ENG2009 – Modelling of Engineering Systems

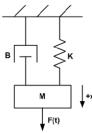
Tutorial 4

State space

State Space:

Example 1:

Find the state space for the following mass-spring-damper system:



Physical Mode

Solution 1:

Step 1: The differential equation of the mass-spring-damper systems in Lecture 2 is (position x(t) is the output and applied force u(t) is the input):

$$\ddot{x}(t) = \frac{1}{M}(-B\dot{x}(t) - Kx(t) + u(t))$$

Step 2: Identify the states:

Let position as 1st states: $x_1(t) = x(t)$ Let velocity as 2nd states: $x_2(t) = \dot{x}(t)$

Step 3: Derivative of states:

$$\dot{x}_1(t) = \dot{x}(t) = x_2(t)$$

$$\dot{x}_2(t) = \ddot{x}(t) = \frac{1}{M}(-B\dot{x}(t) - Kx(t) + u(t))$$

Step 4: Rearrange the derivative of states

$$\dot{x}_1(t) = 0x_1(t) + 1x_2(t) + 0u(t)$$

$$\dot{x}_2(t) = -\frac{K}{M}x_1(t) - \frac{B}{M}x_2(t) + \frac{1}{M}u(t)$$

Step 5: Rewrite in matrix form:

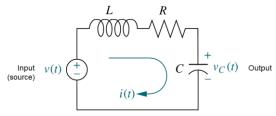
$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -K/M & -B/M \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 1/M \end{bmatrix} u(t)$$

where the output equation

$$y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix}$$

Example 2:

Find the state space equation relating the capacitor voltage $v_c(t)$ (output voltage), to the input voltage, v(t).



Simple RLC circuit

Solution 2:

Step 1: using Kirchoff's voltage law, the differential equation (output: $v_c(t)$, input: v(t)):

$$LC\frac{d^{2}v_{c}(t)}{dt^{2}} + RC\frac{dv_{c}(t)}{dt} + v_{c}(t) = v(t) \text{ or }$$

$$\frac{d^{2}v_{c}(t)}{dt^{2}} = \frac{1}{LC} \left(-RC\frac{dv_{c}(t)}{dt} - v_{c}(t) + v(t) \right)$$

Step 2: Identify the states and inputs:

Let 1^{st} states: $x_1(t) = v_c(t)$

Let 2^{nd} states: $x_2(t) = \dot{v}_c(t)$

Input: u(t) = v(t)

Step 3: Derivative of states:

$$\dot{x}_1(t) = \dot{v}_c(t) = x_2(t)$$

$$\dot{x}_1(t) = \dot{v}_c(t) = x_2(t)$$

$$\dot{x}_2(t) = \ddot{v}_c(t) = \frac{1}{LC}(-RCx_2(t) - x_1(t) + u(t))$$

Step 4: Rearrange the derivative of states

$$\dot{x}_1(t) = 0x_1(t) + 1x_2(t) + 0u(t)$$

$$\dot{x}_2(t) = -\frac{1}{LC}x_1(t) - \frac{R}{L}x_2(t) + \frac{1}{LC}u(t)$$

Step 5: Rewrite in matrix form:

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1/LC & -R/L \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 1/LC \end{bmatrix} u(t)$$

where the output equation

$$y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix}$$

Example 3:

For a DC motor, find the state space equation relating the input voltage $v(t) = e_{in}(t)$, and output shaft speed $\omega(t) = \dot{\theta}(t)$.

Solution 3:

Step 1: Two differential equations (input: $e_{in}(t)$, output: $\dot{\theta}(t)$):

$$J\ddot{\theta} + B_r \,\dot{\theta} = \tau_e = K_t i \tag{A}$$

$$e_{in} = L\frac{di}{dt} + iR + K_e\dot{\theta} \tag{B}$$

Step 2: Identify the states and input:

Let 1^{st} states: $x_1(t) = \theta(t)$

Let 2^{nd} states: $x_2(t) = \dot{\theta}(t)$

Let 3rd states: $x_3(t) = i(t)$

Input: $u(t) = e_{in}(t)$

Step 3: Derivative of states:

$$\dot{x}_1(t) = \dot{\theta}(t) = x_2(t)$$

$$\dot{x}_2(t) = \ddot{\theta}(t) = \frac{1}{I}(-B_r x_2(t) + K_t x_3(t))$$
 (from eq (A)

$$\dot{x}_3(t) = \frac{di}{dt} = \frac{1}{L}(-Rx_3(t) - K_ex_2(t) + u(t))$$
 (from eq (B))

Step 4: Rearrange the derivative of states

$$\begin{split} \dot{x}_1(t) &= 0x_1(t) + 1x_2(t) + 0x_3(t) + 0u(t) \\ \dot{x}_2(t) &= 0x_1(t) - \frac{B_r}{J}x_2(t) + \frac{K_t}{J}x_3(t) + 0u(t) \\ \dot{x}_3(t) &= 0x_1(t) - \frac{K_e}{L}x_2(t) - \frac{R}{L}x_3(t) + \frac{1}{L}u(t) \end{split}$$

Step 5: Rewrite in matrix form:

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \\ \dot{x}_3(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & -B_r/J & K_t/J \\ 0 & -K_e/L & -R/L \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1/L \end{bmatrix} u(t)$$

where the output equation

$$y(t) = \begin{bmatrix} 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \end{bmatrix}$$

Example 4:

Find the eigenvalues for the following system and determine if the system stable?

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & -2 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)$$
$$y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix}$$

Answer:

Eigenvalues λ :

$$\det(A - \lambda I_n) = 0$$

Find λ :

$$\det \begin{pmatrix} \begin{bmatrix} 0 & 1 \\ -1 & -2 \end{bmatrix} - \lambda \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \end{pmatrix} = 0$$
$$\det \begin{pmatrix} \begin{bmatrix} -\lambda & 1 \\ -1 & -2 - \lambda \end{bmatrix} \end{pmatrix} = 0$$
$$(-\lambda)(-2 - \lambda) - (-1)(1) = 0$$
$$\lambda^2 + 2\lambda + 1 = 0$$
$$(\lambda + 1)(\lambda + 1) = 0$$

Therefore eigenvalues (poles) at $\lambda=-1$ and $\lambda=-1$

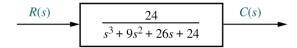
 \Rightarrow Stable system

Exercises

Q1) Find the eigenvalues for the following system and determine if the system stable?

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)$$
$$y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix}$$

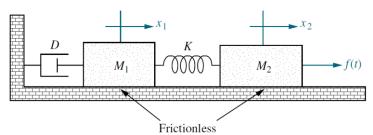
Q2) Find the state-space representation for the transfer function shown below:



- Q3) For the translational mechanical system shown below,
 - (a) Show that the differential equations are given by:

$$M_1 \frac{d^2 x_1}{dt^2} + D \frac{dx_1}{dt} + Kx_1 - Kx_2 = 0$$
$$-Kx_1 + M_2 \frac{d^2 x_2}{dt^2} + Kx_2 = f(t)$$

(b) Find the state space equations (where the input is f(t) and the output is x_2)



SOLUTIONS:

Q1) Solution:

Find the eigenvalues for the following system and determine if the system stable?

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)$$
$$y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix}$$

Answer:

$$\det(A - \lambda I_n) = 0$$

Find λ :

$$\det \begin{pmatrix} \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} - \lambda \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \end{pmatrix} = 0$$
$$\det \begin{pmatrix} \begin{bmatrix} -\lambda & 1 \\ -1 & -\lambda \end{bmatrix} \end{pmatrix} = 0$$
$$(-\lambda)(-\lambda) - (-1)(1) = 0$$
$$\lambda^2 + 1 = 0$$

Therefore eigenvalues (poles) at $\lambda = \pm j$

⇒ marginally stable system (neither positive nor negative poles)

Q2) Solution:

Find the state-space representation for the transfer function shown below:

$$\begin{array}{c|c}
R(s) & 24 & C(s) \\
\hline
s^3 + 9s^2 + 26s + 24 & \end{array}$$

Solution:

given
$$4(5) = \frac{24}{S^1 + 9S^2 + 26S + 24}$$

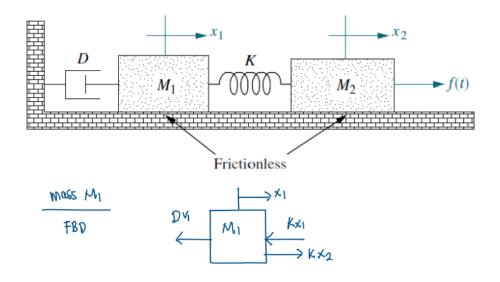
$$7(5)(5^{3}+95^{2}+265+24)=24 \times (5)$$

$$\Rightarrow y + 9y + 26y + 24y = 24 \times (4)$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{y}_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -24 & -26 & -9 \end{bmatrix} \begin{bmatrix} 4 \\ x_1 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 24 \end{bmatrix}$$

Q3) Solution:

3(a)



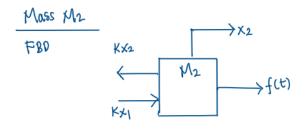
$$\begin{aligned}
& = M_1 \alpha_1 \\
& - DV_1 - K \times_1 + K \times_2 = M_1 \alpha_1 \\
& = M_1 \alpha_1
\end{aligned}$$

$$\begin{aligned}
& = \frac{d \times_1}{d t} = \frac{1}{2} \times_1 \\
& = M_1 \times_1
\end{aligned}$$

$$\begin{aligned}
& = \frac{d^2 \times_1}{d t^2} = X_2
\end{aligned}$$

$$\begin{aligned}
& = DX_1 - K \times_1 + K \times_2 = M_1 \times_1
\end{aligned}$$

rearrange
$$M_1X_1 + PX_1 + KX_1 - KX_2 = 0$$
 (1)



$$\sum F = M_2 \alpha_2$$

 $f(t) + K x_1 - K x_2 = M_2 \alpha_2$ q $\alpha_2 = \frac{dx_2}{dt^2} = x_2$

$$M_2 \overset{\circ}{\times}_3 + k \times_2 - k \times_1 = f(t) * (2)$$

Breval/

Therefore from (1) and (2)

$$M_1 \times_1 + D \times_1 + K \times_1 - K \times_2 = 0$$

 $M_2 \times_2 - K \times_1 + K \times_2 = f(t)$

3(b)

$$\int_{-K_{X_{1}}}^{\infty} w_{1} + w_{2} + w_{1} + w_{2} + w_{2} = \delta$$

$$-K_{X_{1}} + w_{2} + w_{2} + w_{2} = \delta$$

$$(2)$$

Let
$$Z_{1} = x_{1}$$

$$Z_{2} = x_{1}$$

$$Z_{3} = x_{2}$$

$$Z_{4} = x_{2}$$

$$Z_{5} = x_{1}$$

$$Z_{7} = x_{2}$$

$$Z_{7} = x_{2}$$

$$Z_{7} = x_{1}$$

$$Z_{7} = x_{2}$$

$$Z_{7} = x_{2}$$

$$Z_{7} = x_{1}$$

$$Z_{7} = x_{2}$$

$$Z_{7} = x_{3}$$

$$Z_{7} = x_{4}$$

$$Z_{7} =$$

$$\begin{bmatrix} \ddot{z}_{1} \\ \dot{z}_{2} \\ \dot{z}_{3} \\ \ddot{z}_{4} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -k/M_{1} & -D/M_{1} & k/M_{1} & 0 \\ 0 & 0 & 0 & 1 \\ 2 & 0 & 0 & 0 \\ -k/M_{2} & 0 & -k/M_{2} & 1 \end{bmatrix} \begin{bmatrix} z_{1} \\ z_{2} \\ z_{3} \\ z_{4} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} f$$

$$y = \chi_2 = Z_3 = \begin{bmatrix} 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \\ z_3 \\ z_4 \end{bmatrix}$$

Python Example for Q2 solution (eigenvalues vs poles)

```
import numpy as np
from numpy import linalg as LA
A = np.array([[0, 1, 0], [0, 0, 1], [-24, -26, -9]])
print('A:\n',A)
B = np.array([[0], [0], [2]])
print('B:\n',B)
C = np.array([1, 0, 0])
print('C:\n',C)
w, v = LA.eig(A)
print('Eigenvalues:\n', w)
print('Eigenvectors:\n',v)
den=[1, 9, 26, 24]
poles=np.roots(den)
print('poles:\n',poles)
Output:
A:
[[0 1 0]
 [ 0 0 1]
 [-24 -26 -9]]
B:
 [[0]]
 [0]
 [2]]
C:
[1 0 0]
Eigenvalues:
 [-2. -3. -4.]
Eigenvectors:
[[ 0.21821789  0.10482848  0.06052275]
 [-0.43643578 -0.31448545 -0.24209101]
 [ 0.87287156  0.94345635  0.96836405]]
poles:
```

Note that aigenvalues of the matrix A = poles of the system

[-4. -3. -2.]