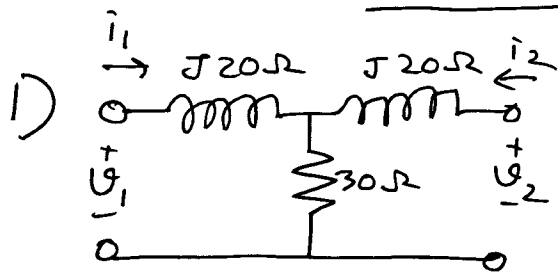


Tutorial 9 Solution



$$\begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$$

$$Z_{11} = \frac{V_1}{i_1} \Big|_{i_2=0} = (30 + j20) \Omega$$

$$Z_{12} = \frac{V_1}{i_2} \Big|_{i_1=0} = 30 \Omega$$

$$Z_{21} = \frac{V_2}{i_1} \Big|_{i_2=0} = 30 \Omega$$

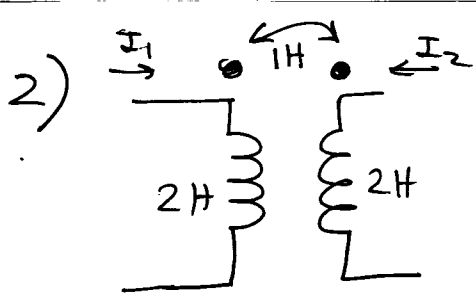
$$Z_{22} = \frac{V_2}{i_2} \Big|_{i_1=0} = (30 + j20) \Omega$$

$$\therefore Z = \begin{bmatrix} 30 + j20 & 30 \\ 30 & 30 + j20 \end{bmatrix} \Omega$$

$$Y = Z^{-1} = \frac{\begin{bmatrix} 30 + j20 & -30 \\ -30 & 30 + j20 \end{bmatrix}}{(30 + j20)^2 - 30^2} \Omega$$

= Do it yourselves.

The network is reciprocal because $Z_{21} = Z_{12}$. Also the network is completely symmetric (and hence also reciprocal) (by observation only and need not verify the mathematical conditions additionally). Also the condition $Z_{11} = Z_{22}$ is satisfied.



$$V_1 = 2j\omega I_1 + j\omega I_2 \quad \left| \begin{array}{l} \omega \text{ is} \\ \text{in rad/sec} \end{array} \right.$$

$$V_2 = 2j\omega I_2 + j\omega I_1$$

$$\therefore \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} 2j\omega & j\omega \\ j\omega & 2j\omega \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} \Omega$$

$$\therefore Z = \begin{bmatrix} 2j\omega & j\omega \\ j\omega & 2j\omega \end{bmatrix} \Omega$$

$$Y = Z^{-1} = \frac{\begin{bmatrix} 2j\omega & -j\omega \\ -j\omega & 2j\omega \end{bmatrix} \Omega}{(4-1)j^2\omega^2} = \frac{\begin{bmatrix} 2j\omega & -j\omega \\ -j\omega & 2j\omega \end{bmatrix} \Omega}{-3\omega^2}$$

Again by observation, the network is symmetric (reciprocal) and reciprocal. Also $Z_{21} = Z_{12}$ and $Z_{11} = Z_{22}$ (symmetric)

$$3) \begin{bmatrix} V_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ V_2 \end{bmatrix}$$

(i) with o/p shorted ($V_2 = 0$)

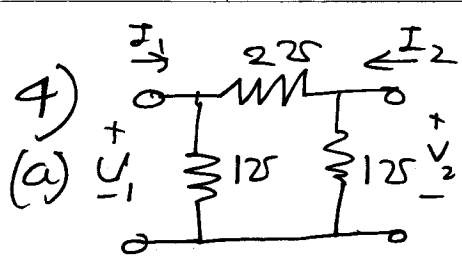
$$h_{11} = \frac{V_1}{I_1} \bigg|_{V_2=0} = \frac{25V}{1A} = 25\Omega$$

$$h_{21} = \frac{I_2}{I_1} \bigg|_{V_2=0} = \frac{2A}{1A} = 2$$

(ii) with i/p open ($I_1 = 0$)

$$h_{12} = \frac{V_1}{V_2} \bigg|_{I_1=0} = \frac{10V}{50V} = \frac{1}{5}$$

$$h_{22} = \frac{I_2}{V_2} \bigg|_{I_1=0} = \frac{2A}{50V} = \frac{1}{25} \Omega$$



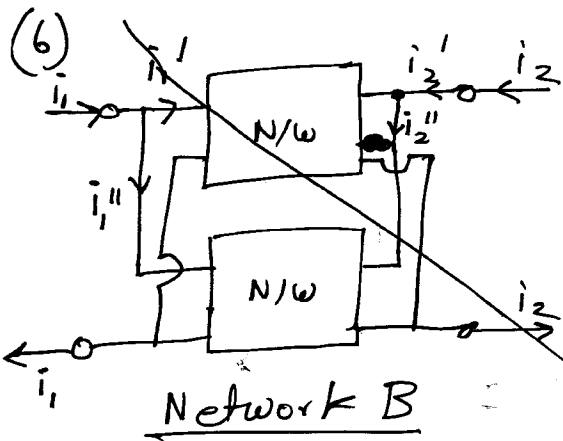
$$\begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

$$Y_{11} = \frac{I_1}{V_1} \bigg|_{V_2=0} = \frac{V_1 (125+225)}{V_1} = 325$$

$$Y_{12} = \frac{I_1}{V_2} \bigg|_{V_1=0} = \frac{-V_2 \times 225}{V_2} = -225$$

From visual/observed symmetry

$$Y_{22} = Y_{11} = 325 \quad \text{and} \quad Y_{21} = Y_{12} = -225$$



$$i_1 = i_1' + i_1''$$

$$i_2 = i_2' + i_2''$$

$$\Rightarrow \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} i_1' \\ i_2' \end{bmatrix} + \begin{bmatrix} i_1'' \\ i_2'' \end{bmatrix}$$

$$= \begin{bmatrix} Y \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} + \begin{bmatrix} Y \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

\therefore the two networks are in parallel
same voltage is applied across them

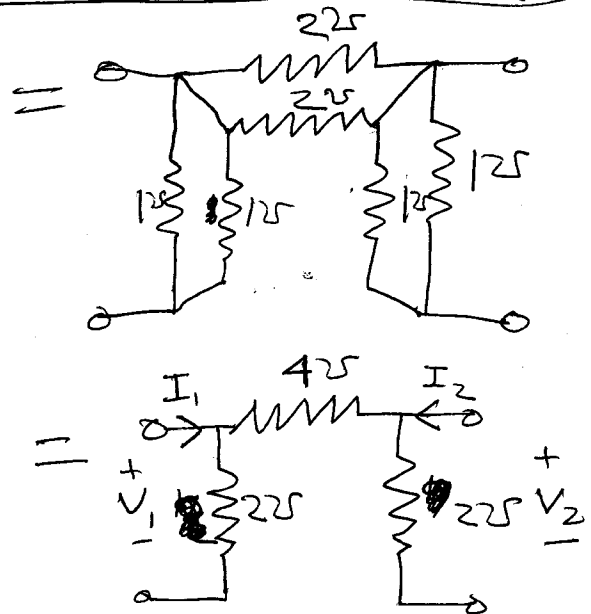
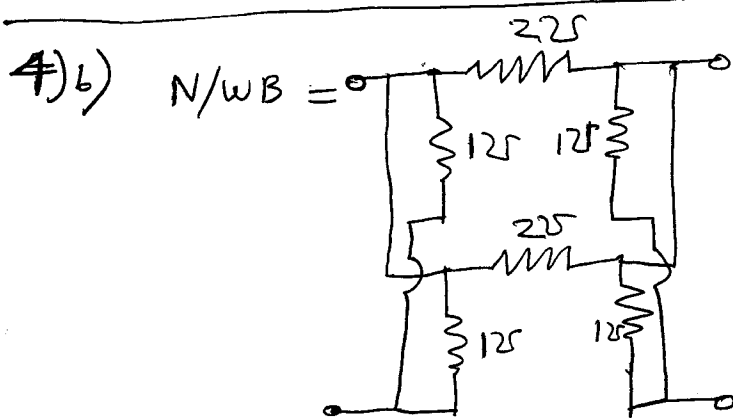
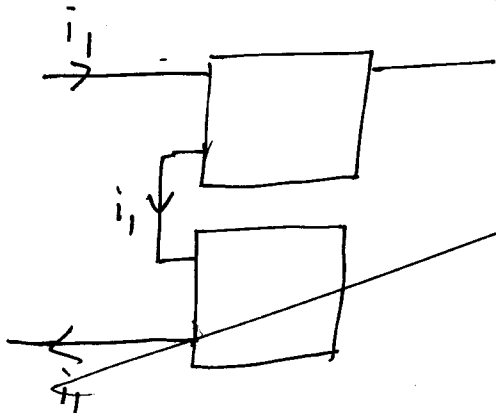
$$= 2 \times \begin{bmatrix} Y \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} 2Y \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

\therefore effective Y-parameters of N/w B

$$= 2 \times \left[Y \text{ param of N/w A} \right]$$

$$= 2 \times \begin{bmatrix} 3 & -2 \\ -2 & 3 \end{bmatrix} = \begin{bmatrix} 6 & -4 \\ -4 & 6 \end{bmatrix}$$

5) N/w A & B are in series,
 i.e. same i_1 & i_2 flows through them.
 But the voltages are added in series



Now

$$\begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

$$y_{11} = \left. \frac{I_1}{V_1} \right|_{V_2=0} = \frac{V_1 (225 + 425)}{V_1} = 650$$

$$y_{12} = \left. \frac{I_1}{V_2} \right|_{V_1=0} = \frac{-V_2 425}{V_2} = -425$$

$$y_{21} = \left. \frac{I_2}{V_1} \right|_{V_2=0} = -\frac{V_1 425}{V_1} = -425$$

$$y_{22} = \left. \frac{I_2}{V_2} \right|_{V_1=0} = \frac{V_2 (425 + 225)}{V_2} = 650$$

5) We have not discussed this theory in our class ~~and it is not~~ but it is very interesting ^{and easy}. You may read D. Roy Choudhary. This will not come in the exam.

$$6) \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} 2 & 1 \\ 3 & 0 \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} \quad (\text{given})$$

$$\Rightarrow V_1 = 2I_1 + I_2 \quad \text{--- (i)}$$

$$V_2 = 3I_1 + 0I_2 \quad \text{--- (ii)}$$

for h-parameters

$$\begin{bmatrix} V_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ V_2 \end{bmatrix}$$

$$\text{or } V_1 = h_{11}I_1 + h_{12}V_2 \quad \text{--- (iii)}$$

$$I_2 = h_{21}I_1 + h_{22}V_2 \quad \text{--- (iv)}$$

$$\text{from (ii)} \quad I_2 = \frac{V_2}{0} - \frac{3}{0}I_1$$

$$\text{putting this in (i)} \quad V_1 = 2I_1 - \frac{3}{0}I_1 + \frac{V_2}{0}$$

$$\text{comparing this with (iii)} \quad h_{11} = 2 - \frac{3}{0} = \text{undefined}$$

$$\text{and } h_{12} = \frac{1}{0} = \text{undefined.}$$

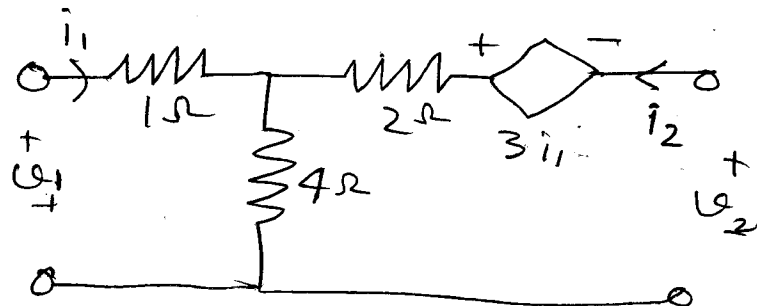
Now from (iv)

$$I_2 = \frac{V_2}{0} - \frac{3}{0}I_1 = -\frac{3}{0}I_1 + \frac{V_2}{0}$$

$$\text{comparing this with (iv)} \quad h_{21} = -\frac{3}{0} = \text{undefined}$$

$$h_{22} = \frac{1}{0} = \text{undefined.}$$

7)



$$\begin{bmatrix} U_2 \\ i_2 \end{bmatrix} = \begin{bmatrix} E & F \\ G & H \end{bmatrix} \begin{bmatrix} U_1 \\ -i_1 \end{bmatrix}$$

$$E = \frac{U_2}{U_1} \Big|_{i_1=0} \quad (\text{secondary open})$$

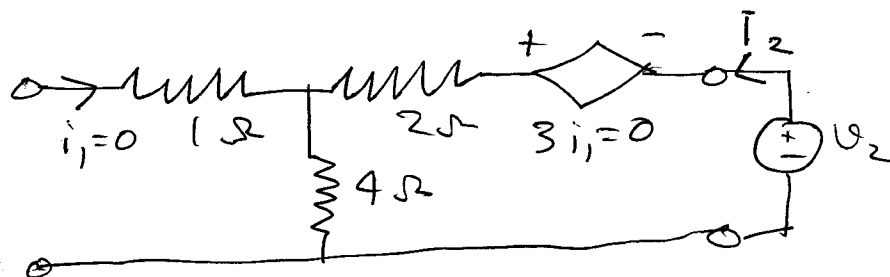
$$= \frac{U_1 \times \frac{4}{5} - 3i_1}{U_1} = \frac{4U_1}{5U_1} - \frac{3}{5} = \frac{4}{5} - \frac{3}{5} = \frac{1}{5}$$

$$G = \frac{i_2}{U_1} \Big|_{i_1=0} \quad (\text{secondary open})$$

$$E = \frac{U_2}{U_1} \Big|_{i_1=0} \quad (\text{primary open and } U_2 \text{ source connected to secondary})$$

$$E = \frac{U_2}{U_1} \Big|_{i_1=0} \quad \text{and } G = \frac{i_2}{U_1} \Big|_{i_1=0}$$

To get E open circuit primary & excite secondary with U_2 and measure U_1



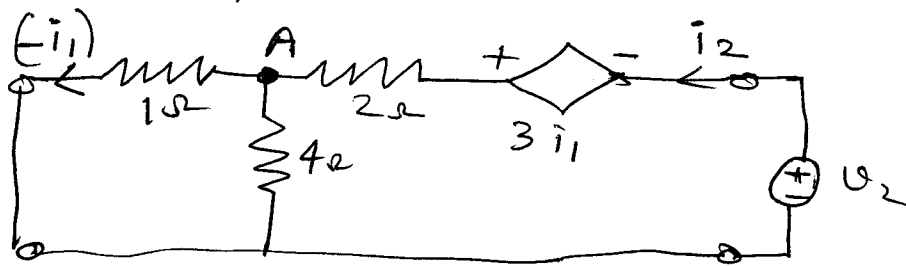
$$i_2 = \frac{U_2}{6}$$

$$U_1 = 4i_2 = \frac{4U_2}{6}$$

$$\therefore E = \frac{U_2}{U_1} \Big|_{i_1=0} = \frac{U_2}{\frac{4}{6}U_2} = \frac{6}{4} = 1.5$$

$$F = \left. \frac{v_2}{-i_1} \right|_{v_1=0}$$

To get F , short circuit primary and excite secondary with v_2 and measure $-i_1$



$$\text{KCL at A} \Rightarrow i_2 = (-i_1) + \underset{\text{outer}}{(-i_1) \times \frac{1\Omega}{4\Omega}} = \frac{5}{4}(-i_1)$$

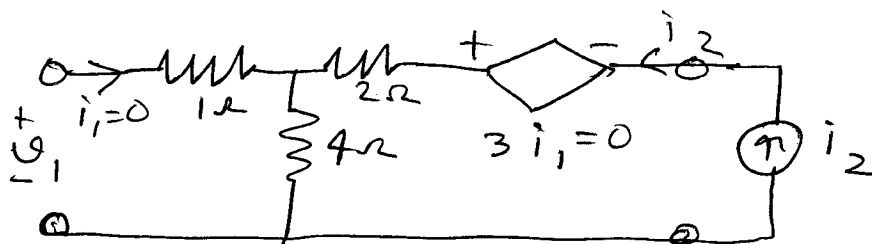
KVL in the ~~right side~~ ^{outer} loop \Rightarrow

$$\begin{aligned} v_2 &= -3i_1 + 2i_2 + 1(-i_1) \\ &= (3+1)(-i_1) + 2 \times \frac{5}{4}(-i_1) \\ &= 6.5(-i_1) \end{aligned}$$

$$\therefore F = \left. \frac{v_2}{(-i_1)} \right|_{v_1=0} = 6.5$$

$$G = \left. \frac{i_2}{v_1} \right|_{i_1=0}$$

To get G open circuit primary, excite secondary with i_2 and measure v_1



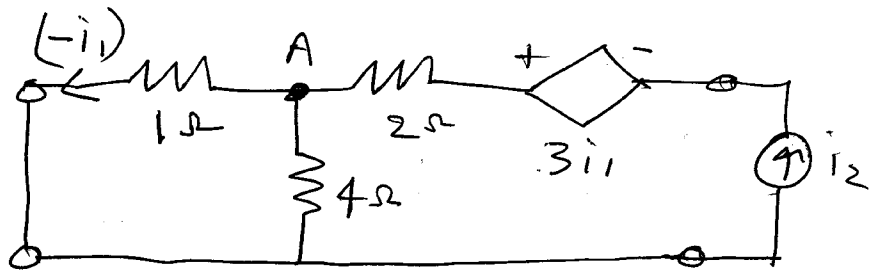
$$v_1 = 4i_2$$

$$\Rightarrow \frac{i_2}{v_1} = \frac{1}{4} = 0.25$$

$$\therefore G = \left. \frac{i_2}{v_1} \right|_{i_1=0} = 0.25$$

$$H = \left. \frac{i_2}{(-i_1)} \right|_{V_1=0}$$

To get H , short circuit primary and excite secondary with i_2 and measure (i_1) .



$$\text{KCL at A} \Rightarrow i_2 = (-i_1) + (-i_1) \times \frac{1\Omega}{4\Omega} = \frac{5}{4}(-i_1)$$

$$\therefore H = \left. \frac{i_2}{-i_1} \right|_{V_1=0} = \frac{5}{4} = 1.25$$

10) Since the network is ~~resistive and~~ linear

$$V = a I_1 + b I_2 \quad \text{for some constant values of } a \text{ \& } b$$

~~Given that~~ from given information

$$80 = a \cdot 8 + b \cdot 12$$

$$\text{and } 0 = a(-8) + b(4)$$

$$(+)\quad 80 = 16b$$

$$\Rightarrow b = 5$$

$$\therefore a = \frac{4b}{8} = 2.5$$

$$\therefore \text{ when } I_1 = I_2 = 20$$

$$V = 2.5 \times 20 + 5 \times 20 = 150$$

$$\therefore V = 150V$$

$$11) \text{ Given } V_1 = 1 I_1 + 2 I_2 \quad \text{--- (i)}$$

$$V_2 = 3 I_1 + 4 I_2 \quad \text{--- (ii)}$$

$$\text{and } V_2 = -5 I_2 \quad \text{--- (iii)}$$

substituting (iii) in (ii)

$$-5 I_2 = 3 I_1 + 4 I_2$$

$$\Rightarrow I_2 = -\frac{1}{3} I_1$$

$$\text{putting this in (i) } V_1 = I_1 + 2 \left(-\frac{1}{3}\right) I_1 \\ = \frac{1}{3} I_1$$

$$\therefore \text{ Driving point impedance} = \frac{V_1}{I_1} = \frac{1}{3} \Omega$$

13) This can have multiple solution. Obviously given a circuit its h-parameters are fixed. But given the h-parameters one can find many circuits which will have same hparameter. Here is one solution [which is motivated from the differential equivalent circuit of a BJT (bipolar Junction transistor)]

$$V_1 = h_{11} I_1 + h_{12} V_2$$

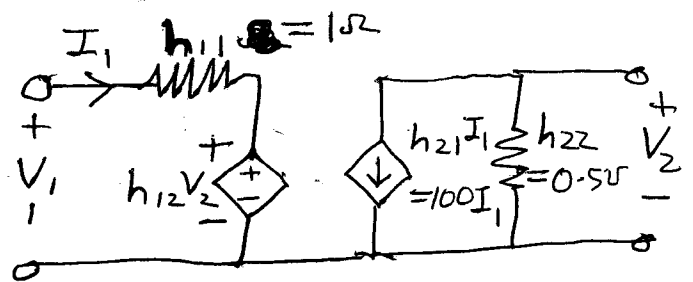
$$I_2 = h_{21} I_1 + h_{22} V_2$$

$$\text{Where } h_{11} = 1 \Omega$$

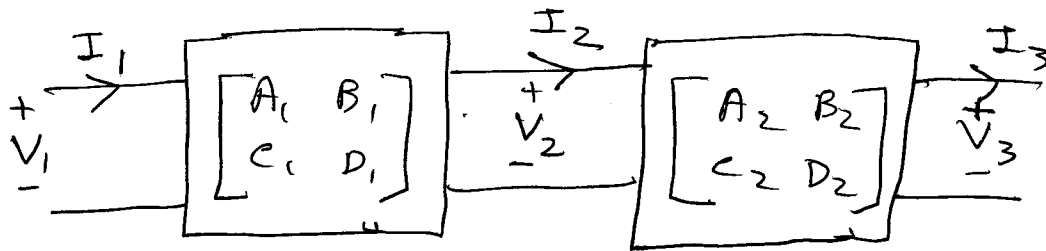
$$h_{12} = 0.1$$

$$h_{21} = 100$$

$$h_{22} = 0.5 \text{ S}$$



12) Theory : If ~~the~~ two ~~to~~ networks with known T-parameters are connected in cascade as follows



then
$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A_1 & B_1 \\ C_1 & D_1 \end{bmatrix} \begin{bmatrix} V_2 \\ I_2 \end{bmatrix} \quad \text{--- (i)}$$

and
$$\begin{bmatrix} V_2 \\ I_2 \end{bmatrix} = \begin{bmatrix} A_2 & B_2 \\ C_2 & D_2 \end{bmatrix} \begin{bmatrix} V_3 \\ I_3 \end{bmatrix} \quad \text{--- (ii)}$$

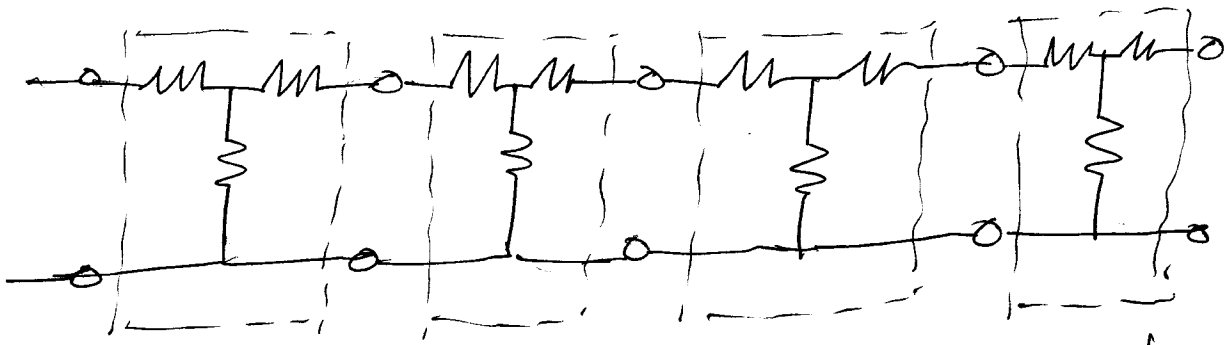
combining (i) & (ii) we get

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A_1 & B_1 \\ C_1 & D_1 \end{bmatrix} \begin{bmatrix} V_2 \\ I_2 \end{bmatrix} = \left(\begin{bmatrix} A_1 & B_1 \\ C_1 & D_1 \end{bmatrix} \begin{bmatrix} A_2 & B_2 \\ C_2 & D_2 \end{bmatrix} \right) \begin{bmatrix} V_3 \\ I_3 \end{bmatrix}$$

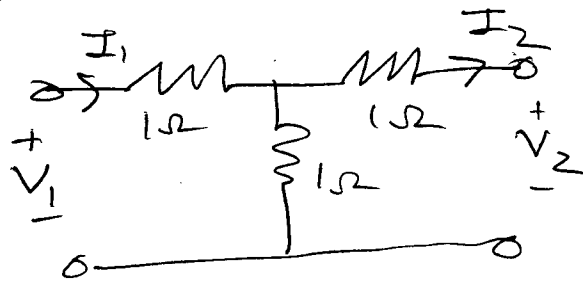
\therefore T-parameters of the two cascaded network is

$$\begin{bmatrix} A_1 & B_1 \\ C_1 & D_1 \end{bmatrix} \times \begin{bmatrix} A_2 & B_2 \\ C_2 & D_2 \end{bmatrix}$$

12) The given network ~~is~~ can be thought to be a cascade of 4 smaller networks



Let us find the T-parameters of an individual network



$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ I_2 \end{bmatrix}$$

$$A = \left. \frac{V_1}{V_2} \right|_{I_2=0} = \frac{V_1}{\frac{V_1}{2}} = 2$$

(secondary open)

$$B = \left. \frac{V_1}{I_2} \right|_{V_2=0} = \frac{V_1}{\frac{I_1}{2}} = \frac{V_1}{\left(\frac{1}{2} \times \frac{V_1}{1+\frac{1}{2}}\right)}$$

(secondary short)

$$= \frac{1}{\frac{1}{2} \times \frac{1}{1.5}} = 3$$

$$C = \left. \frac{I_1}{V_2} \right|_{I_2=0} = \frac{I_1}{I_1 \times 1} = 1$$

(secondary open)

$$D = \left. \frac{I_1}{I_2} \right|_{V_2=0} = \frac{I_1}{\frac{I_1}{2}} = 2$$

(secondary short)

$$\therefore \begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 2 & 3 \\ 1 & 2 \end{bmatrix}$$

\therefore Overall T parameters

$$= \begin{bmatrix} 2 & 3 \\ 1 & 2 \end{bmatrix}^4 = \left(\begin{bmatrix} 2 & 3 \\ 1 & 2 \end{bmatrix} \begin{bmatrix} 2 & 3 \\ 1 & 2 \end{bmatrix} \right)^2$$

$$= \begin{bmatrix} 7 & 12 \\ 4 & 7 \end{bmatrix}^2 = \begin{bmatrix} 7 & 12 \\ 4 & 7 \end{bmatrix} \begin{bmatrix} 7 & 12 \\ 4 & 7 \end{bmatrix}$$

$$= \begin{bmatrix} 97 & 168 \\ 56 & 97 \end{bmatrix}$$

14) Lets find the ABCD parameters of an individual network first



$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ I_2 \end{bmatrix}$$

$$A = \left. \frac{V_1}{V_2} \right|_{I_2=0} = \frac{V_1}{V_1 \times \frac{1}{R + \frac{1}{es}}} = \frac{1}{\frac{1}{1 + Res}} = (1 + Res)$$

$$B = \left. \frac{V_1}{I_2} \right|_{V_2=0} = \left. \frac{V_1}{I_1} \right|_{V_2=0} = \frac{V_1}{\frac{V_1}{R}} = R$$

$$C = \left. \frac{I_1}{V_2} \right|_{I_2=0} = \frac{I_1}{\frac{I_1}{e s}} = e s$$

$$D = \left. \frac{I_1}{I_2} \right|_{V_2=0} = 1$$

$$\therefore \begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1+R e s & R \\ e s & 1 \end{bmatrix}$$

\therefore ABCD Parameters of the overall/cascaded network

$$= \begin{bmatrix} 1+R e s & R \\ e s & 1 \end{bmatrix}^4 = \left(\begin{bmatrix} 1+R e s & R \\ e s & 1 \end{bmatrix} \begin{bmatrix} 1+R e s & R \\ e s & 1 \end{bmatrix} \right)^2$$

$$= \begin{bmatrix} \frac{((1+R e s)^2 + R e s)}{((1+R e s) e s + e s)} & \frac{((1+R e s) R + R)}{(R e s + 1)} \end{bmatrix}^2$$

$$= \begin{bmatrix} \frac{((1+R e s)^2 + R e s)^2 + ((1+R e s) R + R)((1+R e s) e s + e s)}{\text{something}_e} & \text{something}_B \\ \text{something}_e & \text{something}_D \end{bmatrix}$$

$$= \begin{bmatrix} \frac{(1+3 R e s + (R e s)^2)^2 + (2 R + R^2 e s)(2 e s + R^2 e s)}{\text{some } e} & \text{some } B \\ \text{some } e & \text{some } D \end{bmatrix}$$

$$\text{② } \text{~~Final~~} = \begin{bmatrix} \text{some } A & \text{some } B \\ \text{some } e & \text{some } D \end{bmatrix}$$

Where (some A) = $\frac{(1 + 3Rcs + (Rcs)^2)^2 + (2R + R^2cs)(2cs + Rcs^2)}{(1 + 3Rcs + (Rcs)^2)^2 + (2R + R^2cs)(2cs + Rcs^2)}$

~~or~~ V_{in} If we call

V_{in} = input to overall network

V_{out} = output of " "

then $V_{in} = (\text{Some A})V_{out} + (\text{Some B})I_{out}$

Where I_{out} = output current

Now under no load condition ~~or when~~

(as usual in this type of analysis), $I_{out} = 0$

$\therefore V_{out} = \frac{V_{in}}{(\text{Some A})}$ Where some A is

given above.

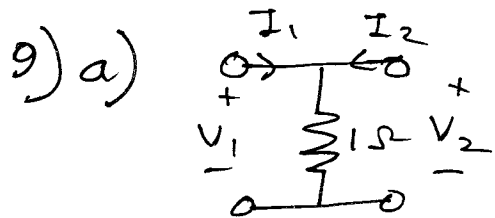
$\therefore H(s) = \frac{V_{out}}{V_{in}} = \frac{1}{\text{some A}}$

$$= \frac{1}{(1 + 3Rcs + (Rcs)^2)^2 + (2R + R^2cs)(2cs + Rcs^2)}$$

$$\therefore H(j\omega) = \frac{1}{(1 + 3Rc\omega j - R^2\omega^2)^2 + (2R + R^2c j\omega)(2c j\omega + R^2\omega^2)}$$

Now if input is $V_i = \cos(\omega t)$

output will be $|H(j\omega)| \cos(\omega t + \angle H(j\omega))$



$$\begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} z_{11} & z_{12} \\ z_{21} & z_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

$$z_{11} = \frac{V_1}{I_1} \Big|_{I_2=0} = 1$$

$$z_{21} = \frac{V_2}{I_1} \Big|_{I_2=0} = 1$$

$$z_{12} = \frac{V_1}{I_2} \Big|_{I_1=0} = 1$$

$$z_{22} = \frac{V_2}{I_2} \Big|_{I_1=0} = 1$$

$$\therefore Z = \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix}$$

so $Y = Z^{-1} = \text{undefined}$
 $[\because \det[Z] = 0]$

$$\begin{bmatrix} V_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ V_2 \end{bmatrix}$$

$$h_{11} = \frac{V_1}{I_1} \Big|_{V_2=0} = 0$$

$$h_{12} = \frac{V_1}{V_2} \Big|_{I_1=0} = 1$$

$$h_{21} = \frac{I_2}{I_1} \Big|_{V_2=0} = -1$$

$$h_{22} = \frac{I_2}{V_2} \Big|_{I_1=0} = 1$$

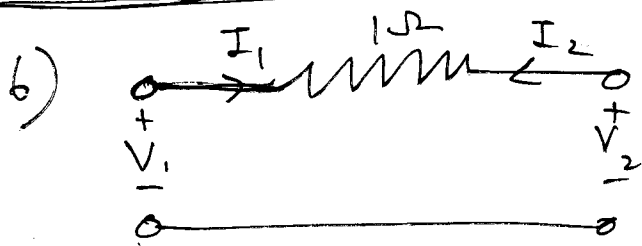
$$\therefore h = \begin{bmatrix} 0 & 1 \\ -1 & 1 \end{bmatrix}$$

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix}$$

$$A = \frac{V_1}{V_2} \Big|_{I_2=0} = 1 \quad C = \frac{I_1}{V_2} \Big|_{I_2=0} = 1$$

$$B = \frac{V_1}{-I_2} \Big|_{V_2=0} = 0 \quad D = \frac{I_1}{-I_2} \Big|_{V_2=0} = 1$$

$$\therefore \begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 1 & 1 \end{bmatrix}$$



$$\begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

$$Y_{11} = \frac{I_1}{V_1} \Big|_{V_2=0} = 1$$

$$Y_{21} = \frac{I_2}{V_1} \Big|_{V_2=0} = -1$$

$$Y_{12} = \frac{I_1}{V_2} \Big|_{V_1=0} = -1$$

$$Y_{22} = \frac{I_2}{V_2} \Big|_{V_1=0} = 1$$

$$\therefore Y = \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

$$\therefore Z = Y^{-1} = \text{undefined}$$

$$[\because \det[Y] = 0]$$

$$\begin{bmatrix} V_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ V_2 \end{bmatrix}$$

$$h_{11} = \frac{V_1}{I_1} \Big|_{V_2=0} = 1$$

$$\therefore h = \begin{bmatrix} 1 & 1 \\ -1 & 0 \end{bmatrix}$$

$$h_{12} = \frac{V_1}{V_2} \Big|_{I_1=0} = 1$$

$$h_{21} = \frac{I_2}{I_1} \Big|_{V_2=0} = -1$$

$$h_{22} = \frac{I_2}{V_2} \Big|_{I_1=0} = 0$$

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix}$$

$$A = \left. \frac{V_1}{V_2} \right|_{I_2=0} = 1 \quad \left| \quad C = \left. \frac{I_1}{V_2} \right|_{I_2=0} = 0 \right.$$

$$B = \left. \frac{V_1}{-I_2} \right|_{V_2=0} = 1 \quad \left| \quad D = \left. \frac{I_1}{-I_2} \right|_{V_2=0} = 1 \right.$$

$$\therefore \begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}$$
