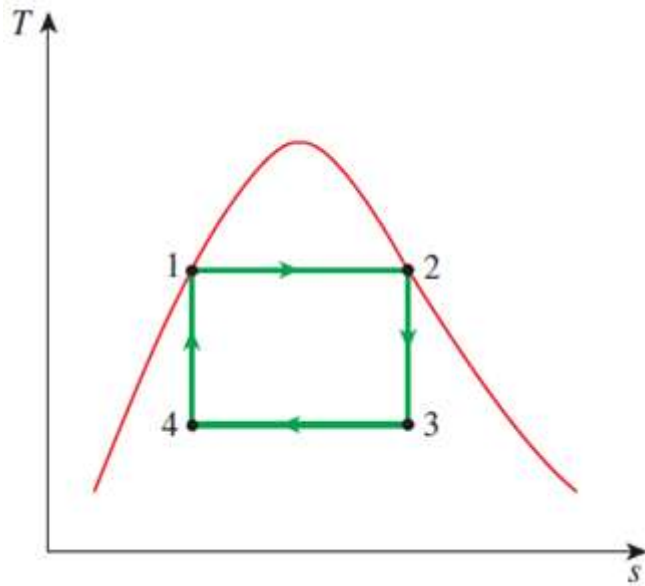
$$\eta_{th,Otto} = 1 - \frac{1}{r^{k-1}}$$



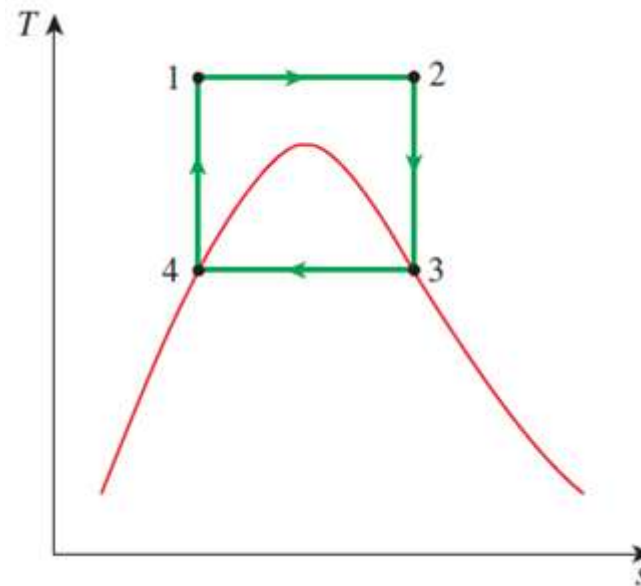
Compression ratio & autoignition/engine knock

TD: Cengel & Boles

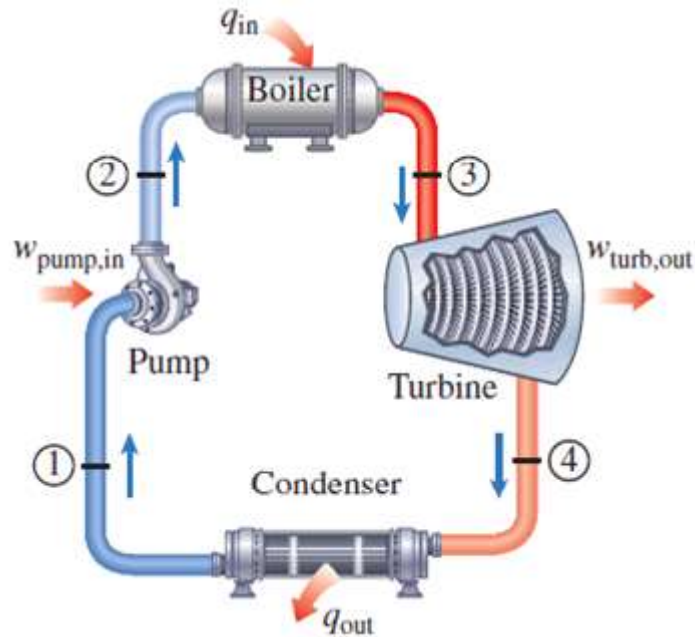
# *Limitation of Carnot Vapor Cycle*



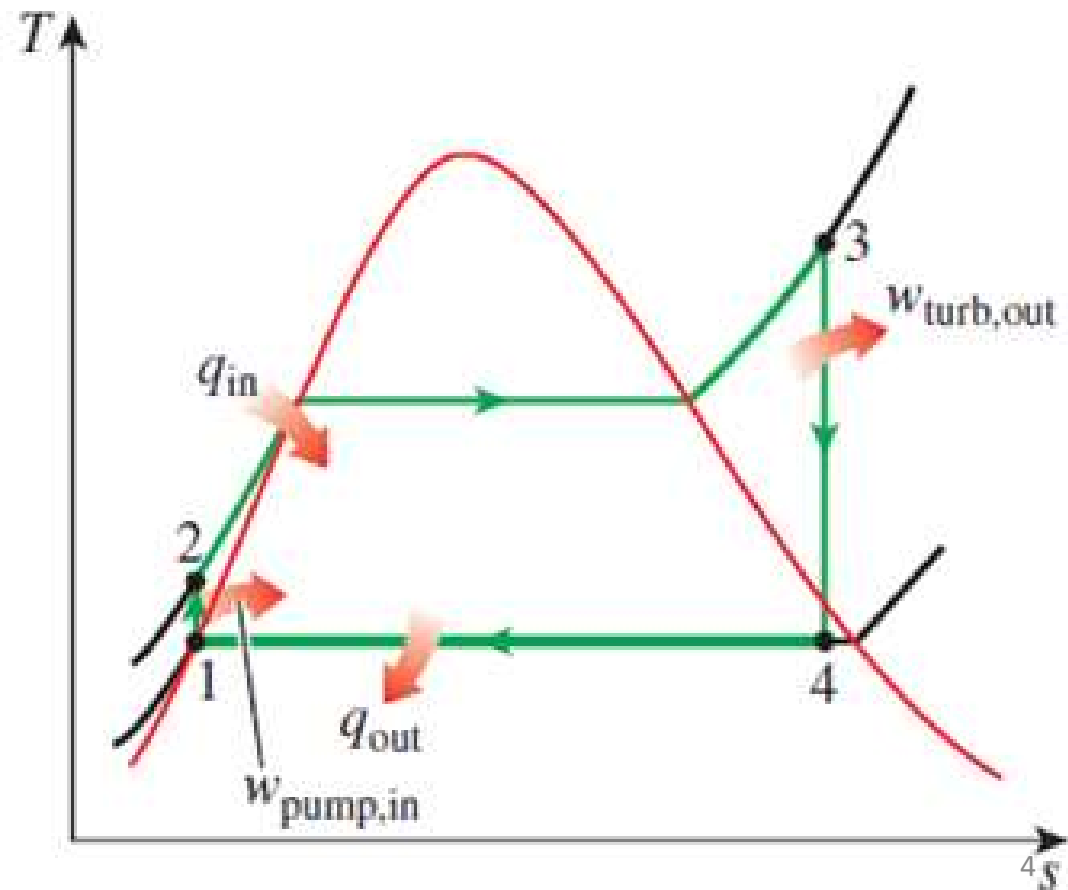
- 1-2** isothermal heat addition in a boiler
- 2-3** isentropic expansion in a turbine
- 3-4** isothermal heat rejection in a condenser
- 4-1** isentropic compression in a compressor



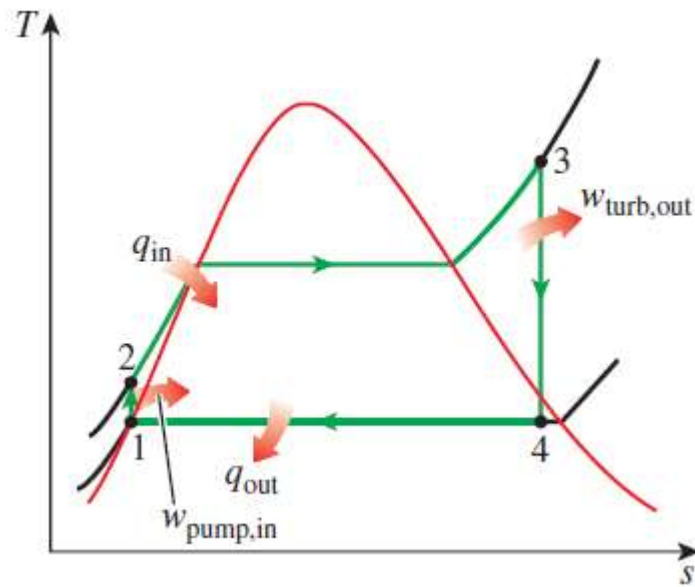
# Motivations & Operations of Rankine Cycle



- 1-2 Isentropic compression in a pump
- 2-3 Constant pressure heat addition in a boiler
- 3-4 Isentropic expansion in a turbine
- 4-1 Constant pressure heat rejection in a condenser



# Analysis of Rankine Cycle



$$(q_{\text{in}} - q_{\text{out}}) + (w_{\text{in}} - w_{\text{out}}) = h_e - h_i \quad (\text{kJ/kg})$$

*Pump* ( $q = 0$ ):

$$w_{\text{pump,in}} = h_2 - h_1$$

$$w_{\text{pump,in}} = v(P_2 - P_1)$$

$$h_1 = h_f @ P_1 \quad \text{and} \quad v \cong v_1 = v_f @ P_1$$

*Boiler* ( $w = 0$ ):

$$q_{\text{in}} = h_3 - h_2$$

*Turbine* ( $q = 0$ ):

$$w_{\text{turb,out}} = h_3 - h_4$$

*Condenser* ( $w = 0$ ):

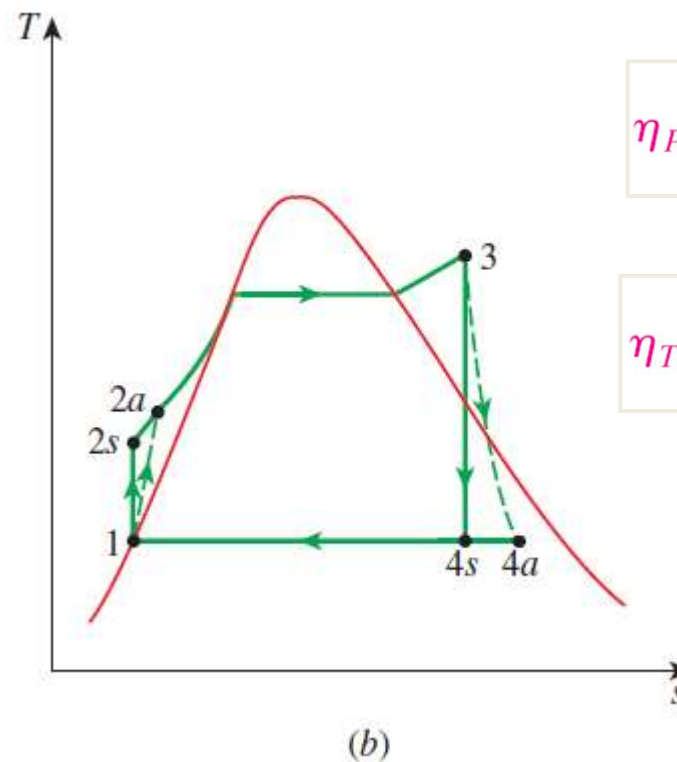
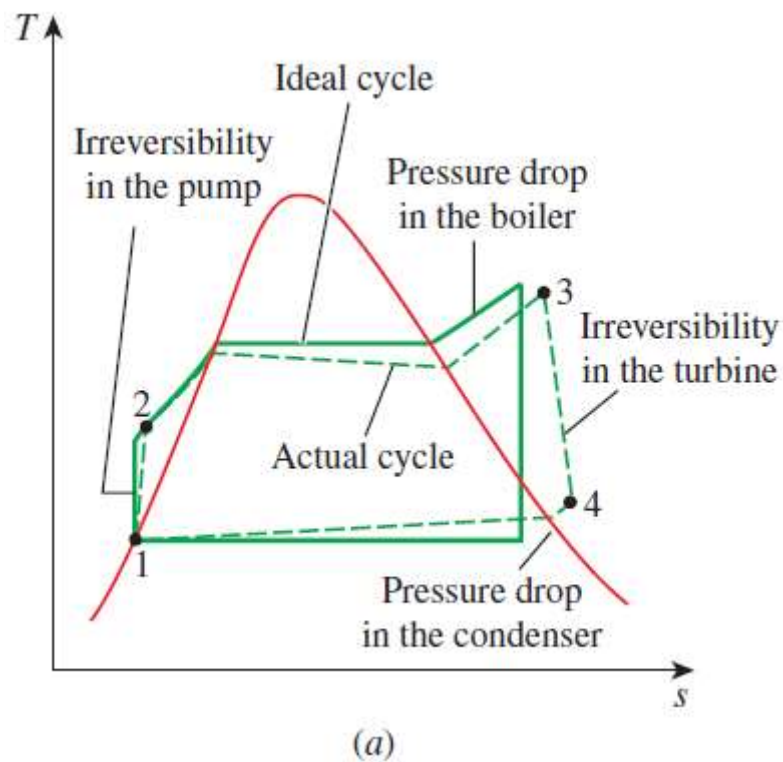
$$q_{\text{out}} = h_4 - h_1$$

$$w_{\text{net}} = q_{\text{in}} - q_{\text{out}} = w_{\text{turb,out}} - w_{\text{pump,in}}$$

$$\eta_{\text{th}} = \frac{w_{\text{net}}}{q_{\text{in}}} = 1 - \frac{q_{\text{out}}}{q_{\text{in}}}$$

# Real Vs. Ideal Rankine Cycle

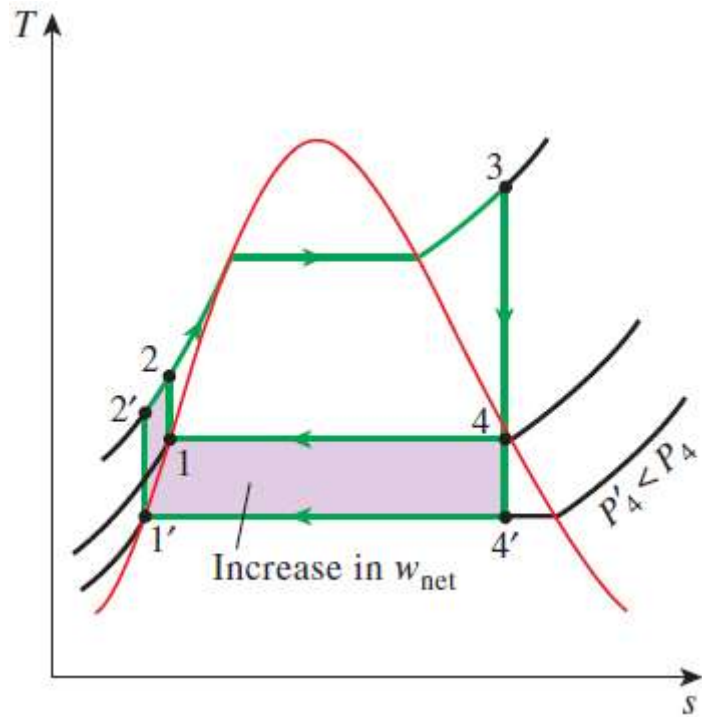
- 1-2 Isentropic compression in a pump
- 2-3 Constant pressure heat addition in a boiler
- 3-4 Isentropic expansion in a turbine
- 4-1 Constant pressure heat rejection in a condenser



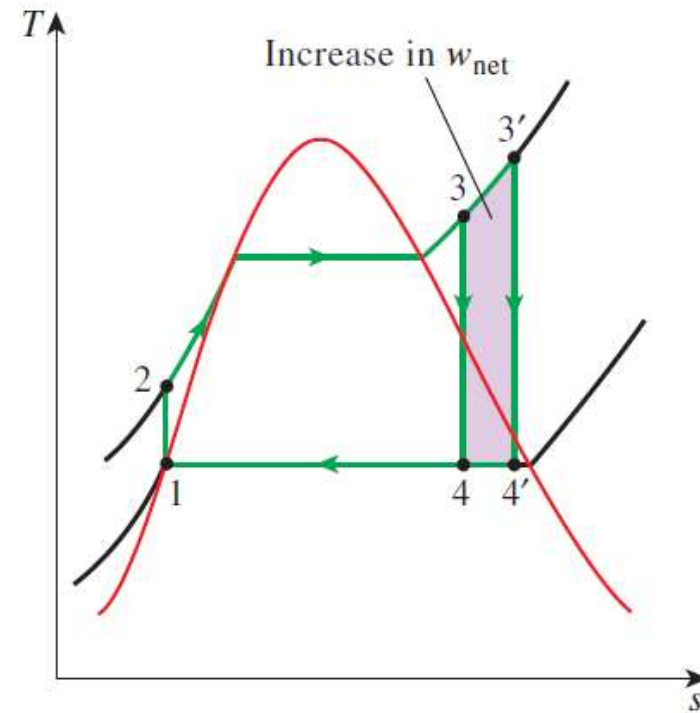
$$\eta_P = \frac{w_s}{w_a} = \frac{h_{2s} - h_1}{h_{2a} - h_1}$$

$$\eta_T = \frac{w_a}{w_s} = \frac{h_3 - h_{4a}}{h_3 - h_{4s}}$$

## *Increasing efficiency: $T_h$ higher & $T_c$ lower*



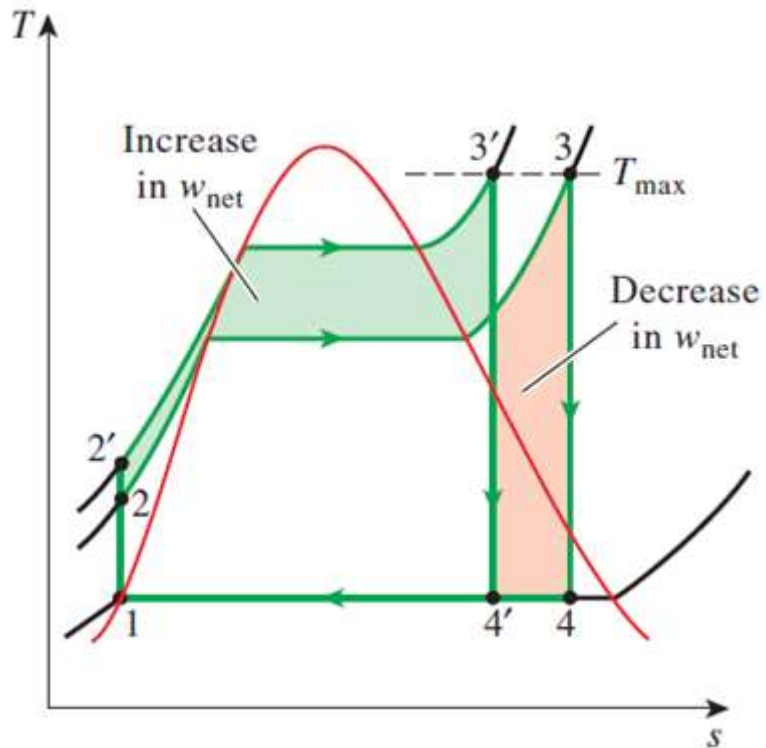
- Small increase in heat requirement
- Pressure should  $>$  sat. pr. of cooling medium
- Increased moisture



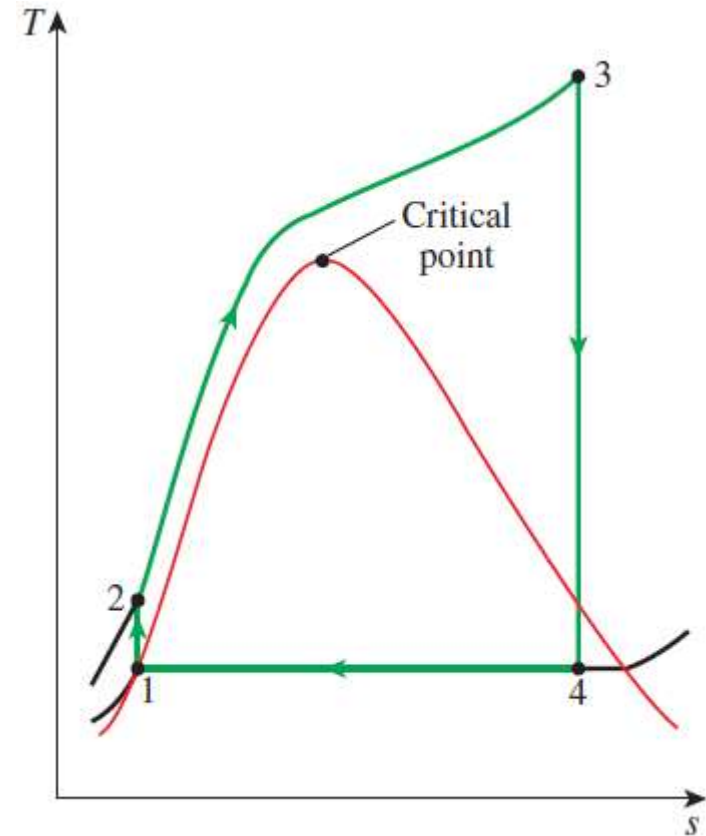
- Decreased moisture
- Material degradation at higher T



# Increasing Boiler Pressure



- Increased moisture
- Reheat





# *What's next?*

- Refrigeration cycles