

Prelab report 6a

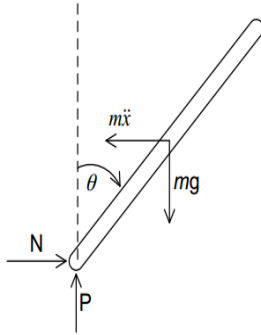
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3.2 Equations of motion of the Mechanical system

Under the small-angle approximation $\sin \theta \approx \theta$ and $\cos \theta \approx 1$, derive the equations of motion (1) and (2) of the inverted pendulum-cart system. In (1), F_a is the force exerted on the cart by the motor.

$$(M + m) \ddot{x} + mL_p \ddot{\theta} = F_a \quad (1)$$

$$mL_p \ddot{x} + \frac{4mL_p^2}{3} \ddot{\theta} - mgL_p \theta = 0 \quad (2)$$



From Newton's second law. We have $F = ma$

In the question

Assume acceleration = a and angular acceleration = α

$F_a = (M + m)a + m\alpha L_p$

And we have $a = \ddot{x}$ $\alpha = \ddot{\theta}$

Then we have $F_a = (m + M)\ddot{x} + m\ddot{\theta}L_p$, which is (1)

Then calculate the moment of the stick, from the left figure, we have $L_p(m\ddot{x}\cos\theta - mg\sin\theta) + I\alpha = 0$, where α is the angular acceleration and I is the moment of inertia.

$$I = \int_0^L r^2 dr = \frac{1}{3} mL^2 = \frac{4}{3} mL_p^2. \text{ So we have } L_p(m\ddot{x}\cos\theta - mg\sin\theta) + \frac{4}{3} mL_p^2 \ddot{\theta} = 0$$

Use linearization $\cos\theta = 1$ and $\sin\theta = \theta$, we have $L_p(m\ddot{x} - mg\theta) + \frac{4}{3} mL_p^2 \ddot{\theta} = 0$, which is (2)

3.2 Full System Dynamics of Linearized System

$$F_a = (m + M)\ddot{x} + m\ddot{\theta}L_p \quad (1)$$

$$L_p(m\ddot{x} - mg\theta) + \frac{4}{3} mL_p^2 \ddot{\theta} = 0 \quad (2)$$

$$F_a = \frac{K_g K_t}{R m^* r} V - \frac{K_m K_g^2 K_t}{R m^* r^2} \dot{x} - \frac{K_g^2 J_m}{r^2} \ddot{x} \quad (3)$$

$$\text{From (1) and (2), we have } (M + m + \frac{K_g^2 J_m}{r^2} - \frac{3m}{4}) \ddot{x} + mL_p \ddot{\theta} = \frac{K_g K_t}{R m^* r} V - \frac{K_m K_g^2 K_t}{R m^* r^2} \dot{x} \quad (4)$$

$$\text{From (3) we have } \ddot{\theta} = \frac{3g}{4L_p} \theta - \frac{3}{4L_p} \ddot{x} \quad (5)$$

From (4) and (5) we have

$$\ddot{x} = -\frac{3g}{4(M + m + \frac{K_g^2 J_m}{r^2} - \frac{3m}{4})} \theta - \frac{K_m K_g^2 K_t}{R m^* r^2 (M + m + \frac{K_g^2 J_m}{r^2} - \frac{3m}{4})} \dot{x} + \frac{K_g K_t}{R m^* r (M + m + \frac{K_g^2 J_m}{r^2} - \frac{3m}{4})} V$$

$$\text{Then } \ddot{\theta} = (\frac{3g}{4L_p} + \frac{9}{16L_p (M + m + \frac{K_g^2 J_m}{r^2} - \frac{3m}{4})}) \theta + \frac{3K_m K_g^2 K_t}{4L_p R m^* r^2 (M + m + \frac{K_g^2 J_m}{r^2} - \frac{3m}{4})} \dot{x} -$$

$$\frac{3Kg*Kt}{4LpRm*r (M+m+\frac{Kg^2*Jm}{r^2} - \frac{3m}{4})} V$$

$$A = \begin{bmatrix} 0 & a_{12} & 0 & 0 \\ 0 & a_{22} & a_{23} & 0 \\ 0 & 0 & 0 & a_{34} \\ 0 & a_{42} & a_{43} & 0 \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ b_2 \\ 0 \\ b_4 \end{bmatrix}$$

So for matrix A,

$$\text{We have } a_{12}=1, a_{22}= -\frac{4Km*Kg^2*Kt}{Rm*(4Mr^2+4mr^2+4Kg^2*Jm)}, a_{23}= -\frac{3mr^2g}{4Mr^2+mr^2+4Kg^2*Jm}$$

$$b_2= \frac{4r*Kg*Kt}{Rm*(4Mr^2+mr^2+4Kg^2*Jm)}, a_{34}=1, a_{42}= \frac{3Km*Kg^2*Kt}{LpRm (4Mr^2+mr^2+4Kg^2*Jm)},$$

$$a_{43}= \frac{3g[Kg^2*Jm+r^2(M+m)]}{Lp(4Mr^2+mr^2+4Kg^2*Jm)}, b_4= -\frac{3r*Kg*Kt}{LpRm (4Mr^2+m r^2+ Kg^2*Jm)}$$

A System Parameters

Parameter	Value	Description
	439.6 counts/cm	Resolution of the cart position encoder
	651.9 counts/rad	Resolution of the angle encoder
M	0.94 kg	Mass of cart and motor
m	0.230 kg	Mass of pendulum
L_p	0.3302 m	Pendulum distance from pivot to center of mass
I_c	$m L_p^2/3$	Moment of inertia of pendulum about its center
I_e	$4m L_p^2/3$	Moment of inertia of pendulum about its end
K_t	$7.67 \cdot 10^{-3}$ Nm/A	Motor torque constant
K_m	$7.67 \cdot 10^{-3}$ Vs/rad	Motor back EMF constant
K_g	3.71	Motor gearbox ratio
R_m	2.6Ω	Motor winding resistance
r	$6.36 \cdot 10^{-3}$ m	Radius of motor gear
J_m	$3.9 \cdot 10^{-7}$ kg m ²	Motor moment of inertia

Table 1: Parameters of the inverted pendulum setup

Put the values in ,we get A=[0 1 0 0; 0 -6.81 -1.50 0; 0 0 0 1;0 15.47 25.66 0]

$$B=[0 ; 1.52 ; 0 ; -3.46]$$

3.3 Analysis and Controller Design

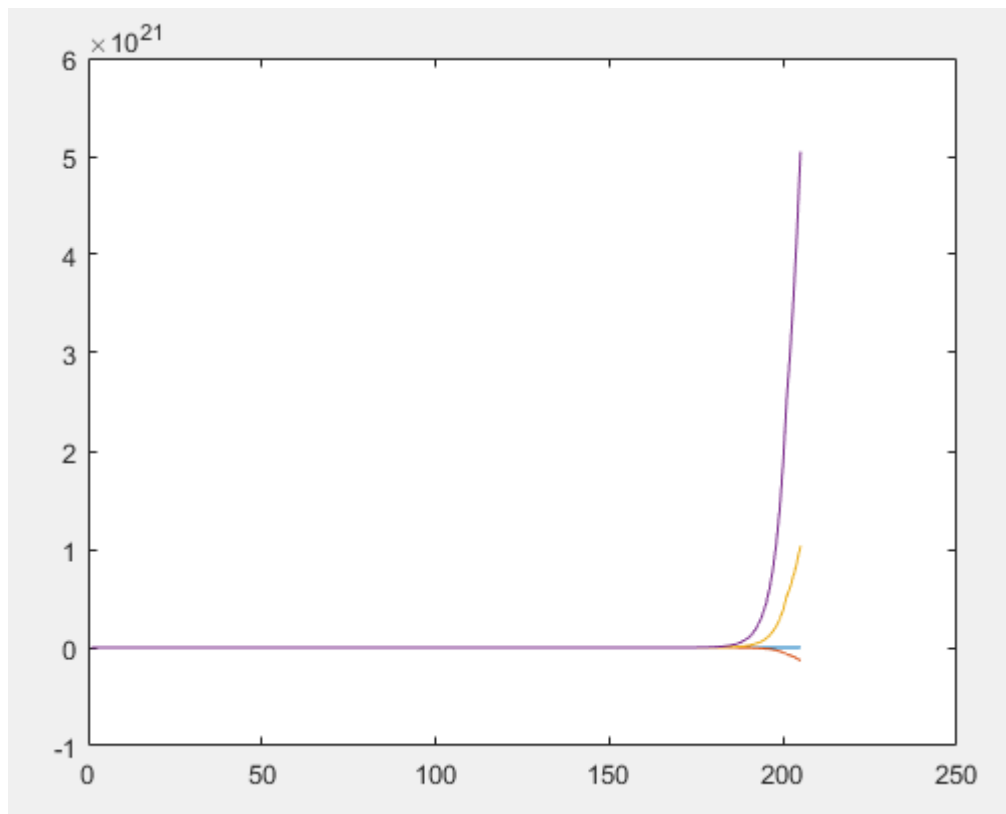
1. Use MATLAB, we get 4 eigenvalues 0 -9.0525 -3.1232 5.3634, we have one pole on the RHP, so it's not internally stable, it's not internally stable, so it can't be BIBO stable.

2. simulation

```
F = @(t,x) [x(1);
            1.52 - 1.50*x(3) - 6.81*x(2);
            x(4);
            15.47*x(2) + 25.66*x(3) - 3.46];

tSpan = [0 10];
initialCondition = [pi/2;0;pi/2;0];
[tSol,xSol] = ode45(F, tSpan, initialCondition);
plot(xSol)
```

plot:



That means in the simulation, the stick will keep rotating as the car goes forward, but actually in the real world's physical system, we expect the stick become stable at a specific angle. I think that's because we have things like friction in real world's physical system, so the stick will lose energy in the process of rotating and finally becomes stable like a tail of the running car, but we don't have interference like friction in simulation, so the stick can't be stable and will keep rotating.

3. (a) $A_k = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -1.52k_1 & -6.81-1.52k_2 & -1.50-1.52k_3 & -1.52k_4 \\ 0 & 0 & 0 & 1 \\ -3.46k_1 & 15.47-3.46k_2 & 25.66-3.46k_3 & -3.46k_4 \end{bmatrix}$

(b) use MATLAB, I get $P(k,s) = \det(sI - A)$ to be $s^4 + (6.81 - 3.46k_4 + 1.52k_2)s^3 + (1.52k_1 - 3.46k_3 - 25.66)s^2 + (-155 - 33.93k_2)s - 33.93k_1$

(c) $P_{des}(s) = (s-s_1)(s-s_2)(s-s_3)(s-s_4) = s^4 + 7s^3 + 120.02s^2 + 347.7s + 440.34$

(d) use the $P(k,s) = P_{des}(s)$, I get $k_1 = -12.98$ $k_2 = -14.72$ $k_3 = -47.85$ $k_4 = -6.54$

Use the command "place", $k_1 = -12.9795$ $k_2 = -14.7230$ $k_3 = -47.8456$ $k_4 = -6.5363$

4. $\dot{x} = Ax + BKr$, use Laplace transform we get $sx(s) = Ax(s) + BKR(s)$

The input of system is x , so we only use the first line, so C is $[1 \ 0 \ 0 \ 0]$

Code:

```

AK = A - B*K;
BK = B*K;
C = [1 0 0 0];
D = zeros(1,4);
[num,den] = ss2tf(AK,BK,C,D,1);
SYS = tf(num,den);
figure(2)
bode(SYS)

```

