

Aeroelastic Analysis of Hypersonic Double-wedge Lifting Surface

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Abstract

1 Numerical Method

The governing equation can be written as

$$m\ddot{\theta} + k\theta = f(\theta, t) \quad (1)$$

where m is the mass of airfoil, k is the stiffness, θ is the angle of attack and f is the aerodynamic load. We use the Piston Theory to calculate the aerodynamic load acting on the airfoil. The pressure distribution on the airfoil can be written as follows

$$\frac{P(x, t)}{P_\infty} = \left(1 + \frac{\gamma - 1}{2} \frac{v_n}{a_\infty}\right)^{\frac{2\gamma}{\gamma - 1}} \quad (2)$$

where $P(x, t)$ is the pressure at point x on the airfoil, P_∞ is the free stream pressure, γ is the ratio of specific heats and a_∞ is the speed of sound. v_n is calculated using the following equation.

$$v_n = \frac{\partial Z(x, t)}{\partial t} + V \frac{\partial Z(x, t)}{\partial x} \quad (3)$$

where V is the free stream velocity and $Z(x, t)$ is the position of airfoil surface. The position of airfoil surface can be related to the angle of attack using the following equation:

$$Z(x, t) = M_r(\theta(t)) Z_0(x) \quad (4)$$

where M_r is the rotation matrix, and $Z_0(x)$ is the initial shape of the airfoil. As can be seen here, the location of surface at time t only depends on the angle of attack at that time, $\theta(t)$. The rotation matrix is defined as

$$M_r = \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix}$$

By expanding Equation (2), and substituting for $Z(x, t)$ from Equation (4), Equation (1) can be rewritten as

$$m\ddot{\theta} + k\theta = \oint_{airfoil} P_\infty \left[\gamma \frac{v_n}{a_\infty} + \frac{\gamma(\gamma + 1)}{4} \left(\frac{v_n}{a_\infty} \right)^2 + 1 \right] ds \quad (5a)$$

$$v_n = \frac{\partial M_r(\theta)}{\partial t} Z_0(x) + V M_r(\theta) \frac{\partial Z_0(x)}{\partial x} \quad (5b)$$

Equation (5) needs to be solved for θ