Convergence of analysis results

Área de Mecánica Computacional

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1 Cantilever beam

Figure 1 shows a cantelever beam under a tip load P. The beam is of length l; moment of inertia I; height 2c and material properties corresponding to Poissons ratio and Young modulos ν and E respectively.

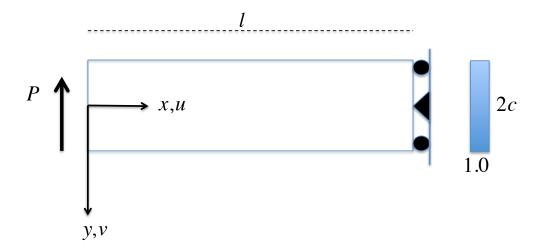


Figure 1: Cantelever beam.

The analytic solution (?) is given by:

$$u = -\frac{P}{2EI}x^{2}y - \frac{\nu P}{6EI}y^{3} + \frac{P}{2IG}y^{3} + \left(\frac{Pl^{2}}{2EI} - \frac{Pc^{2}}{2IG}\right)y$$

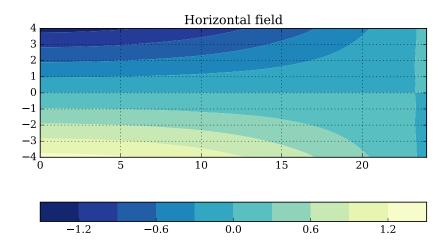
$$v = \frac{\nu P}{2EI}xy^{2} + \frac{P}{6EI}x^{3} - \frac{Pl^{2}}{2EI}x + \frac{Pl^{3}}{3EI}$$

$$\varepsilon_{xx} = \frac{\partial u}{\partial x} \equiv -\frac{P}{EI}xy$$

$$\varepsilon_{yy} = \frac{\partial v}{\partial y} \equiv \frac{\nu P}{EI}xy$$

$$\gamma_{xy} = \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \equiv \frac{P}{2IG}(y^{2} - c^{2})$$

while the particular solution for parameters $E=1000.0,\,\nu=0.30,\,l=24$ and 2c=8 is shwon below:



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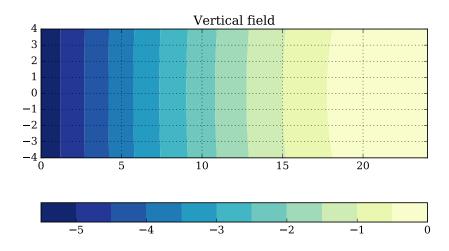


Figure 2: Horizontal field.

The beam was also analyzed with the FEM using solid lineal square elements under plane stress conditions. We conducted 5 different analysis with the following set of characteristic element size

h = [6.0, 3.0, 1.5, 1.0, 0.5]. The meshes are shown in fig. 3

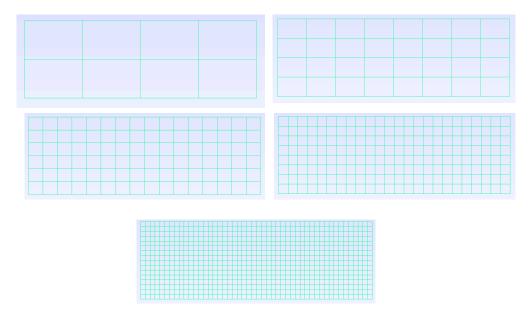


Figure 3: Finite element meshes.

The horizontal and vertical displacement contours for the FE-solution and the analytic solution are compared in fig. 4 for the case h=1.0. Notice that in the finite elment models the load is applied as nodal point loads of the same magnitud distributed along all the nodes at x=0. This implies a uniform load distribution instead of the parabolic load consitent with the shear stress in the analytic solution.

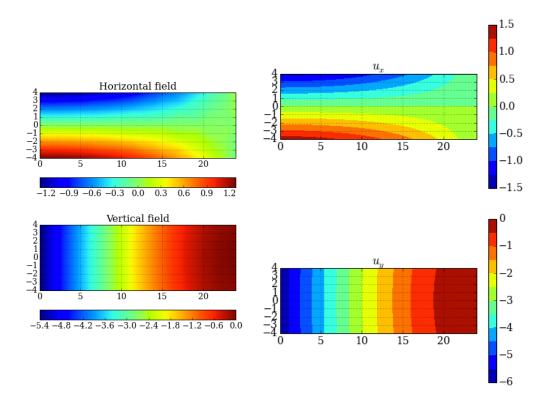


Figure 4: Analytic (left) vs Numerical (right) solution.

$$\begin{split} \prod_{FE} &= -\frac{1}{2}U^T K U \\ \prod_{Exa} &= \frac{\prod_{n=1}^2 - \prod_n \prod_{n=2}}{2\prod_{n=1} - \prod_n - \prod_{n=2}} \end{split}$$

Using n = 5 we have $\prod_{Exa} = -154.09$.

$$\|\vec{u}_{Exa} - \vec{u}_{FE}\| \equiv (\prod_{Exa} - \prod_{FE})^{1/2}$$

| h | \prod_{FE} | $\ \vec{u}_{Exa} - \vec{u}_{FE}\ $ | $rac{\ ec{u}_{Exa} - ec{u}_{FE}\ }{\ ec{u}_{Exa}\ }$ |
|-----|--------------|------------------------------------|---|
| 6.0 | -118.414 | 5.973 | 0.481 |
| 3.0 | -139.273 | 3.849 | 0.310 |
| 1.5 | -145.866 | 2.868 | 0.231 |
| 1.0 | -147.501 | 2.567 | 0.207 |
| 0.5 | -148.811 | 2.298 | 0.185 |

Table 1: Convergence of anlysis results

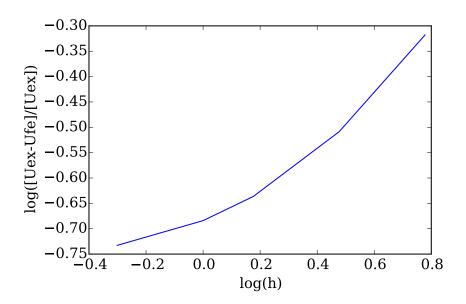


Figure 5: Energy norm of the error

$$\log\left(\|\vec{u}_{Exa} - \vec{u}_{FE}\|\right) = \log c + k \log h$$