

Software Requirements Specification for Slope Stability analysis Program

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1 Reference Material

This section records information for easy reference.

1.1 Table of Units

The unit system used throughout is SI (Système International d’Unités). In addition to the basic units, several derived units are also used. For each unit, the table lists the symbol, a description and the SI name.

Symbol	Description
°	angle (degree)
kg	mass (kilogram)
m	length (metre)
N	force (newton)
Pa	pressure (pascal)
s	time (second)

Table 1

1.2 Table of Symbols

The table that follows summarizes the symbols used in this document along with their units. Throughout the document, values with a subscript i implies that the value will be taken at and analyzed at a slice or slice interface composing the total slip mass.

Symbol	Description	Units
(x, y)	Cartesian Position Coordinates: y is considered parallel to the direction of the force of gravity and x is considered perpendicular to y	m
A	Area: A part of an object or surface	m^2
\mathbf{a}	Acceleration: The rate of change of a body’s velocity	$\frac{m}{s^2}$
\mathbf{b}	Base Width of Slices: in the x-direction	m
C_{den}	Proportionality Constant Denominator: values for each slice that sum together to form the denominator of the interslice normal to shear force proportionality constant	N
C_{num}	Proportionality Constant Numerator: values for each slice that sum together to form the numerator of the interslice normal to shear force proportionality constant	N
c'	Effective Cohesion: internal pressure that sticks particles of soil together	Pa

Symbol	Description	Units
$const_f$	Decision on F: boolean decision on which form of f the user desires: constant if true, or half-sine if false	–
F_{rot}	Force Causing Rotation: a force in the direction of rotation	N
F_S	Factor of Safety: The global stability metric of a slip surface of a slope, defined as the ratio of resistive shear force to mobilized shear force	–
F_x	X-Component of the Force:	N
F_y	Y-Component of the Force:	N
F_S^{min}	Minimum Factor of Safety: The minimum factor of safety associated with the critical slip surface	–
F	Force: An interaction that tends to produce change in the motion of an object	N
\mathbf{F}_x^G	Sums of the Interslice Normal Forces: for each pair of adjacent interslice boundaries	N
\mathbf{F}_x^H	Sums of the Interslice Normal Water Forces: for each pair of adjacent interslice boundaries	N
f	Interslice Normal to Shear Force Ratio Variation Function: function of distance in the x-direction	–
g	Gravitational Acceleration: An expression used in physics to indicate the intensity of a gravitational field	$\frac{m}{s^2}$
G	Interslice Normal Forces: per meter in the z-direction exerted between each pair of adjacent slices	$\frac{N}{m}$
H	Interslice Normal Water Forces: per meter in the z-direction exerted in the x-coordinate direction between each pair of adjacent slices	$\frac{N}{m}$
h	Y-Direction Heights of Slices: heights in the y-direction from the base of each slice to the slope surface, at the x-direction midpoint of the slice	m
\mathbf{h}^L	Heights of the Left Side of Slices: assuming slice surfaces have negative slope	m
\mathbf{h}^R	Heights of the Right Side of Slices: assuming slice surfaces have negative slope	m
\mathbf{h}_z	Heights of Interslice Normal Forces: the heights in the y-direction of the interslice normal forces on each slice	m
$\mathbf{h}_{z,w}$	Heights of the Water Table: the heights in the y-direction from the base of each slice to the watertable	m
i	Index: representing a single slice	–
j	Unit Vector: A vector that has a magnitude of one	–

Symbol	Description	Units
K_c	Seismic Coefficient: proportionality factor of force that weight pushes outwards; caused by seismic earth movements	–
M	Moment: a measure of the tendency of a body to rotate about a specific point or axis	Nm
m	Mass: the quantity of matter in a body	kg
n	Number of Slices: the slip mass has been divided into	–
N	Normal Forces: total reactive forces per meter in the z-direction for each slice of a soil surface subject to a body resting on it	$\frac{N}{m}$
N'	Effective Normal Forces: per meter in the z-direction for each slice of a soil surface, subtracting pore water reactive force from total reactive force	$\frac{N}{m}$
P	Resistive Shear Force: Mohr Coulomb frictional force that describes the limit of mobilized shear force that can be withstood before failure	N
P	Resistive Shear Forces: Mohr Coulomb frictional forces per meter in the z-direction for each slice that describes the limit of mobilized shear force the slice can withstand before failure	$\frac{N}{m}$
Q	External Forces: forces per meter in the z-direction acting into the surface from the midpoint of each slice	$\frac{N}{m}$
r	Length of the Moment Arm: distance between a force causing rotation and the axis of rotation	m
R	Resistive Shear Forces Without the Influence of Interslice Forces: per meter in the z-direction for each slice	$\frac{N}{m}$
r	Displacement: The change in An object's location relative to a reference point	m
S	Mobilized Shear Force: shear force in the direction of potential motion	N
S	Mobilized Shear Forces: per meter in the z-direction for each slice	$\frac{N}{m}$
T	Mobilized Shear Forces Without the Influence of Interslice Forces: per meter in the z-direction for each slice	$\frac{N}{m}$
u	Pore Pressure: from water within the soil	Pa
U_b	Base Hydrostatic Forces: per meter in the z-direction from water pressure within each slice	$\frac{N}{m}$
U_t	Surface Hydrostatic Forces: per meter in the z-direction from water pressure acting into each slice from standing water on the slope surface	$\frac{N}{m}$
V	Volume: the amount of space that a substance or object occupies.	m^3

Symbol	Description	Units
v	Local Index: used as a bound variable index in calculations	–
V_{dry}	Volumes of Dry Soil: amount of space occupied by dry soil for each slice	m^3
V_{sat}	Volumes of Saturated Soil: amount of space occupied by saturated soil for each slice	m^3
V_{wat}	Volumes of Water: amount of space occupied by water for each slice	m^3
W	Weight: The gravitational force acting on an object	N
\mathbf{W}	Weights: downward force per meter in the z-direction on each slice caused by gravity	$\frac{N}{m}$
x	X-Coordinate: in the Cartesian coordinate system	m
x_{slip}^{maxEtr}	Maximum Entry X-Coordinate: maximum potential x-coordinate for the entry point of a slip surface	m
x_{slip}^{maxExt}	Maximum Exit X-Coordinate: maximum potential x-coordinate for the exit point of a slip surface	m
x_{slip}^{minEtr}	Minimum Exit X-Coordinate: minimum potential x-coordinate for the entry point of a slip surface	m
x_{slip}^{minExt}	Minimum Exit X-Coordinate: minimum potential x-coordinate for the exit point of a slip surface	m
\mathbf{X}	Interslice Shear Forces: per meter in the z-direction exerted between adjacent slices	$\frac{N}{m}$
$\mathbf{x}_{cs}, \mathbf{y}_{cs}$	The Set of X and Y Coordinates: describe the vertices of the critical slip surface	m
\mathbf{x}_{slip}	X-Coordinates of the Slip Surface: x-coordinates of points on the slip surface	m
\mathbf{x}_{slope}	X-Coordinates of the Slope: x-coordinates of points on the soil slope	m
\mathbf{x}_{wt}	X-Coordinates of the Water Table: x-positions of the water table	m
y	Y-Coordinate: in the Cartesian coordinate system	m
y_{slip}^{max}	Maximum Y-Coordinate: maximum potential y-coordinate of a point on a slip surface	m
y_{slip}^{min}	Minimum Y-Coordinate: minimum potential y-coordinate of a point on a slip surface	m
\mathbf{y}_{slip}	Y-Coordinates of the Slip Surface: heights of the slip surface	m
\mathbf{y}_{slope}	Y-Coordinates of the Slope: y-coordinates of points on the soil slope	m
\mathbf{y}_{wt}	Y-Coordinates of the Water Table: heights of the water table	m
z	Z-Coordinate: in the Cartesian coordinate system	m

Symbol	Description	Units
	Base Angles: between the base of each slice and the horizontal	°
	Surface Angles: between the surface of each slice and the horizontal	°
γ	Specific Weight: weight per unit volume	$\frac{\text{N}}{\text{m}^3}$
γ_{dry}	Soil Dry Unit Weight: The weight of a dry soil/ground layer divided by the volume of the layer.	$\frac{\text{N}}{\text{m}^3}$
γ_{Sat}	Soil Saturated Unit Weight: The weight of saturated soil/ground layer divided by the volume of the layer.	$\frac{\text{N}}{\text{m}^3}$
γ_w	Unit Weight of Water: The weight of one cubic meter of water.	$\frac{\text{N}}{\text{m}^3}$
λ	Proportionality Constant: for the interslice normal to shear force ratio	—
π	Circumference to Diameter Ratio: The ratio of a circle's circumference to its diameter	—
ρ	Density: mass per unit volume	$\frac{\text{kg}}{\text{m}^3}$
σ	Total Stress: on the soil mass	Pa
σ'	Effective Stress: provided by the soil skeleton	Pa
σ_N'	Effective Normal Stress:	Pa
τ	Shear Strength:	Pa
τ	Torque: A twisting force that tends to cause rotation	Nm
Υ	Minimization Function: generic minimization function or algorithm	—
	First Function for Incorporating Interslice Forces Into Shear Force: converts resistive shear without the influence of interslice forces, to a calculation considering the interslice forces	—
φ'	Effective Angle of Friction: The angle of inclination with respect to the horizontal axis of the Mohr-Coulomb shear resistance line	°
	Second Function for Incorporating Interslice Forces Into Shear Force: converts mobile shear without the influence of interslice forces, to a calculation considering the interslice forces	—
	Imposed Load Angles: between the external force acting into the surface of each slice and the vertical	°
b	Total Base Lengths of Slices: in the direction parallel to the slope of the base of each slice	m

Table 2

1.3 Abbreviations and Acronyms

Abbreviation	Full Form
2D	two-dimensional
3D	three-dimensional
A	Assumption
DD	Data Definition
GD	General Definition
GS	Goal Statement
IM	Instance Model
LC	Likely Change
PS	Physical System Description
R	Requirement
SRS	Software Requirements Specification
SSP	Slope Stability analysis Program
TM	Theoretical Model
UC	Unlikely Change
Uncert.	Typical Uncertainty

Table 3

2 Introduction

A slope of geological mass, composed of soil and rock and sometimes water, is subject to the influence of gravity on the mass. This can cause instability in the form of soil or rock movement. The effects of soil or rock movement can range from inconvenient to seriously hazardous, resulting in significant life and economic losses. Slope stability is of interest both when analysing natural slopes, and when designing an excavated slope. Slope stability analysis is the assessment of the safety of a slope, identifying the surface most likely to experience slip and an index of its relative stability known as the factor of safety. The following section provides an overview of the Software Requirements Specification (SRS) for a slope stability analysis problem. The developed program will be referred to as the Slope Stability analysis Program (SSP). This section explains the purpose of this document, the scope of the system, the characteristics of the intended reader, and the organization of the document.

2.1 Purpose of Document

The primary purpose of this document is to record the requirements of SSP and the models that will be used to meet those requirements. Goals, assumptions, theoretical models, definitions, and other model derivation information are specified, allowing the reader to fully understand and verify the purpose and scientific basis of SSP. With the exception of system constraints in [Section: System Constraints](#), this SRS will remain abstract, describing what problem is being solved, but not how to solve it. This document will be used as a starting

point for subsequent development phases, including writing the design specification and the software verification and validation plan. The design document will show how the requirements are to be realized, including decisions on the numerical algorithms and programming environment. The verification and validation plan will show the steps that will be used to increase confidence in the software documentation and the implementation. Although the SRS fits in a series of documents that follow the so-called waterfall model, the actual development process is not constrained in any way. Even when the waterfall model is not followed, as Parnas and Clements point out [6], the most logical way to present the documentation is still to “fake” a rational design process.

2.2 Scope of Requirements

The scope of the requirements includes stability analysis of a two-dimensional (2D) soil mass, composed of a single homogeneous layer with constant material properties. The soil mass is assumed to extend infinitely in the third dimension. The analysis will be at an instant in time; factors that may change the soil properties over time will not be considered.

2.3 Characteristics of Intended Reader

Reviewers of this documentation should have an understanding of undergraduate level 4 physics and undergraduate level 2 or higher solid mechanics. It would be an asset to understand soil mechanics. The users of SSP can have a lower level of expertise, as explained in [Section: User Characteristics](#).

2.4 Organization of Document

The organization of this document follows the template for an SRS for scientific computing software proposed by Koothoor [4] as well as Smith and Lai [8]. The presentation follows the standard pattern of presenting goals, theories, definitions, and assumptions. For readers that would like a more bottom up approach, they can start reading the instance models in [Section: Instance Models](#) and trace back to find any additional information they require. The goal statements ([Section: Goal Statements](#)) are refined to the theoretical models, and the theoretical models ([Section: Theoretical Models](#)) to the instance models ([Section: Instance Models](#)). The instance models provide the set of algebraic equations that must be solved.

3 General System Description

This section provides general information about the system. It identifies the interfaces between the system and its environment, describes the user characteristics, and lists the system constraints.

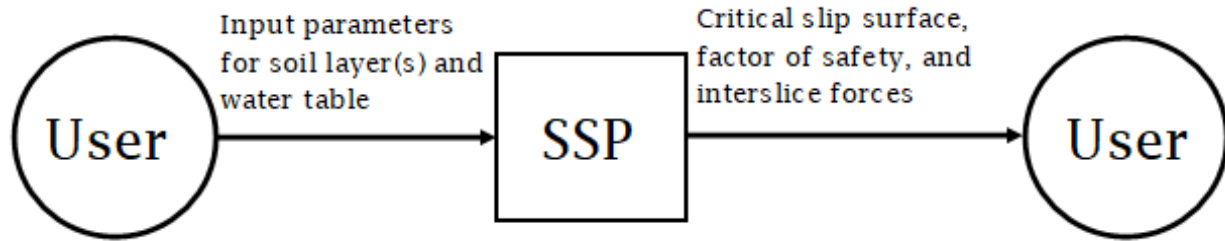


Figure 1: System Context

3.1 System Context

Fig:sysCtxDiag shows the system context. A circle represents an external entity outside the software. A rectangle represents the software system itself (SSP). Arrows are used to show the data flow between the system and its environment. The responsibilities of the user and the system are as follows:

- User Responsibilities
 - Provide the input data related to the soil layer(s) and water table (if applicable), ensuring conformation to input data format required by SSP
 - Ensure that consistent units are used for input variables
 - Ensure required software assumptions (**Section: Assumptions**) are appropriate for the problem to which the user is applying the software
- SSP Responsibilities
 - Detect data type mismatch, such as a string of characters input instead of a floating point number
 - Verify that the inputs satisfy the required physical and other data constraints (**Section: Data Constraints**)
 - Identify the critical slip surface within the possible input range
 - Find the factor of safety for the slope
 - Find the interslice normal force and shear force along the critical slip surface

3.2 User Characteristics

The end user of SSP should have an understanding of undergraduate Level 1 Calculus and Physics, and be familiar with soil and material properties, specifically effective cohesion, effective angle of friction, and unit weight.

3.3 System Constraints

The Morgenstern-Price method [5], which involves dividing the slope into vertical slices, will be used to derive the equations for analysing the slope.

4 Specific System Description

This section first presents the problem description, which gives a high-level view of the problem to be solved. This is followed by the solution characteristics specification, which presents the assumptions, theories, and definitions that are used.

4.1 Problem Description

SSP is a computer program developed to evaluate the factor of safety of a slope's slip surface and identify the critical slip surface of the slope, as well as the interslice normal force and shear force along the critical slip surface. It is intended to be used as an educational tool for introducing slope stability issues, and to facilitate the analysis and design of a safe slope.

4.1.1 Terminology and Definitions

This subsection provides a list of terms that are used in the subsequent sections and their meaning, with the purpose of reducing ambiguity and making it easier to correctly understand the requirements.

- Factor of Safety: The global stability metric of a slip surface of a slope, defined as the ratio of resistive shear force to mobilized shear force
- Slip Surface: A surface within a slope that has the potential to fail or displace due to load or other forces.
- Critical Slip Surface: Slip surface of the slope that has the lowest factor of safety, and is therefore most likely to experience failure.
- Water Table: The upper boundary of a saturated zone in the ground.
- Stress: Forces that are exerted between planes internal to a larger body subject to external loading.
- Strain: A measure of deformation of a body or plane under stress.
- Normal Force: A force applied perpendicular to the plane of the material.
- Shear Force: A force applied parallel to the plane of the material.
- Mobilized Shear Force: Shear force in the direction of potential motion, thus encouraging motion along the plane.

Resistive Shear Force: Shear force in the direction opposite to the direction of potential motion, thus hindering motion along the plane.

Forces and Stresses: The normal force or normal stress carried by the soil skeleton. The total normal force or normal stress is composed of the effective force or stress and the force or stress exerted by water.

Cohesion: An attractive force between adjacent particles that holds the matter together.

Isotropy: A condition where the value of a property is independent of the direction in which it is measured.

Plane Strain: A condition where the resultant stresses in one of the directions of a three-dimensional material can be approximated as zero. This condition results when a body is constrained to not deform in one direction, or when the length of one dimension of the body dominates the others, to the point where it can be assumed as infinite. Stresses in the direction of the dominant dimension can be approximated as zero.

4.1.2 Physical System Description

The Physical System Description (PS) of SSP, as shown in [Fig:PhysicalSystem](#), includes the following elements:

PS1: A slope comprised of one soil layer.

PS2: A water table, which may or may not exist.

Morgenstern-Price analysis [5] of the slope involves representing the slope as a series of vertical slices. As shown in [Fig:IndexConvention](#), the index i is used to denote a value for a single slice, and an interslice value at a given index i refers to the value between slice i and adjacent slice $i + 1$. A free body diagram of the forces acting on a slice is displayed in [Fig:ForceDiagram](#). The specific forces and symbols will be discussed in detail in [Section: General Definitions](#) and [Section: Data Definitions](#).

4.1.3 Goal Statements

Given the shape of the soil mass, the location of the water table, and the material properties of the soil, the goal statements are:

Identify-Crit-and-FS: Identify the critical slip surface and the corresponding factor of safety.

Interslice-Normal-Forces: Determine the interslice normal forces between each pair of vertical slices of the slope.

Interslice-Shear-Forces: Determine the interslice shear forces between each pair of vertical slices of the slope.



Figure 2: An example slope for analysis by SSP, where the dashed line represents the water table



Figure 3: Index convention for slice and interslice values



Figure 4: Free body diagram of forces acting on a slice

4.2 Solution Characteristics Specification

The instance models that govern SSP are presented in [Section: Instance Models](#). The information to understand the meaning of the instance models and their derivation is also presented, so that the instance models can be verified.

4.2.1 Assumptions

This section simplifies the original problem and helps in developing the theoretical model by filling in the missing information for the physical system. The numbers given in the square brackets refer to the Theoretical Models [Section: Theoretical Models](#), General Definitions [Section: General Definitions](#), Data Definitions [Section: Data Definitions](#), Instance Models [Section: Instance Models](#), Likely Changes [Section: Likely Changes](#), or Unlikely Changes [Section: Unlikely Changes](#), in which the respective assumption is used.

Up-Surface-Concave: The slip surface is concave with respect to the slope surface. The $(\mathbf{x}_{slip}, \mathbf{y}_{slip})$ coordinates of a slip surface follow a concave up function. [IM: crtSlpId](#).

Factor-of-Safety: The factor of safety is assumed to be constant across the entire slip surface. [GD: mobShr](#).

Layer-Homogeneous: The soil mass is homogeneous, with consistent soil properties throughout. [GD: sliceWght](#) [GD: resShr](#) [LC: Calculate-Inhomogeneous-Soil-Layers](#).

Soil-Properties: The soil properties are independent of dry or saturated conditions, with the exception of unit weight. [GD: resShr](#).

Soil-Layers-Isotropic: The soil mass is treated as if the effective cohesion and effective angle of friction are isotropic properties. [GD: resShr](#).

Interslice-Forces-Linear: Following the assumption of Morgenstern and Price ([5]), interslice normal forces and interslice shear forces have a proportional relationship, depending on a proportionality constant (λ) and a function (\mathbf{f}) describing variation depending on x position. [IM: nrmShrFor](#) [GD: normShrR](#) [IM: fctSfty](#) [UC: Normal-And-Shear-Linear-Only](#).

Plane-Strain-Conditions: The slope and slip surface extends far into and out of the geometry (z coordinate). This implies plane strain conditions, making 2D analysis appropriate. [GD: srfWtrF](#) [GD: sliceWght](#) [GD: sliceWght](#) [GD: sliceWght](#) [GD: resShr](#) [GD: effNormF](#) [GD: baseWtrF](#).

Effective-Stress-Large: The effective normal stress is large enough that the shear strength to effective normal stress relationship can be approximated as a linear relationship. [TM: equilibrium](#) [UC: 2D-Analysis-Only](#).

Slice-Straight-Lines: The surface and base of a slice are approximated as straight lines. [GD: srfWtrF](#) [GD: sliceWght](#) [TM: mcShrStrgth](#) [DD: slcHeight](#) [DD: angleB](#) [GD: baseWtrF](#) [DD: angleA](#).

Edge-Slices: The interslice forces at the 0th and n th interslice interfaces are zero. **IM:** `nrmShrFor` **IM:** `intsliceFs` **IM:** `fctSfty`.

Seismic-Force: There is no seismic force acting on the slope. **IM:** `nrmShrFor` **IM:** `fctSfty` **LC:** `Calculate-Seismic-Force`.

Surface-Load: There is no imposed surface load, and therefore no external forces, acting on the slope. **IM:** `nrmShrFor` **IM:** `fctSfty` **LC:** `Calculate-External-Force`.

Intersects-Base-Edge: The water table only intersects the base of a slice at an edge of the slice. **GD:** `sliceWght` **GD:** `baseWtrF`.

Intersects-Surface-Edge: The water table only intersects the slope surface at the edge of a slice. **GD:** `srfWtrF` **GD:** `sliceWght`.

Surface-Slope-Seismic: The effect of the slope of the surface of the soil on the seismic force is assumed to be negligible. **GD:** `momentEq1`.

Force-Slice-Midpoint: The resultant surface hydrostatic forces act into the midpoint of each slice surface and the resultant base hydrostatic forces act into the midpoint of each slice base. **GD:** `momentEq1` **GD:** `momentEq1`.

4.2.2 Theoretical Models

This section focuses on the general equations and laws that SSP is based on.

Refname	TM:factOfSafety
Label	Factor of safety
Equation	$F_S = \frac{P}{S}$
Description	<p>F_S is the factor of safety (Unitless)</p> <p>P is the resistive shear force (N)</p> <p>S is the mobilized shear force (N)</p>
Source	[1]
RefBy	GD: <code>mobShr</code> .

Refname	TM:equilibrium
Label	Equilibrium
Equation	$\sum F_x = \sum F_y = \sum M = 0$
Description	<p> F_x is the x-component of the force (N) F_y is the y-component of the force (N) M is the moment (Nm) </p>
Notes	<p>For a body in static equilibrium, the net forces and moments acting on the body will cancel out. Assuming a 2D problem (A: Effective-Norm-Stress-Large), the x-component of the force F_x and y-component of the force F_y will be equal to 0. All forces and their distance from the chosen point of rotation will create a net moment equal to 0.</p>
Source	[1]
RefBy	GD: normForceEq GD: momentEqI GD: bsShrFEq.

Refname	TM:mcShrStrgth
Label	Mohr-Coulumb shear strength
Equation	$\tau = \sigma_N' \tan(\varphi') + c'$
Description	<p> τ is the shear strength (Pa) σ_N' is the effective normal stress (Pa) φ' is the effective angle of friction (°) c' is the effective cohesion (Pa) </p>
Notes	<p>In this model the shear strength τ is proportional to the product of the effective normal stress σ_N' on the plane with its static friction in the angular form $\tan(\varphi')$. The τ versus σ_N' relationship is not truly linear, but assuming the effective normal forces is strong enough, it can be approximated with a linear fit (A: Surface-Base-Slice-between-Interslice-Straight-Lines) where the effective cohesion c' represents the τ intercept of the fitted line.</p>
Source	[1]
RefBy	GD: resShr.

Refname	TM:effStress
Label	Effective stress
Equation	$\sigma' = \sigma - u$
Description	<p>σ' is the effective stress (Pa) σ is the total stress (Pa) u is the pore pressure (Pa)</p>
Notes	σ is defined in DD: stress .
Source	[1]
RefBy	GD: effNormF .

Refname	TM:NewtonSecLawMot
Label	Newton's second law of motion
Equation	$\mathbf{F} = m\mathbf{a}$
Description	<p>\mathbf{F} is the force (N) m is the mass (kg) \mathbf{a} is the acceleration ($\frac{\text{m}}{\text{s}^2}$)</p>
Notes	The net force \mathbf{F} (N) on a body is proportional to the acceleration \mathbf{a} ($\frac{\text{m}}{\text{s}^2}$) of the body, where m (kg) denotes the mass of the body as the constant of proportionality.
Source	—
RefBy	GD: weight.

4.2.3 General Definitions

This section collects the laws and equations that will be used to build the instance models.

Refname	GD:normForceEq
Label	Normal force equilibrium
Units	$\frac{N}{m}$
Equation	$\mathbf{N}_i = (\mathbf{W}_i - \mathbf{X}_{i-1} + \mathbf{X}_i + \mathbf{U}_{t,i} \cos(\alpha_i) + \mathbf{Q}_i \cos(\alpha_i)) \cos(\alpha_i) + (-K_c \mathbf{W}_i - \mathbf{G}_i + \mathbf{G}_{i-1} -$
Description	<p> \mathbf{N} is the normal forces ($\frac{N}{m}$) i is the index (Unitless) \mathbf{W} is the weights ($\frac{N}{m}$) \mathbf{X} is the interslice shear forces ($\frac{N}{m}$) \mathbf{U}_t is the surface hydrostatic forces ($\frac{N}{m}$) α is the surface angles ($^\circ$) \mathbf{Q} is the external forces ($\frac{N}{m}$) β is the imposed load angles ($^\circ$) γ is the base angles ($^\circ$) K_c is the seismic coefficient (Unitless) \mathbf{G} is the interslice normal forces ($\frac{N}{m}$) \mathbf{H} is the interslice normal water forces ($\frac{N}{m}$) </p>
Notes	<p> This equation satisfies TM: equilibrium in the normal direction. \mathbf{W} is defined in GD: sliceWght, \mathbf{U}_t is defined in GD: srfWtrF, α is defined in DD: angleB, and β is defined in DD: angleA. </p>
Source	[7]

RefBy **IM: fctSfty.**

Normal force equilibrium is derived from the free body diagram of **Fig:ForceDiagram** in **Section: Physical System Description**.

Refname	GD:bsShrFEq
Label	Base shear force equilibrium
Units	$\frac{N}{m}$
Equation	$S_i = (W_i - X_{i-1} + X_i + U_{t,i} \cos(i) + Q_i \cos(i)) \sin(i) - (-K_c W_i - G_i + G_{i-1} -$
Description	<p> S is the mobilized shear force ($\frac{N}{m}$) <i>i</i> is the index (Unitless) W is the weights ($\frac{N}{m}$) X is the interslice shear forces ($\frac{N}{m}$) U_t is the surface hydrostatic forces ($\frac{N}{m}$) is the surface angles (°) Q is the external forces ($\frac{N}{m}$) is the imposed load angles (°) is the base angles (°) <i>K_c</i> is the seismic coefficient (Unitless) G is the interslice normal forces ($\frac{N}{m}$) H is the interslice normal water forces ($\frac{N}{m}$) </p>
Notes	<p> This equation satisfies TM: equilibrium in the shear direction. W is defined in GD: sliceWght, U_t is defined in GD: srfWtrF, is defined in DD: angleB, and is defined in DD: angleA. </p>
Source	[7]
RefBy	IM: fctSfty.

Base shear force equilibrium is derived from the free body diagram of **Fig:ForceDiagram** in **Section: Physical System Description**.

Refname	GD:resShr
Label	Resistive shear force
Units	$\frac{\text{N}}{\text{m}}$
Equation	$\mathbf{P}_i = \mathbf{N}'_i \tan(\varphi'_i) + c'_{ib,i}$
Description	<p> \mathbf{P} is the resistive shear forces ($\frac{\text{N}}{\text{m}}$) i is the index (Unitless) \mathbf{N}' is the effective normal forces ($\frac{\text{N}}{\text{m}}$) φ' is the effective angle of friction ($^\circ$) c' is the effective cohesion (Pa) b is the total base lengths of slices (m) </p>
Notes	b is defined in DD: lengthLb .
Source	[7]

RefBy [GD: mobShr](#).

Derived by substituting [DD: stress](#) into the Mohr-Coulomb shear strength, [TM: mcShrStrgth](#), and multiplying both sides of the equation by the area of the slice in the shear- z plane. Since the slope is assumed to extend infinitely in the z -direction ([A: Plane-Strain-Conditions](#)), the resulting forces are expressed per metre in the z -direction. The effective angle of friction φ' and the effective cohesion c' are not indexed by i because they are assumed to be isotropic ([A: Soil-Layers-Isotropic](#)) and the soil is assumed to be homogeneous, with constant soil properties throughout ([A: Soil-Layer-Homogeneous](#), [A: Soil-Properties](#)).

Refname	GD:mobShr
Label	Mobilized shear force
Units	$\frac{\text{N}}{\text{m}}$
Equation	$\mathbf{S}_i = \frac{\mathbf{P}_i}{F_S} = \frac{\mathbf{N}'_i \tan(\varphi'_i) + c'_{ib,i}}{F_S}$
Description	<p>\mathbf{S} is the mobilized shear force ($\frac{\text{N}}{\text{m}}$) i is the index (Unitless) \mathbf{P} is the resistive shear forces ($\frac{\text{N}}{\text{m}}$) F_S is the factor of safety (Unitless) \mathbf{N}' is the effective normal forces ($\frac{\text{N}}{\text{m}}$) φ' is the effective angle of friction ($^\circ$) c' is the effective cohesion (Pa) b is the total base lengths of slices (m)</p>
Notes	b is defined in DD: lengthLb .
Source	[7]
RefBy	IM: fctSfty .

Mobilized shear forces is derived by dividing the definition of the \mathbf{P} from **GD: resShr**. by the definition of the factor of safety from **TM: factOfSafety**. The factor of safety F_S is not indexed by i because it is assumed to be constant for the entire slip surface (**A: Factor-of-Safety**).

Refname	GD:effNormF
Label	Effective normal force
Units	$\frac{\text{N}}{\text{m}}$
Equation	$\mathbf{N}'_i = \mathbf{N}_i - \mathbf{U}_{b,i}$
Description	<p>\mathbf{N}' is the effective normal forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$i$ is the index (Unitless)</p> <p>\mathbf{N} is the normal forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$\mathbf{U}_b$ is the base hydrostatic forces ($\frac{\text{N}}{\text{m}}$)</p>
Notes	\mathbf{U}_b is defined in GD: baseWtrF .
Source	[7]

RefBy

Derived by substituting [DD: stress](#) into [TM: effStress](#) and multiplying both sides of the equation by the the area of the slice in the shear- z plane. Since the slope is assumed to extend infinitely in the z -direction ([A: Plane-Strain-Conditions](#)), the resulting forces are expressed per metre in the z -direction.

Refname	GD:resShearWO
Label	Resistive shear force, without interslice normal and shear forces
Units	$\frac{\text{N}}{\text{m}}$
Equation	$\mathbf{R}_i = ((\mathbf{W}_i + \mathbf{U}_{t,i} \cos(\varphi'_i)) \cos(\alpha_i) + (-\mathbf{H}_i + \mathbf{H}_{i-1} + \mathbf{U}_{t,i} \sin(\alpha_i)) \sin(\alpha_i) - \mathbf{U}_{b,i}) \tan(\varphi'_i)$
Description	<p>\mathbf{R} is the resistive shear forces without the influence of interslice forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$i$ is the index (Unitless)</p> <p>\mathbf{W} is the weights ($\frac{\text{N}}{\text{m}}$)</p> <p>$\mathbf{U}_t$ is the surface hydrostatic forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$\alpha$ is the surface angles ($^\circ$)</p> <p>α_b is the base angles ($^\circ$)</p> <p>\mathbf{H} is the interslice normal water forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$\mathbf{U}_b$ is the base hydrostatic forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$\varphi'$ is the effective angle of friction ($^\circ$)</p> <p>c' is the effective cohesion (Pa)</p> <p>b is the total base lengths of slices (m)</p>
Notes	<p>\mathbf{W} is defined in GD: sliceWght, \mathbf{U}_t is defined in GD: srfWtrF, α_b is defined in DD: angleB, α is defined in DD: angleA, \mathbf{H} is defined in DD: intersliceWtrF, \mathbf{U}_b is defined in GD: baseWtrF, and b is defined in DD: lengthLb.</p>
Source	[7] and [3]
RefBy	IM: intsliceFs IM: fctSfty IM: fctSfty IM: fctSfty.

Refname	GD:mobShearWO
Label	Mobilized shear force, without interslice normal and shear forces
Units	$\frac{\text{N}}{\text{m}}$
Equation	$\mathbf{T}_i = (\mathbf{W}_i + \mathbf{U}_{t,i} \cos(i)) \sin(i) - (-\mathbf{H}_i + \mathbf{H}_{i-1} + \mathbf{U}_{t,i} \sin(i)) \cos(i)$
Description	<p>\mathbf{T} is the mobilized shear forces without the influence of interslice forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$i$ is the index (Unitless)</p> <p>\mathbf{W} is the weights ($\frac{\text{N}}{\text{m}}$)</p> <p>$\mathbf{U}_t$ is the surface hydrostatic forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$i$ is the surface angles ($^\circ$)</p> <p>i is the base angles ($^\circ$)</p> <p>\mathbf{H} is the interslice normal water forces ($\frac{\text{N}}{\text{m}}$)</p>
Notes	<p>\mathbf{W} is defined in GD: sliceWght, \mathbf{U}_t is defined in GD: srfWtrF, i is defined in DD: angleB, i is defined in DD: angleA, and \mathbf{H} is defined in DD: intersliceWtrF.</p>
Source	[7] and [3]
RefBy	IM: intsliceFs IM: fctSfty IM: fctSfty .

Refname	GD:normShrR
Label	Interslice normal and shear force proportionality
Units	$\frac{\text{N}}{\text{m}}$
Equation	$\mathbf{X} = \lambda \mathbf{f} \mathbf{G}$
Description	<p>\mathbf{X} is the interslice shear forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$\lambda$ is the proportionality constant (Unitless)</p> <p>\mathbf{f} is the interslice normal to shear force ratio variation function (Unitless)</p> <p>\mathbf{G} is the interslice normal forces ($\frac{\text{N}}{\text{m}}$)</p>
Notes	Mathematical representation of the primary assumption for the Morgenstern-Price method (A: Interslice-Norm-Shear-Forces-Linear). \mathbf{f} is defined in DD: ratioVariation .
Source	[7]
RefBy	IM: nrmShrFor IM: fctSfty .

Refname	GD:momentEql
Label	Moment equilibrium
Units	N
Equation	$0 = -\mathbf{G}_i \left(\mathbf{h}_{z,i} + \frac{\mathbf{b}_i}{2} \tan(i) \right) + \mathbf{G}_{i-1} \left(\mathbf{h}_{z,i-1} - \frac{\mathbf{b}_i}{2} \tan(i) \right) - \mathbf{H}_i \left(\frac{1}{3} \mathbf{h}_{z,w,i} + \frac{\mathbf{b}_i}{2} \tan(i) \right)$
Description	<p> \mathbf{G} is the interslice normal forces ($\frac{\text{N}}{\text{m}}$) i is the index (Unitless) \mathbf{h}_z is the heights of interslice normal forces (m) \mathbf{b} is the base width of slices (m) i is the base angles ($^\circ$) \mathbf{H} is the interslice normal water forces ($\frac{\text{N}}{\text{m}}$) $\mathbf{h}_{z,w}$ is the heights of the water table (m) \mathbf{X} is the interslice shear forces ($\frac{\text{N}}{\text{m}}$) K_c is the seismic coefficient (Unitless) \mathbf{W} is the weights ($\frac{\text{N}}{\text{m}}$) \mathbf{h} is the y-direction heights of slices (m) \mathbf{U}_t is the surface hydrostatic forces ($\frac{\text{N}}{\text{m}}$) i is the surface angles ($^\circ$) \mathbf{Q} is the external forces ($\frac{\text{N}}{\text{m}}$) i is the imposed load angles ($^\circ$) </p>
Notes	<p> This equation satisfies TM: equilibrium for the net moment. \mathbf{b} is defined in DD: lengthB, i is defined in DD: angleA, \mathbf{W} is defined in GD: sliceWght, \mathbf{h} is defined in DD: slcHeight, \mathbf{U}_t is defined in GD: srfWtrF, and i is defined in DD: angleB. </p>
Source	[7]
RefBy	IM: nrmShrFor.

Moment is equal to torque, so the equation from **DD: torque** will be used to calculate

moments:

$$\tau = \mathbf{r} \times \mathbf{F}$$

Considering one dimension, with moments in the clockwise direction as positive and moments in the counterclockwise direction as negative, and replacing the torque symbol with the moment symbol, the equation simplifies to:

$$M = F_{rot}r$$

where F_{rot} is the force causing rotation and r is the length of the moment arm, or the distance between the force and the axis about which the rotation acts. To represent the moment equilibrium, the moments from each force acting on a slice must be considered and added together. The forces acting on a slice are all shown in [Fig:ForceDiagram](#). The midpoint of the base of a slice is considered as the axis of rotation, from which the length of the moment arm is measured. Considering first the interslice normal force acting on slice interface i , the moment is negative because the force tends to rotate the slice in a counterclockwise direction, and the length of the moment arm is the height of the force plus the difference in height between the base at slice interface i and the base at the midpoint of slice i . Thus, the moment is expressed as:

$$-\mathbf{G}_i \left(\mathbf{h}_{z,i} + \frac{\mathbf{b}_i}{2} \tan(i) \right)$$

For the $i - 1$ th slice interface, the moment is similar but in the opposite direction:

$$\mathbf{G}_{i-1} \left(\mathbf{h}_{z,i-1} - \frac{\mathbf{b}_i}{2} \tan(i) \right)$$

Next, the interslice normal water force is considered. This force is zero at the height of the water table, then increases linearly towards the base of the slice due to the increasing water pressure. For such a triangular distribution, the resultant force acts at one-third of the height. Thus, for the interslice normal water force acting on slice interface i , the moment is:

$$-\mathbf{H}_i \left(\frac{1}{3} \mathbf{h}_{z,w,i} + \frac{\mathbf{b}_i}{2} \tan(i) \right)$$

The moment for the interslice normal water force acting on slice interface $i - 1$ is:

$$\mathbf{H}_{i-1} \left(\frac{1}{3} \mathbf{h}_{z,w,i-1} + \frac{\mathbf{b}_i}{2} \tan(i) \right)$$

The interslice shear force at slice interface i tends to rotate in the clockwise direction, and the length of the moment arm is the length from the slice edge to the slice midpoint, equivalent to half of the width of the slice, so the moment is.:

$$\mathbf{X}_i \frac{\mathbf{b}_i}{2}$$

The interslice shear force at slice interface $i-1$ also tends to rotate in the clockwise direction, and has the same length of the moment arm, so the moment is:

$$\mathbf{X}_{i-1} \frac{\mathbf{b}_i}{2}$$

Seismic forces act over the entire height of the slice. For each horizontal segment of the slice, the seismic force is $K_c \mathbf{W}_i$ where \mathbf{W}_i can be expressed as $\gamma \mathbf{b}_i y$ using **GD: weight** where y is the height of the segment under consideration. The corresponding length of the moment arm is y , the height from the base of the slice to the segment under consideration. In reality, the forces near the surface of the soil mass are slightly different due to the slope of the surface, but this difference is assumed to be negligible (**A: Negligible-Effect-Surface-Slope-Seismic**). The resultant moment from the forces on all of the segments with an equivalent resultant length of the moment arm is determined by taking the integral over the slice height. The forces tend to rotate in the counterclockwise direction, so the moment is negative:

$$- \int_0^{\mathbf{h}_i} K_c \gamma \mathbf{b}_i y dy$$

Solving the definite integral yields:

$$-K_c \gamma \mathbf{b}_i \frac{\mathbf{h}_i^2}{2}$$

Using **GD: weight** again to express $\gamma \mathbf{b}_i \mathbf{h}_i$ as \mathbf{W}_i , the moment is:

$$-K_c \mathbf{W}_i \frac{\mathbf{h}_i}{2}$$

The surface hydrostatic force acts into the midpoint of the surface of the slice (**A: Hydrostatic-Force-Slice-Midpoint**). Thus, the vertical component of the force acts directly towards the point of rotation, and has a moment of zero. The horizontal component of the force tends to rotate in a clockwise direction and the length of the moment arm is the entire height of the slice. Thus, the moment is:

$$\mathbf{U}_{t,i} \sin(i) \mathbf{h}_i$$

The external force again acts into the midpoint of the slice surface, so the vertical component does not contribute to the moment, and the length of the moment arm is again the entire height of the slice. The moment is:

$$\mathbf{Q}_i \sin(i) \mathbf{h}_i$$

The base hydrostatic force and slice weight both act in the direction of the point of rotation (**A: Hydrostatic-Force-Slice-Midpoint**), therefore both have moments of zero. Thus, all of the moments have been determined. The moment equilibrium is then represented by the sum of all moments:

$$0 = -\mathbf{G}_i \left(\mathbf{h}_{z,i} + \frac{\mathbf{b}_i}{2} \tan(i) \right) + \mathbf{G}_{i-1} \left(\mathbf{h}_{z,i-1} - \frac{\mathbf{b}_i}{2} \tan(i) \right) - \mathbf{H}_i \left(\frac{1}{3} \mathbf{h}_{z,w,i} + \frac{\mathbf{b}_i}{2} \tan(i) \right) + \mathbf{H}_{i-1} \left(\frac{1}{3} \mathbf{h}_{z,w,i-1} - \right.$$

Refname	GD:weight
Label	Weight
Units	N
Equation	$W = V\gamma$
Description	<p>W is the weight (N) V is the volume (m³) γ is the specific weight ($\frac{\text{N}}{\text{m}^3}$)</p>
Source	Definition of Weight
RefBy	GD: srfWtrF GD: sliceWght GD: sliceWght GD: sliceWght GD: momentEqI GD: momentEqI GD: baseWtrF.

Under the influence of gravity, and assuming a 2D Cartesian coordinate system with down as positive, an object has an acceleration vector of:

$$\mathbf{a} = \begin{bmatrix} 0 \\ g\mathbf{j} \end{bmatrix}$$

Since there is only one non-zero vector component, the scalar value W will be used for the weight. In this scenario, Newton's second law of motion from [TM: NewtonSecLawMot](#) can be expressed as:

$$W = mg$$

Mass can be expressed as density multiplied by volume, resulting in:

$$W = \rho Vg$$

Substituting specific weight as the product of density and gravitational acceleration yields:

$$W = V\gamma$$

Refname	GD:sliceWght
Label	Slice weight
Units	$\frac{N}{m}$
Equation	$\mathbf{W}_i = \mathbf{b}_i \frac{1}{2} \begin{cases} (\mathbf{y}_{slope,i} - \mathbf{y}_{slip,i} + \mathbf{y}_{slope,i-1} - \mathbf{y}_{slip,i-1}) \gamma_{Sat}, \\ (\mathbf{y}_{slope,i} - \mathbf{y}_{wt,i} + \mathbf{y}_{slope,i-1} - \mathbf{y}_{wt,i-1}) \gamma_{dry} + (\mathbf{y}_{wt,i} - \mathbf{y}_{slip,i} + \mathbf{y}_{wt,i-1} - \mathbf{y}_{slip,i-1}) \gamma_{dry}, \\ (\mathbf{y}_{slope,i} - \mathbf{y}_{slip,i} + \mathbf{y}_{slope,i-1} - \mathbf{y}_{slip,i-1}) \gamma_{dry}, \end{cases}$
Description	<p>\mathbf{W} is the weights ($\frac{N}{m}$) i is the index (Unitless) \mathbf{b} is the base width of slices (m) \mathbf{y}_{slope} is the y-coordinates of the slope (m) \mathbf{y}_{slip} is the y-coordinates of the slip surface (m) γ_{Sat} is the soil saturated unit weight ($\frac{N}{m^3}$) \mathbf{y}_{wt} is the y-coordinates of the water table (m) γ_{dry} is the soil dry unit weight ($\frac{N}{m^3}$)</p>
Notes	<p>This equation is based on the assumption that the surface and the base of a slice are straight lines (A: Surface-Base-Slice-between-Interslice-Straight-Lines). The soil dry unit weight γ_{dry} and the soil saturated unit weight γ_{Sat} are not indexed by i because the soil is assumed to be homogeneous, with constant soil properties throughout (A: Soil-Layer-Homogeneous). \mathbf{b} is defined in DD: lengthB.</p>
Source	[1]
RefBy	GD: resShearWO GD: normForcEq GD: momentEqI GD: mobS-hearWO GD: bsShrFEq.

For the case where the water table is above the slope surface, the weights come from the weight of the saturated soil. Substituting values for saturated soil into the equation for weight from [GD: weight](#) yields:

$$\mathbf{W}_i = \mathbf{V}_{sat,i} \gamma_{Sat}$$

Due to **A: Plane-Strain-Conditions**, only two dimensions are considered, so the areas of saturated soil are considered instead of the volumes of saturated soil. Any given slice has a trapezoidal shape. The area of a trapezoid is the average of the lengths of the parallel sides multiplied by the length between the parallel sides. The parallel sides in this case are the interslice edges and the length between them is the width of the slice. Thus, the weights are defined as:

$$\mathbf{W}_i = \mathbf{b}_i \frac{1}{2} (\mathbf{y}_{slope,i} - \mathbf{y}_{slip,i} + \mathbf{y}_{slope,i-1} - \mathbf{y}_{slip,i-1}) \gamma_{Sat}$$

For the case where the water table is below the slip surface, the weights come from the weight of the dry soil. Substituting values for dry soil into the equation for weight from **GD: weight** yields:

$$\mathbf{W}_i = \mathbf{V}_{dry,i} \gamma_{dry}$$

A: Plane-Strain-Conditions again allows for two-dimensional analysis so the areas of dry soil are considered instead of the volumes of dry soil. The trapezoidal slice shape is the same as in the previous case, so the weights are defined as:

$$\mathbf{W}_i = \mathbf{b}_i \frac{1}{2} (\mathbf{y}_{slope,i} - \mathbf{y}_{slip,i} + \mathbf{y}_{slope,i-1} - \mathbf{y}_{slip,i-1}) \gamma_{dry}$$

For the case where the water table is between the slope surface and slip surface, the weights are the sums of the the weights of the dry portions and weights of the saturated portions of the soil. Substituting values for dry and saturated soil into the equation for weight from **GD: weight** and adding them together yields:

$$\mathbf{W}_i = \mathbf{V}_{dry,i} \gamma_{dry} + \mathbf{V}_{sat,i} \gamma_{Sat}$$

A: Plane-Strain-Conditions again allows for two-dimensional analysis so the areas of dry soil and areas of saturated soil are considered instead of the volumes of dry soil and volumes of saturated soil. The water table is assumed to only intersect a slice surface or base at a slice edge (**A: Water-Intersects-Surface-Edge**, **A: Water-Intersects-Base-Edge**), so the dry and saturated portions each have trapezoidal shape. For the dry portion, the parallel sides of the trapezoid are the lengths between the slope surface and water table at the slice edges. For the saturated portion, the parallel sides of the trapezoid are the lengths between the water table and slip surface at the slice edges. Thus, the weights are defined as:

$$\mathbf{W}_i = \mathbf{b}_i \frac{1}{2} ((\mathbf{y}_{slope,i} - \mathbf{y}_{wt,i} + \mathbf{y}_{slope,i-1} - \mathbf{y}_{wt,i-1}) \gamma_{dry} + (\mathbf{y}_{wt,i} - \mathbf{y}_{slip,i} + \mathbf{y}_{wt,i-1} - \mathbf{y}_{slip,i-1}) \gamma_{Sat})$$

Refname	GD:baseWtrF
Label	Base hydrostatic force
Units	$\frac{\text{N}}{\text{m}}$
Equation	$\mathbf{U}_{b,i} = \mathbf{b}_i \gamma_w \frac{1}{2} \begin{cases} \mathbf{y}_{wt,i} - \mathbf{y}_{slip,i} + \mathbf{y}_{wt,i-1} - \mathbf{y}_{slip,i-1}, & \mathbf{y}_{wt,i} > \mathbf{y}_{slip,i} \vee \mathbf{y}_{wt,i-1} > \mathbf{y}_{slip,i-1} \\ 0, & \mathbf{y}_{wt,i} \leq \mathbf{y}_{slip,i} \wedge \mathbf{y}_{wt,i-1} \leq \mathbf{y}_{slip,i-1} \end{cases}$
Description	<p>\mathbf{U}_b is the base hydrostatic forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$i$ is the index (Unitless)</p> <p>\mathbf{b} is the base width of slices (m)</p> <p>γ_w is the unit weight of water ($\frac{\text{N}}{\text{m}^3}$)</p> <p>$\mathbf{y}_{wt}$ is the y-coordinates of the water table (m)</p> <p>\mathbf{y}_{slip} is the y-coordinates of the slip surface (m)</p>
Notes	This equation is based on the assumption that the base of a slice is a straight line (A: Surface-Base-Slice-between-Interslice-Straight-Lines). \mathbf{b} is defined in DD: lengthB .
Source	[1]

RefBy [GD: resShearWO](#) [GD: effNormF](#) [GD: baseWtrF](#).

The base hydrostatic forces come from the weight of the water above the base of each slice. Substituting values for water into the equation for weight from [GD: weight](#) yields:

$$\mathbf{U}_{b,i} = \mathbf{V}_{wat,i} \gamma_w$$

Due to [A: Plane-Strain-Conditions](#), only two dimensions are considered, so the areas of water are considered instead of the volumes of water. For a given slice, the case where the height of the water table is below the height of the slip surface at one edge and above the height of the slip surface at the other edge is assumed not to occur ([A: Water-Intersects-Base-Edge](#)). In the case where the height of the water table is below the height of the slip surface, the area of the water is zero. In the case where the height of the water table is above the height of the slip surface, the water forms a trapezoid on top of the slip surface. The area of a

trapezoid is the average of the lengths of the parallel sides multiplied by the length between the parallel sides. The parallel sides in this case are the distances between the water table and the slip surface for the edges of the slice, and the length between them is the width of the slice. Thus, the base hydrostatic forces are defined as:

$$\mathbf{U}_{b,i} = \mathbf{b}_i \frac{1}{2} (\mathbf{y}_{wt,i} - \mathbf{y}_{slip,i} + \mathbf{y}_{wt,i-1} - \mathbf{y}_{slip,i-1}) \gamma_w$$

This equation is a rearrangement of the non-zero case of **GD: baseWtrF**.

Refname	GD:srfWtrF
Label	Surface hydrostatic force
Units	$\frac{\text{N}}{\text{m}}$
Equation	$\mathbf{U}_{t,i} = \mathbf{b}_i \gamma_w \frac{1}{2} \begin{cases} \mathbf{y}_{wt,i} - \mathbf{y}_{slope,i} + \mathbf{y}_{wt,i-1} - \mathbf{y}_{slope,i-1}, & \mathbf{y}_{wt,i} > \mathbf{y}_{slope,i} \vee \mathbf{y}_{wt,i-1} > \mathbf{y}_{slope,i-1} \\ 0, & \mathbf{y}_{wt,i} \leq \mathbf{y}_{slope,i} \wedge \mathbf{y}_{wt,i-1} \leq \mathbf{y}_{slope,i-1} \end{cases}$
Description	<p>\mathbf{U}_t is the surface hydrostatic forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$i$ is the index (Unitless)</p> <p>\mathbf{b} is the base width of slices (m)</p> <p>γ_w is the unit weight of water ($\frac{\text{N}}{\text{m}^3}$)</p> <p>$\mathbf{y}_{wt}$ is the y-coordinates of the water table (m)</p> <p>\mathbf{y}_{slope} is the y-coordinates of the slope (m)</p>
Notes	This equation is based on the assumption that the surface of a slice is a straight line (A: Surface-Base-Slice-between-Interslice-Straight-Lines). \mathbf{b} is defined in DD: lengthB .
Source	[1]
RefBy	GD: srfWtrF GD: resShearWO IM: nrmShrForNum GD: norm-ForcEq GD: momentEq GD: mobShearWO GD: bsShrFEq.

The surface hydrostatic forces come from the weight of the water standing on top of the soil of the slope surface. Substituting values for water into the equation for weight from **GD:**

weight yields:

$$\mathbf{U}_{t,i} = \mathbf{V}_{wat,i} \gamma_w$$

Due to **A: Plane-Strain-Conditions**, only two dimensions are considered, so the areas of water are considered instead of the volumes of water. For a given slice, the case where the height of the water table is below the height of the slope surface at one edge and above the height of the slope surface at the other edge is assumed not to occur (**A: Water-Intersects-Surface-Edge**). In the case where the height of the water table is below the height of the slope surface, the area of the water is zero. In the case where the height of the water table is above the height of the slope surface, the water forms a trapezoid on top of the slope surface. The area of a trapezoid is the average of the lengths of the parallel sides multiplied by the length between the parallel sides. The parallel sides in this case are the distances between the water table and the slope surface for the edges of the slice, and the length between them is the width of the slice. Thus, the surface hydrostatic forces are defined as:

$$\mathbf{U}_{t,i} = \mathbf{b}_i \frac{1}{2} (\mathbf{y}_{wt,i} - \mathbf{y}_{slope,i} + \mathbf{y}_{wt,i-1} - \mathbf{y}_{slope,i-1}) \gamma_w$$

This equation is a rearrangement of the non-zero case of **GD: srfWtrF**.

4.2.4 Data Definitions

This section collects and defines all the data needed to build the instance models.

Refname	DD:intersliceWtrF
Label	Interslice normal water forces
Symbol	H
Units	$\frac{\text{N}}{\text{m}}$
Equation	$\mathbf{H} = \begin{cases} \frac{(\mathbf{y}_{slope,i} - \mathbf{y}_{slip,i})^2}{2} \gamma_w + (\mathbf{y}_{wt,i} - \mathbf{y}_{slope,i})^2 \gamma_w, & \mathbf{y}_{wt,i} \geq \mathbf{y}_{slope,i} \\ \frac{(\mathbf{y}_{wt,i} - \mathbf{y}_{slip,i})^2}{2} \gamma_w, & \mathbf{y}_{slope,i} > \mathbf{y}_{wt,i} > \mathbf{y}_{slip,i} \\ 0, & \mathbf{y}_{wt,i} \leq \mathbf{y}_{slip,i} \end{cases}$
Description	<p>H is the interslice normal water forces ($\frac{\text{N}}{\text{m}}$) \mathbf{y}_{slope} is the y-coordinates of the slope (m) <i>i</i> is the index (Unitless) \mathbf{y}_{slip} is the y-coordinates of the slip surface (m) γ_w is the unit weight of water ($\frac{\text{N}}{\text{m}^3}$) \mathbf{y}_{wt} is the y-coordinates of the water table (m)</p>
Source	[1]
RefBy	GD: resShearWO IM: nrmShrForNum GD: mobShearWO.

Refname	DD:angleA
Label	Base angles
Symbol	
Units	°
Equation	$= \arctan \left(\frac{y_{slip,i} - y_{slip,i-1}}{x_{slip,i} - x_{slip,i-1}} \right)$
Description	<p>is the base angles (°)</p> <p>y_{slip} is the y-coordinates of the slip surface (m)</p> <p>i is the index (Unitless)</p> <p>x_{slip} is the x-coordinates of the slip surface (m)</p>
Notes	This equation is based on the assumption that the base of a slice is a straight line (A: Surface-Base-Slice-between-Interslice-Straight-Lines).
Source	[1]
RefBy	GD: resShearWO IM: nrmShrForNum GD: normForcEq GD: momentEqI GD: mobShearWO DD: lengthLb GD: bsShrFEq DD: convertFunc2 DD: convertFunc1.

Refname	DD:angleB
Label	Surface angles
Symbol	
Units	°
Equation	$= \arctan \left(\frac{\mathbf{y}_{slope,i} - \mathbf{y}_{slope,i-1}}{\mathbf{x}_{slope,i} - \mathbf{x}_{slope,i-1}} \right)$
Description	<p>is the surface angles (°)</p> <p>\mathbf{y}_{slope} is the y-coordinates of the slope (m)</p> <p>i is the index (Unitless)</p> <p>\mathbf{x}_{slope} is the x-coordinates of the slope (m)</p>
Notes	This equation is based on the assumption that the surface of a slice is a straight line (A: Surface-Base-Slice-between-Interslice-Straight-Lines).
Source	[1]
RefBy	GD: resShearWO IM: nrmShrForNum GD: normForcEq GD: momentEqI GD: mobShearWO GD: bsShrFEq.

Refname	DD:lengthB
Label	Base width of slices
Symbol	b
Units	m
Equation	$\mathbf{b} = \mathbf{x}_{slip,i} - \mathbf{x}_{slip,i-1}$
Description	<p>b is the base width of slices (m) \mathbf{x}_{slip} is the x-coordinates of the slip surface (m) <i>i</i> is the index (Unitless)</p>
Source	[1]
RefBy	GD: srfWtrF GD: sliceWght IM: nrmShrForNum IM: nrmShrForDen GD: momentEql DD: lengthLb GD: baseWtrF.

Refname	DD:lengthLb
Label	Total base lengths of slices
Symbol	b
Units	m
Equation	$b = \mathbf{b}_i \sec(\textcolor{red}{i})$
Description	b is the total base lengths of slices (m) \mathbf{b} is the base width of slices (m) i is the index (Unitless) is the base angles ($^{\circ}$)
Notes	\mathbf{b} is defined in DD: lengthB and is defined in DD: angleA .
Source	[1]
RefBy	GD: resShr GD: resShearWO GD: mobShr .

Refname	DD:slcHeight
Label	Y-direction heights of slices
Symbol	h
Units	m
Equation	$\mathbf{h} = \frac{1}{2} (\mathbf{h}^R + \mathbf{h}^L)$
Description	<p>h is the y-direction heights of slices (m)</p> <p>\mathbf{h}^R is the heights of the right side of slices (m)</p> <p>\mathbf{h}^L is the heights of the left side of slices (m)</p>
Notes	<p>This equation is based on the assumption that the surface and base of a slice are straight lines (A: Surface-Base-Slice-between-Interslice-Straight-Lines). \mathbf{h}^R and \mathbf{h}^L are defined in DD: sliceHghtRightDD and DD: sliceHghtLeftDD, respectively.</p>
Source	[1]
RefBy	IM: nrmShrForNum GD: momentEq1.

Refname	DD:stress
Label	Total stress
Symbol	σ
Units	Pa
Equation	$\sigma = \frac{\mathbf{F}}{A}$
Description	<p>σ is the total stress (Pa)</p> <p>\mathbf{F} is the force (N)</p> <p>A is the area (m²)</p>
Source	[2]
RefBy	GD: resShr TM: effStress GD: effNormF.

Refname	DD:torque
Label	Torque
Symbol	τ
Units	Nm
Equation	$\tau = \mathbf{r} \times \mathbf{F}$
Description	τ is the torque (Nm) \mathbf{r} is the displacement (m) \mathbf{F} is the force (N)
Notes	The torque on a body measures the the tendency of a force to rotate the body around an axis or pivot.
Source	–
RefBy	GD: momentEql.

Refname	DD:ratioVariation
Label	Interslice normal to shear force ratio variation function
Symbol	f
Units	Unitless
Equation	$\mathbf{f} = \begin{cases} 1, & const_f \\ \sin\left(\pi \frac{\mathbf{x}_{slip,i} - \mathbf{x}_{slip,0}}{\mathbf{x}_{slip,n} - \mathbf{x}_{slip,0}}\right), & \neg const_f \end{cases}$
Description	<p>f is the interslice normal to shear force ratio variation function (Unitless)</p> <p>π is the circumference to diameter ratio (Unitless)</p> <p>\mathbf{x}_{slip} is the x-coordinates of the slip surface (m)</p> <p>i is the index (Unitless)</p> <p>n is the number of slices (Unitless)</p> <p>$const_f$ is the decision on f (Unitless)</p>
Source	[1]
RefBy	IM: nrmShrForDen GD: normShrR DD: convertFunc2 DD: convert-Func1.

Refname	DD:convertFunc1
Label	First function for incorporating interslice forces into shear force
Symbol	
Units	Unitless
Equation	$= (\lambda \mathbf{f}_i \cos ({}_i) - \sin ({}_i)) \tan (\varphi') - (\lambda \mathbf{f}_i \sin ({}_i) + \cos ({}_i)) F_S$
Description	<p>is the first function for incorporating interslice forces into shear force (Unitless)</p> <p>λ is the proportionality constant (Unitless)</p> <p>\mathbf{f} is the interslice normal to shear force ratio variation function (Unitless)</p> <p>i is the index (Unitless)</p> <p>is the base angles ($^{\circ}$)</p> <p>φ' is the effective angle of friction ($^{\circ}$)</p> <p>F_S is the factor of safety (Unitless)</p>
Notes	\mathbf{f} is defined in DD: ratioVariation and is defined in DD: angleA.
Source	[7] and [3]
RefBy	IM: intsliceFs IM: fctSfty DD: convertFunc2.

Refname	DD:convertFunc2
Label	Second function for incorporating interslice forces into shear force
Symbol	
Units	Unitless
Equation	$= \frac{(\lambda \mathbf{f}_i \cos(\alpha_i) - \sin(\alpha_i)) \tan(\varphi') - (\lambda \mathbf{f}_i \sin(\alpha_i) + \cos(\alpha_i)) F_S}{i-1}$
Description	<p>is the second function for incorporating interslice forces into shear force (Unitless)</p> <p>λ is the proportionality constant (Unitless)</p> <p>\mathbf{f} is the interslice normal to shear force ratio variation function (Unitless)</p> <p>i is the index (Unitless)</p> <p>α is the base angles ($^{\circ}$)</p> <p>φ' is the effective angle of friction ($^{\circ}$)</p> <p>F_S is the factor of safety (Unitless)</p> <p>is the first function for incorporating interslice forces into shear force (Unitless)</p>
Notes	\mathbf{f} is defined in DD: ratioVariation , α is defined in DD: angleA , and is defined in DD: convertFunc1 .
Source	[7] and [3]
RefBy	IM: intsliceFs IM: fctSfty IM: fctSfty .

Refname	DD:nrmForceSumDD
Label	Sums of the interslice normal forces
Symbol	\mathbf{F}_x^G
Units	N
Equation	$\mathbf{F}_x^G = \mathbf{G}_i + \mathbf{G}_{i-1}$
Description	<p>\mathbf{F}_x^G is the sums of the interslice normal forces (N)</p> <p>\mathbf{G} is the interslice normal forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$i$ is the index (Unitless)</p>
Source	[1]
RefBy	

Refname	DD:watForceSumDD
Label	Sums of the interslice normal water forces
Symbol	\mathbf{F}_x^H
Units	N
Equation	$\mathbf{F}_x^H = \mathbf{H}_i + \mathbf{H}_{i-1}$
Description	<p>\mathbf{F}_x^H is the sums of the interslice normal water forces (N)</p> <p>\mathbf{H} is the interslice normal water forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$i$ is the index (Unitless)</p>
Source	[1]
RefBy	

Refname	DD:sliceHghtRightDD
Label	Heights of the right side of slices
Symbol	\mathbf{h}^R
Units	m
Equation	$\mathbf{h}^R = \mathbf{y}_{slope,i} - \mathbf{y}_{slip,i}$
Description	<p>\mathbf{h}^R is the heights of the right side of slices (m)</p> <p>\mathbf{y}_{slope} is the y-coordinates of the slope (m)</p> <p>i is the index (Unitless)</p> <p>\mathbf{y}_{slip} is the y-coordinates of the slip surface (m)</p>
Source	[1]
RefBy	DD: slcHeight.

Refname	DD:sliceHghtLeftDD
Label	Heights of the left side of slices
Symbol	\mathbf{h}^L
Units	m
Equation	$\mathbf{h}^L = \mathbf{y}_{slope,i-1} - \mathbf{y}_{slip,i-1}$
Description	\mathbf{h}^L is the heights of the left side of slices (m) \mathbf{y}_{slope} is the y-coordinates of the slope (m) <i>i</i> is the index (Unitless) \mathbf{y}_{slip} is the y-coordinates of the slip surface (m)
Source	[1]
RefBy	DD: slcHeight.

4.2.5 Instance Models

This section transforms the problem defined in [Section: Problem Description](#) into one which is expressed in mathematical terms. It uses concrete symbols defined in [Section: Data Definitions](#) to replace the abstract symbols in the models identified in [Section: Theoretical Models](#) and [Section: General Definitions](#). The goals [GS: Identify-Crit-and-FS](#), [GS: Determine-Normal-Forces](#), and [GS: Determine-Shear-Forces](#) are met by the simultaneous solution of [IM: fctSfty](#), [IM: nrmShrFor](#), and [IM: intsliceFs](#). The goal [GS: Identify-Crit-and-FS](#) is also contributed to by [IM: crtSlpId](#). The Morgenstern-Price method is a vertical slice, limit equilibrium slope stability analysis method. Analysis is performed by breaking the assumed slip surface into a series of vertical slices of mass. Static equilibrium analysis is performed, using two force equations and one moment equation as in [TM: equilibrium](#). The problem is statically indeterminate with only these 3 equations and one constitutive equation (the Mohr Coulomb shear strength of [TM: mcShrStrgth](#)) so the assumption [GD: normShrR](#) and corresponding equation [GD: normShrR](#) are used. The force equilibrium equations can be modified to be expressed only in terms of known physical values, as done in [GD: resShearWO](#)

and GD: mobShearWO.

Refname	IM:fctSfty
Label	Factor of safety
Input	$\mathbf{x}_{slope}, \mathbf{y}_{slope}, \mathbf{y}_{wt}, c', \varphi', \gamma_{dry}, \gamma_{Sat}, \gamma_w, \mathbf{x}_{slip}, \mathbf{y}_{slip}, const_f$
Output	F_S
Input Constraints	
Output constraints	Con-
Equation	$F_S = \frac{\sum_{i=1}^{n-1} \mathbf{R}_i \prod_{v=i}^{n-1} v + \mathbf{R}_n}{\sum_{i=1}^{n-1} \mathbf{T}_i \prod_{v=i}^{n-1} v + \mathbf{T}_n}$
Description	<p>F_S is the factor of safety (Unitless)</p> <p>\mathbf{R} is the resistive shear forces without the influence of interslice forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$i$ is the index (Unitless)</p> <p>γ is the second function for incorporating interslice forces into shear force (Unitless)</p> <p>v is the local index (Unitless)</p> <p>n is the number of slices (Unitless)</p> <p>\mathbf{T} is the mobilized shear forces without the influence of interslice forces ($\frac{\text{N}}{\text{m}}$)</p>
Notes	\mathbf{R} is defined in GD: resShearWO , γ is defined in DD: convertFunc2 , and \mathbf{T} is defined in GD: mobShearWO
Source	[7] and [3]
RefBy	IM: nrmShrFor IM: intsliceFs IM: intsliceFs IM: fctSfty FR: Display-Interslice-Shear-Forces FR: Display-Interslice-Normal-Forces FR: Display-Factor-of-Safety 54 FR: Determine-Critical-Slip-Surface .

The mobilized shear force defined in [GD: bsShrFEq](#) can be substituted into the definition of mobilized shear force based on the factor of safety, from [GD: mobShr](#) yielding Equation (1) below:

$$(\mathbf{W}_i - \mathbf{X}_{i-1} + \mathbf{X}_i + \mathbf{U}_{t,i} \cos(i) + \mathbf{Q}_i \cos(i)) \sin(i) - (-K_c \mathbf{W}_i - \mathbf{G}_i + \mathbf{G}_{i-1} - \mathbf{H}_i + \mathbf{H}_{i-1} + \mathbf{U}_{t,i} \sin(i) +$$

An expression for the effective normal forces, \mathbf{N}' , can be derived by substituting the normal forces equilibrium from [GD: normForceEq](#) into the definition for effective normal forces from [GD: resShearWO](#). This results in Equation (2):

$$\mathbf{N}'_i = (\mathbf{W}_i - \mathbf{X}_{i-1} + \mathbf{X}_i + \mathbf{U}_{t,i} \cos(i) + \mathbf{Q}_i \cos(i)) \cos(i) + (-K_c \mathbf{W}_i - \mathbf{G}_i + \mathbf{G}_{i-1} - \mathbf{H}_i + \mathbf{H}_{i-1} + \mathbf{U}_{t,i} \sin(i) +$$

Substituting Equation (2) into Equation (1) gives:

$$(\mathbf{W}_i - \mathbf{X}_{i-1} + \mathbf{X}_i + \mathbf{U}_{t,i} \cos(i) + \mathbf{Q}_i \cos(i)) \sin(i) - (-K_c \mathbf{W}_i - \mathbf{G}_i + \mathbf{G}_{i-1} - \mathbf{H}_i + \mathbf{H}_{i-1} + \mathbf{U}_{t,i} \sin(i) +$$

Since the interslice shear forces \mathbf{X} and interslice normal forces \mathbf{G} are unknown, they are separated from the other terms as follows:

$$(\mathbf{W}_i + \mathbf{U}_{t,i} \cos(i) + \mathbf{Q}_i \cos(i)) \sin(i) - (-K_c \mathbf{W}_i - \mathbf{H}_i + \mathbf{H}_{i-1} + \mathbf{U}_{t,i} \sin(i) + \mathbf{Q}_i \sin(i)) \cos(i) - (-\mathbf{G}_i + \mathbf{G}_{i-1}) \cos(i) + (-\mathbf{X}_{i-1} + \mathbf{X}_i) \sin(i)$$

Applying assumptions [A: Seismic-Force](#) and [A: Surface-Load](#), which state that the seismic coefficient and the external forces, respectively, are zero, allows for further simplification as shown below:

$$(\mathbf{W}_i + \mathbf{U}_{t,i} \cos(i)) \sin(i) - (-\mathbf{H}_i + \mathbf{H}_{i-1} + \mathbf{U}_{t,i} \sin(i)) \cos(i) - (-\mathbf{G}_i + \mathbf{G}_{i-1}) \cos(i) + (-\mathbf{X}_{i-1} + \mathbf{X}_i) \sin(i)$$

The definitions of [GD: resShearWO](#) and [GD: mobShearWO](#) are present in this equation, and thus can be replaced by \mathbf{R}_i and \mathbf{T}_i , respectively:

$$\mathbf{T}_i + (-\mathbf{X}_{i-1} + \mathbf{X}_i) \sin(i) - (-\mathbf{G}_i + \mathbf{G}_{i-1}) \cos(i) = \frac{\mathbf{R}_i + ((-\mathbf{X}_{i-1} + \mathbf{X}_i) \cos(i) + (-\mathbf{G}_i + \mathbf{G}_{i-1}) \sin(i)) \tan(\varphi')}{F_S}$$

The interslice shear forces \mathbf{X} can be expressed in terms of the interslice normal forces \mathbf{G} using [A: Interslice-Norm-Shear-Forces-Linear](#) and [GD: normShrR](#), resulting in:

$$\mathbf{T}_i + (-\lambda \mathbf{f}_{i-1} \mathbf{G}_{i-1} + \lambda \mathbf{f}_i \mathbf{G}_i) \sin(i) - (-\mathbf{G}_i + \mathbf{G}_{i-1}) \cos(i) = \frac{\mathbf{R}_i + ((-\lambda \mathbf{f}_{i-1} \mathbf{G}_{i-1} + \lambda \mathbf{f}_i \mathbf{G}_i) \cos(i) + (-\mathbf{G}_i + \mathbf{G}_{i-1}) \sin(i)) \tan(\varphi')}{F_S}$$

Rearranging yields the following:

$$\mathbf{G}_i ((\lambda \mathbf{f}_i \cos(i) - \sin(i)) \tan(\varphi') - (\lambda \mathbf{f}_i \sin(i) + \cos(i)) F_S) = \mathbf{G}_{i-1} ((\lambda \mathbf{f}_{i-1} \cos(i) - \sin(i)) \tan(\varphi') - (\lambda \mathbf{f}_{i-1} \sin(i) + \cos(i)) F_S) + \mathbf{R}_i$$

The definitions for \mathbf{G} and \mathbf{R} from [DD: convertFunc1](#) and [DD: convertFunc2](#) simplify the above to Equation (3):

$$\mathbf{G}_{ii} = {}_{i-1}\mathbf{G}_{i-1i-1} + F_S \mathbf{T}_i - \mathbf{R}_i$$

Versions of Equation (3) instantiated for slices 1 to n are shown below:

$$\mathbf{G}_{11} = {}_0\mathbf{G}_{00} + F_S \mathbf{T}_1 - \mathbf{R}_1$$

$$\mathbf{G}_{22} = {}_1\mathbf{G}_{11} + F_S \mathbf{T}_2 - \mathbf{R}_2$$

$$\mathbf{G}_{33} = {}_2\mathbf{G}_{22} + F_S \mathbf{T}_3 - \mathbf{R}_3$$

...

$$\mathbf{G}_{n-2n-2} = {}_{n-3}\mathbf{G}_{n-3n-3} + F_S \mathbf{T}_{n-2} - \mathbf{R}_{n-2}$$

$$\mathbf{G}_{n-1n-1} = {}_{n-2}\mathbf{G}_{n-2n-2} + F_S \mathbf{T}_{n-1} - \mathbf{R}_{n-1}$$

$$\mathbf{G}_{nn} = {}_{n-1}\mathbf{G}_{n-1n-1} + F_S \mathbf{T}_n - \mathbf{R}_n$$

Applying [A: Edge-Slices](#), which says that \mathbf{G}_0 and \mathbf{G}_n are zero, results in the following special cases: Equation (8) for the first slice:

$$\mathbf{G}_{11} = F_S \mathbf{T}_1 - \mathbf{R}_1$$

and Equation (9) for the n th slice:

$$-\left(\frac{F_S \mathbf{T}_n - \mathbf{R}_n}{n-1}\right) = \mathbf{G}_{n-1n-1}$$

Substituting Equation (8) into Equation (4) yields Equation (10):

$$\mathbf{G}_{22} = {}_1(F_S \mathbf{T}_1 - \mathbf{R}_1) + F_S \mathbf{T}_2 - \mathbf{R}_2$$

which can be substituted into Equation (5) to get Equation (11):

$$\mathbf{G}_{33} = {}_2({}_1(F_S \mathbf{T}_1 - \mathbf{R}_1) + F_S \mathbf{T}_2 - \mathbf{R}_2) + F_S \mathbf{T}_3 - \mathbf{R}_3$$

and so on until Equation (12) is obtained from Equation (7):

$$\mathbf{G}_{n-1n-1} = {}_{n-2}({}_{n-3}({}_1(F_S \mathbf{T}_1 - \mathbf{R}_1) + F_S \mathbf{T}_2 - \mathbf{R}_2) + F_S \mathbf{T}_{n-2} - \mathbf{R}_{n-2}) + F_S \mathbf{T}_{n-1} - \mathbf{R}_{n-1}$$

Equation (9) can then be substituted into the left-hand side of Equation (12), resulting in:

$$-\left(\frac{F_S \mathbf{T}_n - \mathbf{R}_n}{n-1}\right) = {}_{n-2}({}_{n-3}({}_1(F_S \mathbf{T}_1 - \mathbf{R}_1) + F_S \mathbf{T}_2 - \mathbf{R}_2) + F_S \mathbf{T}_{n-2} - \mathbf{R}_{n-2}) + F_S \mathbf{T}_{n-1} - \mathbf{R}_{n-1}$$

This can be rearranged by multiplying both sides by $n-1$ and then distributing the multiplication of each over addition to obtain:

$$-(F_S \mathbf{T}_n - \mathbf{R}_n) = {}_{n-1n-21}(F_S \mathbf{T}_1 - \mathbf{R}_1) + {}_{n-1n-22}(F_S \mathbf{T}_2 - \mathbf{R}_2) + {}_{n-1}(F_S \mathbf{T}_{n-1} - \mathbf{R}_{n-1})$$

The multiplication of the terms can be further distributed over the subtractions, resulting in the equation having terms that each either contain an \mathbf{R} or a \mathbf{T} . The equation can then be rearranged so terms containing an \mathbf{R} are on one side of the equality, and terms containing a \mathbf{T} are on the other. The multiplication by the factor of safety is common to all of the \mathbf{T} terms, and thus can be factored out, resulting in:

$$F_S (\textit{\texttt{_n-1_n-21}} \mathbf{T}_1 + \textit{\texttt{_n-1_n-22}} \mathbf{T}_2 + \textit{\texttt{_n-1}} \mathbf{T}_{n-1} + \mathbf{T}_n) = \textit{\texttt{_n-1_n-21}} \mathbf{R}_1 + \textit{\texttt{_n-1_n-22}} \mathbf{R}_2 + \textit{\texttt{_n-1}} \mathbf{R}_{n-1} + \mathbf{R}_n$$

Isolating the factor of safety on the left-hand side and using compact notation for the products and sums yields Equation (13), which can also be seen in [IM: fctSfty](#):

$$F_S = \frac{\sum_{i=1}^{n-1} \mathbf{R}_i \prod_{v=i}^{n-1} v + \mathbf{R}_n}{\sum_{i=1}^{n-1} \mathbf{T}_i \prod_{v=i}^{n-1} v + \mathbf{T}_n}$$

F_S depends on the unknowns λ ([IM: nrmShrFor](#)) and \mathbf{G} ([IM: intsliceFs](#)).

Refname	IM:nrmShrFor
Label	Normal and shear force proportionality constant
Input	$\mathbf{x}_{slope}, \mathbf{y}_{slope}, \mathbf{y}_{wt}, \gamma_w, \mathbf{x}_{slip}, \mathbf{y}_{slip}, const_f$
Output	λ
Input Constraints	
Output constraints	Con-
Equation	$\lambda = \frac{\sum_{i=1}^n \mathbf{C}_{num,i}}{\sum_{i=1}^n \mathbf{C}_{den,i}}$
Description	<p>λ is the proportionality constant (Unitless)</p> <p>\mathbf{C}_{num} is the proportionality constant numerator (N)</p> <p>i is the index (Unitless)</p> <p>\mathbf{C}_{den} is the proportionality constant denominator (N)</p>
Notes	\mathbf{C}_{num} is defined in IM: nrmShrForNum and \mathbf{C}_{den} is defined in IM: nrmShrForDen .
Source	[7] and [3]
RefBy	IM: nrmShrFor IM: nrmShrForNum IM: nrmShrForDen IM: intsliceFs IM: fctSfty FR: Display-Interslice-Shear-Forces FR: Display-Interslice-Normal-Forces FR: Display-Factor-of-Safety FR: Determine-Critical-Slip-Surface .

From the moment equilibrium of **GD: momentEq1** with the primary assumption for the Morgenstern-Price method of **A: Interslice-Norm-Shear-Forces-Linear** and associated def-

initiation **GD: normShrR**, Equation (14) can be derived:

$$0 = -\mathbf{G}_i \left(\mathbf{h}_{z,i} + \frac{\mathbf{b}_i}{2} \tan(i) \right) + \mathbf{G}_{i-1} \left(\mathbf{h}_{z,i-1} - \frac{\mathbf{b}_i}{2} \tan(i) \right) - \mathbf{H}_i \left(\frac{1}{3} \mathbf{h}_{z,w,i} + \frac{\mathbf{b}_i}{2} \tan(i) \right) + \mathbf{H}_{i-1} \left(\frac{1}{3} \mathbf{h}_{z,w,i-1} - \frac{\mathbf{b}_i}{2} \tan(i) \right)$$

Rearranging the equation in terms of λ leads to Equation (15):

$$\lambda = \frac{-\mathbf{G}_i \left(\mathbf{h}_{z,i} + \frac{\mathbf{b}_i}{2} \tan(i) \right) + \mathbf{G}_{i-1} \left(\mathbf{h}_{z,i-1} - \frac{\mathbf{b}_i}{2} \tan(i) \right) - \mathbf{H}_i \left(\frac{1}{3} \mathbf{h}_{z,w,i} + \frac{\mathbf{b}_i}{2} \tan(i) \right) + \mathbf{H}_{i-1} \left(\frac{1}{3} \mathbf{h}_{z,w,i-1} - \frac{\mathbf{b}_i}{2} \tan(i) \right)}{-\frac{\mathbf{b}_i}{2} (\mathbf{G}_i \mathbf{f}_i + \mathbf{G}_{i-1} \mathbf{f}_{i-1})}$$

This equation can be simplified by applying assumptions **A: Seismic-Force** and **A: Surface-Load**, which state that the seismic and external forces, respectively, are zero:

$$\lambda = \frac{-\mathbf{G}_i \left(\mathbf{h}_{z,i} + \frac{\mathbf{b}_i}{2} \tan(i) \right) + \mathbf{G}_{i-1} \left(\mathbf{h}_{z,i-1} - \frac{\mathbf{b}_i}{2} \tan(i) \right) - \mathbf{H}_i \left(\frac{1}{3} \mathbf{h}_{z,w,i} + \frac{\mathbf{b}_i}{2} \tan(i) \right) + \mathbf{H}_{i-1} \left(\frac{1}{3} \mathbf{h}_{z,w,i-1} - \frac{\mathbf{b}_i}{2} \tan(i) \right)}{-\frac{\mathbf{b}_i}{2} (\mathbf{G}_i \mathbf{f}_i + \mathbf{G}_{i-1} \mathbf{f}_{i-1})}$$

Taking the summation of all slices, and applying **A: Edge-Slices** to set \mathbf{G}_0 , \mathbf{G}_n , \mathbf{H}_0 , and \mathbf{H}_n equal to zero, a general equation for the proportionality constant λ is developed in Equation (16), which combines **IM: nrmShrFor**, **IM: nrmShrForNum**, and **IM: nrmShrForDen**:

$$\lambda = \frac{\sum_{i=1}^n \mathbf{b}_i \left(\mathbf{F}_x^G + \mathbf{F}_x^H \right) \tan(i) + \mathbf{h}_i - 2\mathbf{U}_{t,i} \sin(i)}{\sum_{i=1}^n \mathbf{b}_i (\mathbf{G}_i \mathbf{f}_i + \mathbf{G}_{i-1} \mathbf{f}_{i-1})}$$

Equation (16) for λ is a function of the unknown interslice normal forces \mathbf{G} (**IM: intsliceFs**) which itself depends on the unknown factor of safety F_S (**IM: fctSfty**).

Refname	IM:nrmShrForNum
Label	Normal and shear force proportionality constant numerator
Input	$\mathbf{x}_{slope}, \mathbf{y}_{slope}, \mathbf{y}_{wt}, \gamma_w, \mathbf{x}_{slip}, \mathbf{y}_{slip}$
Output	\mathbf{C}_{num}
Input Constraints	
Output Constraints	
Equation	$\mathbf{C}_{num,i} = \begin{cases} \mathbf{b}_1 (\mathbf{G}_1 + \mathbf{H}_1) \tan ({}_1), & i = 1 \\ \mathbf{b}_i (\mathbf{F}_x^G + \mathbf{F}_x^H) \tan ({}_i) + \mathbf{h} - 2\mathbf{U}_{t,i} \sin ({}_i), & 2 \leq i \leq n - 1 \\ \mathbf{b}_n (\mathbf{G}_{n-1} + \mathbf{H}_{n-1}) \tan ({}_{n-1}), & i = n \end{cases}$
Description	<p>\mathbf{C}_{num} is the proportionality constant numerator (N)</p> <p>i is the index (Unitless)</p> <p>\mathbf{b} is the base width of slices (m)</p> <p>\mathbf{G} is the interslice normal forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$\mathbf{H}$ is the interslice normal water forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$\mathbf{h}$ is the base angles ($^\circ$)</p> <p>\mathbf{F}_x^G is the sums of the interslice normal forces (N)</p> <p>\mathbf{F}_x^H is the sums of the interslice normal water forces (N)</p> <p>\mathbf{h} is the y-direction heights of slices (m)</p> <p>\mathbf{U}_t is the surface hydrostatic forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$\mathbf{h}$ is the surface angles ($^\circ$)</p> <p>n is the number of slices (Unitless)</p>
Notes	<p>\mathbf{b} is defined in DD: lengthB, \mathbf{H} is defined in DD: intersliceWtrF, \mathbf{h} is defined in DD: slcHeight, \mathbf{U}_t is defined in GD: srfWtrF, and \mathbf{h} is defined in DD: angleB.</p>
Source	[7] and [3]
RefBy	IM: nrmShrFor IM: nrmShrFor.

See **IM: nrmShrFor** for the derivation of \mathbf{C}_{num} .

Refname	IM:nrmShrForDen
Label	Normal and shear force proportionality constant denominator
Input	$\mathbf{x}_{slip}, const_f$
Output	\mathbf{C}_{den}
Input Constraints	
Output constraints	Con-
Equation	$\mathbf{C}_{den,i} = \begin{cases} \mathbf{b}_1 \mathbf{f}_1 \mathbf{G}_1, & i = 1 \\ \mathbf{b}_i (\mathbf{f}_i \mathbf{G}_i + \mathbf{f}_{i-1} \mathbf{G}_{i-1}), & 2 \leq i \leq n - 1 \\ \mathbf{b}_n \mathbf{G}_{n-1} \mathbf{f}_{n-1}, & i = 1 \end{cases}$
Description	<p>\mathbf{C}_{den} is the proportionality constant denominator (N)</p> <p>i is the index (Unitless)</p> <p>\mathbf{b} is the base width of slices (m)</p> <p>\mathbf{f} is the interslice normal to shear force ratio variation function (Unitless)</p> <p>\mathbf{G} is the interslice normal forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$n$ is the number of slices (Unitless)</p>
Notes	\mathbf{b} is defined in DD: lengthB and \mathbf{f} is defined in DD: ratioVariation .
Source	[7] and [3]
RefBy	IM: nrmShrFor IM: nrmShrFor .
See IM: nrmShrFor for the derivation of \mathbf{C}_{den} .	

Refname	IM:intsliceFs
Label	Interslice normal forces
Input	$\mathbf{x}_{slope}, \mathbf{y}_{slope}, \mathbf{y}_{wt}, c', \varphi', \gamma_{dry}, \gamma_{Sat}, \gamma_w, \mathbf{x}_{slip}, \mathbf{y}_{slip}, const_f$
Output	\mathbf{G}
Input Constraints	
Output constraints	Con-
Equation	$\mathbf{G}_i = \begin{cases} \frac{F_S \mathbf{T}_1 - \mathbf{R}_1}{i}, & i = 1 \\ \frac{{}_{i-1}\mathbf{G}_{i-1}^1 + F_S \mathbf{T}_i - \mathbf{R}_i}{i}, & 2 \leq i \leq n-1 \\ 0, & i = 0 \vee i = n \end{cases}$
Description	<p>\mathbf{G} is the interslice normal forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$i$ is the index (Unitless)</p> <p>F_S is the factor of safety (Unitless)</p> <p>\mathbf{T} is the mobilized shear forces without the influence of interslice forces ($\frac{\text{N}}{\text{m}}$)</p> <p>$\mathbf{R}$ is the resistive shear forces without the influence of interslice forces ($\frac{\text{N}}{\text{m}}$)</p> <p>is the first function for incorporating interslice forces into shear force (Unitless)</p> <p>is the second function for incorporating interslice forces into shear force (Unitless)</p> <p>n is the number of slices (Unitless)</p>
Notes	\mathbf{T} is defined in GD: mobShearWO , \mathbf{R} is defined in GD: resShearWO , is defined in DD: convertFunc1 , and is defined in DD: convertFunc2 .
Source	[7]
RefBy	IM: nrmShrFor IM: intsliceFs IM: intsliceFs IM: fctSfty FR: Display-Interslice-Shear-Forces ⁶² FR: Display-Interslice-Normal-Forces FR: Display-Factor-of-Safety FR: Determine-Critical-Slip-Surface.

This derivation is identical to the derivation for **IM: fctSfty** up until Equation (3) shown again below:

$$\mathbf{G}_{ii} = {}_{i-1}\mathbf{G}_{i-1i-1} + F_S \mathbf{T}_i - \mathbf{R}_i$$

A simple rearrangement of Equation (3) leads to Equation (17), also seen in **IM: intsliceFs**:

$$\mathbf{G}_i = \frac{{}_{i-1}\mathbf{G}_{i-1} + F_S \mathbf{T}_i - \mathbf{R}_i}{i}$$

The cases shown in **IM: intsliceFs** for when $i = 0$, $i = 1$, or $i = n$ are derived by applying **A: Edge-Slices**, which says that \mathbf{G}_0 and \mathbf{G}_n are zero, to Equation (17). \mathbf{G} depends on the unknowns F_S (**IM: fctSfty**) and λ (**IM: nrmShrFor**).

Refname	IM:crtSlpId
Label	Critical slip surface identification
Input	$\mathbf{x}_{slope}, \mathbf{y}_{slope}, \mathbf{x}_{wt}, \mathbf{y}_{wt}, c', \varphi', \gamma_{dry}, \gamma_{Sat}, \gamma_w, const_f$
Output	F_S^{min}
Input Constraints	
Output Constraints	
Equation	$F_S^{min} = \Upsilon (\mathbf{x}_{slope}, \mathbf{y}_{slope}, \mathbf{x}_{wt}, \mathbf{y}_{wt}, c', \varphi', \gamma_{dry}, \gamma_{Sat}, \gamma_w, const_f)$
Description	<p> F_S^{min} is the minimum factor of safety (Unitless) Υ is the minimization function (Unitless) \mathbf{x}_{slope} is the x-coordinates of the slope (m) \mathbf{y}_{slope} is the y-coordinates of the slope (m) \mathbf{x}_{wt} is the x-coordinates of the water table (m) \mathbf{y}_{wt} is the y-coordinates of the water table (m) c' is the effective cohesion (Pa) φ' is the effective angle of friction ($^{\circ}$) γ_{dry} is the soil dry unit weight ($\frac{N}{m^3}$) γ_{Sat} is the soil saturated unit weight ($\frac{N}{m^3}$) γ_w is the unit weight of water ($\frac{N}{m^3}$) $const_f$ is the decision on f (Unitless) </p>
Notes	<p> The minimization function must enforce the constraints on the critical slip surface expressed in A: Slip-Surface-Concave and Table:Out-DataConstraints. The sizes of \mathbf{x}_{wt} and \mathbf{y}_{wt} must be equal and not 1. The sizes of \mathbf{x}_{slope} and \mathbf{y}_{slope} must be equal and at least 2. The first and last \mathbf{x}_{wt} values must be equal to the first and last \mathbf{x}_{slope} values. \mathbf{x}_{wt} and \mathbf{x}_{slope} values must be monotonically increasing. x_{slip}^{maxExt}, x_{slip}^{maxEtr}, x_{slip}^{minExt}, and x_{slip}^{minEtr} must be between or equal to the minimum and maximum \mathbf{x}_{slope} values. y_{slip}^{max} cannot be below the minimum \mathbf{y}_{slope} value. y_{slip}^{min} cannot be above the maximum \mathbf{y}_{slope} value. All x values of $\mathbf{x}_{cs}, \mathbf{y}_{cs}$ must be between x_{slip}^{minEtr} and x_{slip}^{maxExt}. All y values of $\mathbf{x}_{cs}, \mathbf{y}_{cs}$ must not be below y_{slip}^{min}. For any given vertex in $\mathbf{x}_{cs}, \mathbf{y}_{cs}$ </p>

4.2.6 Data Constraints

[Table:InDataConstraints](#) and [Table:OutDataConstraints](#) show the data constraints on the input and output variables, respectively. The column for physical constraints gives the physical limitations on the range of values that can be taken by the variable. The uncertainty column provides an estimate of the confidence with which the physical quantities can be measured. This information would be part of the input if one were performing an uncertainty quantification exercise. The constraints are conservative, to give the user of the model the flexibility to experiment with unusual situations. The column of typical values is intended to provide a feel for a common scenario.

Var	Physical Constraints	Typical Value	Uncert.
c'	$c' > 0$	$10.0 \cdot 10^3$ Pa	10%
x_{slip}^{maxEtr}	—	20.0 m	10%
x_{slip}^{maxExt}	—	100.0 m	10%
x_{slip}^{minEtr}	—	0.0 m	10%
x_{slip}^{minExt}	—	50.0 m	10%
\mathbf{x}_{slope}	—	0.0 m	10%
\mathbf{x}_{wt}	—	0.0 m	10%
y_{slip}^{max}	—	30.0 m	10%
y_{slip}^{min}	—	0.0 m	10%
\mathbf{y}_{slope}	—	0.0 m	10%
\mathbf{y}_{wt}	—	0.0 m	10%
γ_{dry}	$\gamma_{dry} > 0$	$20.0 \cdot 10^3 \frac{\text{N}}{\text{m}^3}$	10%
γ_{Sat}	$\gamma_{Sat} > 0$	$20.0 \cdot 10^3 \frac{\text{N}}{\text{m}^3}$	10%
γ_w	$\gamma_w > 0$	$9.8 \cdot 10^3 \frac{\text{N}}{\text{m}^3}$	10%
φ'	$0 < \varphi' < 90$	25.0 °	10%

Table 4: Input Data Constraints

Var	Physical Constraints
F_S	$F_S > 0$
(x, y)	—

Table 5: Output Data Constraints

4.2.7 Properties of a Correct Solution

FIXME.

5 Requirements

This section provides the functional requirements, the tasks and behaviours that the software is expected to complete, and the non-functional requirements, the qualities that the software is expected to exhibit.

5.1 Functional Requirements

This section provides the functional requirements, the tasks and behaviours that the software is expected to complete.

Read-and-Store: Read the inputs, shown in [Table:inDataTable](#), and store the data.

Verify-Input: Verify that the input data lie within the physical constraints shown in [Table:InData-Constraints](#).

Critical-Slip-Surface: Determine the critical slip surface for the input slope, corresponding to the minimum factor of safety, by using [IM: fctSfty](#), [IM: nrmShrFor](#), and [IM: intsliceFs](#) to calculate the factor of safety for a slip surface and using [IM: crtSlpId](#) to find the slip surface that minimizes it.

Verify-Output: Verify that the minimum factor of safety and critical slip surface satisfy the physical constraints shown in [Table:OutDataConstraints](#).

Display-Input: Display as output the user-supplied inputs listed in [Table:inputsToOutputTable](#).

Display-Graph: Display the critical slip surface of the 2D slope, as determined from [IM: crtSlpId](#), graphically.

Display-Factor-of-Safety: Display the value of the factor of safety for the critical slip surface, as determined from [IM: fctSfty](#), [IM: nrmShrFor](#), and [IM: intsliceFs](#).

Display-Interslice-Normal-Forces: Using [IM: fctSfty](#), [IM: nrmShrFor](#), and [IM: intsliceFs](#), calculate and graphically display the interslice normal forces.

Display-Interslice-Shear-Forces: Using [IM: fctSfty](#), [IM: nrmShrFor](#), and [IM: intsliceFs](#), calculate and graphically display the interslice shear forces.

Write-Results-To-File: Provide the option of writing the output result data, as given in [FR: Display-Input](#), [FR: Display-Graph](#), [FR: Display-Factor-of-Safety](#), [FR: Display-Interslice-Normal-Forces](#), and [FR: Display-Interslice-Shear-Forces](#), to a file.

Symbol	Unit	Name
(x, y)	m	cartesian position coordinates
\mathbf{x}_{slope}	m	x-coordinates of the slope

Symbol	Unit	Name
\mathbf{y}_{slope}	m	y-coordinates of the slope
\mathbf{x}_{wt}	m	x-coordinates of the water table
\mathbf{y}_{wt}	m	y-coordinates of the water table
x_{slip}^{maxExt}	m	maximum exit x-coordinate
x_{slip}^{maxEtr}	m	maximum entry x-coordinate
x_{slip}^{minExt}	m	minimum exit x-coordinate
x_{slip}^{minEtr}	m	minimum exit x-coordinate
y_{slip}^{max}	m	maximum y-coordinate
y_{slip}^{min}	m	minimum y-coordinate
c'	Pa	effective cohesion
φ'	°	effective angle of friction
γ_{dry}	$\frac{N}{m^3}$	soil dry unit weight
γ_{Sat}	$\frac{N}{m^3}$	soil saturated unit weight
γ_w	$\frac{N}{m^3}$	unit weight of water
$const_f$		decision on f

Table 6: Required Inputs

Symbol	Name
$const_f$	decision on f
x_{slip}^{maxExt}	maximum exit x-coordinate
x_{slip}^{maxEtr}	maximum entry x-coordinate
x_{slip}^{minExt}	minimum exit x-coordinate
x_{slip}^{minEtr}	minimum exit x-coordinate
y_{slip}^{max}	maximum y-coordinate
y_{slip}^{min}	minimum y-coordinate

Table 7: Inputs to be returned as output

5.2 Non-Functional Requirements

This section provides the non-functional requirements, the qualities that the software is expected to exhibit.

Correct: The outputs of the code have the properties described in [Section: Properties of a Correct Solution](#).

Understandable: The code is modularized with complete module guide and module interface specification.

Reusable: The code is modularized.

Maintainable: The traceability between requirements, assumptions, theoretical models, general definitions, data definitions, instance models, likely changes, unlikely changes, and modules is completely recorded in traceability matrices in the SRS and module guide.

6 Likely Changes

Homogeneous-Soil-Layers: **A: Soil-Layer-Homogeneous** - The system currently assumes the soil mass is homogeneous. In the future, calculations can be added for inconsistent soil properties throughout.

Late-Seismic-Force: **A: Seismic-Force** - The system currently assumes no seismic force. In the future, calculations can be added for the presence of seismic force.

Late-External-Force: **A: Surface-Load** - The system currently assumes no external forces. In the future, calculations can be added for an imposed surface load on the slope.

7 Unlikely Changes

If changes were to be made with regard to the following, a different algorithm would be needed.

Shear-Linear-Only: Changes related to **A: Interslice-Norm-Shear-Forces-Linear** are not possible due to the dependency of the calculations on the linear relationship between interslice normal forces and interslice shear forces.

2D-Analysis-Only: **A: Effective-Norm-Stress-Large** allows for 2D analysis with these models only because stress along the z -direction is zero. These models do not take into account stress in the z -direction, and therefore cannot be used without manipulation to attempt three-dimensional analysis.

8 Traceability Matrices and Graphs

The purpose of the traceability matrices is to provide easy references on what has to be additionally modified if a certain component is changed. Every time a component is changed, the items in the row of that component that are marked with an “X” should be modified as well. **Table:Tracey** shows the dependencies of items of different sections on each other.

	NFR: Correct	GD: normForcEq	GD: momen
Section: Properties of a Correct Solution	X		
Fig:ForceDiagram		X	X
DD: intersliceWtrF			
Table:InDataConstraints			

	NFR: Correct	GD: normForcEq	GD: momen
Table:OutDataConstraints			
DD: convertFunc1			
Section: Physical System Description	X		
DD: convertFunc2			
DD: angleA	X		X
A: Effective-Norm-Stress-Large			
A: Edge-Slices			
A: Factor-of-Safety			
A: Hydrostatic-Force-Slice-Midpoint			X
A: Interslice-Norm-Shear-Forces-Linear			
A: Negligible-Effect-Surface-Slope-Seismic			X
A: Plane-Strain-Conditions			
A: Surface-Base-Slice-between-Interslice-Straight-Lines			
A: Seismic-Force			
A: Surface-Load			
A: Soil-Layer-Homogeneous			
A: Soil-Layers-Isotropic			
A: Soil-Properties			
A: Slip-Surface-Concave			
A: Water-Intersects-Base-Edge			
A: Water-Intersects-Surface-Edge			
DD: lengthB			X
GD: baseWtrF			
DD: angleB	X		X
GD: bsShrFEq			
IM: crtSlpId			
FR: Display-Factor-of-Safety			
FR: Display-Graph			
FR: Display-Input			
FR: Display-Interslice-Normal-Forces			
FR: Display-Interslice-Shear-Forces			
TM: effStress			
TM: equilibrium	X		X
DD: ratioVariation			
TM: factOfSafety			
IM: fctSfty			
DD: sliceHghtLeftDD			
DD: sliceHghtRightDD			
DD: slcHeight			X
Table:inDataTable			
Table:inputsToOutputTable			

	NFR: Correct	GD: normForcEq	GD: momen
IM: intsliceFs			
DD: lengthLb			
TM: mcShrStrgth			
GD: mobShearWO			
GD: mobShr			
GD: momentEq			
TM: NewtonSecLawMot			
GD: normForcEq			
GD: normShrR			
IM: nrmShrForDen			
IM: nrmShrForNum			
IM: nrmShrFor			
GD: resShearWO			
GD: resShr			
DD: stress			
GD: sliceWght		X	X
GD: srfWtrF		X	X
DD: torque			X
GD: weight			X

9 Values of Auxiliary Constants

There are no auxiliary constants.

10 References

- [1] D. G. Fredlund and J. Krahn. “Comparison of slope stability methods of analysis”. In: *Canadian Geotechnical Journal* 14.3 (Apr. 1977), ”429–439”.
- [2] Ronald Huston and Harold Josephs. *Practical stress analysis in engineering design*. 3rd ed. CRC Press, 2008.
- [3] Brandon Karchewski, Peijun Guo, and Dieter Stolle. “Influence of inherent anisotropy of soil strength on limit equilibrium slope stability analysis”. In: *Proceedings of the 65th annual Canadian GeoTechnical Conference*. Canadian Geotechnical Society. Winnipeg, MB, Canada, 2012.
- [4] Nirmitha Koothoor. “A document drive approach to certifying scientific computing software”. MA thesis. Hamilton, ON, Canada: McMaster University, 2013.

- [5] N. R. Morgenstern and P. E. Price. “The analysis of the stability of general slip surfaces”. In: *Géotechnique* 15 (Jan. 1965), ”79–93”.
- [6] David L. Parnas and P. C. Clements. “A rational design process: How and why to fake it”. In: *IEEE Transactions on Software Engineering* 12.2 (Feb. 1986), ”251–257”.
- [7] Q. H. Qian et al. “A concise algorithm for computing the factor of safety using the morgenstern price method”. In: *Canadian Geotechnical Journal* 42.1 (Feb. 2005), ”272–278”.
- [8] W. Spencer Smith and Lei Lai. “A new requirements template for scientific computing”. In: *Proceedings of the First International Workshop on Situational Requirements Engineering Processes - Methods, Techniques and Tools to Support Situation-Specific Requirements Engineering Processes, SREP’05*. Ed. by PJ Agerfalk, N. Kraiem, and J. Ralyte. In conjunction with 13th IEEE International Requirements Engineering Conference, Paris, France, 2005, ”107–121”.
- [9] Li Yu-Chao et al. “An efficient approach for locating the critical slip surface in slope stability analyses using a real-coded genetic algorithm”. In: *Canadian Geotechnical Journal* 47.7 (June 2010), ”806–820”.