

## Homework 5

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#### 1) MIMO Model

**a.**

The State Space representation of 4-cylinder SI engine is given by,

$$x_1(k) = \frac{c_{T2}}{\sqrt{\tau_o}} p(k-1) + \frac{c_{T3}}{\sqrt{\tau_o}} w(k-1) - \frac{c_{T4}}{\sqrt{\tau_o}} \alpha(k-1)$$

$$x_2(k) = \frac{c_{T6}}{\sqrt{\tau_o}} w(k-1) - \frac{c_{T7}}{\sqrt{\tau_o}} T(k-1)$$

$$x_3(k) = p(k-1)$$

$$x_4(k) = x_3(k-1) = p(k-2)$$

$$x_5(k) = x_4(k-1) = p(k-3); \quad T(k) = K_p p(k-3) + K_v v(k)$$

**State Space Matrices:**

$$\begin{aligned} x(k+1) &= \Phi_T x(k) + \Gamma_T \alpha(k) \\ y(k) &= H_T x(k) + D_T \alpha(k) \end{aligned}$$

$$\Phi_T = \begin{bmatrix} (OM^{-1})_{11} & (OM^{-1})_{12} & 0 & 0 & Q_{12}K_p \\ (OM^{-1})_{21} & (OM^{-1})_{22} & 0 & 0 & Q_{22}K_p \\ (M^{-1})_{11} & (M^{-1})_{12} & 0 & 0 & -(M^{-1}N)_{12}K_p \\ 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 \end{bmatrix} \quad \Gamma_T = \begin{bmatrix} Q_{11} & Q_{12}K_v \\ Q_{21} & Q_{22}K_v \\ -(M^{-1}N)_{11} & -(M^{-1}N)_{12}K_v \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$$

$$H_T = [(M^{-1})_{21} \quad (M^{-1})_{22} \quad 0 \quad 0 \quad -(M^{-1}N)_{22}K_p] \quad D_T = [-(M^{-1}N)_{21} \quad -(M^{-1}N)_{22}K_v]$$

$$M = \begin{bmatrix} \frac{-c_{T1}}{\sqrt{\tau_o}} & \frac{-c_{T3}}{\sqrt{\tau_o}} \\ 0 & \frac{-c_{T5}}{\sqrt{\tau_o}} \end{bmatrix}$$

$$N = \begin{bmatrix} \frac{c_{T4}}{\sqrt{\tau_o}} & 0 \\ 0 & \frac{c_{T7}}{\sqrt{\tau_o}} \end{bmatrix}$$

$$O = \begin{bmatrix} \frac{c_{T2}}{\sqrt{\tau_o}} & \frac{c_{T3}}{\sqrt{\tau_o}} \\ 0 & \frac{c_{T6}}{\sqrt{\tau_o}} \end{bmatrix}$$

$$P = \begin{bmatrix} \frac{-c_{T4}}{\sqrt{\tau_o}} & 0 \\ 0 & \frac{-c_{T7}}{\sqrt{\tau_o}} \end{bmatrix}$$

$$Q = -OM^{-1}N + P$$

*In general,  $X_{ij}$  stands for the element in  $i^{th}$  row and  $j^{th}$  column*

$$\Phi_T = \begin{bmatrix} 0.9724 & -6.1276 & 0 & 0 & 0.0011 \\ 0 & 0.9990 & 0 & 0 & -0.0004 \\ -1.0092 & 3.1353 & 0 & 0 & -0.0006 \\ 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 \end{bmatrix} \quad \Gamma_T = \begin{bmatrix} -91.2330 & 0.5860 \\ 0 & -0.1912 \\ 46.6806 & -0.2998 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$$

$$H_T = [0 \quad -1.0228 \quad 0 \quad 0 \quad 0.0002] \quad D_T = [0 \quad 0.0978]$$

## 2. MIMO – Pole Placement

### Design Specification:

- Settling time (radians) = 300 radian
- Overshoot = 250 rpm

### Calculation for Desired location of the Dominant pole:

Finding the desire root location (region) for dominant poles,

Overshoot:

$$PO \% = 100 * e^{-\frac{\zeta\pi}{\sqrt{1-\zeta^2}}}$$

$$\zeta = 0.34 \text{ (Approx.,)}$$

Settling time:

$$T_s = \frac{4}{\zeta\omega_n} = 300 \text{ rad}$$

$$\omega_n = 0.039 \text{ (Approx.,)}$$

NOTE: The above parameter are in continuous time domain. One converting the above parameters we get the approximate pole location.

### Region of interest:

The region of interest is approximately around (right side of unit circle)  $z = 0.93+0.1i$  (approx). The desired poles are chosen in the region of interest by trial and error method.

### Desired poles:

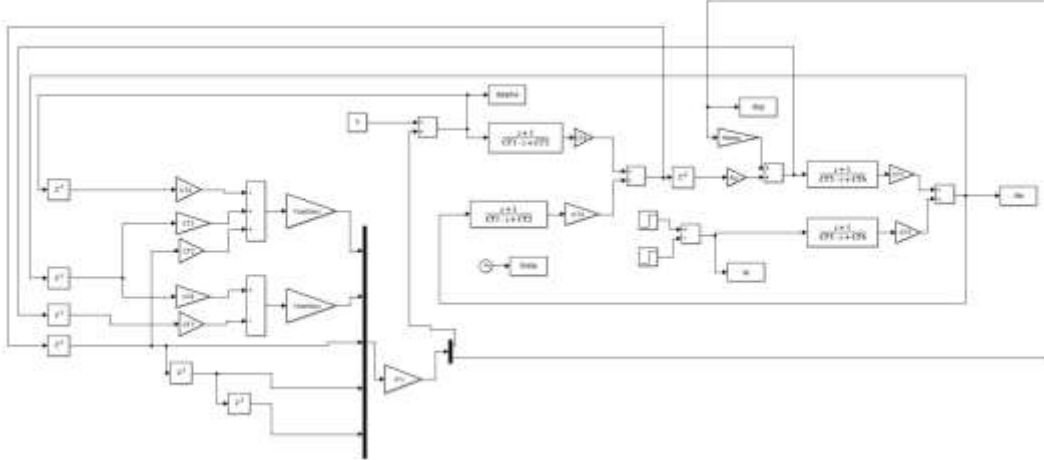
The poles were chosen in the desired region, as follows;

$$\begin{aligned} &0.939+0.1i, \\ &0.939-0.1i, \\ &0.089+0.65i, \\ &0.089-0.65i, \\ &-0.1 \end{aligned}$$

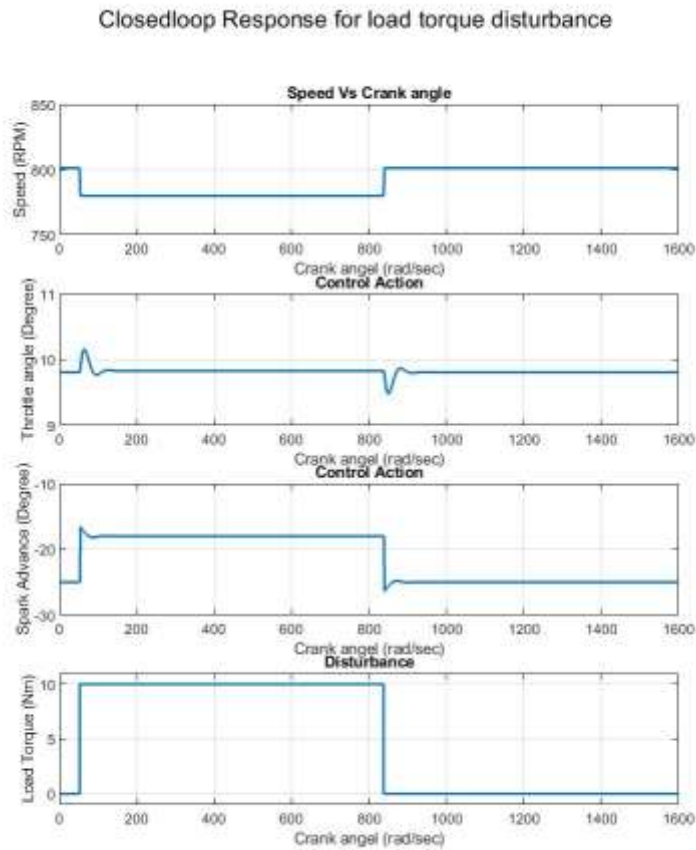
The K matrix is as follows,

$$K = \begin{bmatrix} 0.0448 & 0.0302 & 0.0644 & -0.0289 & 0.0082 \\ 0.0001 & -5.7489 & 0.0001 & 0.0000 & 0.0019 \end{bmatrix}$$

The response is as follows,



**Fig 1: Simulink State Feedback (P alone)**



**Fig 2: Closed Loop Response of State Feedback (P alone)**

**Inference,**

The throttle angle, overshoot and settling time are within desired region.

The steady state error is non-zero (Because of P-alone control action)

**3. MIMO Pole Placement – Augmented Systems;**

The system is augmented to have integral action. The state space matrix is modifies as follows,

$$\Phi_T = \begin{bmatrix} (OM^{-1})_{11} & (OM^{-1})_{12} & 0 & 0 & Q_{12}K_p & 0 \\ (OM^{-1})_{21} & (OM^{-1})_{22} & 0 & 0 & Q_{22}K_p & 0 \\ (M^{-1})_{11} & (M^{-1})_{11} & 0 & 0 & -(M^{-1}N)_{12}K_p & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ (M^{-1})_{21} & (M^{-1})_{22} & 0 & 0 & -(M^{-1}N)_{22}K_p & 1 \end{bmatrix}$$

$$\Gamma_T = \begin{bmatrix} Q_{11} & Q_{12}K_v \\ Q_{21} & Q_{22}K_v \\ -(M^{-1}N)_{11} & -(M^{-1}N)_{12}K_v \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$$

$$H_T = [(M^{-1})_{21} \quad (M^{-1})_{22} \quad 0 \quad 0 \quad -(M^{-1}N)_{22}K_p \quad 0] \quad D_T = [-(M^{-1}N)_{21} \quad -(M^{-1}N)_{22}K_v]$$

$$\Phi_T = \begin{bmatrix} 0.9724 & -6.1276 & 0 & 0 & 0.0011 & 0 \\ 0 & 0.9990 & 0 & 0 & -0.0004 & 0 \\ -1.0092 & 3.1353 & 0 & 0 & -0.0006 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & -1.0228 & 0 & 0 & 0.0002 & 1 \end{bmatrix} \quad \Gamma_T = \begin{bmatrix} -91.2330 & 0.5860 \\ 0 & -0.1912 \\ 46.6806 & -0.2998 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$$

$$H_T = [0 \quad -1.0228 \quad 0 \quad 0 \quad 0.0002 \quad 0]$$

$$D_T = [0 \quad 0.0978]$$

The desired poles for augmented are chosen in region of interest by trial and error method.

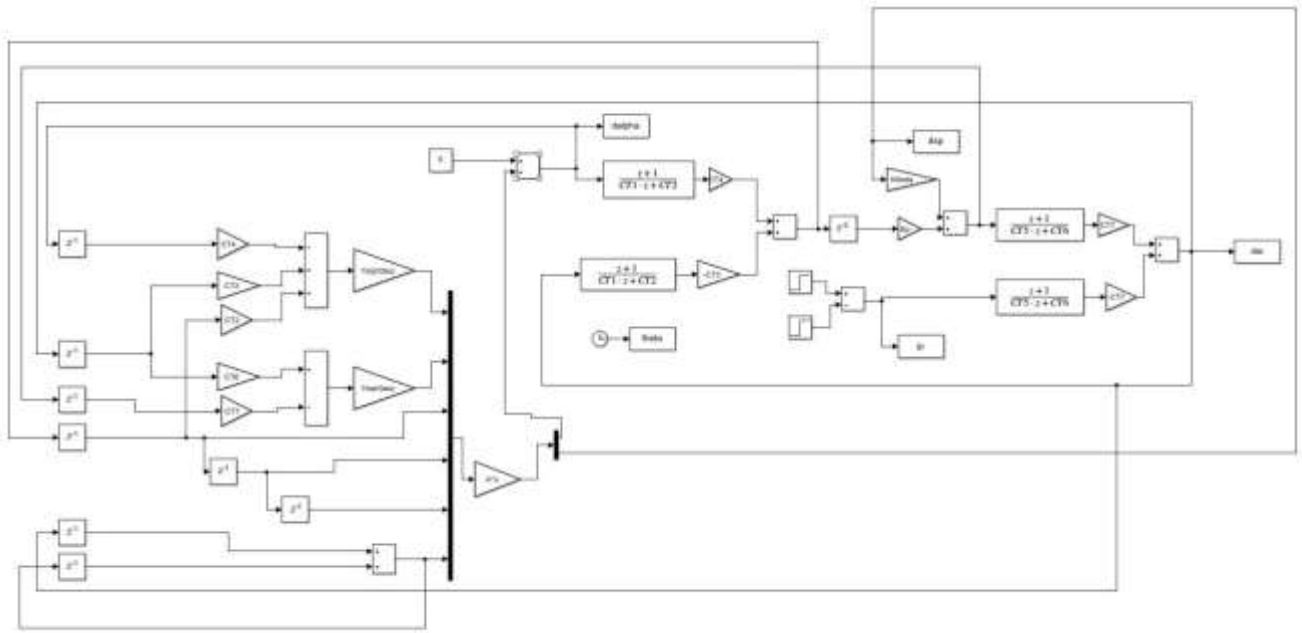
The chosen poles are as follows,

$$\begin{aligned} &0.939+0.1i, \\ &0.939-0.1i \\ &0.089+0.65i \\ &0.089-0.65i \\ &0.73 \\ &-0.1 \end{aligned}$$

The gain matrix k is as follows

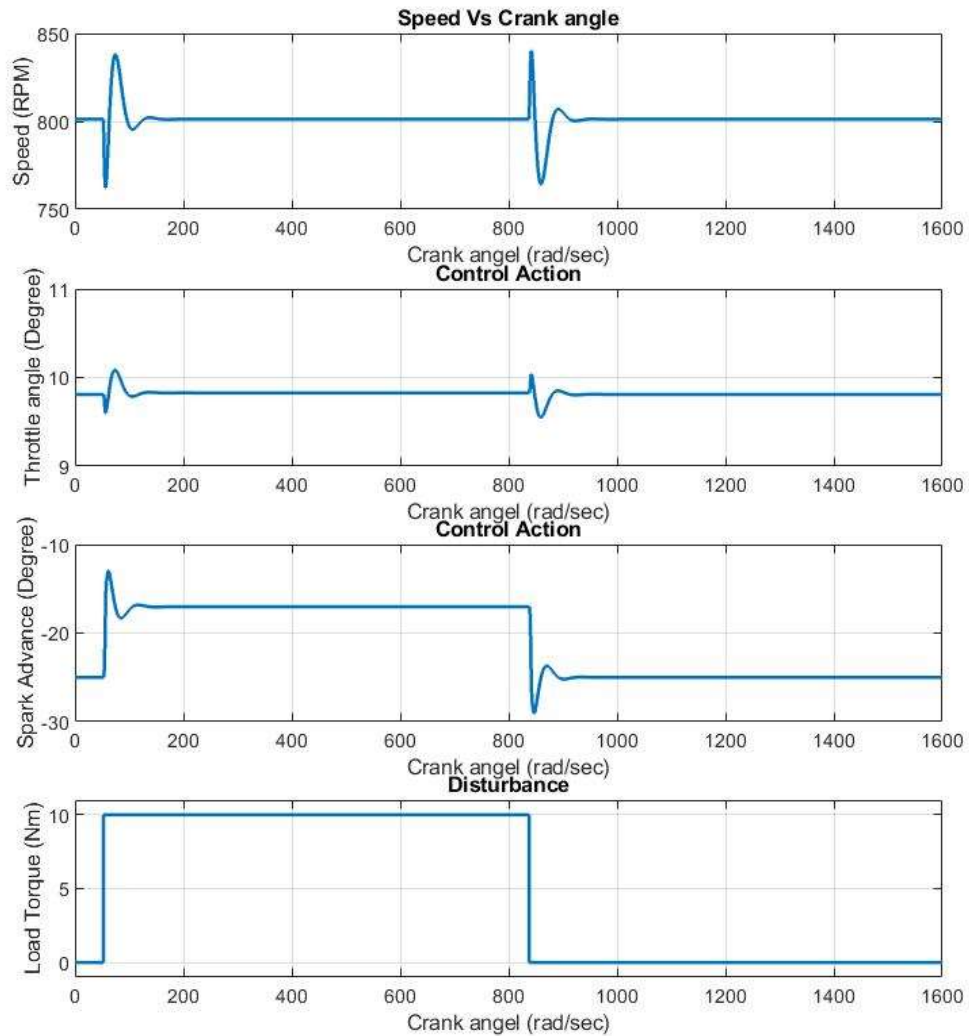
$$K = \begin{bmatrix} 0.0069 & 0.0562 & 0.0146 & -0.0072 & -0.0009 & 0.0013 \\ -0.2741 & -1.5735 & -0.3147 & -0.1534 & -0.0151 & 0.0968 \end{bmatrix}$$

The response of the systems for state feedback (PI) is as follows,



**Fig 3: Simulink State Feedback (PI)**

### Closedloop Response for load torque disturbance

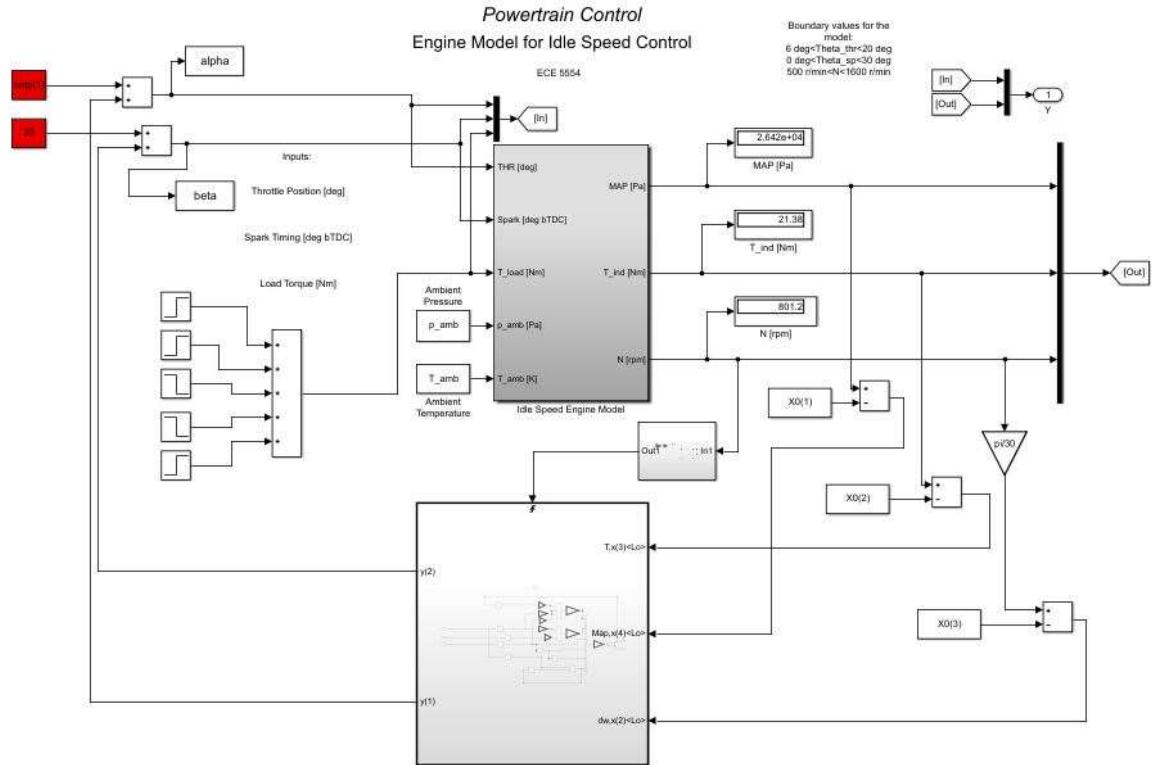


**Fig 4: Closed Loop Response of State Feedback (PI)**

#### **Inference:**

The throttle angel, overshoot, settling time are within desired region.  
The steady state error is zero (Because of integral action)

#### Problem 4:

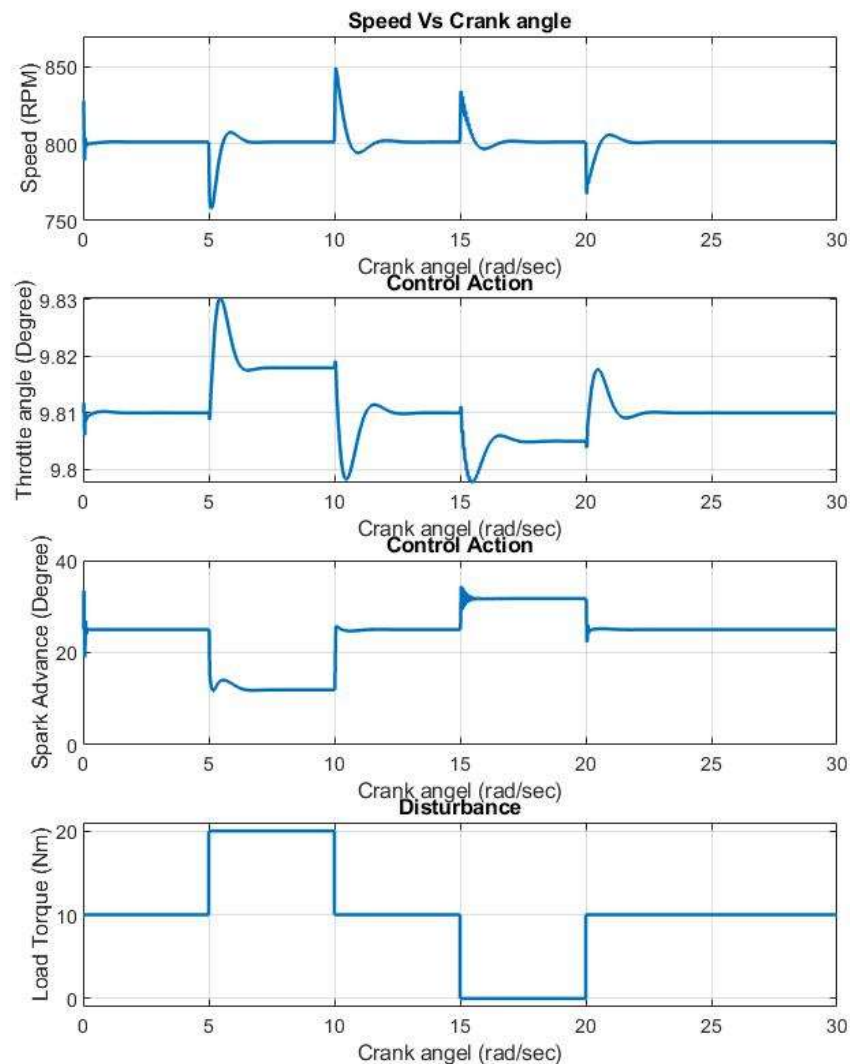


By trial and error, (By adjusting poles, and state feedback gain directly and getting back the poles again), the final control state feedback is found to be of as follows;

$$K = \begin{bmatrix} 0.00009 & 0.003 & -0.0006 & -0.000012 & -0.000043 & 0.000087 \\ 0.0291 & 2.98 & 0.00173 & 0.10000545 & -0.00525 & -0.21 \end{bmatrix}$$

{-0.3409, -0.0022+0.0038i, -0.0022-0.0038i, 0.0044+0.0000i, 0.6885+0.2090i, 0.6885-0.2090i} (Using Trial and error)

## Openloop Response for load torque disturbance



### Inference:

The above graph shows that output has reached the desired value. The throttle is in the desired range, and spark advance is also in the desired range (slightly greater at a few instants). But overall response is desirable and satisfactory.

### Problems with state feedback:

- Needs trial and error

- While entering the desired pole in "place" command, the order of poles matters and will result in different gain matrices for different ordering.

- Placing poles for a SISO system is easy and it becomes difficult in the case of MIMO.

- It has no factor to account for control authority. (No factor to give weight for different inputs in the case of MIMO)